## Vehicle Dynamics Blockset ${ }^{\text {m }}$ Reference

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## Revision History

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$$
1
$$

Drivetrain Blocks
2

Wheel and Tire Blocks
3

Propulsion Blocks
4

Vehicle Dynamics Blocks
5

Vehicle Scenario Blocks
6

3D Simulation Blocks
7

Scenes
8

Vehicle Dimensions
9

10

Classes
11

Apps
12

## Steering and Suspension Blocks

## Dynamic Steering

Dynamic steering for Ackerman, rack-and-pinion, and parallel steering mechanisms

Note Dynamic Steering is not recommended to implement dynamic steering for Ackerman, rack-andpinion, and parallel steering mechanisms. Use Steering System instead. For more information, see "Compatibility Considerations".


## Libraries:

Vehicle Dynamics Blockset / Steering

## Description

The Dynamic Steering block implements dynamic steering to calculate the wheel angles for Ackerman, rack-and-pinion, and parallel steering mechanisms. The block uses the steering wheel input torque, right wheel torque, and left wheel torque to calculate the wheel angles. The block uses the vehicle coordinate system.

If you select Power assist, you can specify a torque assist lookup table that is a function of the vehicle speed and steering wheel input torque. The block uses the steering wheel input torque and torque assist to calculate the steering dynamics.

To specify the steering type, use the Type parameter.

| Setting | Block Implementation |
| :--- | :--- |
| Ackerman | Ideal Ackerman steering. Wheel angles have a common turning circle <br> center. |
| Rack and pinion | Ideal rack-and-pinion steering. Gears convert the steering rotation into <br> linear motion. |
| Parallel | Parallel steering. Wheel angles are equal. |

To specify the type of data for the steering mechanism, use the Parametrized by parameter.

| Setting | Block Implementation |
| :--- | :--- |
| Constant | Steering mechanism uses constant parameter data. |
| Lookup table | Steering mechanism implements tables for parameter data. |

Use the Steered axle parameter to specify whether the front or rear axle is steered.


## Dynamics

To calculate the steering dynamics, the Dynamic Steering block models the steering wheel, shaft, steering mechanism, hysteresis, and, optionally, power assist.


| Calculation | Equations |
| :---: | :---: |
| Steering column and steering shaft dynamics | $\begin{aligned} & J_{1} \ddot{\theta}_{1}=\tau_{\text {in }}-b_{2} \dot{\theta}_{1}-\tau_{\text {hys }} \\ & J_{2} \ddot{\theta}_{2}=\tau_{\text {eq }}-b_{3} \dot{\theta}_{2}+\tau_{\text {hys }}-\tau_{\text {fric }} \end{aligned}$ |
| Hysteresis spring damper | $\begin{aligned} & \delta=\theta_{1}-\theta_{2} \\ & \Delta \delta=\delta_{\text {current }}-\delta_{\text {previous }} \\ & \tau_{\text {hys }}=\left(b_{1} \dot{\delta}-k_{1} \delta\right)\left(1+\exp \left(-\frac{\|\Delta \delta\|}{\beta}\right)\right) \\ & \beta= \begin{cases}\beta_{u} & \text { when } \delta>0 \\ \beta_{l} & \text { when } \delta \leq 0\end{cases} \end{aligned}$ |
| Optional power assist | $\begin{aligned} & \tau_{\text {ast }}=f_{\text {trq }}\left(v, \tau_{\text {in }}\right) \\ & J_{1} \ddot{\theta}_{1}=\tau_{\text {in }}+\tau_{\text {ast }}-b_{2} \dot{\theta}_{1}-\tau_{\text {hys }} \\ & J_{2} \ddot{\theta}_{2}=\tau_{\text {eq }}+\tau_{\text {ast }}-b_{3} \dot{\theta}_{2}+\tau_{\text {hys }}-\tau_{\text {fric }} \end{aligned}$ |

The illustration and equations use these variables.
$J_{1} \quad$ Steering wheel inertia
$J_{2} \quad$ Steering mechanism inertia
$\theta_{1}, \dot{\theta}_{1}, \ddot{\theta}_{1} \quad$ Steering wheel angle, angular velocity, and angular acceleration, respectively
$\theta_{2}, \dot{\theta}_{2}, \ddot{\theta}_{2} \quad$ Shaft angle, angular velocity, and angular acceleration, respectively
$b_{1}, k_{1} \quad$ Hysteresis spring and viscous damping coefficients, respectively

| $b_{2}$ | Steering wheel viscous damping coefficient |
| :--- | :--- |
| $b_{3}$ | Steering mechanism damping coefficient |
| $\tau_{\text {hys }}$ | Hysteresis spring damping torque |
| $\tau_{\text {fric }}$ | Steering mechanism friction torque |
| $\tau_{\text {eq }}$ | Wheel equivalent torque |
| $\tau_{\text {ast }}$ | Torque assist |
| $\beta_{u}, \beta_{l}$ | Upper and lower hysteresis modifiers, respectively |
| $v$ | Vehicle speed |
| $f_{t r q}$ | Torque assist lookup table |

## Steering Types

## Ackerman Steering

For 100\% (ideal) Ackerman steering, all wheels follow circular arcs with the same center point.


To calculate the steered wheel angles, the Ackerman block uses these equations:

$$
\begin{aligned}
& \cot \left(\delta_{L}\right)-\cot \left(\delta_{R}\right)=\frac{T W}{W B} \\
& \delta_{A c k}=\frac{\delta_{i n}}{\gamma} \\
& \delta_{L}=\tan ^{-1}\left(\frac{W B \tan \left(\delta_{A c k}\right)}{W B+0.5 T W \tan \left(\delta_{A c k}\right)}\right) \\
& \delta_{R}=\tan ^{-1}\left(\frac{W B \tan \left(\delta_{A c k}\right)}{W B-0.5 T W \tan \left(\delta_{A c k}\right)}\right)
\end{aligned}
$$

Definition of variables used:

| $\delta_{i n}$ | Pinion angle (steering shaft angle into pinion) |
| :--- | :--- |
| $\delta_{L}$ | Left wheel steer angle |
| $\delta_{R}$ | Right wheel steer angle |
| $\delta_{A c k}$ | Ackerman steer angle |
| $T W$ | Track width |
| $W B$ | Wheel base |
| $\gamma$ | Steering ratio: Ratio of pinion angle to Ackerman angle |
| Rack-and-Pinion |  |

For rack-and-pinion steering, pinion rotation causes linear motion of the rack, which steers the wheels through the tie rods and steering arms.


To calculate the steered wheel angles, the block uses these equations.

$$
\begin{aligned}
& l_{1}=\frac{T W-l_{\text {rack }}}{2}-\Delta P \\
& l_{2}^{2}=l_{1} 2+D^{2} \\
& \Delta P=r \delta_{\text {in }} \\
& \beta=\frac{\Pi}{2}-\tan ^{-1}\left[\frac{D}{l_{1}}\right]-\cos ^{-1}\left[\frac{l_{\text {arm }}{ }^{2}+l_{2} 2-l_{\text {rod }}{ }^{2}}{2 l_{\text {arm }} l_{2}}\right]
\end{aligned}
$$

The illustration and equations use these variables.

| $\delta_{\text {in }}$ | Pinion angle (steering shaft angle into pinion) |
| :--- | :--- |
| $\delta_{L}$ | Left wheel steer angle |
| $\delta_{R}$ | Right wheel steer angle |
| $T W$ | Track width |
| $r$ | Pinion radius |
| $\Delta P$ | Linear change in rack position from "straight ahead" position |
| $D$ | Longitudinal distance between rack and steered axle |
| $l_{\text {rack }}$ | Rack length (distance between inner tie-rod ends) |
| $l_{\text {arm }}$ | Steering arm length |
| $l_{\text {rod }}$ | Tie rod length |

## Parallel

For parallel steering, the wheel angles are equal.


To calculate the steering angles, the block uses this equation.

$$
\delta_{R}=\delta_{L}=\frac{\delta_{i n}}{\gamma}
$$

The illustration and equations use these variables.

| $\delta_{\text {in }}$ | Steering wheel angle |
| :---: | :--- |
| $\delta_{L}$ | Left wheel angle |
| $\delta_{R}$ | Right wheel angle |
| $\gamma$ | Steering ratio |

## Ports

Input
TrqIn - Torque
scalar
Torque, $\tau_{i n}$, in $\mathrm{N} \cdot \mathrm{m}$.
TrqLft - Left wheel torque
scalar
Left wheel torque, $\tau_{L}$, in $\mathrm{N} \cdot \mathrm{m}$.

TrqRght - Right wheel torque
scalar
Right wheel torque, $\tau_{R}$, in $N \cdot \mathrm{~m}$.
VehSpd - Vehicle speed
scalar
Vehicle speed, $v$, in $\mathrm{m} / \mathrm{s}$.

## Dependencies

To create a VehSpd port, select Power assist.

## Output

Info - Bus signal
bus
Bus signal contains these block calculations.

| Signal | Description | Unit |
| :--- | :--- | :--- |
| StrgWhlAng | Steering wheel angle | rad |
| StrgWhlSpd | Steering wheel angular velocity | $\mathrm{rad} / \mathrm{s}$ |
| ShftAng | Shaft angle | rad |
| ShftSpd | Shaft angular velocity | $\mathrm{rad} / \mathrm{s}$ |
| AngLft | Left wheel angle | rad |
| SpdLft | Left wheel angular velocity | $\mathrm{rad} / \mathrm{s}$ |
| AngRght | Right wheel angle | rad |
| SpdRght | Right wheel angular velocity | $\mathrm{rad} / \mathrm{s}$ |
| TrqAst | Torque assist | $\mathrm{N} \cdot \mathrm{m}$ |
| PwrAst | Power assist | W |
| PwrLoss | Power loss | W |
| InstStrgRatio | Instantaneous steering ratio | NA |

AngLft - Left wheel angle

## scalar

Left wheel angle, $\delta_{L}$, in rad.
AngRght - Right wheel angle
scalar
Right wheel angle, $\delta_{R}$, in rad.

## Parameters

Type - Select steering type
Rack and pinion (default)|Ackerman | Parallel

To specify the steering type, use the Type parameter.

| Setting | Block Implementation |
| :--- | :--- |
| Ackerman | Ideal Ackerman steering. Wheel angles have a common turning circle <br> center. |
| Rack and pinion | Ideal rack-and-pinion steering. Gears convert the steering rotation into <br> linear motion. |
| Parallel | Parallel steering. Wheel angles are equal. |

## Dependencies

This table summarizes the Type and Parametrized by parameter dependencies.

| Type | Parameterized By | Creates Parameters |
| :--- | :--- | :--- |
| Ackerman | Constant | Track width, TrckWdth |
| Wheel base, WhlBase |  |  |
| Steering range, StrgRng |  |  |
| Steering ratio, StrgRatio |  |  |, | Track width, TrckWdth |
| :--- |
|  |


| Type | Parameterized By | Creates Parameters |
| :--- | :--- | :--- |
|  | Lookup table | Track width, TrckWdth |
|  |  |  |
|  |  |  |
|  |  |  |
| Rack casing length, RckCsLngth |  |  |
| Tie rod length, TieRodLngth |  |  |
| Parallel | Constant | Pinion radius, PnnRadiusTbl |
|  |  | Steering range, StrgRng |
| Steering ratio, StrgRatio |  |  |, | Steering range, StrgRng |
| :--- |
| Steering angle breakpoints, StrgAngBpts |
| Steering ratio table, StrgRatioTbl |

## Parametrized by - Select parameterization

Lookup table (default) | Constant
To specify the type of data for the steering mechanism, use the Parametrized by parameter.

| Setting | Block Implementation |
| :--- | :--- |
| Constant | Steering mechanism uses constant parameter data. |
| Lookup table | Steering mechanism implements tables for parameter data. |

## Dependencies

This table summarizes the Type and Parametrized by parameter dependencies.

| Type | Parameterized By | Creates Parameters |
| :--- | :--- | :--- |
| Ackerman | Constant | Track width, TrckWdth |
|  |  | Wheel base, WhIBase |
|  |  | Steering range, StrgRng |
| Steering ratio, StrgRatio |  |  |


| Type | Parameterized By | Creates Parameters |
| :---: | :---: | :---: |
|  | Lookup table | Track width, TrckWdth <br> Wheel base, WhlBase <br> Steering range, StrgRng <br> Steering angle breakpoints, StrgAngBpts <br> Steering ratio table, StrgRatioTbl |
| Rack and pinion | Constant | Track width, TrckWdth <br> Steering range, StrgRng <br> Steering arm length, StrgArmLngth <br> Rack casing length, RckCsLngth <br> Tie rod length, TieRodLngth <br> Distance between front axis and rack, $D$ <br> Pinion radius, PnnRadius |
|  | Lookup table | Track width, TrckWdth <br> Steering range, StrgRng <br> Steering angle breakpoints, StrgAngBpts <br> Steering arm length, StrgArmLngth <br> Rack casing length, RckCsLngth <br> Tie rod length, TieRodLngth <br> Distance between front axis and rack, $D$ <br> Pinion radius, PnnRadiusTbl |
| Parallel | Constant | Steering range, StrgRng Steering ratio, StrgRatio |
|  | Lookup table | Steering range, StrgRng <br> Steering angle breakpoints, StrgAngBpts <br> Steering ratio table, StrgRatioTbl |

Power assist - Specify power assist
on (default) | off
If you select Power assist, you can specify a torque assist lookup table, $f_{\text {trq, }}$, that is a function of the vehicle speed, $v$, and steering wheel input torque, $\tau_{i n}$.

$$
\tau_{\text {ast }}=f_{\text {trq }}\left(v, \tau_{\text {in }}\right)
$$

The block uses the steering wheel input torque and torque assist to calculate the steering dynamics. Dependencies

Selecting Power assist creates the VehSpd input port and these parameters.

| Power Assist | Parameters |
| :--- | :--- |
| on | Steering wheel torque breakpoints, TrqBpts |
|  | Vehicle speed breakpoints, VehSpdBpts |
|  | Assisting torque table, TrqTbl |
|  | Assisting torque limit, TrqLmt |
|  | Assisting power limit, PwrLmt |
|  | Assisting torque efficiency, Eta |
| Cutoff frequency, omega_c |  |

## Location - Select location

## Front (default) | Rear

Use the Steered axle parameter to specify whether the front or rear axle is steered.

| Setting | Implementation |
| :--- | :--- |
| Front | Front axle steering |



## General

Track width, TrckWdth - Width
l|scalar
Track width, $T W$, in $m$.

## Dependencies

To create this parameter, set Type to Ackerman or Rack and pinion.
Wheel base, WhIBase - Base
1.524 (default) | scalar

Wheel base, WB, in m.

## Dependencies

To create this parameter, set Type to Ackerman.

## Steering range, StrgRng - Range

1.25*pi (default) | scalar

Steering range, in rad. The block limits the wheel angles to remain within the steering range.

## Steering ratio, StrgRatio - Ratio

13.5 (default) | scalar

Steering ratio, $\gamma$, dimensionless.

## Dependencies

To create this parameter:

- Set Type to Ackerman or Parallel.
- Set Parametrized by to Constant.

Steering angle breakpoints, StrgAngBpts - Breakpoints
[-6.2832 -5.0265-3.7699 -2.5133-1.2566 0 1.2566 2.5133 3.7699 5.0265
6.2832] (default) | vector

Steering angle breakpoints, in rad.

## Dependencies

To create this parameter, set Parametrized by to Lookup table.
Steering ratio table, StrgRatiotbl - Table
$[13.500013 .375013 .250013 .125013 .000013 .000013 .000013 .125013 .2500$
13.3750 13.5000] (default) | vector

Steering ratio table, $\gamma$, dimensionless.

## Dependencies

To create this parameter:

- Set Type to Ackerman or Parallel.
- Set Parametrized by to Lookup table.


## Rack-and-Pinion

Steering arm length, StrgArmLngth - Length
0.1 (default) | scalar

Steering arm length, $l_{\text {arm }}$, in m .

## Dependencies

To create this parameter, set Type to Rack and pinion.
Rack casing length, RckCsLngth - Length
0.5 (default) | scalar

Rack casing length, $l_{\text {rack }}$, in m .

## Dependencies

To create this parameter, set Type to Rack and pinion.
Tie rod length, TieRodLngth - Length
0.248 (default) | scalar

Tie rod length, $l_{\text {rod }}$, in m .

## Dependencies

To create this parameter, set Type to Rack and pinion.
Distance between axis and rack, D - Distance
0.2 (default) | scalar

Distance between axis and rack, $D$, in m.

## Dependencies

To create this parameter, set Type to Rack and pinion.
Pinion radius, PnnRadius - Radius
0.0057 (default) | scalar

Pinion radius, $r$, in $m$.

## Dependencies

To create this parameter:

- Set Type to Rack and pinion.
- Set Parametrized by to Constant.

Pinion radius table, PnnRadiusTbI - Table
[0.0055 0.0055 0.0056 0.0057 0.0057 0.0057 0.0058 0.0057 0.0056 0.0055 $0.0055]$ (default) | vector

Pinion radius table, $r$, in $m$.
Dependencies
To create this parameter:

- Set Type to Rack and pinion.
- Set Parametrized by to Lookup table.


## Dynamics

Steering wheel inertia, J1 - Inertia
0.1 (default) | scalar

Steering wheel inertia, $J_{1}$, in $\mathrm{kg}^{*} \mathrm{~m}^{\wedge} 2$.
Steering mechanism inertia, J2 - Inertia
0.01 (default) | scalar

Steering mechanism inertia, $J_{2}$, in $\mathrm{kg}^{*} \mathrm{~m}^{\wedge} 2$.
Upper hysteresis modifier, beta_u - Upper hysteresis modifier
0.1 (default) | scalar

Upper hysteresis modifier, $\beta_{u}$ dimensionless.
Lower hysteresis modifier, beta_I - Lower hysteresis modifier
0.1 (default) | scalar

Lower hysteresis modifier, $\beta_{l}$, dimensionless.
Hysteresis viscous damping, b1 - Damping
0.001 (default) | scalar

Hysteresis damping, $b_{1}$, in $N \cdot m \cdot \mathrm{~s} / \mathrm{rad}$.

Hysteresis stiffness, k1 - Stiffness
30 (default) | scalar
Hysteresis stiffness, $k_{1}$, in $\mathrm{N} \cdot \mathrm{m} / \mathrm{rad}$.
Steering wheel damping, b2 - Damping
1 (default) | scalar
Steering wheel damping, $b_{2}$, in $\mathrm{N} \cdot \mathrm{m} \cdot \mathrm{s} / \mathrm{rad}$.
Steering mechanism damping, b3 - Damping
0.001 (default) | scalar

Steering mechanism damping, $b_{3}$, in $\mathrm{N} \cdot \mathrm{m} \cdot \mathrm{s} / \mathrm{rad}$.
Initial steering angle, theta_o - Angle
0 (default) | scalar
Initial steering angle, $\theta_{0}$, in rad.
Initial steering angular velocity, omega_o - Angular velocity
0 (default) | scalar
Initial steering angular velocity, $\omega_{o}$, in rad/s.
Friction torque, FricTrq - Torque
0 (default) | scalar
Friction torque, $\tau_{\text {fric }}$, in $\mathrm{N} \cdot \mathrm{m}$.

## Power Assist

Steering wheel torque breakpoints, TrqBpts - Breakpoints
[-100 0 100] (default) | 1-by-M vector
Steering wheel torque breakpoints, in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

Selecting Power assist creates the VehSpd input port and these parameters.

| Power Assist | Parameters |
| :--- | :--- |
| on | Steering wheel torque breakpoints, TrqBpts |
|  | Vehicle speed breakpoints, VehSpdBpts |
|  | Assisting torque table, TrqTbl |
|  | Assisting torque limit, TrqLmt |
|  | Assisting power limit, PwrLmt |
|  | Assisting torque efficiency, Eta |
|  | Cutoff frequency, omega_c |

## Vehicle speed breakpoints, VehSpdBpts - Breakpoints

## [0 20] (default) | 1-by-N vector

Vehicle speed breakpoints, in m/s.

## Dependencies

Selecting Power assist creates the VehSpd input port and these parameters.

| Power Assist | Parameters |
| :--- | :--- |
| on | Steering wheel torque breakpoints, TrqBpts |
|  | Vehicle speed breakpoints, VehSpdBpts |
|  | Assisting torque table, TrqTbl |
|  | Assisting torque limit, TrqLmt |
|  | Assisting power limit, PwrLmt |
|  | Assisting torque efficiency, Eta |
|  | Cutoff frequency, omega_c |

Assisting torque table, TrqTbI - 2D torque table
[0-100;0 0;0 100] (default)|M-by-N matrix
Assisting torque table, $f_{\text {trq }}$, in $\mathrm{N} \cdot \mathrm{m}$.
The torque assist lookup table is a function of the vehicle speed, $v$, and steering wheel input torque, $\tau_{i n}$.

$$
\tau_{a s t}=f_{t r q}\left(v, \tau_{i n}\right)
$$

The block uses the steering wheel input torque and torque assist to calculate the steering dynamics.

## Dependencies

Selecting Power assist creates the VehSpd input port and these parameters.

| Power Assist | Parameters |
| :--- | :--- |
| on | Steering wheel torque breakpoints, TrqBpts |
|  | Vehicle speed breakpoints, VehSpdBpts |
|  | Assisting torque table, TrqTbl |
|  | Assisting torque limit, TrqLmt |
|  | Assisting power limit, PwrLmt |
|  | Assisting torque efficiency, Eta |
| Cutoff frequency, omega_c |  |

Assisting torque limit, TrqLmt - Torque limit 100 (default) | scalar

Assisting torque limit, in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

Selecting Power assist creates the VehSpd input port and these parameters.

| Power Assist | Parameters |
| :--- | :--- |
| on | Steering wheel torque breakpoints, TrqBpts |
|  | Vehicle speed breakpoints, VehSpdBpts |
|  | Assisting torque table, TrqTbl |
|  | Assisting torque limit, TrqLmt |
|  | Assisting power limit, PwrLmt |
|  | Assisting torque efficiency, Eta |
| Cutoff frequency, omega_c |  |

Assisting power limit, PwrLmt - Power limit
1000 (default)| scalar
Assisting power limit, in $\mathrm{N} \cdot \mathrm{m} / \mathrm{s}$.
Dependencies
Selecting Power assist creates the VehSpd input port and these parameters.

| Power Assist | Parameters |
| :--- | :--- |
| on | Steering wheel torque breakpoints, TrqBpts |
|  | Vehicle speed breakpoints, VehSpdBpts |
|  | Assisting torque table, TrqTbl |
|  | Assisting torque limit, TrqLmt |
|  | Assisting power limit, PwrLmt |
|  | Assisting torque efficiency, Eta |
|  | Cutoff frequency, omega_c |

Assisting torque efficiency, Eta - Efficiency
1 (default) | scalar
Assisting torque efficiency, dimensionless.

## Dependencies

Selecting Power assist creates the VehSpd input port and these parameters.

| Power Assist | Parameters |
| :--- | :--- |
| on | Steering wheel torque breakpoints, TrqBpts |
|  | Vehicle speed breakpoints, VehSpdBpts |
|  | Assisting torque table, TrqTbl |
|  | Assisting torque limit, TrqLmt |
|  | Assisting power limit, PwrLmt |
|  | Assisting torque efficiency, Eta |
| Cutoff frequency, omega_c |  |

## Cutoff frequency, omega_c - Cutoff frequency

200 (default) | scalar
Cutoff frequency, in rad/s.

## Dependencies

Selecting Power assist creates the VehSpd input port and these parameters.

| Power Assist | Parameters |
| :--- | :--- |
| on | Steering wheel torque breakpoints, TrqBpts |
|  | Vehicle speed breakpoints, VehSpdBpts |
|  | Assisting torque table, TrqTbl |
|  | Assisting torque limit, TrqLmt |
|  | Assisting power limit, PwrLmt |
|  | Assisting torque efficiency, Eta |
|  | Cutoff frequency, omega_c |

## Version History

## Introduced in R2018a

## R2023a: Dynamic Steering block is not recommended

Not recommended starting in R2023a
The Dynamic Steering is not recommended. Instead, use the Steering System block to implement dynamic steering, including:

- Ackerman percentage that adjusts the ideal Ackerman outside wheel angle. You can use an input port or parameters to specify a constant or table of Ackerman percentages.
- Single or double Cardan joint to model the intermediate steering shaft.
- Friction and compliance effects.
- Input ports for power assistance, Ackerman steering, and kingpin moments.


## References

[1] Crolla, David, David Foster, et al. Encyclopedia of Automotive Engineering. Volume 4, Part 5 (Chassis Systems) and Part 6 (Electrical and Electronic Systems). Chichester, West Sussex, United Kingdom: John Wiley \& Sons Ltd, 2015.
[2] Gillespie, Thomas. Fundamentals of Vehicle Dynamics. Warrendale, PA: Society of Automotive Engineers, 1992.
[3] Vehicle Dynamics Standards Committee. Vehicle Dynamics Terminology. SAE J670. Warrendale, PA: Society of Automotive Engineers, 2008.

## Extended Capabilities

C/C++ Code Generation
Generate C and C++ code using Simulink ${ }^{\circledR}$ Coder ${ }^{\mathrm{TM}}$.

## See Also

Kinematic Steering | Mapped Steering

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"

## Kinematic Steering

Kinematic steering for Ackerman, rack-and-pinion, and parallel steering mechanisms


## Libraries:

Vehicle Dynamics Blockset / Steering

## Description

The Kinematic Steering block implements a steering model to determine the left and right wheel angles for Ackerman, rack-and-pinion, and parallel steering mechanisms. The block uses the vehicle coordinate system.

To specify the steering type, use the Type parameter.

| Setting | Block Implementation |
| :--- | :--- |
| Ackerman | Ideal Ackerman steering, adjusted by percentage Ackerman. Wheel angles <br> have a common turning circle center. |
| Rack and pinion | Ideal rack-and-pinion steering. Gears convert the steering rotation into <br> linear motion. |
| Parallel | Parallel steering. Wheel angles are equal. |

To specify the type of data for the steering mechanism, use the Parametrized by parameter.

| Setting | Block Implementation |
| :--- | :--- |
| Constant | Steering mechanism uses constant parameter data. |
| Lookup table | Steering mechanism implements tables for parameter data. |

Use the Steered axle parameter to specify whether the front or rear axle is steered.

| Setting | Implementation |
| :--- | :--- |
| Front | Front axle steering |
| Rear | Rear axle steering |

## Steering Types

## Ackerman

For ideal Ackerman steering, the wheel angles have a common turning circle.


To calculate the ideal wheel angles, the block uses these equations.

$$
\begin{aligned}
& \cot \left(\delta_{L}\right)-\cot \left(\delta_{R}\right)=\frac{T W}{W B} \\
& \delta_{A c k}=\frac{\delta_{i n}}{\gamma} \\
& \delta_{L}=\tan ^{-1}\left(\frac{W B \tan \left(\delta_{A c k}\right)}{W B+0.5 T W \tan \left(\delta_{A c k}\right)}\right) \\
& \delta_{R}=\tan ^{-1}\left(\frac{W B \tan \left(\delta_{A c k}\right)}{W B-0.5 T W \tan \left(\delta_{A c k}\right)}\right)
\end{aligned}
$$

After the block calculates the ideal wheel angles, it uses the Ackerman percentage to adjust the outside wheel angle.

$$
\delta_{o}=\delta_{i}-p_{A c k}\left(\delta_{i}-\delta_{A c k}\right)
$$

The outside wheel angle depends on the turn direction.

- Right turn
- Outside angle, $\delta_{o}$, is left wheel angle, $\delta_{L}$
- Inside angle, $\delta_{i}$, is right wheel angle, $\delta_{R}$
- Left turn
- Outside angle, $\delta_{0}$, is right wheel angle, $\delta_{R}$
- Inside angle, $\delta_{i}$, is left wheel angle, $\delta_{L}$

The illustration and equations use these variables.

| $\delta_{\text {in }}$ | Steering angle |
| :--- | :--- |
| $\delta_{L}$ | Left wheel angle |


| $\delta_{R}$ | Right wheel angle |
| :--- | :--- |
| $\delta_{o}$ | Outside wheel angle |
| $\delta_{i}$ | Inside wheel angle |
| $p_{A c k}$ | Ackerman percentage |
| $T W$ | Track width |
| $W B$ | Wheel base |
| $\gamma$ | Steering ratio |

## Rack-and-Pinion

For ideal rack-and-pinion steering, the gears convert the steering rotation into linear motion.


To calculate the steering angles, the block uses these equations.

$$
\begin{aligned}
& l_{1}=\frac{T W-l_{\text {rack }}}{2}-\Delta P \\
& l_{2} 2=l_{1} 2+D^{2} \\
& \Delta P=r \delta_{\text {in }} \\
& \beta=\frac{\Pi}{2}-\tan ^{-1}\left[\frac{D}{l_{1}}\right]-\cos ^{-1}\left[\frac{l_{\text {arm }}{ }^{2}+l_{2} 2-l_{\text {rod }}{ }^{2}}{2 l_{\text {arm }} l_{2}}\right]
\end{aligned}
$$

The illustration and equations use these variables.

| $\delta_{\text {in }}$ | Steering wheel angle |
| :--- | :--- |
| $\delta_{L}$ | Left wheel angle |
| $\delta_{R}$ | Right wheel angle |
| $T W$ | Track width |
| $r$ | Pinion radius |
| $\Delta P$ | Linear change in rack position |
| $D$ | Distance between front axis and rack |
| $l_{\text {rack }}$ | Rack casing length |
| $l_{\text {arm }}$ | Steering arm length |
| $l_{\text {rod }}$ | Tie rod length |

## Parallel

For parallel steering, the wheel angles are equal.


To calculate the steering angles, the block uses this equation.

$$
\delta_{R}=\delta_{L}=\frac{\delta_{i n}}{\gamma}
$$

The illustration and equations use these variables.

| $\delta_{i n}$ | Steering wheel angle |
| :---: | :--- |
| $\delta_{L}$ | Left wheel angle |
| $\delta_{R}$ | Right wheel angle |
| $\gamma$ | Steering ratio |

## Ports

Input
Angln - Steering angle
scalar
Steering angle, $\delta_{i n}$, in rad.
Use the Steering range, StrgRng parameter to specify a steering angle range. By default, the value is set to $1.25{ }^{*}$ pi, which limits the steering angle to a range of $-1.25^{*}$ pi to $1.25^{*}$ pi.

PctAckIn - Ackerman percentage
scalar

Ackerman percentage, $\delta_{i n}$, in percent.

## Dependencies

To create this input port:

- Set Type to Ackerman.
- On the Ackerman Steering pane, select Input percent Ackerman.


## Output

Info - Bus signal
bus
Bus signal contains this block calculation.

| Signal | Description | Variable | Unit |
| :--- | :--- | :--- | :--- |
| InstStrgRatio | Instantaneous steering <br> ratio | $\gamma$ | NA |

## AngLft - Left wheel angle

scalar
Left wheel angle, $\delta_{L}$, in rad.
AngRght - Right wheel angle
scalar
Right wheel angle, $\delta_{R}$, in rad.

## Parameters

Type - Select steering type
Ackerman (default)|Rack and pinion|Parallel
To specify the steering type, use the Type parameter.

| Setting | Block Implementation |
| :--- | :--- |
| Ackerman | Ideal Ackerman steering. Wheel angles have a common turning circle <br> center. |
| Rack and pinion | Ideal rack-and-pinion steering. Gears convert the steering rotation into <br> linear motion. |
| Parallel | Parallel steering. Wheel angles are equal. |

Parametrized by - Select parameterization
Constant (default)|Lookup table
To specify the type of data for the steering mechanism, use the Parametrized by parameter.

| Setting | Block Implementation |
| :--- | :--- |
| Constant | Steering mechanism uses constant parameter data. |


| Setting | Block Implementation |
| :--- | :--- |
| Lookup table | Steering mechanism implements tables for parameter data. |

## Location - Select location

Front (default) | Rear
Use the Steered axle parameter to specify whether the front or rear axle is steered.

| Setting | Implementation |
| :---: | :---: |
| Front | Front axle steering |
|  |  |
| Rear | Rear axle steering |
|  |  |

Normalization factor, NrmIFctr - Adjust the steering angle scalar

Factor, $N_{r m}{ }_{\text {Fctr }}$, that the block uses to adjust the steering ratio, $\gamma$ or pinion radius, $r$. The block can only normalize if you have Parametrized by set to Constant.

To adjust the steering ratio or pinion radius, click Normalize.

| Steering Type | Normalization |
| :--- | :--- |
| Ackerman | Block updates the Steering ratio, StrgRatio <br> parameter to the normalized value, $\gamma_{n r m}$, specified by <br> this equation. |
| Parallel | $\gamma_{n r m}=\frac{1}{N r m_{\text {Fctr }}}$ |
| Rack and pinion | Block updates the Pinion radius, PnnRadius <br> parameter to using the normalization factor, $N r m_{\text {Fctr. }}$ |

## General

Track width, TrckWdth - Width
1 (default) | scalar
Track width, $T W$, in m.

## Dependencies

To create this parameter, set Type to Ackerman or Rack and pinion.
Wheel base, WhIBase - Base
1.524 (default) | scalar

Wheel base, WB, in m.

## Dependencies

To create this parameter, set Type to Ackerman.
Deadband, Db - Deadband
0 (default) | scalar
Deadband steering angle before pinion engages the gear, in rad.
Steering range, StrgRng - Steering wheel angle input range
1.25*pi (default) | scalar

Steering wheel angle input range, in rad. The block limits the steering wheel input angles to remain within the steering range.

## Steering ratio, StrgRatio - Ratio <br> 100 (default) | scalar

Steering ratio, $\gamma$, dimensionless.

## Dependencies

To create this parameter:

- Set Type to Ackerman or Parallel.
- Set Parametrized by to Constant.

Steering angle breakpoints, StrgAngBpts - Breakpoints
$[-6.2832-5.0265-3.7699-2.5133-1.256601 .25662 .51333 .76995 .0265$
6.2832] (default) | vector

Steering angle breakpoints, in rad.

## Dependencies

To create this parameter, set Parametrized by to Lookup table.
Steering ratio table, StrgRatioTbl - Table

13.3750 13.5000] (default) |vector

Steering ratio table, $\gamma$, dimensionless.

## Dependencies

To create this parameter:

- Set Type to Ackerman or Parallel.
- Set Parametrized by to Lookup table.


## Rack-and-Pinion

Steering arm length, StrgArmLngth - Length
0.1 (default) | scalar

Steering arm length, $l_{\text {arm }}$, in m .

## Dependencies

To create this parameter, set Type to Rack and pinion.

## Rack casing length, RckCsLngth - Length

0.5 (default) | scalar

Rack casing length, $l_{\text {rack }}$, in m .

## Dependencies

To create this parameter, set Type to Rack and pinion.
Tie rod length, TieRodLngth - Length
0.248 (default) | scalar

Tie rod length, $l_{\text {rod }}$, in m .

## Dependencies

To create this parameter, set Type to Rack and pinion.

## Distance between axis and rack, D - Distance

0.2 (default) | scalar

Distance between axis and rack, $D$, in m .

## Dependencies

To create this parameter, set Type to Rack and pinion.
Pinion radius, PnnRadius - Radius
0.0057 (default) | scalar

Pinion radius, $r$, in $m$.

## Dependencies

To create this parameter:

- Set Type to Rack and pinion.
- Set Parametrized by to Constant.

Pinion radius table, PnnRadiusTbI - Table
[0.0055 0.0055 0.0056 0.0057 0.0057 0.0057 0.0058 0.0057 0.0056 0.0055
0.0055] (default) | vector

Pinion radius table, $r$, in $m$.

## Dependencies

To create this parameter:

- Set Type to Rack and pinion.
- Set Parametrized by to Lookup table.

Ackerman Steering
Input Percent Ackerman - Create PctAckIn input port
off (default) | on
Select to create PctAckIn input port.

## Dependencies

To enable this parameter, set Type to Ackerman.
Percent Ackerman, PctAck - Percent Ackerman constant 100 (default) | scalar

Constant value of percent Ackerman, in percent.

## Dependencies

To enable this parameter:

- Set Type to Ackerman
- Set Parametrized by to Constant
- Clear Input Percent Ackerman

Percent Ackerman table, PctAckTbI - Percent Ackerman table

## ones $(1,11) * 100$ (default) | vector

Table of percent Ackerman values as a function of the steering angle, $\delta_{i n}$, in percent.

## Dependencies

To enable this parameter:

- Set Type to Ackerman
- Set Parametrized by to Constant
- Clear Input Percent Ackerman


## Version History

## Introduced in R2018a

## References

[1] Crolla, David, David Foster, et al. Encyclopedia of Automotive Engineering. Volume 4, Part 5 (Chassis Systems) and Part 6 (Electrical and Electronic Systems). Chichester, West Sussex, United Kingdom: John Wiley \& Sons Ltd, 2015.
[2] Gillespie, Thomas. Fundamentals of Vehicle Dynamics. Warrendale, PA: Society of Automotive Engineers, 1992.
[3] Vehicle Dynamics Standards Committee. Vehicle Dynamics Terminology. SAE J670. Warrendale, PA: Society of Automotive Engineers, 2008.

## Extended Capabilities

C/C++ Code Generation
Generate C and C++ code using Simulink ${ }^{\circledR}$ Coder ${ }^{\mathrm{TM}}$.

## See Also

Dynamic Steering | Mapped Steering
Topics
"Coordinate Systems in Vehicle Dynamics Blockset"

## Mapped Steering

Mapped steering with speed-dependent option


## Libraries:

Vehicle Dynamics Blockset / Steering

## Description

The Mapped Steering block implements lookup tables to calculate the right and left wheel angles. Use the Speed dependent parameter to implement a speed-dependent table for the steering angle calculations. The block uses the vehicle coordinate system.

## Steering Wheel Angle

If you set Steering type to Steering wheel angle, the block implements these tables.

| Speed Dependen t | Implementation | Calculations |
| :---: | :---: | :---: |
| on (default) | Block uses three tables: <br> - $f_{s}$ - Function of vehicle speed <br> - $f_{L}$ - Function of superimposed steering wheel angle <br> - $f_{R}$ - Function of superimposed steering wheel angle | $\begin{aligned} & \delta_{\text {SpdF }}=f_{s}(v) \\ & \delta_{\text {SuprImp }}=\delta_{\text {SpdF }} \cdot \delta_{\text {in }} \\ & \delta_{L}=f_{L}\left(\delta_{\text {SuprImp }}\right) \\ & \delta_{R}=f_{R}\left(\delta_{\text {SuprImp }}\right) \end{aligned}$ |
| off | Block uses two tables: <br> - $f_{L}$ - Function of steering wheel angle <br> - $f_{R}$ - Function of steering wheel angle | $\begin{aligned} & \delta_{L}=f_{L}\left(\delta_{i n}\right) \\ & \delta_{R}=f_{R}\left(\delta_{i n}\right) \end{aligned}$ |

## Rack Travel Displacement

If you set Steering type to Rack travel displacement, the block implements these tables.

| Speed <br> Dependen <br> t | Implementation | Calculations |
| :--- | :--- | :--- |
| on | Block uses three tables: |  |
|  | $-f_{s}$ - Function of vehicle speed | $\delta_{\text {SpdF }}=f_{S}(v)$ |
|  | $-f_{L}$ - Function of rack displacement | $\delta_{\text {RuprImp }}=\delta_{\text {SpdF }} \cdot \delta_{\text {in }}$ |
|  | - $f_{R}$ - Function of rack displacement | $\delta_{L}=f_{L}\left(\Delta_{\text {Rack }}\right)$ |
|  |  | $\delta_{R}=f_{R}\left(\Delta_{\text {Rack }}\right)$ |
| off | Block uses two tables: | $\Delta_{\text {Rack }}=\delta_{\text {in }} \cdot G r$ |
|  | - $f_{L}$ - Function of rack displacement | $\delta_{L}=f_{L}\left(\Delta_{\text {Rack }}\right)$ |
|  | - $f_{R}$ - Function of rack displacement | $\delta_{R}=f_{R}\left(\Delta_{\text {Rack }}\right)$ |

The block uses a gear ratio to adjust the rack displacement. To use a

- Constant gear ratio, set Gear ratio parameterized by to Constant.
- Gear ratio as a function of steering angle, set Gear ratio parameterized by to Lookup table.

The equations use these variables.

| $\delta_{\text {in }}$ | Steering wheel angle |
| :--- | :--- |
| $\delta_{\text {SpdF }}$ | Steering wheel angle speed factor |
| $\delta_{\text {SuprImp }}$ | Superimposed steering wheel angle |
| $\delta_{L}, \delta_{R}$ | Left and right wheel angles, respectively |
| $\Delta_{\text {Rack }}$ | Rack displacement |
| $G r$ | Gear ratio |

## Ports

## Input

## Angln - Steering angle <br> scalar

Steering angle, $\delta_{i n}$, in rad.
Use the Steering angle breakpoints, StrgAngBpts parameter to specify a steering angle range. By default, the value is set to $1.25^{*}$ pi, which limits the steering angle to a range of $-1.25^{*}$ pi to $1.25^{*}$ pi.

VehSpd - Vehicle speed
scalar
Vehicle speed, $V e h_{\text {spd }}$, in $\mathrm{m} / \mathrm{s}$.

## Dependencies

To create this port, select Speed dependent.

## Output

Info - Bus signal
bus
Bus signal containing these block calculations.

| Signal | Description | Variable | Unit |
| :--- | :--- | :--- | :--- |
| AngLft | Left wheel angle | $\delta_{L}$ | rad |
| AngRght | Left wheel angle | $\delta_{R}$ | rad |

AngLft - Left wheel angle scalar

Left wheel angle, $\delta_{L}$, in rad.
AngRght - Right wheel angle
scalar
Right wheel angle, $\delta_{R}$, in rad.

## Parameters

## Options

Speed dependent - Use speed-dependent tables
on (default) | off
Select to use speed-dependent tables.

## Dependencies

Selecting this parameter creates input port VehSpd.

## Steering type - Use speed-dependent tables

Steering wheel angle (default)|Rack travel displacement
If you set Steering type to Steering wheel angle, the block implements these tables.

| Speed Dependent | Implementation |
| :--- | :--- |
| on (default) | Block uses three tables: |
|  | - $f_{s}-$ Function of vehicle speed |
|  | - $f_{L}-$ Function of superimposed steering wheel angle |
|  | - $f_{R}-$ Function of superimposed steering wheel angle |
| off | Block uses two tables: |
|  | - $f_{L}-$ Function of steering wheel angle |
|  | - $f_{R}-$ Function of steering wheel angle |

If you set Steering type to Rack travel displacement, the block implements these tables.

| Speed Dependent | Implementation |
| :--- | :--- |
| on (default) | Block uses three tables: |
|  | - $f_{s}$ - Function of vehicle speed |
|  | - $f_{L}-$ Function of rack displacement |
|  | - $f_{R}-$ Function of rack displacement |
| off | Block uses two tables: |
|  | - $f_{L}-$ Function of rack displacement |
|  | - $f_{R}$ - Function of rack displacement |

Steering angle breakpoints, StrgAngBpts - Steering angle breakpoints
[-1.5*pi 1.5*pi] (default)|vector
Steering angle breakpoints, in rad.

## Dependencies

If you set Steering type to Rack travel displacement, to enable this parameter, set Gear ratio parameterized by to Lookup table.

Rack displacement breakpoints, RackDispBpts - Rack displacement breakpoints
[-40-19.2 -4.53 4.53 19.2 40] (default)|vector
Rack displacement breakpoints, in mm.

## Dependencies

To enable this parameter, set Steering type to Rack travel displacement and Gear ratio parameterized by to Lookup table.

Gear ratio table, GrTbI - Gear ratio table
[9.87 9.87 7.16 7.16 9.87 9.87]*2*pi (default) |vector
Gear ratio table as a function of rack displacement, in mm/rev.

## Dependencies

To enable this parameter, set Steering type to Rack travel displacement and Gear ratio parameterized by to Lookup table.

Gear ratio constant, $\mathbf{G r}$ - Gear ratio constant
8.28*2*pi (default) | scalar

Gear ratio constant, in $\mathrm{mm} / \mathrm{rev}$.

## Dependencies

To enable this parameter, set Steering type to Rack travel displacement and Gear ratio parameterized by to Constant.

Left wheel angle table, WhILftTbl - Left wheel angle table
[-1.5*pi 1.5*pi]/13.5] (default)|vector
Left wheel angle table, $\delta_{L}$, in rad.

Right wheel angle table, WhIRghtTb - Right wheel angle table
[-1.5*pi 1.5*pi]/13.5] (default)|vector
Right wheel angle table, $\delta_{R}$, in rad.
Vehicle speed breakpoints, VehSpdBpts - Vehicle speed breakpoints
[-1 1] (default) |vector
Vehicle speed breakpoints, in m/s.

## Dependencies

To create this parameter, select Speed dependent.
Superimposed speed factor table, SpdFctTbI - Speed factor
[1 1] (default)| vector
Superimposed speed factor table, $f_{s}$, dimensionless. The table is a factor of vehicle speed, $v$.

## Dependencies

To create this parameter, select Speed dependent.

## Version History

Introduced in R2018a

## References

[1] Crolla, David, David Foster, et al. Encyclopedia of Automotive Engineering. Volume 4, Part 5 (Chassis Systems) and Part 6 (Electrical and Electronic Systems). Chichester, West Sussex, United Kingdom: John Wiley \& Sons Ltd, 2015.
[2] Gillespie, Thomas. Fundamentals of Vehicle Dynamics. Warrendale, PA: Society of Automotive Engineers, 1992.
[3] Vehicle Dynamics Standards Committee. Vehicle Dynamics Terminology. SAE J670. Warrendale, PA: Society of Automotive Engineers, 2008.

## Extended Capabilities

C/C++ Code Generation
Generate C and C++ code using Simulink ${ }^{\circledR}$ Coder ${ }^{\mathrm{TM}}$.

## See Also

Dynamic Steering | Kinematic Steering

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"

## Steering System

Steering system for Ackerman and rack-and-pinion steering mechanisms


## Libraries:

Vehicle Dynamics Blockset / Steering

## Description

The Steering System block implements dynamic steering to calculate the wheel steer angles for rack-and-pinion mechanisms with friction, compliance, and Ackerman steering features. The block uses the steering wheel input angle or torque input, vehicle speed, caster angle, and right and left wheel feedbacks to calculate the wheel steer angles. The block uses the vehicle coordinate system.

If you select the Power assist parameter, you can specify a torque assist lookup table that is a function of the vehicle speed and steering wheel input torque. The block uses the steering wheel input torque and torque assist to calculate the steering dynamics. If you select the Ackerman steering parameter, you can specify a lookup table of percentage Ackerman values to calculate the Ackerman steering effects, or a constant Ackerman percentage, where 100 percent means perfect Ackerman steering.

If you select the Power assist, Ackerman steering, or Kingpin moment parameters in the Input signals section, you can specify additional inputs for the external power assist torques, percent Ackerman values, or kingpin moments.

Use the Steered axle parameter to specify whether the front or rear axle is steered.

| Setting | Implementation |
| :--- | :--- |
| Front | Front axle steering |
| Rear | Rear axle steering |

## Steering

## Rack-and-Pinion

For rack-and-pinion steering, pinion rotation causes linear motion of the rack, which steers the wheels through the tie rods and steering arms.


To calculate the steered wheel angles, the block uses these equations.

$$
\begin{aligned}
& l_{1}=\frac{T W-l_{\text {rack }}}{2}-\Delta P \\
& l_{2} 2=l_{1} 2+D^{2} \\
& \Delta P=r \delta_{\text {in }} \\
& \beta=\frac{\Pi}{2}-\tan ^{-1}\left[\frac{D}{l_{1}}\right]-\cos ^{-1}\left[\frac{l_{\text {arm }}{ }^{2}+l_{2} 2-l_{\text {rod }}{ }^{2}}{2 l_{\text {arm }} l_{2}}\right]
\end{aligned}
$$

The illustration and equations use these variables.

| $\delta_{i n}$ | Pinion angle (steering shaft angle into pinion) |
| :--- | :--- |
| $\delta_{L}$ | Left wheel steer angle |
| $\delta_{R}$ | Right wheel steer angle |
| $T W$ | Track width |
| $r$ | Pinion radius |
| $\Delta P$ | Linear change in rack position from "straight ahead" position |
| $D$ | Longitudinal distance between rack and steered axle |
| $l_{\text {rack }}$ | Rack length (distance between inner tie-rod ends) |
| $l_{\text {arm }}$ | Steering arm length |
| $l_{\text {rod }}$ | Tie rod length |

## Ackerman Steering

For $100 \%$ (ideal) Ackerman steering, all wheels follow circular arcs with the same center point.


To calculate the steered wheel angles, the Ackerman block uses these equations:

$$
\begin{aligned}
& \cot \left(\delta_{L}\right)-\cot \left(\delta_{R}\right)=\frac{T W}{W B} \\
& \delta_{A c k}=\frac{\delta_{i n}}{\gamma} \\
& \delta_{L}=\tan ^{-1}\left(\frac{W B \tan \left(\delta_{A c k}\right)}{W B+0.5 T W \tan \left(\delta_{A c k}\right)}\right) \\
& \delta_{R}=\tan ^{-1}\left(\frac{W B \tan \left(\delta_{A c k}\right)}{W B-0.5 T W \tan \left(\delta_{A c k}\right)}\right)
\end{aligned}
$$

Definition of variables used:
$\delta_{\text {in }} \quad$ Pinion angle (steering shaft angle into pinion)

| $\delta_{L}$ | Left wheel steer angle |
| :--- | :--- |
| $\delta_{R}$ | Right wheel steer angle |
| $\delta_{\text {Ack }}$ | Ackerman steer angle |
| $T W$ | Track width |
| $W B$ | Wheel base |
| $\gamma$ | Steering ratio: Ratio of pinion angle to Ackerman angle |

## Ports

Input
VehSpd - Vehicle speed
scalar
Vehicle speed, $v$, in $\mathrm{m} / \mathrm{s}$, specified as a scalar. This is the magnitude of the vehicle CG longitudinal velocity vector.

## CstrAng - Wheel caster angle

1-by-2 vector
Wheel caster angle, $\tau_{L}$, in radians, specified as a 1-by- 2 vector. The first element is the angle for the left wheel and the second is the angle for the right wheel.

## Dependencies

To enable this port, clear Input signals > Kingpin moment.
WhIAngFdk - Wheel steer angle feedback
1-by-2 vector
Wheel steer angle feedback, in radians, specified as a 1-by-2 vector. The first element is the angle feedback from the left wheel and the second element is the angle feedback from the right wheel.

## Dependencies

To enable this port, clear Input signals > Kingpin moment.
Angln - Steering wheel angle input
scalar
Steering wheel angle input from driver, in radians, specified as a scalar.

## Dependencies

To enable this port, select Steering inputs > Angle.
TrqIn - Steering torque input

## scalar

Steering wheel torque input from driver, in $\mathrm{N}^{*} \mathrm{~m}$, specified as a scalar.

## Dependencies

To enable this port, select Steering inputs > Torque.

## PwrAstTrq - Power assist torque

scalar
The torque value of power assist on the steering shaft, in $N * m$, specified as a scalar. Supplied externally into this port.

## Dependencies

To enable this port, select Input signals > Power assist.
PctAck - Percent Ackerman value
scalar
The Ackerman value in percent, specified as a scalar. Supplied externally into this port.
Dependencies
To enable this port, select Input signals > Ackerman steering.
TireFdk - Tire forces and moments feedback
1-by-12 vector
Tire forces and moments feedback from both right and left tires, specified as a 1-by-12 vector that contains the following values, in order:

| Description | Unit |
| :--- | :--- |
| $x$-directional Force, Left | N |
| $x$-directional Force, Right | N |
| $y$-directional Force, Left | N |
| $y$-directional Force, Right | N |
| $z$-directional Force, Left | N |
| $z$-directional Force, Right | N |
| $x$-directional Moment, Left | $\mathrm{N}^{*} \mathrm{~m}$ |
| $x$-directional Moment, Right | $\mathrm{N}^{*} \mathrm{~m}$ |
| $y$-directional Moment, Left | $\mathrm{N}^{*} \mathrm{~m}$ |
| $y$-directional Moment, Right | $\mathrm{N}^{*} \mathrm{~m}$ |
| $z$-directional Moment, Left | $\mathrm{N}^{*} \mathrm{~m}$ |
| $z$-directional Moment, Right | $\mathrm{N}^{*} \mathrm{~m}$ |

## Dependencies

To enable this port, clear Input signals > Kingpin moment.

## LftKpM - Left kingpin moment

scalar
Left kingpin moment, in $\mathrm{N}^{*}$ m, specified as a scalar.

## Dependencies

To enable this port, select Input signals > Kingpin moment.

RghtKpM — Right kingpin moment
scalar
Right kingpin moment, in $N *$, specified as a scalar.

## Dependencies

To enable this port, select Input signals > Kingpin moment.

## Output

Info - Vehicle dynamics information
bus
Vehicle dynamics information, returned as a bus signal that contains the following:

| Signal | Description | Unit |
| :--- | :--- | :--- |
| StrWhlAngFdk | Steering wheel angle | rad |
| AstTrq | Torque applied by power assist | $\mathrm{N} \cdot \mathrm{m}$ |
| AstPwr | Power applied by power assist | W |
| LftTieRodForce | Axial force in left tie rod | N |
| RghtTieRodForce | Axial force in right tie rod | N |
| LftKpM | Left kingpin moment | $\mathrm{N} \cdot \mathrm{m}$ |
| RghtKpM | Right kingpin moment | $\mathrm{N} \cdot \mathrm{m}$ |
| LftWhlAng | Left wheel steer angle | rad |
| RghtWhlAng | Right wheel steer angle | rad |
| LftWhlSpd | Left wheel steer angle velocity | $\mathrm{rad} / \mathrm{s}$ |
| RghtWhlSpd | Right wheel steer angle velocity | $\mathrm{rad} / \mathrm{s}$ |
| TrqIn | Torque applied by driver on <br> steering wheel | $\mathrm{N} \cdot \mathrm{m}$ |

AngLft - Left wheel steer angle
scalar
Left wheel steer angle, $\delta_{L}$, in radians, returned as a scalar.
AngRght - Right wheel steer angle
scalar
Right wheel steer angle, $\delta_{R}$, in radians, returned as a scalar.

## Parameters

## Block Options

Type - Steering type
Rack and pinion (default)
Steering type for the Steering System.

Intermediate shaft type - Intermediate shaft type Single Cardan joint (default)|Double Cardan joints

Whether to model the intermediate shaft type using single or double Cardan joints.
Power assist - Whether to model power assist
on (default) | off
Select to model power assist within the Steering System.

## Dependencies

To enable this parameter, in the Input signals section, clear Power assist.
Ackerman steering - Whether to use Ackerman steering
on (default) | off
Select to set Ackerman steering percentage within the Steering System block.

## Dependencies

To enable this parameter, in the Input signals section, clear Ackerman steering.
Input Signals
Power assist - Specifies power assist torque externally
off (default) | on
Select this parameter to enable the PwrAstTrq port.
Ackerman steering - Specifies percent Ackerman value externally
off (default) | on
Select this parameter to enable the PctAck port.
Kingpin moment - Specifies left and right kingpin moments
off (default) | on
Select this parameter to enable the $\mathbf{L f t K p M}$ and RghtKpM ports.
Steered axle - Location of steering system
Front (default) | Rear
Select either the front or rear axle as the location of the Steering System.
Steering inputs - Steering wheel angle or torque
Angle (default) | Torque
This selection enables either the AngIn or TrqIn port as the driver input.

## General

Track width, TrckWdth - Track width
1 (default) | scalar
Track width, $T W$, in m , specified as a scalar.

Steering angle input range, StrRng - Steering wheel range
1.25*pi (default)|scalar

Steering wheel angle from straight-ahead to either left or right lock, in rad, specified as a scalar. This causes both steered wheels to remain within their designed steering range.

Steering angle input deadband width, DbWdth - Steering angle input deadband width 0 (default) | scalar

The steering wheel deadband angle, in radians, from left-engagement to right-engagement.
Steering wheel inertia, StrWhlInert - Steering wheel inertia
0.1 (default) | scalar

Steering wheel moment of inertia, in $\mathrm{kg}^{*} \mathrm{~m}^{2}$, specified as a scalar.
Steering shaft inertia, StrColInert - Inertia of steering shaft
0.01 (default) | scalar

Steering shaft moment of inertia, in $\mathrm{kg}^{*} \mathrm{~m}^{2}$, specified as a scalar.
Kingpin offset, KngpnOfst - Kingpin offset
0.075 (default) | scalar

Kingpin offset, in m, specified as a scalar.
Kingpin inclination angle, Lambda - Kingpin inclination angle
0. 2094 (default) | scalar

Kingpin inclination angle, in rad, specified as a scalar.
Hub lead, HbLead - Hub lead
4.00E-05 (default) | scalar

Hub lead, in m, specified as a scalar.
Static loaded radius, StcLdRadius - Static loaded radius
0.4 (default) | scalar

Static loaded tire radius, in m , specified as a scalar.
Overall steering ratio, OvrlStrRatio - Overall steering ratio
17.42 (default) | scalar

Overall steering ratio, specified as a scalar.
Steering angle breakpoints, StrgAngBpts - Steering wheel angle breakpoints

6.2832] (default)

Steering wheel angle breakpoints, in rad, specified as a 1-by-11 vector. Is used to parameterize either Ackerman value or rack gain.

## Dependencies

To enable this parameter, set one of these parameters to Lookup table:

- Rack and pinion > Rack gain parameterized by
- Ackerman steering > Percent Ackerman parameterized by

CstrAng - Caster angle
0 (default) | scalar
Caster angle, in rad, specified as a scalar.

## Dependencies

To enable this parameter, select Input signals > Kingpin moment.

## Rack and Pinion

Rack gain parameterized by - Rack gain parameterization
Constant (default)|Lookup table
Whether to parameterize the rack gain as a constant value or by using a lookup table.
Rack gain, RckGn - Rack gain
0.062 (default) | scalar

Rack gain, in $\mathrm{m} / \mathrm{rev}$, specified as a scalar.

## Dependencies

To enable this parameter, set Rack gain parameterized by to Constant.
Rack gain table, RckGnTbl - Rack gain table
ones $(1,11) * 0.0057 * 2 *$ pi (default) | 1-by-11 vector
Rack gain table, in m/rev, specified as a 1-by-11 vector.
Dependencies
To enable this parameter, set Rack gain parameterized by to Lookup table.
Steering arm length, StrgArmLngth - Steering arm length
0.1 (default) | scalar

Steering arm length, in m , specified as a scalar.
Rack casing length, RckCsLngth - Rack length
0.5 (default) | scalar

Rack length (distance between inner tie rod ends), in $m$, specified as a scalar.
Tie rod length, TieRodLngth - Tie rod length
0.248 (default) | scalar

Tie rod length, $l_{\text {rod }}$, in $m$, specified as a scalar.
Distance between axis and rack, Dst - Distance between axle and rack
0.2 (default) | scalar

Longitudinal distance between the steered axle and rack centerline, $D$, in m , specified as a scalar.

Efficiency of gears, Epsilon - Efficiency of gears
0.9 (default) | scalar

Efficiency of the rack and pinion mechanism, $\varepsilon$, specified as a scalar.
Pinion inertia, PnInert - Pinion inertia
0.1 (default) | scalar

Pinion inertia, in $\mathrm{kg}^{*} \mathrm{~m}^{2}$, specified as a scalar.

## Single Cardan Joint

Spatial angle for the single Cardan joint, SptlAng - Spatial angle for the single Cardan joint 2.6178 (default) | scalar

Spatial angle for the single Cardan joint, in rad, specified as a scalar.

## Dependencies

To enable this parameter, set Intermediate shaft type to Single Cardan joint.

## Double Cardan Joints

Spatial angle for the upper Cardan joint, Alpha_b - Spatial angle for upper Cardan joint
2.6178 (default) | scalar

Spatial angle for the upper Cardan joint, in rad, specified as a scalar.

## Dependencies

To enable this parameter, set Intermediate shaft type to Double Cardan joints.
Spatial angle for the lower Cardan joint, Alpha_c - Spatial angle for lower Cardan joint 2.7051 (default) | scalar

Spatial angle for the lower Cardan joint, in rad, specified as a scalar.

## Dependencies

To enable this parameter, set Intermediate shaft type to Double Cardan joints.
Edge view angle between the planes of the two joints, Sigma_bc - Edge view angle between planes of the two joints
0.2618 (default) | scalar

Edge view angle between the planes of the two joints, in rad, specified as a scalar.

## Dependencies

To enable this parameter, set Intermediate shaft type to Double Cardan joints.
Phase angle, Gamma - Phase angle
0.2618 (default) | scalar

Rotation phase angle between the two joints, in rad, specified as a scalar.

## Dependencies

To enable this parameter, set Intermediate shaft type to Double Cardan joints.

## Power Assist

Steering wheel torque breakpoints, TrqBpts - Steering wheel torque breakpoints
[-100 0 100] (default)| 1-by-M vector
Steering wheel torque breakpoints, in $N \cdot m$, specified as a 1-by- $M$ vector.

## Dependencies

To enable this parameter, select the Power assist Block Option.
Vehicle speed breakpoints, VehSpdBpts - Vehicle speed breakpoints
[0 20] (default)| 1-by-N vector
Vehicle speed breakpoints, in m/s, specified as a 1-by- $N$ vector.

## Dependencies

To enable this parameter, select the Power assist Block Option.
Assisting torque table, TrqTbI - Torque assist table
[0 -100;0 0;0 100] (default)|M-by-N matrix
Torque assist table, $f_{\text {trq }}$, in $\mathrm{N} \cdot \mathrm{m}$, specified as an $M$-by- $N$ matrix.
The torque assist lookup table is a function of the vehicle speed, $v$, and steering wheel input torque, $\tau_{i n}$ :
$\tau_{\text {ast }}=f_{t r q}\left(v, \tau_{\text {in }}\right)$.
The block applies the steering wheel input torque and torque assist to the pinion.

## Dependencies

To enable this parameter, select the Power assist Block Option.
Assisting torque limit, TrqLmt - Torque assist limit
100 (default) | scalar
Torque assist limit, in $\mathrm{N} \cdot \mathrm{m}$, specified as a scalar.

## Dependencies

To enable this parameter, select the Power assist Block Option.
Assisting power limit, PwrLmt - Assist power limit
1000 (default) | scalar
Assist power limit, in watts, specified as a scalar.

## Dependencies

To enable this parameter, select the Power assist Block Option.
Assisting torque efficiency, Eta - Torque assist efficiency
1 (default) | scalar
Torque assist efficiency, specified as a scalar.

## Dependencies

To enable this parameter, select the Power assist Block Option.

## Cutoff frequency, CutOmege [rad/s] - Cutoff frequency <br> 200 (default) | scalar

Cutoff frequency, in rad/s, specified as a scalar.

## Dependencies

To enable this parameter, select the Power assist Block Option.

## Ackerman Steering

Percent Ackerman parameterized by - Ackerman parameterization
Constant (default)| Lookup table
Whether to parameterize the Ackerman values as a constant value or by a lookup table.

## Dependencies

To enable this parameter, select the Ackerman steering Block Option.
Percent Ackerman, PctAck - Percent Ackerman
100 (default) | scalar
Percent Ackerman, specified as a scalar.

## Dependencies

To enable this parameter, select the Ackerman steering Block Option and set Percent Ackerman parameterized by to Constant.

Percent Ackerman table, PctAckTbI - Percent Ackerman table
ones (1,11)*100 (default)
Percent Ackerman table, specified as a 1-by-11 vector.

## Dependencies

To enable this parameter, select the Ackerman steering Block Option and set Percent Ackerman parameterized by to Lookup table.

Friction and Compliance
Sealing stiffness, SlgStf - Sealing stiffness
1.5e4 (default) | scalar

Sealing stiffness, in $\mathrm{N}^{*} \mathrm{~m} / \mathrm{rad}$, specified as a scalar.
Upper boundary friction, UpprFric - Upper boundary friction
1 (default) | scalar
Upper boundary friction, in N , specified as a scalar.
Pressure change due to friction boundary increase, PrsFric - Pressure change due to friction boundary increase
1e-5 (default) | scalar

Pressure change due to friction boundary increase, in N/bar, specified as a scalar.
Maxwell element stiffness, MaxStf - Maxwell element stiffness
10000 (default) | scalar
Maxwell element stiffness, in $N * m / r a d$, specified as a scalar.
Maxwell element upper boundary friction, MaxUpprFric - Maxwell element upper boundary friction
0.2 (default) | scalar

Maxwell element upper boundary friction, in N , specified as a scalar.
Maxwell linear damping coefficient, MaxDamp - Maxwell linear damping coefficient 1 (default) | scalar

Maxwell linear damping coefficient, specified as a scalar.
Torsion bar stiffness coefficient, TorStf - Torsional stiffness of steering shaft
30 (default) | scalar
Torsional stiffness of steering shaft, in $\mathrm{N} * \mathrm{~m} / \mathrm{rad}$, specified as a scalar.
Torsion bar damping coefficient, TorDamp - Torsional viscous damping in steering shaft
1 (default) | scalar
Torsional viscous damping in steering shaft, in $\mathrm{N} * \mathrm{~m} *$ s/rad, specified as a scalar.

## Version History

Introduced in R2022b

## References

[1] Crolla, David, David Foster, et al. Encyclopedia of Automotive Engineering. Volume 4, Part 5 (Chassis Systems) and Part 6 (Electrical and Electronic Systems). Chichester, West Sussex, United Kingdom: John Wiley \& Sons Ltd, 2015.
[2] Gillespie, Thomas. Fundamentals of Vehicle Dynamics. Warrendale, PA: Society of Automotive Engineers, 1992.
[3] Vehicle Dynamics Standards Committee. Vehicle Dynamics Terminology. SAE J670. Warrendale, PA: Society of Automotive Engineers, 2008.

## Extended Capabilities

## C/C++ Code Generation

Generate C and C++ code using Simulink $\circledR_{\circledR}$ Coder ${ }^{\mathrm{TM}}$.

## See Also

Kinematic Steering | Mapped Steering

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"

## Independent Suspension - Double Wishbone

Double wishbone independent suspension



## Libraries:

Vehicle Dynamics Blockset / Suspension

## Description

The Independent Suspension - Double Wishbone block implements an independent double wishbone suspension for multiple axles with multiple wheels per axle.

The block models the suspension compliance, damping, and geometric effects as functions of the relative positions and velocities of the vehicle and wheel carrier with axle-specific compliance and damping parameters. Using the suspension compliance and damping, the block calculates the suspension force on the vehicle and wheel. The block uses the Z-down coordinate system (defined in SAE J670).

| For Each | You Can Specify |
| :--- | :--- |
| Axle | - Multiple wheels |
|  | - An anti-sway bar for axles with two wheels |
|  | - Suspension parameters |
| Wheel | - Steering angles |

The block contains energy-storing spring elements and energy-dissipating damper elements. It does not contain energy-storing mass elements. The block assumes that the vehicle (sprung) and wheel (unsprung) blocks connected to the block store the mass-related suspension energy.

This table summarizes the block parameter settings for a vehicle with:

- Two axles
- Two wheels per axle
- Steering angle input for both wheels on the front axle
- An anti-sway bar on the front axle

| Parameter | Setting |
| :--- | :--- |
| Number of axles, NumAxl | 2 |
| Number of wheels by axle, NumWhlsByAxl | $\left[\begin{array}{ll}2 & 2\end{array}\right]$ |
| Steered axle enable by axle, StrgEnByAxl | $\left[\begin{array}{ll}1 & 0\end{array}\right]$ |
| Anti-Sway axle enable by axle, <br> AntiSwayEnByAxl | $\left[\begin{array}{ll}1 & 0\end{array}\right]$ |

The block uses the wheel number, $t$, to index the input and output signals. This table summarizes the wheel, axle, and corresponding wheel number for a vehicle with:

- Two axles
- Two wheels per axle

| Wheel | Axle | Wheel Number |
| :--- | :--- | :--- |
| Front left | Front | 1 |
| Front right | Front | 2 |
| Rear left | Rear | 1 |
| Rear right | Rear | 2 |

## Suspension Compliance and Damping

The block uses a linear spring and damper to model the vertical dynamic effects of the suspension system. Using the relative positions and velocities of the vehicle and wheel carrier, the block calculates the vertical suspension forces on the wheel and vehicle. The block uses a linear equation that relates the vertical damping and compliance to the suspension height, suspension height rate of change, and absolute value of the steering angles.

The block implements this equation.

$$
F_{w z_{a, t}}=F_{z 0_{a}}+k_{z_{a}}\left(z_{v_{a, t}}-z_{w_{a, t}}+m_{\text {hsteer }_{a}}\left|\delta_{\text {steer }_{a, t}}\right|\right)+c\left(\dot{z}_{v_{a, t}}-\dot{z}_{w_{a, t}}\right)+F_{z h s t o p_{a, t}}+F_{z a s w y_{a, t}}
$$

The damping coefficient, $c$, depends on the Enable active damping parameter setting.

| Enable active damping <br> Setting | Damping |
| :--- | :--- |
| off | Constant, $c=c_{z_{a}}$ |
| on | Lookup table that is a function of active damper duty cycle and <br> actuator velocity |
|  | $c=f\left(\right.$ duty, $\left.\left(\dot{z}_{v_{a, t}}-\dot{z}_{w_{a, t}}\right)\right)$ |

The block assumes that the suspension elements have no mass. Therefore, the suspension forces and moments applied to the vehicle are equal to the suspension forces and moments applied to the wheel.

$$
\begin{aligned}
& F_{v x_{a, t}}=F_{w x_{a, t}} \\
& F_{v y_{a, t}}=F_{w y_{a, t}} \\
& F_{v z_{a, t}}=-F_{w z_{a, t}} \\
& M_{v x_{a, t}}=M_{w x_{a, t}}+F_{w y_{a, t}}\left(R e_{w y_{a, t}}+H_{a, t}\right) \\
& M_{v y_{a, t}}=M_{w y_{a, t}}+F_{w x_{a, t}}\left(R e_{w x_{a, t}}+H_{a, t}\right) \\
& M_{v x_{a, t}}=M_{w x_{a, t}}
\end{aligned}
$$

The block sets the wheel positions and velocities equal to the vehicle lateral and longitudinal positions and velocities.

$$
\begin{aligned}
& x_{w_{a, t}}=x_{v_{a, t}} \\
& y_{w_{a, t}}=y_{v_{a, t}} \\
& \dot{x}_{w_{a, t}}=\dot{x}_{v_{a, t}} \\
& \dot{y}_{w_{a, t}}=\dot{y}_{v_{a, t}}
\end{aligned}
$$

The equations use these variables.

| $F_{w z_{z_{l}, t}} M_{w z_{a, t}}$ | Suspension force and moment applied to the wheel on axle $a$, wheel $t$ along wheel-fixed $z$-axis |
| :---: | :---: |
| $F_{w x_{\alpha, t}} M_{w x_{\alpha, t}}$ | Suspension force and moment applied to the wheel on axle $a$, wheel $t$ along wheel-fixed $x$-axis |
| $F_{w y_{d, t}} M_{w y_{a, t}}$ | Suspension force and moment applied to the wheel on axle $a$, wheel $t$ along wheel-fixed $y$-axis |
| $F_{v z_{a}, t^{\prime}} M_{v z_{a, t}}$ | Suspension force and moment applied to the vehicle on axle a, wheel $t$ along wheel-fixed $z$-axis |
| $F_{v x_{a}, t}, M_{v x_{a, t}}$ | Suspension force and moment applied to the vehicle on axle a, wheel t along wheel-fixed $x$-axis |
| $F_{v y_{a, t}} M_{v y_{a, t}}$ | Suspension force and moment applied to the vehicle on axle a, wheel t along wheel-fixed $y$-axis |
| $F_{z 0_{a}}$ | Vertical suspension spring preload force applied to the wheels on axle a |
| $k_{z_{a}}$ | Vertical spring constant applied to wheels on axle a |
| $k w a_{z}$ | Wheel and axle interface compliance constant |
| $m_{\text {hsteer }}$ | Steering angle to vertical force slope applied at wheel carrier for wheels on axle a |
| $\delta_{\text {steer }}{ }_{\text {at, }}$ | Steering angle input for axle a, wheel t |
| $C_{z_{a}}$ | Vertical damping constant applied to wheels on axle a |
| cwa ${ }_{z}$ | Wheel and axle interface damping constant |
| $R e_{w_{a, t}}$ | Effective wheel radius for axle a, wheel t |
| $F_{z h s t o p_{a, t}}$ | Vertical hardstop force at axle a , wheel t , along the vehicle-fixed $z$-axis |
| $F_{\text {zaswy }{ }_{\text {a }}}$ | Vertical anti-sway force at axle a , wheel t , along the vehicle-fixed $z$-axis |
| $F w a_{z 0}$ | Wheel and axle interface compliance constant |
| $z_{v_{a, t}} \dot{z}_{v_{a, t}}$ | Vehicle displacement and velocity at axle $a$, wheel t , along the vehiclefixed $z$-axis |
| $z_{w_{a, t},} \dot{z}_{w_{a, t}}$ | Wheel displacement and velocity at axle $a$, wheel t , along the vehicle-fixed $z$-axis |
| $\chi_{v_{a, t}} \dot{\chi}_{v_{a, t}}$ | Vehicle displacement and velocity at axle $a$, wheel $t$, along the vehiclefixed $z$-axis |
| $\chi_{w_{a, t}} \dot{\chi}_{w_{a t t}}$ | Wheel displacement and velocity at axle a, wheel t , along the vehicle-fixed $z$-axis |
| $y_{v_{a, t}} \dot{y}_{v_{a, t}}$ | Vehicle displacement and velocity at axle $a$, wheel $t$, along the vehiclefixed $y$-axis |


| $y_{w_{a, t}} \dot{y}_{w_{a, t}}$ | Wheel displacement and velocity at axle a, wheel t, along the vehicle-fixed |
| :--- | :--- |
| $H_{a, t}$ | $y$-axis |
| $R e_{w_{a, t}}$ | Suspension height at axle a, wheel t |

## Hardstop Forces

The hardstop feedback force, $F_{\text {zhstop } a_{a, 1}}$ that the block applies depends on whether the suspension is compressing or extending. The block applies the force:

- In compression, when the suspension is compressed more than the maximum distance specified by the Suspension maximum height, Hmax parameter.
- In extension, when the suspension extension is greater than maximum extension specified by the Suspension maximum height, Hmax parameter.

To calculate the force, the block uses a stiffness based on a hyperbolic tangent and exponential scaling.

## Anti-Sway Bar

Optionally, use the Anti-sway axle enable by axle, AntiSwayEnByAxl parameter to implement an anti-sway bar force, $F_{z a s w y_{a, t}}$ for axles that have two wheels. This figure shows how the anti-sway bar transmits torque between two independent suspension wheels on a shared axle. Each independent suspension applies a torque to the anti-sway bar via a radius arm that extends from the anti-sway bar back to the independent suspension connection point.


To calculate the sway bar force, the block implements these equations.

| Calculation | Equation |
| :--- | :--- |
| Anti-sway bar angular deflection <br> for a given axle and wheel, $\Delta \theta_{a, t}$ | $\theta_{0 a}=\tan ^{-1}\left(\frac{z_{0}}{r}\right)$ |
|  | $\Delta \theta_{a, t}=\tan ^{-1}\left(\frac{r \tan \theta_{0 a}-z_{w_{a, t}}+z_{v_{a, t}}}{r}\right)$ |


| Calculation | Equation |
| :--- | :--- |
| Anti-sway bar twist angle, $\theta_{a}$ | $\theta_{a}=-\tan ^{-1}\left(\frac{r \tan \theta_{0 a}-z_{w_{a, 1}}+z_{v_{a, 1}}}{r}\right)$ |
|  | $-\tan ^{-1}\left(\frac{r \tan \theta_{0 a}-z_{w_{a, 2}}+z_{v_{a, 2}}}{r}\right)$ |
| Anti-sway bar torque, $\tau_{a}$ | $\tau_{a}=k_{a} \theta_{a}$ |
| Anti-sway bar forces applied to <br> the wheel on axle $a$, wheel t <br> along wheel-fixed $z$-axis | $F_{z a s w y_{a, 1}}=\left(\frac{\tau_{a}}{r}\right) \cos \left(\theta_{0 a}-\tan ^{-1}\left(\frac{r \tan \theta_{0 a}-z_{w_{a, 1}}+z_{v_{a, 1}}}{r}\right)\right)$ |
|  | $F_{z a s w y_{a, 2}}=\left(\frac{\tau_{a}}{r}\right) \cos \left(\theta_{0 a}-\tan ^{-1}\left(\frac{r \tan \theta_{0 a}-z_{w_{a, 2}}+z_{v_{a, 2}}}{r}\right)\right)$ |

The equations and figure use these variables.

| $\tau_{a}$ | Anti-sway bar torque |
| :--- | :--- |
| $\theta$ | Anti-sway bar twist angle |
| $\theta_{0 a}$ | Initial anti-sway bar twist angle |
| $\Delta \theta_{a, t}$ | Anti-sway bar angular deflection at axle a, wheel t |
| $r$ | Anti-sway bar arm radius |
| $z_{0}$ | Vertical distance from anti-sway bar connection point to anti-sway bar centerline |
| $F_{z s w a y_{a, t}}$ | Anti-sway bar force applied to the wheel on axle a, wheel t along wheel-fixed $z$-axis |
| $z_{v_{a, t}}$ | Vehicle displacement at axle a, wheel t , along the vehicle-fixed $z$-axis |
| $z_{w_{a, t}}$ | Wheel displacement at axle a, wheel t, along the vehicle-fixed $z$-axis |

## Camber, Caster, and Toe Angles

To calculate the camber, caster, and toe angles, block uses linear functions of the suspension height and steering angle.

$$
\begin{aligned}
& \xi_{a, t}=\xi_{0 a}+m_{\text {hcamber }_{a}}\left(z_{w_{a, t}}-z_{v_{a, t}}-m_{\text {hsteer }_{a}}\left|\delta_{\text {steer }_{a}, t}\right|\right)+m_{\text {cambersteer }_{a}}\left|\delta_{\text {steer }_{a, t}}\right| \\
& \eta_{a, t}=\eta_{0 a}+m_{\text {hcaster }_{a}}\left(z_{w_{a, t}}-z_{v_{a, t}}-m_{\text {hsteer }_{a}}\left|\delta_{\text {steer }_{a}, t}\right|\right)+m_{\text {castersteer }_{a}}\left|\delta_{\text {steer }_{a, t}}\right| \\
& \zeta_{a, t}=\zeta_{0 a}+m_{\text {htoe }_{a}}\left(z_{w_{a, t}}-z_{v_{a, t}}-m_{\text {hsteer }_{a}}\left|\delta_{\text {steer }_{a, t}}\right|\right)+m_{\text {toesteer }_{a}}\left|\delta_{\text {steer }_{a}, t}\right|
\end{aligned}
$$

The equations use these variables.

| $\xi_{a, t}$ | Camber angle of wheel on axle a, wheel t |
| :--- | :--- |
| $\eta_{a, t}$ | Caster angle of wheel on axle a, wheel t |
| $\zeta_{a, t}$ | Toe angle of wheel on axle a, wheel t |
| $\xi_{0 a}, \eta_{0 a}, \zeta_{0 a}$ | Nominal suspension axle a camber, caster, and toe angles, respectively, at <br> $m_{\text {camber }_{a^{\prime}}}$ <br> $m_{\text {hcosteo }_{a}{ }^{\prime}}$ |
| zero steering angle |  |
| Camber, caster, and toe angles, respectively, versus suspension height slope |  |
| for axle a |  |

$m_{\text {camberster }_{a^{\prime}}} m_{\text {casterster }_{a^{\prime}}}$ Camber, caster, and toe angles, respectively, versus steering angle slope for
$m_{\text {toesteer }_{a}} \quad$ axle a
$m_{h s t e r_{a}} \quad$ Steering angle versus vertical force slope for axle a
$\delta_{\text {steer }_{a, t}} \quad$ Steering angle input for axle a, wheel t
$z_{v_{a t}}$
$z_{w_{a, t}}$

Vehicle displacement at axle a, wheel t , along the vehicle-fixed $z$-axis Wheel displacement at axle a, wheel t , along the vehicle-fixed $z$-axis

## Steering Angles

Optionally, use the Steered axle enable by axle, StrgEnByAxl parameter to input steering angles for the wheels. To calculate the steering angles for the wheels, the block offsets the input steering angles with a linear function of the suspension height.

$$
\delta_{\text {whlsteer }_{a, t}}=\delta_{\text {steer }_{a, t}}+m_{\text {htoe }_{a}}\left(z_{w_{a, t}}-z_{v_{a, t}}-m_{\text {hsteer }_{a}}\left|\delta_{\text {steer }_{a, t}}\right|\right)+m_{\text {toesteer }_{a}}\left|\delta_{\text {steer }_{a, t}}\right|
$$

The equation uses these variables.

| $m_{\text {toesteer }_{a}}$ | Axle a toe angle versus steering angle slope |
| :--- | :--- |
| $m_{\text {hsteer }_{a}}$ | Axle a steering angle versus vertical force slope |
| $m_{\text {htoe }_{a}}$ | Axle a toe angle versus suspension height slope |
| $\delta_{\text {whlster }_{a, t}}$ | Wheel steering angle for axle a, wheel t |
| $\delta_{\text {stee }_{a, t}}$ | Steering angle input for axle a, wheel t |
| $z_{v_{a, t}}$ | Vehicle displacement at axle a, wheel t , along the vehicle-fixed $z$-axis |
| $z_{w_{a, t}}$ | Wheel displacement at axle a , wheel t , along the vehicle-fixed $z$-axis |

## Power and Energy

The block calculates these suspension characteristics for each axle, a , wheel, t .

| Calculation | Equation |
| :---: | :---: |
| Dissipated power, $P_{\text {susp }_{a, t}}$ | $P_{\text {susp }_{a, t}}=F_{\text {wzlookup }^{\prime}}\left(\dot{z}_{v_{a, t}}-\dot{z}_{w_{a, t} t^{\prime}} \dot{z}_{v_{a, t}}-\dot{z}_{w_{a, t^{\prime}}} \delta_{\text {steer }_{a, t}}\right)$ |
| Absorbed energy, $E_{\text {susp }_{\text {a }}}$ | $E_{\text {susp }_{a, t}}=F_{\text {wzlookup }_{a}}\left(\dot{z}_{v_{a, t}}-\dot{z}_{w_{a, t}} \dot{z}_{v_{a, t}}-\dot{z}_{w_{a, t^{\prime}}} \delta_{\text {steer }}{ }_{a, t}\right)$ |
| Suspension height, $H_{a, t}$ | $H_{a, t}=-\left(z_{v_{a, t}}-z_{w_{a, t}}+\frac{F_{z 0_{a}}}{k_{z_{a}}}+m_{\text {hsteer }}\left\|\delta_{\text {steer }_{a, t}}\right\|\right)$ |
| Distance from wheel carrier center to tire/road interface | $z_{w t r_{a, t}}=R e_{w_{a, t}}+H_{a, t}$ |

The equations use these variables.
$m_{\text {hsteer }}^{a} \quad$ Steering angle to vertical force slope applied at wheel carrier for wheels on axle a
$\delta_{\text {steer }_{a}} \quad$ Steering angle input for axle a , wheel t
$R e_{w_{a, t}} \quad$ Axle a, wheel $t$ effective wheel radius from wheel carrier center to tire/road interface
$F_{z 0_{a}} \quad$ Vertical suspension spring preload force applied to the wheels on axle a
$z_{\text {wtr }_{a, t}} \quad$ Distance from wheel carrier center to tire/road interface, along the vehicle-fixed $z$ axis
$z_{v_{a t}, t}{\dot{v_{a, t}}} \quad$ Vehicle displacement and velocity at axle a, wheel t , along the vehicle-fixed $z$-axis
$z_{w_{a, t}} \dot{z}_{w_{a, t}} \quad$ Wheel displacement and velocity at axle a, wheel t , along the vehicle-fixed $z$-axis

## Ports

Input
WhIPz - Wheel z-axis displacement
array
Wheel displacement, $z_{w}$, along wheel-fixed $z$-axis, in m . Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlPz:

- Signal array dimensions are [1×4].

$$
\mathrm{WhlPz}=z_{w}=\left[z_{w_{1,1}} z_{w_{1,2}} z_{w_{2,1}} z_{w_{2,2}}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlPz $(1,1)$ | 1 | 1 |
| Front right | WhlPz $(1,2)$ | 1 | 2 |
| Rear left | WhlPz $(1,3)$ | 2 | 1 |
| Rear right | WhlPz $(1,4)$ | 2 | 2 |

WhIRe - Wheel effective radius
array
Effective wheel radius, $R e_{w}$, in m. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlRe:

- Signal array dimensions are [1×4].

WhlRe $=\operatorname{Re} e_{w}=\left[R e_{w_{1,1}} R e_{w_{1,2}} R e_{w_{2,1}} R e_{w_{2}, 2}\right]$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlRe $(1,1)$ | 1 | 1 |
| Front right | WhlRe $(1,2)$ | 1 | 2 |
| Rear left | WhlRe $(1,3)$ | 2 | 1 |
| Rear right | WhlRe $(1,4)$ | 2 | 2 |

WhIVz - Wheel z-axis velocity
array
Wheel velocity, $\dot{z}_{w}$, along wheel-fixed $z$-axis, in m. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlVz:

- Signal array dimensions are [1×4].

WhlVz $=\dot{z}_{w}=\left[\begin{array}{lll}\dot{z}_{w_{1,1}} & \dot{z}_{w_{1,2}} & \dot{z}_{w_{2,1}}\end{array} \dot{z}_{w_{2,2}}\right]$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlVz $(1,1)$ | 1 | 1 |
| Front right | WhlVz $(1,2)$ | 1 | 2 |
| Rear left | WhlVz $(1,3)$ | 2 | 1 |
| Rear right | WhlVz $(1,4)$ | 2 | 2 |

WhIFx - Longitudinal wheel force on vehicle
array
Longitudinal wheel force applied to vehicle, $F_{w x}$, along the vehicle-fixed $x$-axis. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlFx:

- Signal array dimensions are [1×4].

WhlFx $=F_{w x}=\left[F_{w x_{1,1}} F_{w x_{1,2}} F_{w x_{2,1}} F_{w x_{2}, 2}\right]$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlFx $(1,1)$ | 1 | 1 |
| Front right | WhlFx $(1,2)$ | 1 | 2 |
| Rear left | WhlFx $(1,3)$ | 2 | 1 |
| Rear right | WhlFx $(1,4)$ | 2 | 2 |

WhIFy - Lateral wheel force on vehicle
array
Lateral wheel force applied to vehicle, $F_{w y}$, along the vehicle-fixed $y$-axis. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlFy:

- Signal array dimensions are [1×4].

$$
\text { WhlFy }=F_{w y}=\left[F_{w y 1,1} F_{w y 1,2} F_{w y 2,1} F_{w y_{2,2}}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlFy $(1,1)$ | 1 | 1 |
| Front right | WhlFy $(1,2)$ | 1 | 2 |
| Rear left | WhlFy $(1.3)$ | 2 | 1 |
| Rear right | WhlFy $(1,4)$ | 2 | 2 |

WhIM - Suspension moment on wheel
array
Longitudinal, lateral, and vertical suspension moments at axle a, wheel $t$, applied to the wheel at the axle wheel carrier reference coordinate, in $N \cdot m$. Input array dimensions are 3 by the number of wheels on the vehicle.

- WhlM ( $1, \ldots$ ) - Suspension moment applied to the wheel about the vehicle-fixed $x$-axis (longitudinal)
- WhlM ( $2, \ldots$ ) - Suspension moment applied to the wheel about the vehicle-fixed $y$-axis (lateral)
- WhlM ( $3, \ldots$ ) - Suspension moment applied to the wheel about the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the WhlM:

- Signal dimensions are [3×4].
- Signal contains suspension moments applied to four wheels according to their axle and wheel locations.

$$
\text { WhlM }=M_{w}=\left[\begin{array}{lllll}
M_{w x_{1,1}} & M_{w x_{1,2}} & M_{w x_{2,1}} & M_{w x_{2,2}} \\
M_{w y_{1,1}} & M_{w y_{1,2}} & M_{w y_{2,1}} & M_{w y_{2,2}} \\
M_{w z_{1,1}} & M_{w z_{1,2}} & M_{w z_{2,1}} & M_{w z_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel Numbe r | Moment Axis |
| :---: | :---: | :---: | :---: | :---: |
| Front left | WhlM(1,1) | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front right | WhlM (1,2) | 1 | 2 |  |
| Rear left | WhlM ( 1,3 ) | 2 | 1 |  |
| Rear right | WhlM (1,4) | 2 | 2 |  |
| Front left | WhlM( 2,1 ) | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front right | WhlM (2,2) | 1 | 2 |  |
| Rear left | WhlM (2,3) | 2 | 1 |  |
| Rear right | WhlM ( 2,4 ) | 2 | 2 |  |
| Front left | WhlM (3,1) | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front right | WhlM (3,2) | 1 | 2 |  |


| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Moment Axis |
| :--- | :--- | :--- | :--- | :--- |
| Rear <br> left | WhlM(3,3) | 2 | 1 |  |
| Rear <br> right | WhlM(3,4) | 2 | 2 |  |

VehP - Vehicle displacement
array
Vehicle displacement from axle a, wheel $t$ along vehicle-fixed coordinate system, in m. Input array dimensions are 3 the number of wheels on the vehicle.

- $\operatorname{VehP}(1, \ldots)-$ Vehicle displacement from wheel, $x_{v}$, along the vehicle-fixed $x$-axis
- $\operatorname{VehP}(2, \ldots)$ - Vehicle displacement from wheel, $y_{v}$, along the vehicle-fixed $y$-axis
- $\operatorname{VehP}(3, \ldots)-$ Vehicle displacement from wheel, $z_{v}$, along the vehicle-fixed $z$-axis

For example, for a two-axle vehicle with two wheels per axle, the VehP:

- Signal dimensions are [3x4].
- Signal contains four displacements according to their axle and wheel locations.

VehP $=\left[\begin{array}{l}x_{v} \\ y_{v} \\ z_{v}\end{array}\right]=\left[\begin{array}{llll}x_{v_{1,1}} & x_{v_{1,2}} & x_{v_{2,1}} & x_{v_{2,2}} \\ y_{v_{1,1}} & y_{v_{1,2}} & y_{v_{2,1}} & y_{v_{2,2}} \\ z_{v_{1,1}} & z_{v_{1,2}} & z_{v_{2,1}} & z_{v_{2,2}}\end{array}\right]$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | $\operatorname{VehP}(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis |
| Front <br> right | $\operatorname{VehP}(1,2)$ | 1 | 2 |  |
| Rear <br> left | $\operatorname{VehP}(1,3)$ | 2 | 1 |  |
| Rear <br> right | $\operatorname{VehP}(1,4)$ | 2 | 2 |  |
| Front <br> left | $\operatorname{VehP}(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis |
| Front <br> right | $\operatorname{VehP}(2,2)$ | 1 | 2 |  |
| Rear <br> left | $\operatorname{VehP}(2,3)$ | 2 | 1 |  |
| Rear <br> right | $\operatorname{VehP}(2,4)$ | 2 | 2 |  |


| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | $\operatorname{VehP}(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis |
| Front <br> right | $\operatorname{VehP}(3,2)$ | 1 | 2 |  |
| Rear <br> left | $\operatorname{VehP}(3,3)$ | 2 | 1 |  |
| Rear <br> right | $\operatorname{VehP}(3,4)$ | 2 | 2 |  |

## VehV - Vehicle velocity

array
Vehicle velocity at axle a, wheel $t$ along vehicle-fixed coordinate system, in m. Input array dimensions are 3 by the number of wheels on the vehicle.

- $\operatorname{VehV}(1, \ldots)-$ Vehicle velocity at wheel, $x_{v}$, along the vehicle-fixed $x$-axis
- $\operatorname{VehV}(2, \ldots)$ - Vehicle velocity at wheel, $y_{v}$, along the vehicle-fixed $y$-axis
- $\operatorname{VehV}(3, \ldots)-$ Vehicle velocity at wheel, $z_{v}$, along the vehicle-fixed $z$-axis

For example, for a two-axle vehicle with two wheels per axle, the VehV:

- Signal dimensions are [3x4].
- Signal contains 4 velocities according to their axle and wheel locations.

$$
\text { VehV }=\left[\begin{array}{c}
\dot{x}_{v} \\
\dot{y}_{v} \\
\dot{z}_{v}
\end{array}\right]=\left[\begin{array}{llll}
\dot{x}_{v_{1,1}} & \dot{x}_{v_{1,2}} & \dot{x}_{v_{2,1}} & \dot{x}_{v_{2,2}} \\
\dot{y}_{v_{1,1}} & \dot{y}_{v_{1,2}} & \dot{y}_{v_{2,1}} & \dot{y}_{v_{2,2}} \\
\dot{z}_{v_{1,1}} & \dot{z}_{v_{1,2}} & \dot{z}_{v_{2,1}} & \dot{z}_{v_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | VehV $(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis |
| Front <br> right | VehV $(1,2)$ | 1 | 2 |  |
| Rear <br> left | $\operatorname{VehV}(1,3)$ | 2 | 1 |  |
| Rear <br> right | $\operatorname{VehV}(1,4)$ | 2 | 2 |  |
| Front <br> left | $\operatorname{VehV}(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis |
| Front <br> right | $\operatorname{VehV}(2,2)$ | 1 | 2 |  |


| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Axis |
| :--- | :--- | :--- | :--- | :--- |
| Rear <br> left | VehV $(2,3)$ | 2 | 1 |  |
| Rear <br> right | VehV $(2,4)$ | 2 | 2 |  |
| Front <br> left | VehV $(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis |
| Front <br> right | VehV(3,2) | 1 | 2 |  |
| Rear <br> left | VehV $(3,3)$ | 2 | 1 |  |
| Rear <br> right | $\operatorname{VehV(3,4)}$ | 2 | 2 |  |

StrgAng - Steering angle, optional array

Optional steering angle for each wheel, $\delta$. Input array dimensions are 1 by the number of steered wheels.

For example, for a two-axle vehicle with two wheels per axle, you can input steering angles for both wheels on the first axle.

- To create the StrgAng port, set Steered axle enable by axle, StrgEnByAxl to [1 0]. The input signal array dimensions are [1×2].
- The StrgAng signal contains two steering angles according to their axle and wheel locations.

$$
\operatorname{StrgAng}=\delta_{\text {steer }}=\left[\delta_{\text {steer }_{1,1}} \delta_{\text {steer }_{1,2}}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | StrgAng $(1,1)$ | 1 | 1 |
| Front right | StrgAng $(1,2)$ | 1 | 2 |

## Dependencies

To create input port StrgAng, set an element of the Steered axle enable by axle, StrgEnByAxl vector to 1 .

## Output

Info - Bus signal
bus
Bus signal containing block values. The signals are arrays that depend on the wheel location.
For example, here are the indices for a two-axle, two-wheel vehicle. The total number of wheels is four.

- 1D array signal (1-by-4)

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | $(1,1)$ | 1 | 1 |
| Front right | $(1,2)$ | 1 | 2 |
| Rear left | $(1,3)$ | 2 | 1 |
| Rear right | $(1,4)$ | 2 | 2 |

- 3D array signal (3-by-4)

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | $(1,1)$ | 1 | 1 |
| Front right | $(1,2)$ | 1 | 2 |
| Rear left | $(1,3)$ | 2 | 1 |
| Rear right | $(1,4)$ | 2 | 2 |
| Front left | $(2,1)$ | 1 | 1 |
| Front right | $(2,2)$ | 1 | 2 |
| Rear left | $(2,3)$ | 2 | 1 |
| Rear right | $(2,4)$ | 2 | 2 |
| Front left | $(3,1)$ | 1 | 1 |
| Front right | $(3,2)$ | 2 | 1 |
| Rear left | $(3,3)$ | 2 | 2 |
| Rear right | $(3,4)$ |  |  |


| Signal | Description | Array Signal | Variable | Units |
| :---: | :---: | :---: | :---: | :---: |
| Camber | Wheel angles according to the axle and wheel location. | 1D | WhlAng $[1, \ldots]=\xi=\left[\xi_{a, t}\right]$ | rad |
| Caster |  |  | WhlAng $[2, \ldots]=\eta=\left[\eta_{a, t}\right]$ |  |
| Toe |  |  | WhlAng $[3, \ldots]=\zeta=\left[\zeta_{a, t}\right]$ |  |
| Height | Suspension height | 1D | H | m |
| Power | Suspension power dissipation | 1D | $P_{\text {susp }}$ | W |
| Energy | Suspension absorbed energy | 1D | $E_{\text {susp }}$ | J |


| Signal | Description | Array Signal | Variable Units |
| :---: | :---: | :---: | :---: |
| VehF | Suspension forces applied to the vehicle | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { VehF }=F_{v}= \\ & {\left[\begin{array}{llll} F_{v x_{1,1}} & F_{v x_{1,2}} & F_{v x_{2,1}} & F_{v x_{2,2}} \\ F_{v v_{1,1}} & F_{v y_{1,2}} & F_{v y_{2,1}} & F_{v y_{2,2}} \\ F_{v z_{1,1}} & F_{v z_{1,2}} & F_{v z_{2,1}} & F_{v z_{2,2}} \end{array}\right.} \end{aligned}$ |
| VehM | Suspension moments applied to vehicle | 3D | For a two-axle, two wheels <br> per axle vehicle:VehM $=M_{v}=$$\left[\begin{array}{llll}M_{v x_{1,1}} & M_{v x_{1,2}} & M_{v x_{2,1}} & M_{v \chi_{2,2}} \\ M_{v y_{1,1}} & M_{v y y_{1,2}} & M_{v y 2,1} & M_{v y 2,2} \\ M_{v z_{1,1}} & M_{v z_{1,2}} & M_{v z_{2,1}} & M_{v z_{2,2}}\end{array}\right]$ |
| WhlF | Suspension force applied to wheel | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { WhlF }=F_{w}= \\ & {\left[\begin{array}{llll} F_{w x_{1}, 1} & F_{w x_{1,2}} & F_{w x_{2,1}} & F_{w x_{2}, 2} \\ F_{w y 1,1} & F_{w y_{1,2}} & F_{w y 2,1} & F_{w y 2,2} \\ F_{w z_{1,1}} & F_{w z_{1,2}} & F_{w z 2,1} & F_{w 2_{2,2}} \end{array}\right.} \end{aligned}$ |


| Signal | Description | Array Signal | Variable | Units |
| :---: | :---: | :---: | :---: | :---: |
| WhlP | Wheel displacement | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { WhlP }=\left[\begin{array}{l} x_{w} \\ y_{w} \\ z_{w} \end{array}\right]= \\ & {\left[\begin{array}{llll} x_{w_{1,1}} & x_{w_{1,2}} & x_{w_{2,1}} & x_{w_{2},} \\ y_{w_{1,1}} & y_{w_{1,2}} & y_{w_{2,1}} & y_{w{ }_{2}} \\ z_{w t r_{1,1}} & z_{w t r_{1,2}} & z_{w t r_{2,1}} & z_{w t r_{2}} \end{array}\right.} \end{aligned}$ |  |
| Whlv | Wheel velocity | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { WhlV }=\left[\begin{array}{l} \dot{x}_{w} \\ \dot{y}_{w} \\ \dot{z}_{w} \end{array}\right] \\ & = \\ & {\left[\begin{array}{lll} \dot{x}_{w_{1,1}} & \dot{x}_{w_{1,2}} & \dot{x}_{w_{2,1}} \\ \dot{x}_{w_{2,2}} \\ \dot{y}_{w_{1,1}} & \dot{y}_{w_{1,2}} & \dot{y}_{w_{2,1}} \\ \dot{y}_{w_{2,2}} \\ \dot{z}_{w_{1,1}} & \dot{z}_{w_{1,2}} & \dot{z}_{w_{2,1}} \\ \dot{z}_{w_{2,2}} \end{array}\right]} \end{aligned}$ | m/s |
| WhlAng | Wheel camber, caster, toe angles | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { WhlAng }=\left[\begin{array}{l} \xi \\ \eta \\ \zeta \end{array}\right] \\ & =\left[\begin{array}{lll} \xi_{1,1} & \xi_{1,2} & \xi_{2,1} \\ \eta_{1,1} & \xi_{1,2} & \eta_{2,1} \\ \eta_{2,2} \\ \zeta_{1,1} & \zeta_{1,2} & \zeta_{2,1} \\ \zeta_{2,2} \end{array}\right] \end{aligned}$ | rad |

VehF - Suspension force on vehicle array

Longitudinal, lateral, and vertical suspension force at axle a, wheel $t$, applied to the vehicle at the suspension connection point, in N. Array dimensions are 3 by the number of wheels on the vehicle.

- VehF (1, ...) - Suspension force applied to vehicle along the vehicle-fixed $x$-axis (longitudinal)
- $\operatorname{VehF}(2, \ldots)-$ Suspension force applied to vehicle along the vehicle-fixed $y$-axis (lateral)
- VehF (3, . . ) - Suspension force applied to vehicle along the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the VehF:

- Signal dimensions are [3x4].
- Signal contains suspension forces applied to the vehicle according to the axle and wheel locations.

$$
\text { VehF }=F_{v}=\left[\begin{array}{llll}
F_{v x_{1,1}} & F_{v x_{1,2}} & F_{v x_{2,1}} & F_{v x_{2,2}} \\
F_{v y_{1,1}} & F_{v y_{1,2}} & F_{v y_{2,1}} & F_{v y_{2,2}} \\
F_{v z_{1,1}} & F_{v z_{1,2}} & F_{v z_{2,1}} & F_{v z_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel Numbe r | Force Axis |
| :---: | :---: | :---: | :---: | :---: |
| Front left | $\operatorname{VehF}(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front right | $\operatorname{VehF}(1,2)$ | 1 | 2 |  |
| Rear left | $\operatorname{VehF}(1,3)$ | 2 | 1 |  |
| Rear right | $\operatorname{VehF}(1,4)$ | 2 | 2 |  |
| Front left | $\operatorname{VehF}(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front right | $\operatorname{VehF}(2,2)$ | 1 | 2 |  |
| Rear left | $\operatorname{VehF}(2,3)$ | 2 | 1 |  |
| Rear right | $\operatorname{VehF}(2,4)$ | 2 | 2 |  |
| Front left | $\operatorname{VehF}(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front right | $\operatorname{VehF}(3,2)$ | 1 | 2 |  |
| Rear left | $\operatorname{VehF}(3,3)$ | 2 | 1 |  |
| Rear right | $\operatorname{VehF}(3,4)$ | 2 | 2 |  |

VehM - Suspension moment on vehicle
array
Longitudinal, lateral, and vertical suspension moment at axle $a$, wheel $t$, applied to the vehicle at the suspension connection point, in $N \cdot m$. Array dimensions are 3 by the number of wheels on the vehicle.

- VehM (1, ...) - Suspension moment applied to the vehicle about the vehicle-fixed $x$-axis (longitudinal)
- VehM ( $2, \ldots$ ) - Suspension moment applied to the vehicle about the vehicle-fixed $y$-axis (lateral)
- VehM (3, ...) - Suspension moment applied to the vehicle about the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the VehM:

- Signal dimensions are [3×4].
- Signal contains suspension moments applied to vehicle according to the axle and wheel locations.

$$
\text { VehM }=M_{v}=\left[\begin{array}{llll}
M_{v x_{1,1}} & M_{v x_{1,2}} & M_{v x_{2,1}} & M_{v x_{2,2}} \\
M_{v y 1,1} & M_{v y 1,2} & M_{v x_{2,1}} & M_{v y_{2,2}} \\
M_{v z_{1,1}} & M_{v z_{1,2}} & M_{v z_{2,1}} & M_{v z_{2,2}}
\end{array}\right]
$$

| Array Element | Axle | Wheel Number | Moment Axis |
| :---: | :---: | :---: | :---: |
| $\operatorname{VehM}(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| $\operatorname{VehM}(1,2)$ | 1 | 2 |  |
| $\operatorname{VehM}(1,3)$ | 2 | 1 |  |
| VehM (1,4) | 2 | 2 |  |
| $\operatorname{VehM}(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| VehM (2,2) | 1 | 2 |  |
| VehM (2,3) | 2 | 1 |  |
| $\operatorname{VehM}(2,4)$ | 2 | 2 |  |
| $\operatorname{VehM}(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| $\operatorname{VehM}(3,2)$ | 1 | 2 |  |
| $\operatorname{VehM}(3,3)$ | 2 | 1 |  |
| VehM ( 3,4 ) | 2 | 2 |  |

WhIF - Suspension force on wheel
array
Longitudinal, lateral, and vertical suspension forces at axle a, wheel $t$, applied to the wheel at the axle wheel carrier reference coordinate, in N. Array dimensions are 3 by the number of wheels on the vehicle.

- $\operatorname{WhlF}(1, \ldots)$ - Suspension force on wheel along the vehicle-fixed $x$-axis (longitudinal)
- $\operatorname{WhlF}(2, \ldots)$ - Suspension force on wheel along the vehicle-fixed $y$-axis (lateral)
- $\operatorname{WhlF}(3, \ldots)$ - Suspension force on wheel along the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the WhlF:

- Signal dimensions are [3×4].
- Signal contains wheel forces applied to the vehicle according to the axle and wheel locations.

$$
\text { WhlF }=F_{w}=\left[\begin{array}{lllll}
F_{w x_{1,1}} & F_{w x_{1,2}} & F_{w x_{2,1}} & F_{w x_{2,2}} \\
F_{w y_{1,1}} & F_{w y 1,2} & F_{w y 2,1} & F_{w y 2,2} \\
F_{w z_{1,1}} & F_{w z_{1,2}} & F_{w z 2,1} & F_{w z_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | WhlF $(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front <br> right | WhlF $(1,2)$ | 1 | 2 |  |
| Rear <br> left | WhlF $(1,3)$ | 2 | 1 |  |
| Rear <br> right | WhlF $(1,4)$ | 2 | 2 |  |
| Front <br> left | WhlF $(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front <br> right | WhlF $(2,2)$ | 1 | 2 |  |
| Rear <br> left | WhlF $(2,3)$ | 2 | 1 |  |
| Rear <br> right | WhlF $(2,4)$ | 2 | 2 |  |
| Front <br> left | WhlF $(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front <br> right | WhlF $(3,2)$ | 1 | 2 |  |
| Rear <br> left | WhlF $(3,3)$ | 2 | 1 |  |
| Rear <br> right | WhlF $(3,4)$ | 2 | 2 |  |

WhIV - Wheel velocity
array
Longitudinal, lateral, and vertical wheel velocity at axle a, wheel $t$, in $m / s$. Array dimensions are 3 by the number of wheels on the vehicle.

- WhlV (1, ...) - Wheel velocity along the vehicle-fixed $x$-axis (longitudinal)
- WhlV $(2, \ldots)$ - Wheel velocity along the vehicle-fixed $y$-axis (lateral)
- WhlV $(3, \ldots)-$ Wheel velocity along the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the Whlv:

- Signal dimensions are [3×4].
- Signal contains wheel forces applied to the vehicle according to the axle and wheel locations.

$$
\text { WhlV }=\left[\begin{array}{c}
\dot{x}_{w} \\
\dot{y}_{w} \\
\dot{z}_{w}
\end{array}\right]=\left[\begin{array}{llll}
\dot{x}_{w_{1,1}} & \dot{x}_{w_{1,2}} & \dot{x}_{w_{2,1}} & \dot{x}_{w_{2,2}} \\
\dot{y}_{w_{1,1}} & \dot{y}_{w_{1,2}} & \dot{y}_{w_{2,1}} & \dot{y}_{w_{2,2}} \\
\dot{z}_{w_{1,1}} & \dot{z}_{w_{1,2}} & \dot{z}_{w_{2,1}} & \dot{z}_{w_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | WhlV $(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front <br> right | WhlV $(1,2)$ | 1 | 2 |  |
| Rear <br> left | WhlV $(1,3)$ | 2 | 1 |  |
| Rear <br> right | WhlV $(1,4)$ | 2 | 2 |  |
| Front <br> left | WhlV $(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front <br> right | WhlV $(2,2)$ | 1 | 2 |  |
| Rear <br> left | WhlV $(2,3)$ | 2 | 1 |  |
| Rear <br> right | WhlV $(2,4)$ | 2 | 2 |  |
| Front <br> left | WhlV $(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front <br> right | WhlV $(3,2)$ | 1 | 2 |  |
| Rear <br> left | WhlV $(3,3)$ | 2 | 1 |  |
| Rear <br> right | WhlV $(3,4)$ | 2 | 2 |  |

WhIAng - Wheel camber, caster, toe angles
array
Camber, caster, and toe angles at axle a, wheel $t$, in rad. Array dimensions are 3 by the number of wheels on the vehicle.

- WhlAng (1,...) - Camber angle
- WhlAng $(2, \ldots)$ - Caster angle
- WhlAng $(3, \ldots)$ - Toe angle

For example, for a two-axle vehicle with two wheels per axle, the WhlAng:

- Signal dimensions are [3x4].
- Signal contains angles according to the axle and wheel locations.

$$
\text { WhlAng }=\left[\begin{array}{l}
\xi \\
\eta \\
\zeta
\end{array}\right]=\left[\begin{array}{llll}
\xi_{1,1} & \xi_{1,2} & \xi_{2,1} & \xi_{2,2} \\
\eta_{1,1} & \eta_{1,2} & \eta_{2,1} & \eta_{2,2} \\
\zeta_{1,1} & \zeta_{1,2} & \zeta_{2,1} & \zeta_{2,2}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Angle |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | WhlAng (1,1) | 1 | 1 | Camber |
| Front <br> right | WhlAng (1,2) | 1 | 2 |  |
| Rear <br> left | WhlAng (1,3) | 2 | 1 |  |
| Rear <br> right | WhlAng (1,4) | 2 | 2 |  |
| Front <br> left | WhlAng (2,1) | 1 | 1 | Caster |
| Front <br> right | WhlAng (2,2) | 1 | 2 |  |
| Rear <br> left | WhlAng (2,3) | 2 | 1 |  |
| Rear <br> right | WhlAng (2,4) | 2 | 2 |  |
| Front <br> left | WhlAng (3,1) | 1 | 1 | Toe |
| Front <br> right | WhlF(3,2) | 1 | 2 |  |
| Rear <br> left | WhlF(3,3) | 2 | 1 |  |
| Rear <br> right | WhlF(3,4) | 2 | 2 |  |

## Parameters

## Enable active damping - Include damping

off (default) | off
Include damping

## Dependencies

Selecting this parameter creates:

## - Damping coefficient map, f_act_susp_cz

- Damping actuator duty cycle breakpoints, f_act_susp_duty_bpt
- Damping actuator velocity breakpoints, f_act_susp_zdot_bpt

Number of axles, NumAxI - Number of axles
2 (default) | scalar
Number of axles, $N_{a}$, dimensionless.
Number of wheels by axle, NumWhlsByAxI - Number of wheels per axle
[2 2] (default) |vector
Number of wheels per axle, $N t_{a}$, dimensionless. Vector is 1 by the number of vehicle axles, $N_{a}$. For example, [1,2] represents one wheel on axle one and two wheels on axle two.

Steered axle enable by axle, StrgEnByAxI - Boolean vector to enable axle steering
[1 0] (default)|vector
Boolean vector that enables axle steering, $E n_{\text {steer }}$, dimensionless. Vector is 1 by the number of vehicle axles, $N_{a}$. For example:

- [10] — For a two-axle vehicle, enables axle 1 steering and disables axle 2 steering
- [ll $\left.\begin{array}{ll}1 & 1\end{array}\right]$ - For a two-axle vehicle, enables axle 1 and axle 2 steering


## Dependencies

Setting any element of the Steered axle enable by axle, StrgEnByAxl vector to 1 creates:

- Input port StrgAng.
- Parameters:
- Toe angle vs steering angle slope, ToeStrgSlp
- Caster angle vs steering angle slope, CasterStrgSlp
- Camber angle vs steering angle slope, CamberStrgSlp
- Suspension height vs steering angle slope, StrgHgtSIp

For example, for a two-axle vehicle with two wheels per axle, you can input steering angles for both wheels on the first axle.

- To create the StrgAng port, set Steered axle enable by axle, StrgEnByAxl to [1 0]. The input signal array dimensions are [1×2].
- The StrgAng signal contains two steering angles according to their axle and wheel locations.

$$
\text { StrgAng }=\delta_{\text {steer }}=\left[\delta_{\text {steer }_{1,1}} \delta_{\text {steer }_{1,2}}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | StrgAng $(1,1)$ | 1 | 1 |
| Front right | StrgAng $(1,2)$ | 1 | 2 |

Anti-sway axle enable by axle, AntiSwayEnByAxI - Boolean vector to enable axle anti-sway [0 0] (default)|vector

Boolean vector that enables axle anti-sway for axle $a$, dimensionless. For example, [10] enables axle 1 anti-sway and disables axle 2 anti-sway. Vector is 1 by the number of vehicle axles, $N_{a}$.

## Dependencies

Setting an element of the Anti-sway axle enable by axle, AntiSwayEnByAxl vector to 1 creates these anti-sway parameters:

- Anti-sway arm radius, AntiSwayR
- Anti-sway arm neutral angle, AntiSwayNtrlAng
- Anti-sway torsion spring constant, AntiSwayTrsK


## Suspension

Compliance and Damping - Passive
Suspension spring constant, Kz - Suspension spring constant
64370 (default) | scalar | vector
Linear vertical spring constant for independent suspension wheels on axle a, $k_{z_{\alpha^{\prime}}}$ in $\mathrm{N} / \mathrm{m}$.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Suspension spring preload, FOz - Suspension spring preload

9810 (default) | scalar | vector
Vertical preload spring force applied to the wheels on the axle at wheel carrier reference coordinates, $F_{z 0_{a^{\prime}}}$ in N. Positive preload forces:

- Cause the vehicle to lift.
- Point along the negative vehicle-fixed $z$-axis.

Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

Suspension shock damping constant, Cz - Suspension shock damping constant 10000 (default) | scalar | vector

Linear vertical damping constant for independent suspension wheels on axle a, $c_{z_{d^{\prime}}}$ in $\mathrm{Ns} / \mathrm{m}$.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Dependencies

To create this parameter, clear Enable active damping.

## Suspension maximum height, Hmax - Height

0.5 (default) | scalar | vector

Maximum suspension extension or minimum suspension compression height, $H_{\text {max }}$, for axle a before the suspension reaches a hardstop, in $m$.

Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Compliance and Damping - Active

## Damping coefficient map, f_act_susp_cz - Lookup table

[10000 10000;10000 10000] (default) | M-by-N array
Damping coefficient table as a function of active duty cycle and actuator compression velocity, in $\mathrm{N} \cdot \mathrm{s} / \mathrm{m}$. Each value specifies the damping for a specific combination of actuator duty cycle and velocity. The array dimensions must match the duty cycle, M , and actuator velocity, N , breakpoint vector dimensions.

## Dependencies

To create this parameter, clear Enable active damping.
Damping actuator duty cycle breakpoints, f_act_susp_duty_bpt - Duty cycle breakpoints [0 1] (default) | 1-by-M vector

Damping actuator duty cycle breakpoints, dimensionless.

## Dependencies

To create this parameter, clear Enable active damping.
Damping actuator velocity breakpoints, f_act_susp_zdot_bpt - Velocity breakpoints
[-1 1] (default) | 1-by-N vector
Damping actuator velocity breakpoints, in m/s.

## Dependencies

To create this parameter, clear Enable active damping.

## Geometry

Toe angle at steering center, Toe - Toe angle
0.0349 (default) | scalar

Nominal suspension toe angle at zero steering angle, $\zeta_{0 a}$, in rad.
Roll steer vs suspension height slope, RollStrgSIp - Steer angle suspension slope -0. 2269 (default) | scalar | vector

Roll steer angle versus suspension height, $m_{\text {htoe } a_{a}}$, in rad $/ \mathrm{m}$.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

Toe angle vs steering angle slope, ToeStrgSIp - Toe angle steering slope
0.01 (default) | scalar | vector

Toe angle versus steering angle slope, $m_{\text {toesteer }_{a^{\prime}}}$ dimensionless.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Dependencies

To create input port StrgAng, set an element of the Steered axle enable by axle, StrgEnByAxl vector to 1 .

Caster angle at steering center, Caster - Caster angle at steering center 0.0698 (default) | scalar

Nominal suspension caster angle at zero steering angle, $\eta_{0 a}$, in rad.
Caster angle vs suspension height slope, CasterHslp - Caster angle versus suspension height slope
-0. 2269 (default) | scalar | vector
Caster angle versus suspension height, $m_{\text {haster }_{a^{\prime}}}$ in rad $/ \mathrm{m}$.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

Caster angle vs steering angle slope, CasterStrgSIp - Caster angle versus steering angle slope 0.01 (default) | scalar | vector

Caster angle versus steering angle slope, $m_{\text {castersteer }_{a^{\prime}}}$ dimensionless.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Dependencies

To create input port StrgAng, set an element of the Steered axle enable by axle, StrgEnByAxl vector to 1 .

Camber angle at steering center, Camber - Camber angle at steering center 0.0698 (default) | scalar

Nominal suspension camber angle at zero steering angle, $\xi_{0 a}$, in rad.
Camber angle vs suspension height slope, CamberHslp - Camber angle versus suspension height slope
-0. 2269 (default) | scalar | vector
Camber angle versus suspension height, $m_{\text {hcamber }{ }_{a}}$ in rad $/ \mathrm{m}$.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

Camber angle vs steering angle slope, CamberStrgSIp - Camber angle versus steering angle slope
0.01 (default) | scalar | vector

Camber angle versus steering angle slope, $m_{\text {cambersteer }_{a}}$, dimensionless.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Dependencies

To create input port StrgAng, set an element of the Steered axle enable by axle, StrgEnByAxl vector to 1 .

Suspension height vs steering angle slope, StrgHgtSIp - Suspension height versus steering angle slope
0.1432 (default) | scalar | vector

Steering angle to vertical force slope applied at suspension wheel carrier reference point, $m_{\text {hsteer }_{a^{\prime}}}$ in $\mathrm{m} / \mathrm{rad}$.

Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Dependencies

To create input port StrgAng, set an element of the Steered axle enable by axle, StrgEnByAxl vector to 1 .

Anti-Sway
Anti-sway arm radius, AntiSwayR - Anti-sway arm radius
0.2 (default) | scalar | vector

Anti-sway arm radius, $r$, in m.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Dependencies

Setting an element of the Anti-sway axle enable by axle, AntiSwayEnByAxl vector to 1 creates these anti-sway parameters:

- Anti-sway arm radius, AntiSwayR
- Anti-sway arm neutral angle, AntiSwayNtrlAng
- Anti-sway torsion spring constant, AntiSwayTrsK

Anti-sway arm neutral angle, AntiSwayNtrIAng - Anti-sway arm neutral angle
0.5236 (default) | scalar | vector

Anti-sway arm neutral angle, $\theta_{0 a}$, at nominal suspension height, in rad.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Dependencies

Setting an element of the Anti-sway axle enable by axle, AntiSwayEnByAxl vector to 1 creates these anti-sway parameters:

- Anti-sway arm radius, AntiSwayR
- Anti-sway arm neutral angle, AntiSwayNtrlAng
- Anti-sway torsion spring constant, AntiSwayTrsK

Anti-sway torsion spring constant, AntiSwayTrsK - Anti-sway torsion spring constant $5.7296 \mathrm{e}+03$ (default) | scalar | vector

Anti-sway bar torsion spring constant, $k_{a}$, in $\mathrm{N} \cdot \mathrm{m} / \mathrm{rad}$.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Dependencies

Setting an element of the Anti-sway axle enable by axle, AntiSwayEnByAxl vector to 1 creates these anti-sway parameters:

- Anti-sway arm radius, AntiSwayR
- Anti-sway arm neutral angle, AntiSwayNtrlAng
- Anti-sway torsion spring constant, AntiSwayTrsK


## Version History

## Introduced in R2018a

## R2022b: Parameter name change from NumTracksByAxl to NumWhlsByAxl Behavior changed in R2022b

The Number of tracks by axle, NumTracksByAxl parameter is renamed to Number of wheels by axle, NumWhlsByAxl.

The block uses the number of wheels per axle to index the input and output block signals.

## References

[1] Gillespie, Thomas. Fundamentals of Vehicle Dynamics. Warrendale, PA: Society of Automotive Engineers, 1992.
[2] Vehicle Dynamics Standards Committee. Vehicle Dynamics Terminology. SAE J670. Warrendale, PA: Society of Automotive Engineers, 2008.
[3] Technical Committee. Road vehicles - Vehicle dynamics and road-holding ability - Vocabulary. ISO 8855:2011. Geneva, Switzerland: International Organization for Standardization, 2011.

## Extended Capabilities

C/C++ Code Generation
Generate C and C++ code using Simulink ${ }^{\circledR}$ Coder $^{\mathrm{TM}}$.

## See Also

Independent Suspension - MacPherson | Independent Suspension - Mapped | Independent Suspension - K and C

## Independent Suspension - MacPherson

MacPherson independent suspension


## Libraries:

Vehicle Dynamics Blockset / Suspension

## Description

The Independent Suspension - MacPherson block implements an independent MacPherson suspension for multiple axles with multiple wheels per axle.

The block models the suspension compliance, damping, and geometric effects as functions of the relative positions and velocities of the vehicle and wheel carrier with axle-specific compliance and damping parameters. Using the suspension compliance and damping, the block calculates the suspension force on the vehicle and wheel. The block uses the Z-down coordinate system (defined in SAE J670).

| For Each | You Can Specify |
| :--- | :--- |
| Axle | $\bullet \quad$ Multiple wheels |
|  | $\bullet \quad$ An anti-sway bar for axles with two wheels |
|  | $\bullet \quad$ Suspension parameters |
| Wheel | $\bullet \quad$ Steering angles |

The block contains energy-storing spring elements and energy-dissipating damper elements. It does not contain energy-storing mass elements. The block assumes that the vehicle (sprung) and wheel (unsprung) blocks connected to the block store the mass-related suspension energy.

This table summarizes the block parameter settings for a vehicle with:

- Two axles
- Two wheels per axle
- Steering angle input for both wheels on the front axle
- An anti-sway bar on the front axle

| Parameter | Setting |
| :--- | :--- |
| Number of axles, NumAxl | 2 |
| Number of wheels by axle, NumWhlsByAxl | $\left[\begin{array}{ll}2 & 2\end{array}\right]$ |
| Steered axle enable by axle, StrgEnByAxl | $\left[\begin{array}{ll}1 & 0\end{array}\right]$ |
| Anti-Sway axle enable by axle, <br> AntiSwayEnByAxl | $\left[\begin{array}{ll}1 & 0\end{array}\right]$ |

The block uses the wheel number, $t$, to index the input and output signals. This table summarizes the wheel, axle, and corresponding wheel number for a vehicle with:

- Two axles
- Two wheels per axle

| Wheel | Axle | Wheel Number |
| :--- | :--- | :--- |
| Front left | Front | 1 |
| Front right | Front | 2 |
| Rear left | Rear | 1 |
| Rear right | Rear | 2 |

## Suspension Compliance and Damping

The block uses a linear spring and damper to model the vertical dynamic effects of the suspension system. Using the relative positions and velocities of the vehicle and wheel carrier, the block calculates the vertical suspension forces on the wheel and vehicle. The block uses a linear equation that relates the vertical damping and compliance to the suspension height, suspension height rate of change, and absolute value of the steering angles.

The block implements this equation.

$$
F_{w z_{a, t}}=F_{z 0_{a}}+k_{z_{a}}\left(z_{v_{a, t}}-z_{w_{a, t}}+m_{\text {hsteer }_{a}}\left|\delta_{\text {steer }_{a, t}}\right|\right)+c\left(\dot{z}_{v_{a, t}}-\dot{z}_{w_{a, t}}\right)+F_{z h s t o p_{a, t}}+F_{z a s w y_{a, t}}
$$

The damping coefficient, $c$, depends on the Enable active damping parameter setting.

| Enable active damping <br> Setting | Damping |
| :--- | :--- |
| off | Constant, $c=c_{z_{a}}$ |
| on | Lookup table that is a function of active damper duty cycle and <br> actuator velocity |
|  | $c=f\left(\right.$ duty, $\left.\left(\dot{z}_{v_{a, t}}-\dot{z}_{w_{a, t}}\right)\right)$ |

The block assumes that the suspension elements have no mass. Therefore, the suspension forces and moments applied to the vehicle are equal to the suspension forces and moments applied to the wheel.

$$
\begin{aligned}
& F_{v x_{a, t}}=F_{w x_{a, t}} \\
& F_{v y_{a, t}}=F_{w y_{a, t}} \\
& F_{v z_{a, t}}=-F_{w z_{a, t}} \\
& M_{v x_{a, t}}=M_{w x_{a, t}}+F_{w y_{a, t}}\left(R e_{w y_{a, t}}+H_{a, t}\right) \\
& M_{v y_{a, t}}=M_{w y_{a, t}}+F_{w x_{a, t}}\left(R e_{w x_{a, t}}+H_{a, t}\right) \\
& M_{v x_{a, t}}=M_{w z_{a, t}}
\end{aligned}
$$

The block sets the wheel positions and velocities equal to the vehicle lateral and longitudinal positions and velocities.

$$
\begin{aligned}
& x_{w_{a, t}}=x_{v_{a, t}} \\
& y_{w_{a, t}}=y_{v_{a, t}} \\
& \dot{x}_{w_{a, t}}=\dot{x}_{v_{a, t}} \\
& \dot{y}_{w_{a, t}}=\dot{y}_{v_{a, t}}
\end{aligned}
$$

The equations use these variables.

| $F_{w z_{a, t}} M_{w z_{0, t}}$ | Suspension force and moment applied to the wheel on axle a, wheel $t$ along wheel-fixed $z$-axis |
| :---: | :---: |
| $F_{w \chi_{a, t}} M_{w x_{a, t}}$ | Suspension force and moment applied to the wheel on axle $a$, wheel $t$ along wheel-fixed $x$-axis |
| $F_{w y_{a, t}} M_{w y_{a, t}}$ | Suspension force and moment applied to the wheel on axle $a$, wheel $t$ along wheel-fixed $y$-axis |
| $F_{v z_{a, l}} M_{v z_{\text {a }}, t}$ | Suspension force and moment applied to the vehicle on axle a, wheel t along wheel-fixed $z$-axis |
| $F_{v \chi_{a, t}} M_{v \chi^{\prime}, t}$ | Suspension force and moment applied to the vehicle on axle a, wheel t along wheel-fixed $x$-axis |
| $F_{v y_{a, t}} M_{v y^{\prime}, t}$ | Suspension force and moment applied to the vehicle on axle a, wheel t along wheel-fixed $y$-axis |
| $F_{z 0_{a}}$ | Vertical suspension spring preload force applied to the wheels on axle a |
| $k_{z_{a}}$ | Vertical spring constant applied to wheels on axle a |
| $k w a_{z}$ | Wheel and axle interface compliance constant |
| $m_{\text {hsteer }}^{\text {a }}$ | Steering angle to vertical force slope applied at wheel carrier for wheels on axle a |
| $\delta_{\text {ster }_{\text {at }}}$ | Steering angle input for axle a, wheel t |
| $c_{z_{a}}$ | Vertical damping constant applied to wheels on axle a |
| cwa ${ }_{z}$ | Wheel and axle interface damping constant |
| $R e_{w_{a, t}}$ | Effective wheel radius for axle a, wheel t |
| $F_{z h s t o p_{a, t}}$ | Vertical hardstop force at axle a , wheel t , along the vehicle-fixed $z$-axis |
| $F_{z a s w y a t e}$ | Vertical anti-sway force at axle a, wheel t , along the vehicle-fixed $z$-axis |
| $F w a_{z 0}$ | Wheel and axle interface compliance constant |
| $z_{v_{a, t}} \dot{z}_{v_{a, t}}$ | Vehicle displacement and velocity at axle $a$, wheel $t$, along the vehiclefixed $z$-axis |
| $z_{w_{w_{a, t}}} \dot{z}_{w_{a, t}}$ | Wheel displacement and velocity at axle a, wheel t , along the vehicle-fixed $z$-axis |
| $\chi_{v_{a, t}} \dot{\chi}_{v_{a, t}}$ | Vehicle displacement and velocity at axle a , wheel t , along the vehiclefixed $z$-axis |
| $\chi_{w_{w_{t, t}}} \dot{\chi}_{w_{a, t}}$ | Wheel displacement and velocity at axle $a$, wheel $t$, along the vehicle-fixed $z$-axis |
| $y_{v_{a, t}} \dot{y}_{v_{a, t}}$ | Vehicle displacement and velocity at axle a , wheel t , along the vehiclefixed $y$-axis |


| $y_{w_{a, t}} \dot{y}_{w_{a, t}}$ | Wheel displacement and velocity at axle a, wheel t, along the vehicle-fixed |
| :--- | :--- |
| $H_{a, t}$ | $y$-axis |
| $R e_{w_{a, t}}$ | Suspension height at axle a, wheel t |
|  | Effective wheel radius at axle a, wheel t |

## Hardstop Forces

The hardstop feedback force, $F_{\text {zhstop } a_{a, 1}}$ that the block applies depends on whether the suspension is compressing or extending. The block applies the force:

- In compression, when the suspension is compressed more than the maximum distance specified by the Suspension maximum height, Hmax parameter.
- In extension, when the suspension extension is greater than maximum extension specified by the Suspension maximum height, Hmax parameter.

To calculate the force, the block uses a stiffness based on a hyperbolic tangent and exponential scaling.

## Anti-Sway Bar

Optionally, use the Anti-sway axle enable by axle, AntiSwayEnByAxl parameter to implement an anti-sway bar force, $F_{z a s w y_{a, t}}$ for axles that have two wheels. This figure shows how the anti-sway bar transmits torque between two independent suspension wheels on a shared axle. Each independent suspension applies a torque to the anti-sway bar via a radius arm that extends from the anti-sway bar back to the independent suspension connection point.


To calculate the sway bar force, the block implements these equations.

| Calculation | Equation |
| :--- | :--- |
| Anti-sway bar angular deflection <br> for a given axle and wheel, $\Delta \theta_{a, t}$ | $\theta_{0 a}=\tan ^{-1}\left(\frac{z_{0}}{r}\right)$ |
|  | $\Delta \theta_{a, t}=\tan ^{-1}\left(\frac{r \tan \theta_{0 a}-z_{w_{a, t}}+z_{v_{a, t}}}{r}\right)$ |


| Calculation | Equation |
| :--- | :--- |
| Anti-sway bar twist angle, $\theta_{a}$ | $\theta_{a}=-\tan ^{-1}\left(\frac{r \tan \theta_{0 a}-z_{w_{a, 1}}+z_{v_{a, 1}}}{r}\right)$ |
|  | $-\tan ^{-1}\left(\frac{r \tan \theta_{0 a}-z_{w_{a, 2}}+z_{v_{a, 2}}}{r}\right)$ |
| Anti-sway bar torque, $\tau_{a}$ | $\tau_{a}=k_{a} \theta_{a}$ |
| Anti-sway bar forces applied to <br> the wheel on axle $a$, wheel t <br> along wheel-fixed $z$-axis | $F_{z a s w y_{a, 1}}=\left(\frac{\tau_{a}}{r}\right) \cos \left(\theta_{0 a}-\tan ^{-1}\left(\frac{r \tan \theta_{0 a}-z_{w_{a, 1}}+z_{v_{a, 1}}}{r}\right)\right)$ |
|  | $F_{z a s w y_{a, 2}}=\left(\frac{\tau_{a}}{r}\right) \cos \left(\theta_{0 a}-\tan ^{-1}\left(\frac{r \tan \theta_{0 a}-z_{w_{a, 2}}+z_{v_{a, 2}}}{r}\right)\right)$ |

The equations and figure use these variables.

| $\tau_{a}$ | Anti-sway bar torque |
| :--- | :--- |
| $\theta$ | Anti-sway bar twist angle |
| $\theta_{0 a}$ | Initial anti-sway bar twist angle |
| $\Delta \theta_{a, t}$ | Anti-sway bar angular deflection at axle a, wheel t |
| $r$ | Anti-sway bar arm radius |
| $z_{0}$ | Vertical distance from anti-sway bar connection point to anti-sway bar centerline |
| $F_{z s w a y_{a, t}}$ | Anti-sway bar force applied to the wheel on axle a, wheel t along wheel-fixed $z$-axis |
| $z_{v_{a, t}}$ | Vehicle displacement at axle a, wheel t , along the vehicle-fixed $z$-axis |
| $z_{w_{a, t}}$ | Wheel displacement at axle a, wheel t, along the vehicle-fixed $z$-axis |

## Camber, Caster, and Toe Angles

To calculate the camber, caster, and toe angles, block uses linear functions of the suspension height and steering angle.

$$
\begin{aligned}
& \xi_{a, t}=\xi_{0 a}+m_{\text {hcamber }_{a}}\left(z_{w_{a, t}}-z_{v_{a, t}}-m_{\text {hsteer }_{a}}\left|\delta_{\text {steer }_{a}, t}\right|\right)+m_{\text {cambersteer }_{a}}\left|\delta_{\text {steer }_{a, t}}\right| \\
& \eta_{a, t}=\eta_{0 a}+m_{\text {hcaster }_{a}}\left(z_{w_{a, t}}-z_{v_{a, t}}-m_{\text {hsteer }_{a}}\left|\delta_{\text {steer }_{a}, t}\right|\right)+m_{\text {castersteer }_{a}}\left|\delta_{\text {steer }_{a, t}}\right| \\
& \zeta_{a, t}=\zeta_{0 a}+m_{\text {htoe }_{a}}\left(z_{w_{a, t}}-z_{v_{a, t}}-m_{\text {hsteer }_{a}}\left|\delta_{\text {steer }_{a, t}}\right|\right)+m_{\text {toesteer }_{a}}\left|\delta_{\text {steer }_{a}, t}\right|
\end{aligned}
$$

The equations use these variables.

| $\xi_{a, t}$ | Camber angle of wheel on axle a, wheel t |
| :--- | :--- |
| $\eta_{a, t}$ | Caster angle of wheel on axle a, wheel t |
| $\zeta_{a, t}$ | Toe angle of wheel on axle a, wheel t |
| $\xi_{0 a}, \eta_{0 a}, \zeta_{0 a}$ | Nominal suspension axle a camber, caster, and toe angles, respectively, at <br> $m_{\text {camber }_{a^{\prime}}}$ <br> $m_{\text {hcosteo }_{a}{ }^{\prime}}$ |
| zero steering angle |  |
| Camber, caster, and toe angles, respectively, versus suspension height slope |  |
| for axle a |  |

$m_{\text {cambersteer }_{a^{\prime}}} m_{\text {castersteer }_{a^{\prime}}}$ Camber, caster, and toe angles, respectively, versus steering angle slope for $m_{\text {toesteer }_{a}} \quad$ axle a
$m_{\text {hsteer }_{a}} \quad$ Steering angle versus vertical force slope for axle a
$\delta_{\text {steer }_{a, t}} \quad$ Steering angle input for axle a, wheel t
$z_{v_{a, t}}$
$z_{w_{a, t}}$
Vehicle displacement at axle a , wheel t , along the vehicle-fixed $z$-axis Wheel displacement at axle $a$, wheel $t$, along the vehicle-fixed $z$-axis

## Steering Angles

Optionally, use the Steered axle enable by axle, StrgEnByAxl parameter to input steering angles for the wheels. To calculate the steering angles for the wheels, the block offsets the input steering angles with a linear function of the suspension height.

$$
\delta_{\text {whlsteer }_{a, t}}=\delta_{\text {steer }_{a, t}}+m_{\text {htoe }_{a}}\left(z_{w_{a, t}}-z_{v_{a, t}}-m_{\text {hsteer }_{a}}\left|\delta_{\text {steer }_{a, t}}\right|\right)+m_{\text {toesteer }_{a}}\left|\delta_{\text {steer }_{a, t}}\right|
$$

The equation uses these variables.

| $m_{\text {toesteer }_{a}}$ | Axle a toe angle versus steering angle slope |
| :--- | :--- |
| $m_{\text {hsteer }_{a}}$ | Axle a steering angle versus vertical force slope |
| $m_{\text {htoe }_{a}}$ | Axle a toe angle versus suspension height slope |
| $\delta_{\text {whlsteer }_{a, t}}$ | Wheel steering angle for axle $a$, wheel t |
| $\delta_{\text {steer }_{a, t}}$ | Steering angle input for axle a, wheel t |
| $z_{v_{a, t}}$ | Vehicle displacement at axle $a$, wheel t , along the vehicle-fixed $z$-axis |
| $z_{w_{a, t}}$ | Wheel displacement at axle $a$, wheel t , along the vehicle-fixed $z$-axis |

## Power and Energy

The block calculates these suspension characteristics for each axle, $a$, wheel, $t$.

| Calculation | Equation |
| :---: | :---: |
| Dissipated power, $P_{\text {susp }_{\text {a,t }}}$ | $P_{\text {susp }_{a, t}}=F_{\text {wzlookup }}\left(\dot{z}_{v_{a, t}}-\dot{z}_{w_{a, t}{ }^{\prime}} \dot{z}_{v_{a, t}}-\dot{z}_{w_{a, t^{\prime}}} \delta_{\text {steer }_{a, t}}\right)$ |
| Absorbed energy, $E_{\text {susp }_{\text {a }}}$ | $E_{\text {susp }_{a, t}}=F_{w z \text { lookup }_{a}}\left(\dot{z}_{v_{a, t}}-\dot{z}_{w_{a, t}{ }^{\prime}} \dot{z}_{v_{a, t}}-\dot{z}_{w_{a, t}} \delta_{\text {steer }}^{a, t}\right.$ $)$ |
| Suspension height, $H_{a, t}$ | $H_{a, t}=-\left(z_{v_{a, t}}-z_{w_{a, t}}+\frac{F_{z 0_{a}}}{k_{z_{a}}}+m_{\text {hsteer }_{a}}\left\|\delta_{\text {steer }_{a, t}}\right\|\right)$ |
| Distance from wheel carrier center to tire/road interface | $z_{w t r_{a, t}}=R e_{w_{a, t}}+H_{a, t}$ |

The equations use these variables.
$m_{\text {hsteer }_{a}} \quad$ Steering angle to vertical force slope applied at wheel carrier for wheels on axle a
$\delta_{\text {steer }_{a, t}} \quad$ Steering angle input for axle a, wheel t
$R e_{w_{a, t}} \quad$ Axle a, wheel $t$ effective wheel radius from wheel carrier center to tire/road interface
$F_{z 0_{a}} \quad$ Vertical suspension spring preload force applied to the wheels on axle a
$z_{\text {wtr }_{a, t}} \quad$ Distance from wheel carrier center to tire/road interface, along the vehicle-fixed $z$ axis
$z_{v_{a t}, t}{\dot{v_{a, t}}} \quad$ Vehicle displacement and velocity at axle a, wheel t , along the vehicle-fixed $z$-axis
$z_{w_{a, t}} \dot{z}_{w_{a, t}} \quad$ Wheel displacement and velocity at axle a, wheel t , along the vehicle-fixed $z$-axis

## Ports

Input
WhIPz - Wheel z-axis displacement
array
Wheel displacement, $z_{w}$, along wheel-fixed $z$-axis, in m . Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlPz:

- Signal array dimensions are [1×4].

$$
\mathrm{WhlPz}=z_{w}=\left[z_{w_{1,1}} z_{w_{1,2}} z_{w_{2,1}} z_{w_{2,2}}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlPz $(1,1)$ | 1 | 1 |
| Front right | WhlPz $(1,2)$ | 1 | 2 |
| Rear left | WhlPz $(1,3)$ | 2 | 1 |
| Rear right | WhlPz $(1,4)$ | 2 | 2 |

WhIRe - Wheel effective radius
array
Effective wheel radius, $R e_{w}$, in m. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlRe:

- Signal array dimensions are [1×4].

WhlRe $=\operatorname{Re} e_{w}=\left[R e_{w_{1,1}} R e_{w_{1,2}} R e_{w_{2,1}} R e_{w_{2}, 2}\right]$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlRe $(1,1)$ | 1 | 1 |
| Front right | WhlRe $(1,2)$ | 1 | 2 |
| Rear left | WhlRe $(1,3)$ | 2 | 1 |
| Rear right | WhlRe $(1,4)$ | 2 | 2 |

WhIVz - Wheel z-axis velocity
array
Wheel velocity, $\dot{z}_{w}$, along wheel-fixed $z$-axis, in m. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlVz:

- Signal array dimensions are [1×4].

WhlVz $=\dot{z}_{w}=\left[\begin{array}{lll}\dot{z}_{w_{1,1}} & \dot{z}_{w_{1,2}} & \dot{z}_{w_{2,1}}\end{array} \dot{z}_{w_{2}, 2}\right]$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlVz $(1,1)$ | 1 | 1 |
| Front right | WhlVz $(1,2)$ | 1 | 2 |
| Rear left | WhlVz $(1,3)$ | 2 | 1 |
| Rear right | WhlVz $(1,4)$ | 2 | 2 |

WhIFx - Longitudinal wheel force on vehicle
array
Longitudinal wheel force applied to vehicle, $F_{w x}$, along the vehicle-fixed $x$-axis. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlFx:

- Signal array dimensions are [1×4].

WhlFx $=F_{w x}=\left[F_{w x_{1,1}} F_{w x_{1,2}} F_{w x_{2,1}} F_{w x_{2}, 2}\right]$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlFx $(1,1)$ | 1 | 1 |
| Front right | WhlFx $(1,2)$ | 1 | 2 |
| Rear left | WhlFx $(1,3)$ | 2 | 1 |
| Rear right | WhlFx $(1,4)$ | 2 | 2 |

WhIFy - Lateral wheel force on vehicle
array
Lateral wheel force applied to vehicle, $F_{w y}$, along the vehicle-fixed $y$-axis. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlFy:

- Signal array dimensions are [1×4].

$$
\text { WhlFy }=F_{w y}=\left[F_{w y 1,1} F_{w y 1,2} F_{w y 2,1} F_{w y_{2,2}}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlFy $(1,1)$ | 1 | 1 |
| Front right | WhlFy $(1,2)$ | 1 | 2 |
| Rear left | WhlFy $(1.3)$ | 2 | 1 |
| Rear right | WhlFy $(1,4)$ | 2 | 2 |

WhIM - Suspension moment on wheel
array
Longitudinal, lateral, and vertical suspension moments at axle a, wheel $t$, applied to the wheel at the axle wheel carrier reference coordinate, in $N \cdot m$. Input array dimensions are 3 by the number of wheels on the vehicle.

- WhlM ( $1, \ldots$ ) - Suspension moment applied to the wheel about the vehicle-fixed $x$-axis (longitudinal)
- WhlM ( $2, \ldots$ ) - Suspension moment applied to the wheel about the vehicle-fixed $y$-axis (lateral)
- WhlM ( $3, \ldots$ ) - Suspension moment applied to the wheel about the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the WhlM:

- Signal dimensions are [3×4].
- Signal contains suspension moments applied to four wheels according to their axle and wheel locations.

$$
\text { WhlM }=M_{w}=\left[\begin{array}{lllll}
M_{w x_{1,1}} & M_{w x_{1,2}} & M_{w x_{2,1}} & M_{w x_{2,2}} \\
M_{w y_{1,1}} & M_{w y_{1,2}} & M_{w y_{2,1}} & M_{w y_{2,2}} \\
M_{w z_{1,1}} & M_{w z_{1,2}} & M_{w z_{2,1}} & M_{w z_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel Numbe r | Moment Axis |
| :---: | :---: | :---: | :---: | :---: |
| Front left | WhlM (1,1) | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front right | WhlM (1,2) | 1 | 2 |  |
| Rear left | WhlM(1,3) | 2 | 1 |  |
| Rear right | WhlM (1,4) | 2 | 2 |  |
| Front left | WhlM $(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front right | WhlM (2,2) | 1 | 2 |  |
| $\begin{array}{\|l} \hline \begin{array}{l} \text { Rear } \\ \text { left } \end{array} \\ \hline \end{array}$ | WhlM (2,3) | 2 | 1 |  |
| Rear right | WhlM (2,4) | 2 | 2 |  |
| Front left | WhlM (3,1) | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front right | WhlM (3,2) | 1 | 2 |  |


| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Moment Axis |
| :--- | :--- | :--- | :--- | :--- |
| Rear <br> left | WhlM(3,3) | 2 | 1 |  |
| Rear <br> right | WhlM(3,4) | 2 | 2 |  |

VehP - Vehicle displacement
array
Vehicle displacement from axle a, wheel $t$ along vehicle-fixed coordinate system, in m. Input array dimensions are 3 the number of wheels on the vehicle.

- $\operatorname{VehP}(1, \ldots)$ - Vehicle displacement from wheel, $\chi_{v}$, along the vehicle-fixed $x$-axis
- $\operatorname{VehP}(2, \ldots)$ - Vehicle displacement from wheel, $y_{v}$, along the vehicle-fixed $y$-axis
- $\operatorname{VehP}(3, \ldots)-$ Vehicle displacement from wheel, $z_{v}$, along the vehicle-fixed $z$-axis

For example, for a two-axle vehicle with two wheels per axle, the VehP:

- Signal dimensions are [3x4].
- Signal contains four displacements according to their axle and wheel locations.

VehP $=\left[\begin{array}{l}x_{v} \\ y_{v} \\ z_{v}\end{array}\right]=\left[\begin{array}{llll}x_{v_{1,1}} & x_{v_{1,2}} & x_{v_{2,1}} & x_{v_{2,2}} \\ y_{v_{1,1}} & y_{v_{1,2}} & y_{v_{2,1}} & y_{v_{2,2}} \\ z_{v_{1,1}} & z_{v_{1,2}} & z_{v_{2,1}} & z_{v_{2,2}}\end{array}\right]$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | $\operatorname{VehP}(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis |
| Front <br> right | $\operatorname{VehP}(1,2)$ | 1 | 2 |  |
| Rear <br> left | $\operatorname{VehP}(1,3)$ | 2 | 1 |  |
| Rear <br> right | $\operatorname{VehP}(1,4)$ | 2 | 2 |  |
| Front <br> left | $\operatorname{VehP}(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis |
| Front <br> right | $\operatorname{VehP}(2,2)$ | 1 | 2 |  |
| Rear <br> left | $\operatorname{VehP}(2,3)$ | 2 | 1 |  |
| Rear <br> right | $\operatorname{VehP}(2,4)$ | 2 | 2 |  |


| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | $\operatorname{VehP}(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis |
| Front <br> right | $\operatorname{VehP}(3,2)$ | 1 | 2 |  |
| Rear <br> left | $\operatorname{VehP}(3,3)$ | 2 | 1 |  |
| Rear <br> right | $\operatorname{VehP}(3,4)$ | 2 | 2 |  |

## VehV - Vehicle velocity

array
Vehicle velocity at axle a, wheel $t$ along vehicle-fixed coordinate system, in $m$. Input array dimensions are 3 by the number of wheels on the vehicle.

- $\operatorname{VehV}(1, \ldots)-$ Vehicle velocity at wheel, $x_{v}$, along the vehicle-fixed $x$-axis
- $\operatorname{VehV}(2, \ldots)$ - Vehicle velocity at wheel, $y_{v}$, along the vehicle-fixed $y$-axis
- $\operatorname{VehV}(3, \ldots)-$ Vehicle velocity at wheel, $z_{v}$, along the vehicle-fixed $z$-axis

For example, for a two-axle vehicle with two wheels per axle, the VehV:

- Signal dimensions are [3x4].
- Signal contains 4 velocities according to their axle and wheel locations.

$$
\text { VehV }=\left[\begin{array}{c}
\dot{x}_{v} \\
\dot{y}_{v} \\
\dot{z}_{v}
\end{array}\right]=\left[\begin{array}{llll}
\dot{x}_{v_{1,1}} & \dot{x}_{v_{1,2}} & \dot{x}_{v_{2,1}} & \dot{x}_{v_{2,2}} \\
\dot{y}_{v_{1,1}} & \dot{y}_{v_{1,2}} & \dot{y}_{v_{2,1}} & \dot{y}_{v_{2,2}} \\
\dot{z}_{v_{1,1}} & \dot{z}_{v_{1,2}} & \dot{z}_{v_{2,1}} & \dot{z}_{v_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | VehV(1,1) | 1 | 1 | Vehicle-fixed $x$-axis |
| Front <br> right | VehV(1,2) | 1 | 2 |  |
| Rear <br> left | VehV(1,3) | 2 | 1 |  |
| Rear <br> right | VehV(1,4) | 2 | 2 |  |
| Front <br> left | VehV(2,1) | 1 | 1 | Vehicle-fixed $y$-axis |
| Front <br> right | VehV(2,2) | 1 | 2 |  |


| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Axis |
| :--- | :--- | :--- | :--- | :--- |
| Rear <br> left | VehV $(2,3)$ | 2 | 1 |  |
| Rear <br> right | VehV $(2,4)$ | 2 | 2 |  |
| Front <br> left | VehV $(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis |
| Front <br> right | VehV(3,2) | 1 | 2 |  |
| Rear <br> left | VehV $(3,3)$ | 2 | 1 |  |
| Rear <br> right | $\operatorname{VehV(3,4)}$ | 2 | 2 |  |

StrgAng - Steering angle, optional
array
Optional steering angle for each wheel, $\delta$. Input array dimensions are 1 by the number of steered wheels.

For example, for a two-axle vehicle with two wheels per axle, you can input steering angles for both wheels on the first axle.

- To create the StrgAng port, set Steered axle enable by axle, StrgEnByAxl to [10]. The input signal array dimensions are [1×2].
- The StrgAng signal contains two steering angles according to their axle and wheel locations.

$$
\operatorname{StrgAng}=\delta_{\text {steer }}=\left[\delta_{\text {steer }_{1,1}} \delta_{\text {steer }_{1,2}}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | StrgAng $(1,1)$ | 1 | 1 |
| Front right | StrgAng $(1,2)$ | 1 | 2 |

## Dependencies

To create input port StrgAng, set an element of the Steered axle enable by axle, StrgEnByAxl vector to 1 .

## Output

Info - Bus signal
bus
Bus signal containing block values. The signals are arrays that depend on the wheel location.
For example, here are the indices for a two-axle, two-wheel vehicle. The total number of wheels is four.

- 1D array signal (1-by-4)

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | $(1,1)$ | 1 | 1 |
| Front right | $(1,2)$ | 1 | 2 |
| Rear left | $(1,3)$ | 2 | 1 |
| Rear right | $(1,4)$ | 2 | 2 |

- 3D array signal (3-by-4)

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | $(1,1)$ | 1 | 1 |
| Front right | $(1,2)$ | 1 | 2 |
| Rear left | $(1,3)$ | 2 | 1 |
| Rear right | $(1,4)$ | 2 | 2 |
| Front left | $(2,1)$ | 1 | 1 |
| Front right | $(2,2)$ | 1 | 2 |
| Rear left | $(2,3)$ | 2 | 1 |
| Rear right | $(2,4)$ | 2 | 2 |
| Front left | $(3,1)$ | 1 | 1 |
| Front right | $(3,2)$ | 2 | 1 |
| Rear left | $(3,3)$ | 2 | 2 |
| Rear right | $(3,4)$ |  |  |


| Signal | Description | Array Signal | Variable | Units |
| :---: | :---: | :---: | :---: | :---: |
| Camber | Wheel angles according to the axle and wheel location. | 1D | WhlAng $[1, \ldots]=\xi=\left[\xi_{a, t}\right]$ | rad |
| Caster |  |  | WhlAng $[2, \ldots]=\eta=\left[\eta_{a, t}\right]$ |  |
| Toe |  |  | WhlAng $[3, \ldots]=\zeta=\left[\zeta_{a, t}\right]$ |  |
| Height | Suspension height | 1D | H | m |
| Power | Suspension power dissipation | 1D | $P_{\text {susp }}$ | W |
| Energy | Suspension absorbed energy | 1D | $E_{\text {susp }}$ | J |


| Signal | Description | Array Signal | Variable Units |
| :---: | :---: | :---: | :---: |
| VehF | Suspension forces applied to the vehicle | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { VehF }=F_{v}= \\ & {\left[\begin{array}{llll} F_{v x_{1,1}} & F_{v x_{1,2}} & F_{v x_{2,1}} & F_{v x_{2,2}} \\ F_{v v_{1,1}} & F_{v y_{1,2}} & F_{v y_{2,1}} & F_{v y_{2,2}} \\ F_{v z_{1,1}} & F_{v z_{1,2}} & F_{v z_{2,1}} & F_{v z_{2,2}} \end{array}\right.} \end{aligned}$ |
| VehM | Suspension moments applied to vehicle | 3D | For a two-axle, two wheels <br> per axle vehicle:VehM $=M_{v}=$$\left[\begin{array}{llll}M_{v x_{1,1}} & M_{v x_{1,2}} & M_{v x_{2,1}} & M_{v \chi_{2,2}} \\ M_{v y_{1,1}} & M_{v y y_{1,2}} & M_{v y 2,1} & M_{v y 2,2} \\ M_{v z_{1,1}} & M_{v z_{1,2}} & M_{v z_{2,1}} & M_{v z_{2,2}}\end{array}\right]$ |
| WhlF | Suspension force applied to wheel | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { WhlF }=F_{w}= \\ & {\left[\begin{array}{llll} F_{w x_{1}, 1} & F_{w x_{1,2}} & F_{w x_{2,1}} & F_{w x_{2}, 2} \\ F_{w y 1,1} & F_{w y_{1,2}} & F_{w y 2,1} & F_{w y 2,2} \\ F_{w z_{1,1}} & F_{w z_{1,2}} & F_{w z 2,1} & F_{w 2_{2,2}} \end{array}\right.} \end{aligned}$ |


| Signal | Description | Array Signal | Variable | Units |
| :---: | :---: | :---: | :---: | :---: |
| WhlP | Wheel displacement | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { WhlP }=\left[\begin{array}{l} x_{w} \\ y_{w} \\ z_{w} \end{array}\right]= \\ & {\left[\begin{array}{llll} x_{w_{1,1}} & x_{w_{1,2}} & x_{w_{2,1}} & x_{w_{2},} \\ y_{w_{1,1}} & y_{w_{1,2}} & y_{w_{2,1}} & y_{w{ }_{2}} \\ z_{w t r_{1,1}} & z_{w t r_{1,2}} & z_{w t r_{2,1}} & z_{w t r_{2}} \end{array}\right.} \end{aligned}$ |  |
| Whlv | Wheel velocity | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { WhlV }=\left[\begin{array}{l} \dot{x}_{w} \\ \dot{y}_{w} \\ \dot{z}_{w} \end{array}\right] \\ & = \\ & {\left[\begin{array}{lll} \dot{x}_{w_{1,1}} & \dot{x}_{w_{1,2}} & \dot{x}_{w_{2,1}} \\ \dot{x}_{w_{2,2}} \\ \dot{y}_{w_{1,1}} & \dot{y}_{w_{1,2}} & \dot{y}_{w_{2,1}} \\ \dot{y}_{w_{2,2}} \\ \dot{z}_{w_{1,1}} & \dot{z}_{w_{1,2}} & \dot{z}_{w_{2,1}} \\ \dot{z}_{w_{2,2}} \end{array}\right]} \end{aligned}$ | m/s |
| WhlAng | Wheel camber, caster, toe angles | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { WhlAng }=\left[\begin{array}{l} \xi \\ \eta \\ \zeta \end{array}\right] \\ & =\left[\begin{array}{lll} \xi_{1,1} & \xi_{1,2} & \xi_{2,1} \\ \eta_{1,1} & \xi_{1,2} & \eta_{2,1} \\ \eta_{2,2} \\ \zeta_{1,1} & \zeta_{1,2} & \zeta_{2,1} \\ \zeta_{2,2} \end{array}\right] \end{aligned}$ | rad |

VehF - Suspension force on vehicle array

Longitudinal, lateral, and vertical suspension force at axle a, wheel $t$, applied to the vehicle at the suspension connection point, in N. Array dimensions are 3 by the number of wheels on the vehicle.

- VehF (1, ...) - Suspension force applied to vehicle along the vehicle-fixed $x$-axis (longitudinal)
- VehF (2,...) - Suspension force applied to vehicle along the vehicle-fixed $y$-axis (lateral)
- VehF (3, . . ) - Suspension force applied to vehicle along the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the VehF:

- Signal dimensions are [3x4].
- Signal contains suspension forces applied to the vehicle according to the axle and wheel locations.

$$
\text { VehF }=F_{v}=\left[\begin{array}{llll}
F_{v x_{1,1}} & F_{v x_{1}, 2} & F_{v x_{2,1}} & F_{v x_{2,2}} \\
F_{v y_{1,1}} & F_{v y_{1,2}} & F_{v y_{2,1}} & F_{v y_{2,2}} \\
F_{v z_{1,1}} & F_{v z_{1,2}} & F_{v z_{2,1}} & F_{v z_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel Numbe r | Force Axis |
| :---: | :---: | :---: | :---: | :---: |
| Front left | $\operatorname{VehF}(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front right | $\operatorname{VehF}(1,2)$ | 1 | 2 |  |
| Rear left | $\operatorname{VehF}(1,3)$ | 2 | 1 |  |
| Rear right | $\operatorname{VehF}(1,4)$ | 2 | 2 |  |
| Front left | $\operatorname{VehF}(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front right | $\operatorname{VehF}(2,2)$ | 1 | 2 |  |
| Rear left | $\operatorname{VehF}(2,3)$ | 2 | 1 |  |
| Rear right | $\operatorname{VehF}(2,4)$ | 2 | 2 |  |
| Front left | $\operatorname{VehF}(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front right | $\operatorname{VehF}(3,2)$ | 1 | 2 |  |
| Rear left | $\operatorname{VehF}(3,3)$ | 2 | 1 |  |
| Rear right | $\operatorname{VehF}(3,4)$ | 2 | 2 |  |

VehM - Suspension moment on vehicle
array
Longitudinal, lateral, and vertical suspension moment at axle $a$, wheel $t$, applied to the vehicle at the suspension connection point, in $N \cdot m$. Array dimensions are 3 by the number of wheels on the vehicle.

- VehM (1, ...) - Suspension moment applied to the vehicle about the vehicle-fixed $x$-axis (longitudinal)
- VehM ( $2, \ldots$ ) - Suspension moment applied to the vehicle about the vehicle-fixed $y$-axis (lateral)
- VehM (3, ...) - Suspension moment applied to the vehicle about the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the VehM:

- Signal dimensions are [3×4].
- Signal contains suspension moments applied to vehicle according to the axle and wheel locations.

$$
\text { VehM }=M_{v}=\left[\begin{array}{llll}
M_{v x_{1,1}} & M_{v x_{1,2}} & M_{v x_{2,1}} & M_{v x_{2,2}} \\
M_{v y 1,1} & M_{v y 1,2} & M_{v x_{2,1}} & M_{v y_{2,2}} \\
M_{v z_{1,1}} & M_{v z_{1,2}} & M_{v z_{2,1}} & M_{v z_{2,2}}
\end{array}\right]
$$

| Array Element | Axle | Wheel Number | Moment Axis |
| :---: | :---: | :---: | :---: |
| $\operatorname{VehM}(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| $\operatorname{VehM}(1,2)$ | 1 | 2 |  |
| $\operatorname{VehM}(1,3)$ | 2 | 1 |  |
| VehM (1,4) | 2 | 2 |  |
| $\operatorname{VehM}(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| VehM (2,2) | 1 | 2 |  |
| VehM (2,3) | 2 | 1 |  |
| $\operatorname{VehM}(2,4)$ | 2 | 2 |  |
| $\operatorname{VehM}(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| $\operatorname{VehM}(3,2)$ | 1 | 2 |  |
| $\operatorname{VehM}(3,3)$ | 2 | 1 |  |
| VehM ( 3,4 ) | 2 | 2 |  |

WhIF - Suspension force on wheel
array
Longitudinal, lateral, and vertical suspension forces at axle a, wheel $t$, applied to the wheel at the axle wheel carrier reference coordinate, in N. Array dimensions are 3 by the number of wheels on the vehicle.

- $\operatorname{WhlF}(1, \ldots)$ - Suspension force on wheel along the vehicle-fixed $x$-axis (longitudinal)
- $\operatorname{WhlF}(2, \ldots)$ - Suspension force on wheel along the vehicle-fixed $y$-axis (lateral)
- $\operatorname{WhlF}(3, \ldots)$ - Suspension force on wheel along the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the WhlF:

- Signal dimensions are [3×4].
- Signal contains wheel forces applied to the vehicle according to the axle and wheel locations.

$$
\text { WhlF }=F_{w}=\left[\begin{array}{lllll}
F_{w x_{1,1}} & F_{w x_{1,2}} & F_{w x_{2,1}} & F_{w x_{2,2}} \\
F_{w y_{1,1}} & F_{w y 1,2} & F_{w y 2,1} & F_{w y 2,2} \\
F_{w z_{1,1}} & F_{w z_{1,2}} & F_{w z 2,1} & F_{w z_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel Numbe r | Force Axis |
| :---: | :---: | :---: | :---: | :---: |
| Front left | WhlF (1,1) | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front right | WhlF(1,2) | 1 | 2 |  |
| Rear left | WhlF(1,3) | 2 | 1 |  |
| Rear right | WhlF(1,4) | 2 | 2 |  |
| Front left | WhlF (2,1) | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front right | WhlF (2,2) | 1 | 2 |  |
| $\begin{array}{\|l} \text { Rear } \\ \text { left } \end{array}$ | WhlF (2,3) | 2 | 1 |  |
| Rear right | WhlF (2,4) | 2 | 2 |  |
| $\begin{aligned} & \text { Front } \\ & \text { left } \end{aligned}$ | WhlF (3,1) | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front right | WhlF(3,2) | 1 | 2 |  |
| Rear left | WhlF (3, 3) | 2 | 1 |  |
| Rear right | WhlF (3,4) | 2 | 2 |  |

WhIV - Wheel velocity
array
Longitudinal, lateral, and vertical wheel velocity at axle a, wheel $t$, in $m / s$. Array dimensions are 3 by the number of wheels on the vehicle.

- WhlV (1, ...) - Wheel velocity along the vehicle-fixed $x$-axis (longitudinal)
- WhlV $(2, \ldots)$ - Wheel velocity along the vehicle-fixed $y$-axis (lateral)
- WhlV $(3, \ldots)-$ Wheel velocity along the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the Whlv:

- Signal dimensions are [3×4].
- Signal contains wheel forces applied to the vehicle according to the axle and wheel locations.

$$
\text { WhlV }=\left[\begin{array}{c}
\dot{x}_{w} \\
\dot{y}_{w} \\
\dot{z}_{w}
\end{array}\right]=\left[\begin{array}{llll}
\dot{x}_{w_{1,1}} & \dot{x}_{w_{1,2}} & \dot{x}_{w_{2,1}} & \dot{x}_{w_{2,2}} \\
\dot{y}_{w_{1,1}} & \dot{y}_{w_{1,2}} & \dot{y}_{w_{2,1}} & \dot{y}_{w_{2,2}} \\
\dot{z}_{w_{1,1}} & \dot{z}_{w_{1,2}} & \dot{z}_{w_{2,1}} & \dot{z}_{w_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | WhlV $(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front <br> right | WhlV $(1,2)$ | 1 | 2 |  |
| Rear <br> left | WhlV $(1,3)$ | 2 | 1 |  |
| Rear <br> right | WhlV $(1,4)$ | 2 | 2 |  |
| Front <br> left | WhlV $(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front <br> right | WhlV $(2,2)$ | 1 | 2 |  |
| Rear <br> left | WhlV $(2,3)$ | 2 | 1 |  |
| Rear <br> right | WhlV $(2,4)$ | 2 | 2 |  |
| Front <br> left | WhlV $(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front <br> right | WhlV $(3,2)$ | 1 | 2 |  |
| Rear <br> left | WhlV $(3,3)$ | 2 | 1 |  |
| Rear <br> right | WhlV $(3,4)$ | 2 | 2 |  |

WhIAng - Wheel camber, caster, toe angles
array
Camber, caster, and toe angles at axle a, wheel $t$, in rad. Array dimensions are 3 by the number of wheels on the vehicle.

- WhlAng (1,...) - Camber angle
- WhlAng $(2, \ldots)$ - Caster angle
- Whlang $(3, \ldots)$ - Toe angle

For example, for a two-axle vehicle with two wheels per axle, the WhlAng:

- Signal dimensions are [3x4].
- Signal contains angles according to the axle and wheel locations.

$$
\text { WhlAng }=\left[\begin{array}{l}
\xi \\
\eta \\
\zeta
\end{array}\right]=\left[\begin{array}{llll}
\xi_{1,1} & \xi_{1,2} & \xi_{2,1} & \xi_{2,2} \\
\eta_{1,1} & \eta_{1,2} & \eta_{2,1} & \eta_{2,2} \\
\zeta_{1,1} & \zeta_{1,2} & \zeta_{2,1} & \zeta_{2,2}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Angle |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | WhlAng (1,1) | 1 | 1 | Camber |
| Front <br> right | WhlAng (1,2) | 1 | 2 |  |
| Rear <br> left | WhlAng (1,3) | 2 | 1 |  |
| Rear <br> right | WhlAng (1,4) | 2 | 2 |  |
| Front <br> left | WhlAng (2,1) | 1 | 1 | Caster |
| Front <br> right | WhlAng (2,2) | 1 | 2 |  |
| Rear <br> left | WhlAng (2,3) | 2 | 1 |  |
| Rear <br> right | WhlAng (2,4) | 2 | 2 |  |
| Front <br> left | WhlAng (3,1) | 1 | 1 | Toe |
| Front <br> right | WhlF(3,2) | 1 | 2 |  |
| Rear <br> left | WhlF(3,3) | 2 | 1 |  |
| Rear <br> right | WhlF(3,4) | 2 | 2 |  |

## Parameters

## Enable active damping - Include damping

off (default) | off
Include damping

## Dependencies

Selecting this parameter creates:

## - Damping coefficient map, f_act_susp_cz

- Damping actuator duty cycle breakpoints, f_act_susp_duty_bpt
- Damping actuator velocity breakpoints, f_act_susp_zdot_bpt

Number of axles, NumAxI - Number of axles
2 (default) | scalar
Number of axles, $N_{a}$, dimensionless.
Number of wheels by axle, NumWhlsByAxI - Number of wheels per axle
[2 2] (default)|vector
Number of wheels per axle, $N t_{a}$, dimensionless. Vector is 1 by the number of vehicle axles, $N_{a}$. For example, [1,2] represents one wheel on axle one and two wheels on axle two.

Steered axle enable by axle, StrgEnByAxI - Boolean vector to enable axle steering
[1 0] (default)|vector
Boolean vector that enables axle steering, $E n_{\text {steer }}$, dimensionless. Vector is 1 by the number of vehicle axles, $N_{a}$. For example:

- [10 $\left.\begin{array}{ll}1 & 0\end{array}\right]$ - For a two-axle vehicle, enables axle 1 steering and disables axle 2 steering
- [ll $\left.\begin{array}{ll}1 & 1\end{array}\right]$ - For a two-axle vehicle, enables axle 1 and axle 2 steering


## Dependencies

Setting any element of the Steered axle enable by axle, StrgEnByAxl vector to 1 creates:

- Input port StrgAng.
- Parameters:
- Toe angle vs steering angle slope, ToeStrgSlp
- Caster angle vs steering angle slope, CasterStrgSlp
- Camber angle vs steering angle slope, CamberStrgSlp
- Suspension height vs steering angle slope, StrgHgtSIp

For example, for a two-axle vehicle with two wheels per axle, you can input steering angles for both wheels on the first axle.

- To create the StrgAng port, set Steered axle enable by axle, StrgEnByAxl to [1 0]. The input signal array dimensions are [1×2].
- The StrgAng signal contains two steering angles according to their axle and wheel locations.

$$
\operatorname{StrgAng}=\delta_{\text {steer }}=\left[\delta_{\text {steer }_{1,1}} \delta_{\text {steer }_{1,2}}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | StrgAng $(1,1)$ | 1 | 1 |
| Front right | StrgAng $(1,2)$ | 1 | 2 |

Anti-sway axle enable by axle, AntiSwayEnByAxI - Boolean vector to enable axle anti-sway [0 0] (default) |vector

Boolean vector that enables axle anti-sway for axle $a$, dimensionless. For example, [10] enables axle 1 anti-sway and disables axle 2 anti-sway. Vector is 1 by the number of vehicle axles, $N_{a}$.

## Dependencies

Setting an element of the Anti-sway axle enable by axle, AntiSwayEnByAxl vector to 1 creates these anti-sway parameters:

- Anti-sway arm radius, AntiSwayR
- Anti-sway arm neutral angle, AntiSwayNtrlAng
- Anti-sway torsion spring constant, AntiSwayTrsK


## Suspension

Compliance and Damping - Passive
Suspension spring constant, Kz - Suspension spring constant
64370 (default) | scalar | vector
Linear vertical spring constant for independent suspension wheels on axle a, $k_{z_{\alpha^{\prime}}}$ in $\mathrm{N} / \mathrm{m}$.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Suspension spring preload, FOz - Suspension spring preload

9810 (default) | scalar | vector
Vertical preload spring force applied to the wheels on the axle at wheel carrier reference coordinates, $F_{z 0_{a^{\prime}}}$ in N. Positive preload forces:

- Cause the vehicle to lift.
- Point along the negative vehicle-fixed $z$-axis.

Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

Suspension shock damping constant, Cz - Suspension shock damping constant 10000 (default) | scalar | vector

Linear vertical damping constant for independent suspension wheels on axle a, $c_{z_{a^{\prime}}}$ in $\mathrm{Ns} / \mathrm{m}$.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Dependencies

To create this parameter, clear Enable active damping.

## Suspension maximum height, Hmax - Height

0.5 (default) | scalar | vector

Maximum suspension extension or minimum suspension compression height, $H_{\text {max }}$, for axle a before the suspension reaches a hardstop, in $m$.

Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Compliance and Damping - Active

## Damping coefficient map, f_act_susp_cz - Lookup table

[10000 10000;10000 10000] (default) | M-by-N array
Damping coefficient table as a function of active duty cycle and actuator compression velocity, in $\mathrm{N} \cdot \mathrm{s} / \mathrm{m}$. Each value specifies the damping for a specific combination of actuator duty cycle and velocity. The array dimensions must match the duty cycle, M , and actuator velocity, N , breakpoint vector dimensions.

## Dependencies

To create this parameter, clear Enable active damping.
Damping actuator duty cycle breakpoints, f_act_susp_duty_bpt - Duty cycle breakpoints [0 1] (default) | 1-by-M vector

Damping actuator duty cycle breakpoints, dimensionless.

## Dependencies

To create this parameter, clear Enable active damping.
Damping actuator velocity breakpoints, f_act_susp_zdot_bpt - Velocity breakpoints
[-1 1] (default) | 1-by-N vector
Damping actuator velocity breakpoints, in $\mathrm{m} / \mathrm{s}$.

## Dependencies

To create this parameter, clear Enable active damping.

## Geometry

Toe angle at steering center, Toe - Toe angle
0.0349 (default) | scalar

Nominal suspension toe angle at zero steering angle, $\zeta_{0 a}$, in rad.
Roll steer vs suspension height slope, RollStrgSIp - Steer angle suspension slope -0. 2269 (default) | scalar | vector

Roll steer angle versus suspension height, $m_{\text {htoe } a_{a}}$, in rad $/ \mathrm{m}$.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

Toe angle vs steering angle slope, ToeStrgSIp - Toe angle steering slope
0.01 (default) | scalar | vector

Toe angle versus steering angle slope, $m_{\text {toesteer }_{a^{\prime}}}$ dimensionless.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Dependencies

To create input port StrgAng, set an element of the Steered axle enable by axle, StrgEnByAxl vector to 1 .

Caster angle at steering center, Caster - Caster angle at steering center 0.0698 (default) | scalar

Nominal suspension caster angle at zero steering angle, $\eta_{0 a}$, in rad.
Caster angle vs suspension height slope, CasterHslp - Caster angle versus suspension height slope
-0. 2269 (default) | scalar | vector
Caster angle versus suspension height, $m_{\text {haster }_{a^{\prime}}}$ in rad $/ \mathrm{m}$.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

Caster angle vs steering angle slope, CasterStrgSIp - Caster angle versus steering angle slope 0.01 (default) | scalar | vector

Caster angle versus steering angle slope, $m_{\text {castersteer }_{a^{\prime}}}$ dimensionless. .
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Dependencies

To create input port StrgAng, set an element of the Steered axle enable by axle, StrgEnByAxl vector to 1 .

Camber angle at steering center, Camber - Camber angle at steering center 0.0698 (default) | scalar

Nominal suspension camber angle at zero steering angle, $\xi_{0 a}$, in rad.
Camber angle vs suspension height slope, CamberHslp - Camber angle versus suspension height slope

- 0.2269 (default) | scalar | vector

Camber angle versus suspension height, $m_{\text {hcamber }{ }_{a}}$ in rad $/ \mathrm{m}$.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

Camber angle vs steering angle slope, CamberStrgSIp - Camber angle versus steering angle slope
0.01 (default) | scalar | vector

Camber angle versus steering angle slope, $m_{\text {cambersteer }_{a}}$, dimensionless.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Dependencies

To create input port StrgAng, set an element of the Steered axle enable by axle, StrgEnByAxl vector to 1 .

Suspension height vs steering angle slope, StrgHgtSIp - Suspension height versus steering angle slope
0.1432 (default) | scalar | vector

Steering angle to vertical force slope applied at suspension wheel carrier reference point, $m_{\text {hsteer }_{a^{\prime}}}$ in $\mathrm{m} / \mathrm{rad}$.

Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Dependencies

To create input port StrgAng, set an element of the Steered axle enable by axle, StrgEnByAxl vector to 1 .

Anti-Sway
Anti-sway arm radius, AntiSwayR - Anti-sway arm radius
0.2 (default) | scalar | vector

Anti-sway arm radius, $r$, in m.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Dependencies

Setting an element of the Anti-sway axle enable by axle, AntiSwayEnByAxl vector to 1 creates these anti-sway parameters:

- Anti-sway arm radius, AntiSwayR
- Anti-sway arm neutral angle, AntiSwayNtrlAng
- Anti-sway torsion spring constant, AntiSwayTrsK

Anti-sway arm neutral angle, AntiSwayNtrIAng - Anti-sway arm neutral angle
0.5236 (default) | scalar | vector

Anti-sway arm neutral angle, $\theta_{0 a}$, at nominal suspension height, in rad.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Dependencies

Setting an element of the Anti-sway axle enable by axle, AntiSwayEnByAxl vector to 1 creates these anti-sway parameters:

- Anti-sway arm radius, AntiSwayR
- Anti-sway arm neutral angle, AntiSwayNtrlAng
- Anti-sway torsion spring constant, AntiSwayTrsK

Anti-sway torsion spring constant, AntiSwayTrsK - Anti-sway torsion spring constant
$5.7296 \mathrm{e}+03$ (default) | scalar | vector
Anti-sway bar torsion spring constant, $k_{a}$, in $\mathrm{N} \cdot \mathrm{m} / \mathrm{rad}$.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Dependencies

Setting an element of the Anti-sway axle enable by axle, AntiSwayEnByAxl vector to 1 creates these anti-sway parameters:

- Anti-sway arm radius, AntiSwayR
- Anti-sway arm neutral angle, AntiSwayNtrlAng
- Anti-sway torsion spring constant, AntiSwayTrsK


## Version History

## Introduced in R2018a

## R2022b: Parameter name change from NumTracksByAxl to NumWhlsByAxl Behavior changed in R2022b

The Number of tracks by axle, NumTracksByAxl parameter is renamed to Number of wheels by axle, NumWhlsByAxl.

The block uses the number of wheels per axle to index the input and output block signals.

## References

[1] Gillespie, Thomas. Fundamentals of Vehicle Dynamics. Warrendale, PA: Society of Automotive Engineers, 1992.
[2] Vehicle Dynamics Standards Committee. Vehicle Dynamics Terminology. SAE J670. Warrendale, PA: Society of Automotive Engineers, 2008.
[3] Technical Committee. Road vehicles - Vehicle dynamics and road-holding ability - Vocabulary. ISO 8855:2011. Geneva, Switzerland: International Organization for Standardization, 2011.

## Extended Capabilities

C/C++ Code Generation
Generate C and C++ code using Simulink ${ }^{\circledR}$ Coder $^{\mathrm{TM}}$.

## See Also

Independent Suspension - Double Wishbone | Independent Suspension - Mapped | Independent Suspension - K and C

## Independent Suspension - Mapped

Mapped independent suspension


## Libraries:

Vehicle Dynamics Blockset / Suspension

## Description

The Independent Suspension - Mapped block implements a mapped independent suspension for multiple axles with multiple wheels per axle. You can use the block to model suspension geometry, compliance, and damping effects from measured or simulated suspension response data.

The block models the suspension compliance, damping, and geometric effects as functions of the relative positions and velocities of the vehicle and wheel carrier with axle-specific compliance and damping parameters. Using the suspension compliance and damping, the block calculates the suspension force on the vehicle and wheel. The block uses the Z-down coordinate system (defined in SAE J670).

| For Each | You Can Specify |
| :--- | :--- |
| Axle | $\bullet \quad$ Multiple wheels |
|  | $\bullet \quad$ An anti-sway bar for axles with two wheels |
|  | $\bullet \quad$ Suspension parameters |
| Wheel | $\bullet \quad$ Steering angles |

The block contains energy-storing spring elements and energy-dissipating damper elements. It does not contain energy-storing mass elements. The block assumes that the vehicle (sprung) and wheel (unsprung) blocks connected to the block store the mass-related suspension energy.

This table summarizes the block parameter settings for a vehicle with:

- Two axles
- Two wheels per axle
- Steering angle input for both wheels on the front axle
- An anti-sway bar on the front axle

| Parameter | Setting |
| :--- | :--- |
| Number of axles, NumAxl | 2 |
| Number of wheels by axle, NumWhlsByAxl | $\left[\begin{array}{ll}2 & 2\end{array}\right]$ |
| Steered axle enable by axle, StrgEnByAxl | $\left[\begin{array}{ll}1 & 0\end{array}\right]$ |
| Anti-sway axle enable by axle, <br> AntiSwayEnByAxl | $\left[\begin{array}{ll}1 & 0\end{array}\right]$ |

The block uses the wheel number, $t$, to index the input and output signals. This table summarizes the wheel, axle, and corresponding wheel number for a vehicle with:

- Two axles
- Two wheels per axle

| Wheel | Axle | Wheel Number |
| :--- | :--- | :--- |
| Front left | Front | 1 |
| Front right | Front | 2 |
| Rear left | Rear | 1 |
| Rear right | Rear | 2 |

## Suspension Compliance and Damping

The block uses a lookup table that relates the vertical damping and compliance to the suspension height, suspension height rate of change, and steering angle. You can calibrate the wheel force lookup table so that steering angle changes from the nominal center position generate a force that increases the vehicle height.

The block implements these equations.

$$
\begin{aligned}
& F_{w z l o o k u p_{a}}=f\left(z_{v_{a, t}}-z_{w_{a, t}} \dot{z}_{v_{a, t}}-\dot{z}_{w_{a, t},} \delta_{\text {steer }_{a, t}}\right) \\
& F_{w z_{a, t}}=F_{w z l o o k u p_{a}}+F_{z a s w y_{a, t}}
\end{aligned}
$$

The block assumes that the suspension elements have no mass. Therefore, the suspension forces and moments applied to the vehicle are equal to the suspension forces and moments applied to the wheel.

$$
\begin{aligned}
& F_{v x_{a, t}}=F_{w x_{a, t}} \\
& F_{v y_{a, t}}=F_{w y_{a, t}} \\
& F_{v z_{a, t}}=-F_{w z_{a, t}} \\
& M_{v x_{a, t}}=M_{w x_{a, t}}+F_{w y_{a, t}}\left(R e_{w y_{a, t}}+H_{a, t}\right) \\
& M_{v y_{a, t}}=M_{w y_{a, t}}+F_{w x_{a, t}}\left(R e_{w x_{a, t}}+H_{a, t}\right) \\
& M_{v z_{a, t}}=M_{w z_{a, t}}
\end{aligned}
$$

The block sets the wheel positions and velocities equal to the vehicle lateral and longitudinal positions and velocities.

$$
\begin{aligned}
x_{w_{a, t}} & =x_{v_{a, t}} \\
y_{w_{a, t}} & =y_{v_{a, t}} \\
\dot{x}_{w_{a, t}} & =\dot{x}_{v_{a, t}} \\
\dot{y}_{w_{a, t}} & =\dot{y}_{v_{a, t}}
\end{aligned}
$$

The equations use these variables.

| $F_{w z_{a, t},} M_{w z_{a, t}}$ | Suspension force and moment applied to the wheel on axle a, wheel $t$ along wheel-fixed $z$-axis |
| :---: | :---: |
| $F_{w x_{a, t}} M_{w \chi_{a, t}}$ | Suspension force and moment applied to the wheel on axle a, wheel $t$ along wheel-fixed $x$-axis |
| $F_{w y_{y_{a}, t}} M_{w y_{a, t}}$ | Suspension force and moment applied to the wheel on axle a, wheel $t$ along wheel-fixed $y$-axis |
| $F_{v z_{a, t}} M_{v z_{a, t}}$ | Suspension force and moment applied to the vehicle on axle a, wheel t along wheel-fixed $z$-axis |
| $F_{v x_{a, t}} M_{v x_{0}, t}$ | Suspension force and moment applied to the vehicle on axle a, wheel t along wheel-fixed $x$-axis |
| $F_{v y_{a, t}} M_{v y^{\prime}, t}$ | Suspension force and moment applied to the vehicle on axle a, wheel t along wheel-fixed $y$-axis |
| $F_{z 0_{a}}$ | Vertical suspension spring preload force applied to the wheels on axle a |
| $k_{z_{a}}$ | Vertical spring constant applied to wheels on axle a |
| kwa ${ }_{\text {z }}$ | Wheel and axle interface compliance constant |
| $m_{\text {hsteer }}^{\text {a }}$ | Steering angle to vertical force slope applied at wheel carrier for wheels on axle a |
| $\delta_{\text {steer }}{ }_{\text {at }}$ | Steering angle input for axle a, wheel t |
| $C_{z_{a}}$ | Vertical damping constant applied to wheels on axle a |
| $c w a_{z}$ | Wheel and axle interface damping constant |
| $R e_{w_{a, t}}$ | Effective wheel radius for axle a, wheel t |
| $F_{z h s t o p a t}$ | Vertical hardstop force at axle a , wheel t , along the vehicle-fixed $z$-axis |
| $F_{\text {zaswy }}^{\text {a }}$, | Vertical anti-sway force at axle a , wheel t , along the vehicle-fixed $z$-axis |
| $F w a_{z 0}$ | Wheel and axle interface compliance constant |
| $z_{v_{a, t}} \dot{z}_{v_{a, t}}$ | Vehicle displacement and velocity at axle $a$, wheel $t$, along the vehiclefixed $z$-axis |
| $z_{w_{a, t}} \dot{z}_{w_{a}, t}$ | Wheel displacement and velocity at axle a , wheel t , along the vehicle-fixed $z$-axis |
| $\chi_{v_{a, t}}, \dot{\chi}_{v_{a, t}}$ | Vehicle displacement and velocity at axle $a$, wheel $t$, along the vehiclefixed $z$-axis |
| $\chi_{w_{a, t}} \dot{x}_{w_{a, t}}$ | Wheel displacement and velocity at axle a, wheel t , along the vehicle-fixed $z$-axis |
| $y_{v_{a, t}} \dot{y}_{v_{a, t}}$ | Vehicle displacement and velocity at axle a , wheel t , along the vehiclefixed $y$-axis |
| $y_{w_{a, t}} \dot{y}_{w_{a, t}}$ | Wheel displacement and velocity at axle $a$, wheel $t$, along the vehicle-fixed $y$-axis |
| $H_{a, t}$ | Suspension height at axle a, wheel t |
| $R e_{w_{a, t}}$ | Effective wheel radius at axle a , wheel t |

## Anti-Sway Bar

Optionally, use the Anti-sway axle enable by axle, AntiSwayEnByAxl parameter to implement an anti-sway bar force, $F_{\text {zaswy } y_{a},}$ for axles that have two wheels. This figure shows how the anti-sway bar transmits torque between two independent suspension wheels on a shared axle. Each independent
suspension applies a torque to the anti-sway bar via a radius arm that extends from the anti-sway bar back to the independent suspension connection point.


To calculate the sway bar force, the block implements these equations.
\(\left.$$
\begin{array}{|l|l|}\hline \text { Calculation } & \text { Equation } \\
\hline \begin{array}{l}\text { Anti-sway bar angular deflection } \\
\text { for a given axle and wheel, } \Delta \theta_{a, t}\end{array} & \begin{array}{l}\theta_{0 a}=\tan ^{-1}\left(\frac{z_{0}}{r}\right) \\
\\
\Delta \theta_{a, t}=\tan ^{-1}\left(\frac{r \tan \theta_{0 a}-z_{w_{a, t}}+z_{v_{a, t}}}{r}\right)\end{array}
$$ <br>
\hline Anti-sway bar twist angle, \theta_{a} \& \theta_{a}=-\tan ^{-1}\left(\frac{r \tan \theta_{0 a}-z_{w_{a, 1}}+z_{v_{a, 1}}}{r}\right) <br>

-\tan ^{-1}\left(\frac{r \tan \theta_{0 a}-z_{w_{a, 2}}+z_{v_{a, 2}}}{r}\right)\end{array}\right]\)\begin{tabular}{ll|}

\hline | Anti-sway bar forces applied to |
| :--- |
| the wheel on axle a, wheel t |
| along wheel-fixed $z$-axis | \& $F_{z a s w y_{a, 1}}=\left(\frac{\tau_{a}}{r}\right) \cos \left(\theta_{0 a}-\tan ^{-1}\left(\frac{r \tan \theta_{0 a}-z_{w_{a, 1}}+z_{v_{a, 1}}}{r}\right)\right)$ <br>

\hline
\end{tabular}

The equations and figure use these variables.

| $\tau_{a}$ | Anti-sway bar torque |
| :--- | :--- |
| $\theta$ | Anti-sway bar twist angle |
| $\theta_{0 a}$ | Initial anti-sway bar twist angle |
| $\Delta \theta_{a, t}$ | Anti-sway bar angular deflection at axle a, wheel t |
| $r$ | Anti-sway bar arm radius |
| $z_{0}$ | Vertical distance from anti-sway bar connection point to anti-sway bar centerline |

$F_{z s w a y}^{a t} \quad$ Anti-sway bar force applied to the wheel on axle a, wheel $t$ along wheel-fixed $z$-axis
$z_{v_{a, t}} \quad$ Vehicle displacement at axle a, wheel t , along the vehicle-fixed $z$-axis
$z_{w_{a, t}} \quad$ Wheel displacement at axle a, wheel t , along the vehicle-fixed $z$-axis

## Camber, Caster, and Toe Angles

To calculate the camber, caster, and toe angles, the block uses a lookup table, $G_{\text {alookup }}$, that is a function of the suspension height and steering angle.

$$
\left[\xi_{a, t} \eta_{a, t} \zeta_{a, t}\right]=G_{a l o o k u p} f\left(z_{w_{a, t}}-z_{v_{a, t^{\prime}}} \delta_{\text {steer }_{a, t}}\right)
$$

The equations use these variables.

| $\xi_{a, t}$ | Camber angle of wheel on axle a , wheel t |
| :--- | :--- |
| $\eta_{a, t}$ | Caster angle of wheel on axle a , wheel t |
| $\zeta_{a, t}$ | Toe angle of wheel on axle a, wheel t |
| $\delta_{\text {steer }}^{a, t}$ |  |$\quad$| $z_{v_{a, t}}$ | Steering angle input for axle a, wheel t |
| :--- | :--- |
| $z_{w_{a, t}}$ | Vehicle displacement at axle a, wheel t , along vehicle-fixed $z$-axis |
|  | Wheel displacement at axle a, wheel t , along vehicle-fixed $z$-axis |

## Steering Angles

Optionally, you can input steering angles for the wheels. To calculate the steering angles for the wheels, the block offsets the input steering angles as a function of the suspension height. For the calculation, the block uses a lookup table, $G_{\text {alookup }}$, that is a function of the suspension position and steering angle.

$$
\delta_{\text {whlsteer }_{a, t}}=\delta_{\text {steer }_{a, t}}+G_{\text {alookup }} f\left(z_{w_{a, t}}-z_{v_{a, t^{\prime}}} \delta_{\text {steer }_{a, t}}\right)
$$

The equation uses these variables.
$\delta_{\text {whlster }_{a t}} \quad$ Wheel steering angle for axle a, wheel t
$\delta_{\text {steer }_{\text {at }}} \quad$ Steering angle input for axle a, wheel t
$z_{v_{a, t}} \quad$ Vehicle displacement at axle a, wheel t , along the vehicle-fixed $z$-axis
$z_{w_{a, t}} \quad$ Wheel displacement at axle a, wheel t , along the vehicle-fixed $z$-axis

## Power and Energy

The block calculates these suspension characteristics for each axle, a , wheel, t .

| Calculation | Equation |
| :---: | :---: |
| Dissipated power, $P_{\text {susp }}^{a, t}$ | $P_{\text {susp }_{a, t}}=F_{\text {wzlookupa }\left(\dot{z}_{v_{a, t}}-\dot{z}_{w_{a, t}}, \dot{z}_{v_{a, t}}-\dot{z}_{w_{a, t}} \delta_{\text {steer }_{a, t}}\right)}$ |
| Absorbed energy, $E_{\text {susp }_{a, t}}$ | $E_{\text {susp }_{a, t}}=F_{\text {wzlookupa }\left(\dot{z}_{v_{a, t}}-\dot{z}_{w_{a, t},{ }^{\prime}} \dot{z}_{v_{a, t}}-\dot{z}_{w_{a, t^{\prime}}} \delta_{\text {steer }_{a, t}}\right)}$ |
| Suspension height, $H_{a, t}$ | $H_{a, t}=-\left(z_{v_{a, t}}-z_{w_{a, t}}-\operatorname{median}\left(f_{-}\right.\right.$susp_d $\left.\left.z_{-} b p\right)\right)$ |


| Calculation |  |
| :--- | :--- |
| Distance from wheel carrier <br> center to tire/road interface |  |
| The equations use these variables. |  |

$m_{\text {hsteer }_{a}} \quad$ Steering angle to vertical force slope applied at wheel carrier for wheels on axle a
$\delta_{\text {steer }_{\text {at }}} \quad$ Steering angle input for axle a , wheel t
$R e_{w_{a, t}} \quad$ Axle a, wheel $t$ effective wheel radius from wheel carrier center to tire/road interface
f_susp_dz_bp Vertical axis suspension height breakpoints
$z_{w t r_{a t}} \quad$ Distance from wheel carrier center to tire/road interface, along the vehicle-fixed $z$ axis
$z_{v_{a t i}} \dot{z}_{v_{a, t}} \quad$ Vehicle displacement and velocity at axle a, wheel t , along the vehicle-fixed $z$-axis
$z_{w_{a, t}} \dot{z}_{w_{a, t}} \quad$ Wheel displacement and velocity at axle a, wheel t , along the vehicle-fixed $z$-axis

## Ports

## Input

WhIPz - Wheel z-axis displacement
array
Wheel displacement, $z_{w}$, along wheel-fixed $z$-axis, in m . Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlPz:

- Signal array dimensions are [1x4].

$$
\text { WhlPz }=z_{w}=\left[\begin{array}{llll}
z_{w_{1,1}} & z_{w_{1,2}} & z_{w_{2,1}} & z_{w_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlPz $(1,1)$ | 1 | 1 |
| Front right | WhlPz $(1,2)$ | 1 | 2 |
| Rear left | WhlPz $(1,3)$ | 2 | 1 |
| Rear right | WhlPz $(1,4)$ | 2 | 2 |

WhIRe - Wheel effective radius
array
Effective wheel radius, $R e_{w}$, in m. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlRe:

- Signal array dimensions are [1x4].

$$
\text { WhlRe }=R e_{w}=\left[\begin{array}{lll}
R e_{w_{1,1}} & R e_{w_{1,2}} & R e_{w_{2,1}}
\end{array} R e_{w_{2,2}}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlRe $(1,1)$ | 1 | 1 |
| Front right | WhlRe $(1,2)$ | 1 | 2 |
| Rear left | WhlRe $(1,3)$ | 2 | 1 |
| Rear right | WhlRe $(1,4)$ | 2 | 2 |

WhIVz - Wheel z-axis velocity array

Wheel velocity, $\dot{z}_{w}$, along wheel-fixed $z$-axis, in m. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlVz:

- Signal array dimensions are [1×4].

$$
\text { WhlVz }=\dot{z}_{w}=\left[\dot{z}_{w_{1,1}} \dot{z}_{w_{1,2}} \dot{z}_{w_{2,1}} \dot{z}_{w_{2,2}}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlVz $(1,1)$ | 1 | 1 |
| Front right | WhlVz $(1,2)$ | 1 | 2 |
| Rear left | WhlVz $(1,3)$ | 2 | 1 |
| Rear right | WhlVz $(1,4)$ | 2 | 2 |

WhIFx - Longitudinal wheel force on vehicle
array
Longitudinal wheel force applied to vehicle, $F_{w x}$, along the vehicle-fixed $x$-axis. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlFx:

- Signal array dimensions are [1×4].

WhlFx $=F_{w x}=\left[F_{w x_{1,1}} F_{w x_{1,2}} F_{w x_{2,1}} F_{w x_{2,2}}\right]$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlFx(1,1) | 1 | 1 |
| Front right | WhlFx(1,2) | 1 | 2 |
| Rear left | WhlFx(1,3) | 2 | 1 |
| Rear right | WhlFx(1,4) | 2 | 2 |

WhIFy - Lateral wheel force on vehicle
array
Lateral wheel force applied to vehicle, $F_{w y}$, along the vehicle-fixed $y$-axis. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlFy:

- Signal array dimensions are [1x4].

$$
\text { WhlFy }=F_{w y}=\left[F_{w y_{1,1}} F_{w y_{1,2}} F_{w y_{2,1}} F_{w y_{2,2}}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlFy $(1,1)$ | 1 | 1 |
| Front right | WhlFy $(1,2)$ | 1 | 2 |
| Rear left | WhlFy $(1.3)$ | 2 | 1 |
| Rear right | WhlFy $(1,4)$ | 2 | 2 |

WhIM - Suspension moment on wheel
array
Longitudinal, lateral, and vertical suspension moments at axle a, wheel $t$, applied to the wheel at the axle wheel carrier reference coordinate, in $\mathrm{N} \cdot \mathrm{m}$. Input array dimensions are 3 by the number of wheels on the vehicle.

- WhlM (1, . . ) - Suspension moment applied to the wheel about the vehicle-fixed $x$-axis (longitudinal)
- $\operatorname{WhlM}(2, \ldots)$ - Suspension moment applied to the wheel about the vehicle-fixed $y$-axis (lateral)
- WhlM $(3, \ldots)$ - Suspension moment applied to the wheel about the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the WhlM:

- Signal dimensions are [3×4].
- Signal contains suspension moments applied to four wheels according to their axle and wheel locations.

$$
\text { WhlM }=M_{w}=\left[\begin{array}{lllll}
M_{w x_{1,1}} & M_{w x_{1,2}} & M_{w x_{2,1}} & M_{w x_{2,2}} \\
M_{w y_{1,1}} & M_{w y 1,2} & M_{w y_{2,1}} & M_{w y 2,2} \\
M_{w z_{1,1}} & M_{w z_{1,2}} & M_{w z_{2,1}} & M_{w z_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Moment Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | WhlM(1,1) | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front <br> right | WhlM(1,2) | 1 | 2 |  |
| Rear <br> left | WhlM $(1,3)$ | 2 | 1 |  |
| Rear <br> right | WhlM(1,4) | 2 | 2 |  |
| Front <br> left | WhlM $(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |


| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Moment Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> right | WhlM $(2,2)$ | 1 | 2 |  |
| Rear <br> left | WhlM $(2,3)$ | 2 | 1 |  |
| Rear <br> right | WhlM $(2,4)$ | 2 | 2 |  |
| Front <br> left | WhlM $(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front <br> right | WhlM $(3,2)$ | 1 | 2 |  |
| Rear <br> left | WhlM(3,3) | 2 | 1 |  |
| Rear <br> right | WhlM(3,4) | 2 | 2 |  |

VehP - Vehicle displacement
array
Vehicle displacement from axle a, wheel $t$ along vehicle-fixed coordinate system, in m. Input array dimensions are 3 the number of wheels on the vehicle.

- $\operatorname{VehP}(1, \ldots)$ - Vehicle displacement from wheel, $\chi_{v}$, along the vehicle-fixed $x$-axis
- $\operatorname{VehP}(2, \ldots)$ - Vehicle displacement from wheel, $y_{v}$, along the vehicle-fixed $y$-axis
- $\operatorname{VehP}(3, \ldots)$ - Vehicle displacement from wheel, $z_{v}$, along the vehicle-fixed $z$-axis

For example, for a two-axle vehicle with two wheels per axle, the VehP:

- Signal dimensions are [3×4].
- Signal contains four displacements according to their axle and wheel locations.

VehP $=\left[\begin{array}{l}x_{v} \\ y_{v} \\ z_{v}\end{array}\right]=\left[\begin{array}{llll}x_{v_{1,1}} & x_{v_{1,2}} & x_{v_{2,1}} & x_{v_{2,2}} \\ y_{v_{1,1}} & y_{v_{1,2}} & v_{v_{2,1}} & y_{v_{2,2}} \\ z_{v_{1,1}} & z_{v_{1,2}} & z_{v_{2,1}} & z_{v_{2,2}}\end{array}\right]$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | VehP $(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis |
| Front <br> right | $\operatorname{VehP}(1,2)$ | 1 | 2 |  |
| Rear <br> left | $\operatorname{VehP}(1,3)$ | 2 | 1 |  |


| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Axis |
| :--- | :--- | :--- | :--- | :--- |
| Rear <br> right | $\operatorname{VehP}(1,4)$ | 2 | 2 |  |
| Front <br> left | $\operatorname{VehP}(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis |
| Front <br> right | $\operatorname{VehP}(2,2)$ | 1 | 2 |  |
| Rear <br> left | $\operatorname{VehP}(2,3)$ | 2 | 1 |  |
| Rear <br> right | $\operatorname{VehP}(2,4)$ | 2 | 2 |  |
| Front <br> left | $\operatorname{VehP}(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis |
| Front <br> right | $\operatorname{VehP}(3,2)$ | 1 | 2 |  |
| Rear <br> left | $\operatorname{VehP}(3,3)$ | 2 | 1 |  |
| Rear <br> right | $\operatorname{VehP}(3,4)$ | 2 | 2 |  |

VehV - Vehicle velocity
array
Vehicle velocity at axle $a$, wheel $t$ along vehicle-fixed coordinate system, in $m$. Input array dimensions are 3 by the number of wheels on the vehicle.

- $\operatorname{VehV}(1, \ldots)-$ Vehicle velocity at wheel, $x_{v}$, along the vehicle-fixed $x$-axis
- VehV $(2, \ldots)-$ Vehicle velocity at wheel, $y_{v}$, along the vehicle-fixed $y$-axis
- VehV $(3, \ldots)-$ Vehicle velocity at wheel, $z_{v}$, along the vehicle-fixed $z$-axis

For example, for a two-axle vehicle with two wheels per axle, the VehV:

- Signal dimensions are [3×4].
- Signal contains 4 velocities according to their axle and wheel locations.

VehV $=\left[\begin{array}{l}\dot{x}_{v} \\ \dot{y}_{v} \\ \dot{z}_{v}\end{array}\right]=\left[\begin{array}{lllll}\dot{x}_{v_{1,1}} & \dot{x}_{v_{1,2}} & \dot{x}_{v_{2,1}} & \dot{x}_{v_{2,2}} \\ \dot{y}_{v_{1,1}} & \dot{y}_{v_{1,2}} & \dot{y}_{v_{2,1}} & \dot{y}_{v_{2,2}} \\ \dot{z}_{v_{1,1}} & \dot{z}_{v_{1,2}} & \dot{z}_{v_{2,1}} & \dot{z}_{v_{2,2}}\end{array}\right]$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> $\mathbf{r}$ | Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | VehV $(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis |


| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> right | VehV $(1,2)$ | 1 | 2 |  |
| Rear <br> left | VehV $(1,3)$ | 2 | 1 |  |
| Rear <br> right | VehV $(1,4)$ | 2 | 2 |  |
| Front <br> left | VehV $(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis |
| Front <br> right | VehV(2,2) | 1 | 2 |  |
| Rear <br> left | VehV(2,3) | 2 | 1 |  |
| Rear <br> right | VehV(2,4) | 2 | 2 |  |
| Front <br> left | VehV(3,1) | 1 | 1 | Vehicle-fixed $z$-axis |
| Front <br> right | VehV(3,2) | 1 | 2 |  |
| Rear <br> left | VehV(3,3) | 2 | 1 |  |
| Rear <br> right | VehV(3,4) | 2 | 2 |  |

## StrgAng - Steering angle, optional

array
Optional steering angle for each wheel, $\delta$. Input array dimensions are 1 by the number of steered wheels.

For example, for a two-axle vehicle with two wheels per axle, you can input steering angles for both wheels on the first axle.

- To create the StrgAng port, set Steered axle enable by axle, StrgEnByAxl to [1 0]. The input signal array dimensions are [1×2].
- The StrgAng signal contains two steering angles according to their axle and wheel locations.

$$
\text { StrgAng }=\delta_{\text {steer }}=\left[\delta_{\text {steer }_{1,1}} \delta_{\text {steer }_{1,2}}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | StrgAng $(1,1)$ | 1 | 1 |
| Front right | StrgAng $(1,2)$ | 1 | 2 |

## Dependencies

To create input port StrgAng, set an element of the Steered axle enable by axle, StrgEnByAxl vector to 1 .

## Output

Info - Bus signal
bus
Bus signal containing block values. The signals are arrays that depend on the wheel location.
For example, here are the indices for a two-axle, two-wheel vehicle. The total number of wheels is four.

- 1D array signal (1-by-4)

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | $(1,1)$ | 1 | 1 |
| Front right | $(1,2)$ | 1 | 2 |
| Rear left | $(1,3)$ | 2 | 1 |
| Rear right | $(1,4)$ | 2 | 2 |

- 3D array signal (3-by-4)

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | $(1,1)$ | 1 | 1 |
| Front right | $(1,2)$ | 1 | 2 |
| Rear left | $(1,3)$ | 2 | 1 |
| Rear right | $(1,4)$ | 2 | 2 |
| Front left | $(2,1)$ | 1 | 1 |
| Front right | $(2,2)$ | 1 | 2 |
| Rear left | $(2,3)$ | 2 | 1 |
| Rear right | $(2,4)$ | 2 | 2 |
| Front left | $(3,1)$ | 1 | 1 |
| Front right | $(3,2)$ | 1 | 2 |
| Rear left | $(3,3)$ | 2 | 1 |
| Rear right | $(3,4)$ | 2 | 2 |

$\begin{array}{|l|l|l|l|l|}\hline \text { Signal } & \text { Description } & \text { Array Signal } & \text { Variable } & \text { Units } \\ \hline \text { Camber } & \text { Wheel angles according } & \text { 1D } & \text { WhlAng }[1, \ldots]=\xi=\left[\xi_{a, t}\right] & \text { rad } \\$\cline { 1 - 3 } \& to the axle and wheel\end{array}$)$

| Signal | Description | Array Signal | Variable | Units |
| :---: | :---: | :---: | :---: | :---: |
| Power | Suspension power dissipation | 1D | $P_{\text {susp }}$ | W |
| Energy | Suspension absorbed energy | 1D | $E_{\text {susp }} \mathrm{J}$ | J |
| VehF | Suspension forces applied to the vehicle | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { VehF }=F_{v}= \\ & {\left[\begin{array}{llll} F_{v x_{1,1}} & F_{v x_{1,2}} & F_{v x_{2,1}} & F_{v x_{2}, 2} \\ F_{v v_{1,1}} & F_{v v_{1,2}} & F_{v v_{2,1}} & F_{v y_{2,2}} \\ F_{v z 1,1} & F_{v z_{1,2}} & F_{v z_{2,1}} & F_{v z_{2,2}} \end{array}\right.} \end{aligned}$ | $\mathrm{N}$ |
| VehM | Suspension moments applied to vehicle | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { VehM }=M_{v}= \\ & {\left[\begin{array}{lllll} M_{v x_{1}, 1} & M_{v x_{1}, 2} & M_{v x_{2}, 1} & M_{v \times 2} \\ M_{v y_{1}, 1} & M_{v y_{1}, 2} & M_{v y 2,1} & M_{v y 2} \\ M_{v z_{1,1}} & M_{v z_{1,2}} & M_{v z_{2,1}} & M_{v z_{2}} \end{array}\right.} \end{aligned}$ | $\mathrm{N} \cdot \mathrm{~m}$ <br> 2,2 <br> 2,2 <br> 2,2 |


| Signal | Description | Array Signal | Variable | Units |
| :---: | :---: | :---: | :---: | :---: |
| WhlF | Suspension force applied to wheel | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { WhlF }=F_{w}= \\ & {\left[\begin{array}{llll} F_{w x_{1}, 1} & F_{w x_{1,2}} & F_{w x_{2}, 1} & F_{w x_{2}} \\ F_{w y 1,1} & F_{w y_{1,2}} & F_{w y 2,1} & F_{w y_{2}} \\ F_{w z_{1,1}} & F_{w z_{1,2}} & F_{w z_{2,1}} & F_{w z_{2}} \end{array}\right.} \end{aligned}$ |  |
| WhlP | Wheel displacement | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { WhlP }=\left[\begin{array}{l} x_{w} \\ y_{w} \\ z_{w} \end{array}\right]= \\ & {\left[\begin{array}{llll} x_{w_{1,1}} & x_{w_{1,2}} & x_{w_{2,1}} & x_{w_{2}}, \\ y_{w_{1,1}} & y_{w_{1,2}} & y_{w_{2,1}} & y_{w y_{2}} \\ z_{w t r_{1,1}} & z_{w t t_{1,2}} & z_{w t r_{2,1}} & z_{w t r_{2}} \end{array}\right.} \end{aligned}$ |  |
| Whlv | Wheel velocity | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { WhlV }=\left[\begin{array}{c} \dot{x}_{w} \\ \dot{y}_{w} \\ \dot{z}_{w} \end{array}\right] \\ & = \\ & {\left[\begin{array}{lll} \dot{x}_{w_{1,1}} & \dot{x}_{w_{1,2}} & \dot{x}_{w_{2,1}} \\ \dot{x}_{w_{2,2}} \\ \dot{y}_{w_{1,1}} & \dot{y}_{w_{1,2}} & \dot{y}_{w_{2,1}} \\ \dot{y}_{w_{2,2}} \\ \dot{z}_{w_{1,1}} & \dot{z}_{w_{1,2}} & \dot{z}_{w_{2,1}} \\ \dot{z}_{w_{2,2}} \end{array}\right]} \end{aligned}$ | m/s |


| Signal | Description | Array Signal | Variable | Units |
| :---: | :---: | :---: | :---: | :---: |
| WhlAng | Wheel camber, caster toe angles | 3D | For a two-axle, two wheels per axle vehicle: $\left.\begin{array}{l} \text { WhlAng }=\left[\begin{array}{l} \xi \\ \eta \\ \zeta \end{array}\right] \\ =\left[\begin{array}{lll} \xi_{1,1} & \xi_{1,2} & \xi_{2,1} \\ \xi_{2,2} \\ \eta_{1,1} & \eta_{1,2} & \eta_{2,1} \\ \eta_{2,2} \\ \zeta_{1,1} & \zeta_{1,2} & \zeta_{2,1} \end{array} \zeta_{2,2}\right. \end{array}\right] . \begin{aligned} & \eta_{2} \end{aligned}$ | rad |

## VehF - Suspension force on vehicle

array
Longitudinal, lateral, and vertical suspension force at axle a, wheel $t$, applied to the vehicle at the suspension connection point, in N . Array dimensions are 3 by the number of wheels on the vehicle.

- $\operatorname{VehF}(1, \ldots)$ - Suspension force applied to vehicle along the vehicle-fixed $x$-axis (longitudinal)
- $\operatorname{VehF}(2, \ldots)$ - Suspension force applied to vehicle along the vehicle-fixed $y$-axis (lateral)
- $\operatorname{VehF}(3, \ldots)$ - Suspension force applied to vehicle along the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the VehF:

- Signal dimensions are [3×4].
- Signal contains suspension forces applied to the vehicle according to the axle and wheel locations.

$$
\text { VehF }=F_{v}=\left[\begin{array}{lllll}
F_{v x_{1,1}} & F_{v x_{1,2}} & F_{v x_{2,1}} & F_{v x_{2,2}} \\
F_{v y_{1,1}} & F_{v y_{1,2}} & F_{v y_{2,1}} & F_{v y_{2,2}} \\
F_{v z_{1,1}} & F_{v z_{1,2}} & F_{v z_{2,1}} & F_{v z_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | $\operatorname{VehF}(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front <br> right | $\operatorname{VehF}(1,2)$ | 1 | 2 |  |
| Rear <br> left | $\operatorname{VehF}(1,3)$ | 2 | 1 |  |
| Rear <br> right | $\operatorname{VehF}(1,4)$ | 2 | 2 |  |
| Front <br> left | $\operatorname{VehF}(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front <br> right | $\operatorname{VehF}(2,2)$ | 1 | 2 |  |


| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Rear <br> left | $\operatorname{VehF}(2,3)$ | 2 | 1 |  |
| Rear <br> right | $\operatorname{VehF}(2,4)$ | 2 | 2 |  |
| Front <br> left | $\operatorname{VehF}(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front <br> right | $\operatorname{VehF}(3,2)$ | 1 | 2 |  |
| Rear <br> left | $\operatorname{VehF}(3,3)$ | 2 | 1 |  |
| Rear <br> right | $\operatorname{VehF}(3,4)$ | 2 | 2 |  |

VehM - Suspension moment on vehicle
array
Longitudinal, lateral, and vertical suspension moment at axle a, wheel $t$, applied to the vehicle at the suspension connection point, in $\mathrm{N} \cdot \mathrm{m}$. Array dimensions are 3 by the number of wheels on the vehicle.

- VehM (1, ...) - Suspension moment applied to the vehicle about the vehicle-fixed $x$-axis (longitudinal)
- VehM ( $2, \ldots$ ) - Suspension moment applied to the vehicle about the vehicle-fixed $y$-axis (lateral)
- Vehm ( $3, \ldots$ ) - Suspension moment applied to the vehicle about the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the VehM:

- Signal dimensions are [3×4].
- Signal contains suspension moments applied to vehicle according to the axle and wheel locations.

VehM $=M_{v}=\left[\begin{array}{lllll}M_{v x_{1,1}} & M_{v x_{1,2}} & M_{v x_{2,1}} & M_{v x_{2,2}} \\ M_{v y_{1,1}} & M_{v y_{1,2}} & M_{v y_{2,1}} & M_{v y_{2,2}} \\ M_{v z_{1,1}} & M_{v z_{1,2}} & M_{v z_{2,1}} & M_{v z_{2,2}}\end{array}\right]$

| Array Element | Axle | Wheel <br> Number | Moment Axis |
| :--- | :--- | :--- | :--- |
| $\operatorname{VehM}(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| $\operatorname{VehM}(1,2)$ | 1 | 2 |  |
| $\operatorname{VehM}(1,3)$ | 2 | 1 |  |
| $\operatorname{VehM}(1,4)$ | 2 | 2 |  |
| $\operatorname{VehM}(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| $\operatorname{VehM}(2,2)$ | 1 | 2 |  |


| Array Element | Axle | Wheel <br> Number | Moment Axis |
| :--- | :--- | :--- | :--- |
| $\operatorname{VehM}(2,3)$ | 2 | 1 |  |
| $\operatorname{VehM}(2,4)$ | 2 | 2 |  |
| $\operatorname{VehM}(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| $\operatorname{VehM}(3,2)$ | 1 | 2 |  |
| $\operatorname{VehM}(3,3)$ | 2 | 1 |  |
| $\operatorname{VehM}(3,4)$ | 2 | 2 |  |

WhIF - Suspension force on wheel
array
Longitudinal, lateral, and vertical suspension forces at axle a, wheel $t$, applied to the wheel at the axle wheel carrier reference coordinate, in N . Array dimensions are 3 by the number of wheels on the vehicle.

- $\operatorname{WhlF}(1, \ldots)$ - Suspension force on wheel along the vehicle-fixed $x$-axis (longitudinal)
- $\operatorname{WhlF}(2, \ldots)$ - Suspension force on wheel along the vehicle-fixed $y$-axis (lateral)
- WhlF $(3, \ldots)$ - Suspension force on wheel along the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the WhlF:

- Signal dimensions are [3×4].
- Signal contains wheel forces applied to the vehicle according to the axle and wheel locations.

WhlF $=F_{w}=\left[\begin{array}{lllll}F_{w x_{1,1}} & F_{w x_{1,2}} & F_{w x_{2,1}} & F_{w x_{2,2}} \\ F_{w y_{1,1}} & F_{w y_{1,2}} & F_{w y_{2,1}} & F_{w y_{2,2}} \\ F_{w z_{1,1}} & F_{w z_{1,2}} & F_{w z_{2,1}} & F_{w z_{2,2}}\end{array}\right]$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | WhlF $(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front <br> right | WhlF $(1,2)$ | 1 | 2 |  |
| Rear <br> left | WhlF $(1,3)$ | 2 | 1 |  |
| Rear <br> right | WhlF $(1,4)$ | 2 | 2 |  |
| Front <br> left | WhlF $(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front <br> right | WhlF $(2,2)$ | 1 | 2 |  |


| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Rear <br> left | WhlF $(2,3)$ | 2 | 1 |  |
| Rear <br> right | WhlF $(2,4)$ | 2 | 2 |  |
| Front <br> left | WhlF (3,1) | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front <br> right | WhlF (3,2) | 1 | 2 |  |
| Rear <br> left | WhlF $(3,3)$ | 2 | 1 |  |
| Rear <br> right | WhlF (3,4) | 2 | 2 |  |

WhIV - Wheel velocity
array
Longitudinal, lateral, and vertical wheel velocity at axle a, wheel t , in $\mathrm{m} / \mathrm{s}$. Array dimensions are 3 by the number of wheels on the vehicle.

- WhlV (1, ...) - Wheel velocity along the vehicle-fixed $x$-axis (longitudinal)
- WhlV $(2, \ldots)$ - Wheel velocity along the vehicle-fixed $y$-axis (lateral)
- WhlV $(3, \ldots)-$ Wheel velocity along the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the Whlv:

- Signal dimensions are [3×4].
- Signal contains wheel forces applied to the vehicle according to the axle and wheel locations.

$$
\text { WhlV }=\left[\begin{array}{l}
\dot{x}_{w} \\
\dot{y}_{w} \\
\dot{z}_{w}
\end{array}\right]=\left[\begin{array}{llll}
\dot{x}_{w_{1,1}} & \dot{x}_{w_{1,2}} & \dot{x}_{w_{2,1}} & \dot{x}_{w_{2,2}} \\
\dot{y}_{w_{1,1}} & \dot{y}_{w_{1,2}} & \dot{y}_{w_{2,1}} & \dot{y}_{w_{2,2}} \\
\dot{z}_{w_{1,1}} & \dot{z}_{w_{1,2}} & \dot{z}_{w_{2,1}} & \dot{z}_{w_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | WhlV $(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front <br> right | WhlV $(1,2)$ | 1 | 2 |  |
| Rear <br> left | WhlV $(1,3)$ | 2 | 1 |  |
| Rear <br> right | WhlV $(1,4)$ | 2 | 2 |  |


| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | WhlV $(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front <br> right | WhlV $(2,2)$ | 1 | 2 |  |
| Rear <br> left | WhlV $(2,3)$ | 2 | 1 |  |
| Rear <br> right | WhlV $(2,4)$ | 2 | 2 |  |
| Front <br> left | WhlV $(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front <br> right | WhlV $(3,2)$ | 1 | 2 |  |
| Rear <br> left | WhlV(3,3) | 2 | 1 |  |
| Rear <br> right | WhlV(3,4) | 2 | 2 |  |

WhIAng - Wheel camber, caster, toe angles
array
Camber, caster, and toe angles at axle $a$, wheel $t$, in rad. Array dimensions are 3 by the number of wheels on the vehicle.

- WhlAng (1,...) - Camber angle
- WhlAng $(2, \ldots)$ - Caster angle
- Whlang $(3, \ldots)$ - Toe angle

For example, for a two-axle vehicle with two wheels per axle, the WhlAng:

- Signal dimensions are [3x4].
- Signal contains angles according to the axle and wheel locations.

$$
\text { WhlAng }=\left[\begin{array}{l}
\xi \\
\eta \\
\zeta
\end{array}\right]=\left[\begin{array}{llll}
\xi_{1,1} & \xi_{1,2} & \xi_{2,1} & \xi_{2,2} \\
\eta_{1,1} & \eta_{1,2} & \eta_{2,1} & \eta_{2,2} \\
\zeta_{1,1} & \zeta_{1,2} & \zeta_{2,1} & \zeta_{2,2}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Angle |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | WhlAng (1,1) | 1 | 1 | Camber |
| Front <br> right | WhlAng (1,2) | 1 | 2 |  |


| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Angle |
| :--- | :--- | :--- | :--- | :--- |
| Rear <br> left | WhlAng (1,3) | 2 | 1 |  |
| Rear <br> right | WhlAng (1,4) | 2 | 2 |  |
| Front <br> left | WhlAng (2,1) | 1 | 1 | Caster |
| Front <br> right | WhlAng (2,2) | 1 | 2 |  |
| Rear <br> left | WhlAng (2,3) | 2 | 1 |  |
| Rear <br> right | WhlAng(2,4) | 2 | 2 |  |
| Front <br> left | WhlAng(3,1) | 1 | 1 | Toe |
| Front <br> right | WhlF(3,2) | 1 | 2 |  |
| Rear <br> left | WhlF(3,3) | 2 | 1 |  |
| Rear <br> right | WhlF(3,4) | 2 | 2 |  |

## Parameters

## Axles

Number of axles, NumAxI - Number of axles
2 (default) | scalar
Number of axles, $N_{a}$, dimensionless.
Number of wheels by axle, NumWhlsByAxI - Number of wheels per axle
[2 2] (default)|vector
Number of wheels per axle, $N t_{a}$, dimensionless. Vector is 1 by the number of vehicle axles, $N_{a}$. For example, [1,2] represents one wheel on axle one and two wheels on axle two.

Steered axle enable by axle, StrgEnByAxI - Boolean vector to enable axle steering
[1 0] (default)| vector
Boolean vector that enables axle steering, $E n_{\text {steer }}$, dimensionless. Vector is 1 by the number of vehicle axles, $N_{a}$. For example:

- [10] - For a two-axle vehicle, enables axle 1 steering and disables axle 2 steering
- [ll 1 1] - For a two-axle vehicle, enables axle 1 and axle 2 steering


## Dependencies

Setting any element of the Steered axle enable by axle, StrgEnByAxl vector to 1 creates:

- Input port StrgAng.
- Parameters:
- Toe angle vs steering angle slope, ToeStrgSlp
- Caster angle vs steering angle slope, CasterStrgSlp
- Camber angle vs steering angle slope, CamberStrgSlp
- Suspension height vs steering angle slope, StrgHgtSlp

For example, for a two-axle vehicle with two wheels per axle, you can input steering angles for both wheels on the first axle.

- To create the StrgAng port, set Steered axle enable by axle, StrgEnByAxl to [1 0]. The input signal array dimensions are [1×2].
- The StrgAng signal contains two steering angles according to their axle and wheel locations.

$$
\text { StrgAng }=\delta_{\text {steer }}=\left[\delta_{\text {steer }_{1,1}} \delta_{\text {steer }_{1,2}}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | StrgAng $(1,1)$ | 1 | 1 |
| Front right | StrgAng $(1,2)$ | 1 | 2 |

Anti-sway axle enable by axle, AntiSwayEnByAxI - Boolean vector to enable axle anti-sway [0 0] (default)|vector

Boolean vector that enables axle anti-sway for axle $a$, dimensionless. For example, [10] enables axle 1 anti-sway and disables axle 2 anti-sway. Vector is 1 by the number of vehicle axles, $N_{a}$.

## Dependencies

Setting an element of the Anti-sway axle enable by axle, AntiSwayEnByAxl vector to 1 creates these anti-sway parameters:

- Anti-sway arm radius, AntiSwayR
- Anti-sway arm neutral angle, AntiSwayNtrlAng
- Anti-sway torsion spring constant, AntiSwayTrsK


## Suspension

## Mapped

Axle breakpoints, f_susp_axl_bp - Breakpoints
[1 2] (default) | 1-by-P array
Axle breakpoints, dimensionless.
Vertical axis suspension height breakpoints, f_susp_dz_bp - Breakpoints
1-by-M array
Vertical axis suspension height breakpoints, in $m$.

## Vertical axis suspension height velocity breakpoints, f_susp_dzdot_bp - Breakpoints

 1-by-N arrayVertical axis suspension height velocity breakpoints, in $\mathrm{m} / \mathrm{s}$.

## Vertical axis suspension force and moment responses, f_susp_fmz - Output array

 zeros (31, 31, 61, 2, 4) (default) | M-by-N-by-0-by-P-by-4 arrayArray of output values as a function of:

- Vertical suspension height, $M$
- Vertical suspension height velocity, $N$
- Steering angle, $O$
- Axle, $P$
- 4 output types
- 1 - Vertical force, in N
- 2 - User-defined
- 3-Stored energy, in J
- 4 - Absorbed power, in W

The array dimensions must match the breakpoint dimensions
Suspension geometry responses, f_susp_geom - Suspension geometry responses zeros (31,61, 2, 3) (default) | M-by-0-by-P-by-3 array

Array of geometric suspension values as a function of:

- Vertical suspension height, $M$
- Steering angle, $O$
- Axle, $P$
- 3 output types
- 1 - Camber angle, in rad
- 2 - Caster angle, in rad
- 3-Toe angle, in rad

The array dimensions must match the breakpoint dimensions
Steering angle breakpoints, f_susp_strgdelta_bp - Steering angle breakpoints 1-by-0 array

Steering angle breakpoints, in rad.

## Anti-Sway

Anti-sway arm radius, AntiSwayR - Anti-sway arm radius
0.2 (default) | scalar | vector

Anti-sway arm radius, $r$, in m.

Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Dependencies

Setting an element of the Anti-sway axle enable by axle, AntiSwayEnByAxl vector to 1 creates these anti-sway parameters:

- Anti-sway arm radius, AntiSwayR
- Anti-sway arm neutral angle, AntiSwayNtrlAng
- Anti-sway torsion spring constant, AntiSwayTrsK

Anti-sway arm neutral angle, AntiSwayNtrIAng - Anti-sway arm neutral angle 0.5236 (default) | scalar | vector

Anti-sway arm neutral angle, $\theta_{0 a}$, at nominal suspension height, in rad.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Dependencies

Setting an element of the Anti-sway axle enable by axle, AntiSwayEnByAxl vector to 1 creates these anti-sway parameters:

- Anti-sway arm radius, AntiSwayR
- Anti-sway arm neutral angle, AntiSwayNtrlAng
- Anti-sway torsion spring constant, AntiSwayTrsK

Anti-sway torsion spring constant, AntiSwayTrsK - Anti-sway torsion spring constant $5.7296 \mathrm{e}+03$ (default) | scalar | vector

Anti-sway bar torsion spring constant, $k_{a}$, in $\mathrm{N} \cdot \mathrm{m} / \mathrm{rad}$.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Dependencies

Setting an element of the Anti-sway axle enable by axle, AntiSwayEnByAxl vector to 1 creates these anti-sway parameters:

- Anti-sway arm radius, AntiSwayR
- Anti-sway arm neutral angle, AntiSwayNtrlAng
- Anti-sway torsion spring constant, AntiSwayTrsK


## Version History

## Introduced in R2018a

## R2022b: Parameter name change from NumTracksByAxl to NumWhlsByAxl Behavior changed in R2022b

The Number of tracks by axle, NumTracksByAxl parameter is renamed to Number of wheels by axle, NumWhlsByAxl.

The block uses the number of wheels per axle to index the input and output block signals.

## References

[1] Gillespie, Thomas. Fundamentals of Vehicle Dynamics. Warrendale, PA: Society of Automotive Engineers, 1992.
[2] Vehicle Dynamics Standards Committee. Vehicle Dynamics Terminology. SAE J670. Warrendale, PA: Society of Automotive Engineers, 2008.
[3] Technical Committee. Road vehicles - Vehicle dynamics and road-holding ability - Vocabulary. ISO 8855:2011. Geneva, Switzerland: International Organization for Standardization, 2011.

## Extended Capabilities

C/C++ Code Generation
Generate C and $\mathrm{C}++$ code using Simulink ${ }^{\circledR}$ Coder $^{\text {TM }}$.

## See Also

Independent Suspension - Double Wishbone | Independent Suspension - MacPherson | Independent Suspension - K and C

## Solid Axle Suspension - Mapped

Mapped solid axle suspension


## Libraries:

Vehicle Dynamics Blockset / Suspension

## Description

The Solid Axle Suspension - Mapped block implements a mapped solid axle suspension for multiple axles with multiple wheels per axle.

The block models the suspension compliance, damping, and geometric effects as functions of the wheel positions and velocities, with axle-specific compliance and damping parameters. Using the wheel position and velocity, the block calculates the vertical wheel position and suspension forces on the vehicle and wheel. The block uses the Z-down (defined in SAE J670) and a solid axle coordinate system. The solid axle coordinate system, shown here, is aligned with the Z-down vehicle coordinate system, with the $x$-axis in the direction of forward vehicle motion.


| For Each | You Can Specify |
| :--- | :--- |
| Axle | • Multiple wheels |
|  | - Suspension parameters |
| Wheel | • Steering angles |

The block contains energy-storing spring elements and energy-dissipating damper elements. The block also stores energy via the axle roll angular acceleration and axle center of mass vertical and lateral acceleration.

This table summarizes the block parameter settings for a vehicle with:

- Two axles
- Two wheels per axle
- Steering angle input for both wheels on the front axle

| Parameter | Setting |
| :--- | :--- |
| Number of axles, NumAxl | 2 |
| Number of wheels by axle, NumWhlsByAxl | $\left[\begin{array}{ll}2 & 2\end{array}\right]$ |
| Steered axle enable by axle, StrgEnByAxl | $\left[\begin{array}{ll}1 & 0\end{array}\right]$ |

The block uses the wheel number, $t$, to index the input and output signals. This table summarizes the wheel, axle, and corresponding wheel number for a vehicle with:

- Two axles
- Two wheels per axle

| Wheel | Axle | Wheel Number |
| :--- | :--- | :--- |
| Front left | Front | 1 |
| Front right | Front | 2 |
| Rear left | Rear | 1 |
| Rear right | Rear | 2 |

## Suspension Compliance and Damping

The block uses a lookup table that relates the vertical damping and compliance to the suspension height, suspension height rate of change, and steering angle. You can calibrate the wheel force lookup table so that steering angle changes from the nominal center position generate a force that increases the vehicle height. Specifically, the block:

| Uses | To Calculate |
| :--- | :--- |
| -Longitudinal and lateral displacement and <br> velocity of the vehicle. | -Suspension forces applied to the axle center. <br> - <br> Lorgitudinal and lateral displacement and <br> velocity of the wheel. <br> - Vertical wheel forces applied to the vehicle. <br> vehicle and wheel. |
|  | -Longitudinal, lateral, and vertical suspension <br> forces and moments applied to the vehicle. <br> Longitudinal, lateral, and vertical suspension <br> forces and moments applied to the wheel. |

To calculate the dynamics of the axle, the block implements these equations. The block neglects the effects of:

- Lateral and longitudinal translational velocity.
- Angular velocity about the vertical and lateral axes.

$$
\begin{aligned}
& {\left[\begin{array}{l}
\ddot{x}_{a} \\
\ddot{y}_{a} \\
\ddot{z}_{a}
\end{array}\right]=\frac{1}{M_{a}}\left[\begin{array}{l}
F_{x a} \\
F_{y a} \\
F_{z a}
\end{array}\right]+\left[\begin{array}{c}
\dot{x}_{a} \\
\dot{y}_{a} \\
\dot{z}_{a}
\end{array}\right] \times\left[\begin{array}{l}
p \\
q \\
r
\end{array}\right]=\frac{1}{M_{a}}\left[\begin{array}{c}
0 \\
0 \\
F_{z a}
\end{array}\right]+\left[\begin{array}{c}
0 \\
0 \\
\dot{z}_{a}
\end{array}\right] \times\left[\begin{array}{l}
p \\
0 \\
0
\end{array}\right]+\left[\begin{array}{l}
0 \\
0 \\
g
\end{array}\right]=\left[\begin{array}{c}
0 \\
p \dot{z}_{a} \\
\frac{F_{z a}}{M_{a}}+g
\end{array}\right]} \\
& {\left[\begin{array}{l}
\dot{p} \\
\dot{q} \\
\dot{r}
\end{array}\right]=\left[\left[\begin{array}{l}
M_{x} \\
M_{y} \\
M_{z}
\end{array}\right]-\left[\begin{array}{l}
p \\
q \\
r
\end{array}\right] \times\left[\begin{array}{ccc}
I_{x x} & 0 & 0 \\
0 & I_{y y} & 0 \\
0 & 0 & I_{z z}
\end{array}\right]\left[\begin{array}{c}
p \\
q \\
r
\end{array}\right]\left[\begin{array}{ccc}
I_{x x} & 0 & 0 \\
0 & I_{y y} & 0 \\
0 & 0 & I_{z z}
\end{array}\right]-1\right.} \\
& =\left[\left[\begin{array}{c}
M_{x} \\
0 \\
0
\end{array}\right]-\left[\begin{array}{c}
p \\
q \\
0
\end{array}\right] \times\left[\begin{array}{ccc}
I_{x x} & 0 & 0 \\
0 & I_{y y} & 0 \\
0 & 0 & I_{z z}
\end{array}\right]\left[\begin{array}{c}
p \\
0 \\
0
\end{array}\right]\left[\begin{array}{ccc}
I_{x x} & 0 & 0 \\
0 & I_{y y} & 0 \\
0 & 0 & I_{z z}
\end{array}\right]^{-1}=\left[\begin{array}{c}
\frac{M_{x}}{I_{x x}} \\
0 \\
0
\end{array}\right]\right.
\end{aligned}
$$

For the forces and moments, the block uses lookup tables.

$$
\begin{aligned}
& F_{w z_{a, t}}=f\left(z_{v_{a, t}}-z_{w_{a, t}, z} \dot{v}_{v_{a, t}}-\dot{z}_{w_{a, t}} \delta_{\text {steer }_{a, t}}\right) \\
& M_{v z_{a, t}}=f\left(z_{v_{a, t}}-z_{w_{a, t}} \dot{z}_{v_{a, t}}-\dot{z}_{w_{a, t^{\prime}}} \delta_{\text {steer }_{a, t}}\right)
\end{aligned}
$$

The suspension forces and moments applied to the vehicle are equal to the suspension forces and moments applied to the wheel.

$$
\begin{aligned}
& F_{v x_{a, t}}=F_{w x_{a, t}} \\
& F_{v y_{a, t}}=F_{w y_{a, t}} \\
& F_{v x_{a, t}}=-F_{w z_{a, t}} \\
& M_{v x_{a, t}}=M_{w x_{a, t}}+F_{w y_{a, t}}\left(R e_{w y_{a, t}}+H_{a, t}\right) \\
& M_{v y_{a, t}}=M_{w y_{a, t}}+F_{w x_{a, t}}\left(R e_{w x_{a, t}}+H_{a, t}\right) \\
& M_{v x_{a, t}}=M_{w z_{a, t}}
\end{aligned}
$$

The equations use these variables.

| $F_{w z_{a, t}}, M_{w z_{a, t}}$ | Suspension force and moment applied to the wheel on axle a, wheel t <br> along wheel-fixed $z$-axis |
| :--- | :--- |
| $F_{w x_{a, t}} M_{w x_{a, t}}$ | Suspension force and moment applied to the wheel on axle a, wheel t <br> along wheel-fixed $x$-axis |
| $F_{w y_{a, t}}, M_{w y_{a, t}}$ | Suspension force and moment applied to the wheel on axle a, wheel t <br> along wheel-fixed $y$-axis |
| $F_{v z_{a, t}}, M_{v z_{a, t}}$ | Suspension force and moment applied to the vehicle on axle a, wheel t <br> along wheel-fixed $z$-axis |
| $F_{v x_{a, t}}, M_{v x_{a, t}}$ | Suspension force and moment applied to the vehicle on axle a, wheel t <br> along wheel-fixed $x$-axis |
| $F_{v y_{a, t}}, M_{v y_{a, t}}$ | Suspension force and moment applied to the vehicle on axle a, wheel t <br> along wheel-fixed $y$-axis |
| $F_{z 0_{a}}$ | Vertical suspension spring preload force applied to the wheels on axle a |


| $k_{z_{a}}$ | Vertical spring constant applied to wheels on axle a |
| :---: | :---: |
| $k w a_{z}$ | Wheel and axle interface compliance constant |
| $m_{\text {hsteer }}{ }_{\text {a }}$ | Steering angle to vertical force slope applied at wheel carrier for wheels on axle a |
| $\delta_{\text {steer }_{a, t}}$ | Steering angle input for axle a, wheel t |
| $C_{z_{a}}$ | Vertical damping constant applied to wheels on axle a |
| cwaz | Wheel and axle interface damping constant |
| $R e_{w_{a, t}}$ | Effective wheel radius for axle a, wheel t |
| $F_{z h s t o p_{a, t}}$ | Vertical hardstop force at axle a, wheel t , along the vehicle-fixed $z$-axis |
| $F_{z a s w y_{\text {at }}}$ | Vertical anti-sway force at axle $a$, wheel $t$, along the vehicle-fixed $z$-axis |
| $F w a_{z 0}$ | Wheel and axle interface compliance constant |
| $z_{v_{a, t}} \dot{z}_{v_{a, t}}$ | Vehicle displacement and velocity at axle a, wheel $t$, along the vehiclefixed $z$-axis |
| $z_{w_{a, t}} \dot{z}_{w_{a, t}}$ | Wheel displacement and velocity at axle $a$, wheel $t$, along the vehicle-fixed $z$-axis |
| $\chi_{v_{a, t}} \dot{\chi}_{v_{a, t}}$ | Vehicle displacement and velocity at axle $a$, wheel $t$, along the vehiclefixed $z$-axis |
| $\chi_{w_{a, t}} \dot{x}_{w_{a, t}}$ | Wheel displacement and velocity at axle $a$, wheel $t$, along the vehicle-fixed $z$-axis |
| $y_{v_{a, t}} \dot{y}_{v_{a, t}}$ | Vehicle displacement and velocity at axle $a$, wheel $t$, along the vehiclefixed $y$-axis |
| $y_{w_{a, t}} \dot{y}_{w_{a, t}}$ | Wheel displacement and velocity at axle a, wheel $t$, along the vehicle-fixed $y$-axis |
| $H_{a, t}$ | Suspension height at axle a, wheel t |
| $R e_{w_{a, t}}$ | Effective wheel radius at axle a , wheel t |

## Camber, Caster, and Toe Angles

To calculate the camber, caster, and toe angles, the block uses a lookup table, $G_{\text {alookup }}$, that is a function of the suspension height and steering angle.

$$
\left[\xi_{a, t} \eta_{a, t} \zeta_{a, t}\right]=G_{a l o o k u p} f\left(z_{w_{a, t}}-z_{v_{a, t^{\prime}}} \delta_{\text {steer }_{a, t}}\right)
$$

The equations use these variables.

| $\xi_{a, t}$ | Camber angle of wheel on axle $a$, wheel t |
| :--- | :--- |
| $\eta_{a, t}$ | Caster angle of wheel on axle $a$, wheel t |
| $\zeta_{a, t}$ | Toe angle of wheel on axle a, wheel t |
| $\delta_{\text {steer }}^{a, t}$ |  |
| $z_{v_{a, t}}$ | Steering angle input for axle $a$, wheel t |
| $z_{w_{a, t}}$ | Vehicle displacement at axle $a$, wheel t , along vehicle-fixed $z$-axis |
|  | Wheel displacement at axle $a$, wheel t , along vehicle-fixed $z$-axis |

## Steering Angles

Optionally, you can input steering angles for the wheels. To calculate the steering angles for the wheels, the block offsets the input steering angles as a function of the suspension height. For the
calculation, the block uses a lookup table, $G_{\text {alookup }}$, that is a function of the suspension position and steering angle.

$$
\delta_{\text {whlsteer }_{a, t}}=\delta_{\text {steer }_{a, t}}+G_{\text {alookup }} f\left(z_{w_{a, t}}-z_{v_{a, t}}, \delta_{\text {steer }_{a, t}}\right)
$$

The equation uses these variables.

| $\delta_{\text {whlsteer }_{a, t}}$ | Wheel steering angle for axle a, wheel t |
| :--- | :--- |
| $\delta_{\text {steer }_{a, t}}$ | Steering angle input for axle a, wheel t |
| $z_{\mathrm{v}_{a, t}}$ | Vehicle displacement at axle a, wheel t , along the vehicle-fixed $z$-axis |
| $z_{w_{a, t}}$ | Wheel displacement at axle a, wheel t , along the vehicle-fixed $z$-axis |

## Power and Energy

The block calculates these suspension characteristics for each axle, $a$, wheel, $t$.

| Calculation | Equation |
| :--- | :--- |
| Dissipated power, $P_{\text {susp }_{a, t}}$ | $P_{\text {susp }_{a, t}}=F_{\text {wzlookup }_{a}}\left(\dot{z}_{v_{a, t}}-\dot{z}_{w_{a, t}} \dot{z}_{v_{a, t}}-\dot{z}_{w_{a, t},} \delta_{\text {steer }_{a, t}}\right)$ |
| Absorbed energy, $E_{\text {susp }_{a, t}}$ | $E_{\text {susp }_{a, t}}=F_{w z l o o k u p_{a}}\left(\dot{z}_{v_{a, t}}-\dot{z}_{w_{a, t}} \dot{z}_{v_{a, t}}-\dot{z}_{w_{a, t},} \delta_{s t e e r_{a, t}}\right)$ |
| Suspension height, $H_{a, t}$ | $\left.H_{a, t}=-\left(z_{v_{a, t}}-z_{w_{a, t}}-\operatorname{median(f\_ \text {susp_}} d z_{-} b p\right)\right)$ |
| Distance from wheel carrier <br> center to tire/road interface | $z_{w t r_{a, t}}=\operatorname{Re}_{w_{a, t}}+H_{a, t}$ |

The equations use these variables.
$m_{\text {hsteer }_{a}} \quad$ Steering angle to vertical force slope applied at wheel carrier for wheels on axle a
$\delta_{\text {steer }_{a, t}} \quad$ Steering angle input for axle a, wheel t
$R e_{w_{a, t}} \quad$ Axle a, wheel $t$ effective wheel radius from wheel carrier center to tire/road interface
$f$ _susp_dz_bp Vertical axis suspension height breakpoints
$z_{w t r_{a, t}} \quad$ Distance from wheel carrier center to tire/road interface, along the vehicle-fixed $z$ axis
$z_{v_{a, t}} \dot{v}_{v_{a t t}} \quad$ Vehicle displacement and velocity at axle a, wheel t , along the vehicle-fixed $z$-axis
$z_{w_{a, t}} \dot{z}_{w_{a, t}} \quad$ Wheel displacement and velocity at axle a, wheel t , along the vehicle-fixed $z$-axis

## Ports

Input
WhIPz - Wheel z-axis displacement
array
Wheel displacement, $z_{w}$, along wheel-fixed $z$-axis, in m. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlPz:

- Signal array dimensions are [1x4].

WhlPz $=z_{w}=\left[z_{w_{1,1}} z_{w_{1,2}} z_{w_{2,1}} z_{w_{2,2}}\right]$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlPz $(1,1)$ | 1 | 1 |
| Front right | WhlPz $(1,2)$ | 1 | 2 |
| Rear left | WhlPz $(1,3)$ | 2 | 1 |
| Rear right | WhlPz $(1,4)$ | 2 | 2 |

WhIRe - Wheel effective radius
array
Effective wheel radius, $R e_{w}$, in m. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlRe:

- Signal array dimensions are [1×4].

WhlRe $=R e_{w}=\left[\begin{array}{ll}R e_{w_{1,1}} & R e_{w_{1,2}} R e_{w_{2,1}} R e_{w_{2,2}}\end{array}\right]$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlRe $(1,1)$ | 1 | 1 |
| Front right | WhlRe $(1,2)$ | 1 | 2 |
| Rear left | WhlRe $(1,3)$ | 2 | 1 |
| Rear right | WhlRe $(1,4)$ | 2 | 2 |

WhIVz - Wheel z-axis velocity
array
Wheel velocity, $\dot{z}_{w}$, along wheel-fixed $z$-axis, in m. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlVz:

- Signal array dimensions are [1x4].

WhlVz $=\dot{z}_{w}=\left[\begin{array}{lll}\dot{z}_{1,1} & \dot{z}_{w_{1,2}} & \dot{z}_{w_{2,1}} \\ \dot{z}_{w_{2,2}}\end{array}\right]$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlVz $(1,1)$ | 1 | 1 |
| Front right | WhlVz $(1,2)$ | 1 | 2 |
| Rear left | WhlVz $(1,3)$ | 2 | 1 |
| Rear right | WhlVz $(1,4)$ | 2 | 2 |

WhIFx - Longitudinal wheel force on vehicle
array

Longitudinal wheel force applied to vehicle, $F_{w x}$, along the vehicle-fixed $x$-axis. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlFx:

- Signal array dimensions are [1×4].

$$
\mathrm{WhlFx}=F_{w x}=\left[\begin{array}{ll}
F_{w x_{1,1}} & F_{w x_{1,2}} \\
F_{w x_{2,1}} & F_{w x_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlFx $(1,1)$ | 1 | 1 |
| Front right | WhlFx $(1,2)$ | 1 | 2 |
| Rear left | WhlFx $(1,3)$ | 2 | 1 |
| Rear right | WhlFx $(1,4)$ | 2 | 2 |

WhIFy - Lateral wheel force on vehicle
array
Lateral wheel force applied to vehicle, $F_{w y}$, along the vehicle-fixed $y$-axis. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlFy:

- Signal array dimensions are [1x4].

$$
\text { WhlFy }=F_{w y}=\left[F_{w y_{1,1}} F_{w y_{1,2}} F_{w y_{2,1}} F_{w y_{2,2}}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlFy $(1,1)$ | 1 | 1 |
| Front right | WhlFy $(1,2)$ | 1 | 2 |
| Rear left | WhlFy $(1.3)$ | 2 | 1 |
| Rear right | WhlFy $(1,4)$ | 2 | 2 |

WhIM - Suspension moment on wheel
array
Longitudinal, lateral, and vertical suspension moments at axle a, wheel $t$, applied to the wheel at the axle wheel carrier reference coordinate, in $N \cdot m$. Input array dimensions are 3 by the number of wheels on the vehicle.

- WhlM (1, ...) - Suspension moment applied to the wheel about the vehicle-fixed $x$-axis (longitudinal)
- WhlM ( $2, \ldots$ ) - Suspension moment applied to the wheel about the vehicle-fixed $y$-axis (lateral)
- WhlM ( $3, \ldots$ ) - Suspension moment applied to the wheel about the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the WhlM:

- Signal dimensions are [3×4].
- Signal contains suspension moments applied to four wheels according to their axle and wheel locations.

$$
\text { WhlM }=M_{w}=\left[\begin{array}{llll}
M_{w x_{1,1}} & M_{w x_{1,2}} & M_{w x_{2,1}} & M_{w x_{2,2}} \\
M_{w y_{1,1}} & M_{w y 1,2} & M_{w y 2,1} & M_{w y 2,2} \\
M_{w z_{1,1}} & M_{w z_{1,2}} & M_{w z_{2,1}} & M_{w z 2,2}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Moment Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | WhlM(1,1) | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front <br> right | WhlM(1,2) | 1 | 2 |  |
| Rear <br> left | WhlM(1,3) | 2 | 1 |  |
| Rear <br> right | WhlM(1,4) | 2 | 2 |  |
| Front <br> left | WhlM(2,1) | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front <br> right | WhlM(2,2) | 1 | 2 |  |
| Rear <br> left | WhlM(2,3) | 2 | 1 |  |
| Rear <br> right | WhlM(2,4) | 2 | 2 |  |
| Front <br> left | WhlM(3,1) | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front <br> right | WhlM(3,2) | 1 | 2 |  |
| Rear <br> left | WhlM(3,3) | 2 | 1 |  |
| Rear <br> right | WhlM(3,4) | 2 | 2 |  |

VehP - Vehicle displacement
array
Vehicle displacement from axle a, wheel $t$ along vehicle-fixed coordinate system, in m. Input array dimensions are 3 the number of wheels on the vehicle.

- VehP $(1, \ldots)$ - Vehicle displacement from wheel, $\chi_{v}$, along the vehicle-fixed $x$-axis
- $\operatorname{VehP}(2, \ldots)$ - Vehicle displacement from wheel, $y_{v}$, along the vehicle-fixed $y$-axis
- $\operatorname{VehP}(3, \ldots)-$ Vehicle displacement from wheel, $z_{v}$, along the vehicle-fixed $z$-axis

For example, for a two-axle vehicle with two wheels per axle, the VehP:

- Signal dimensions are [3x4].
- Signal contains four displacements according to their axle and wheel locations.

$$
\text { VehP }=\left[\begin{array}{l}
x_{v} \\
y_{v} \\
z_{v}
\end{array}\right]=\left[\begin{array}{llll}
x_{v_{1,1}} & x_{v_{1,2}} & x_{v_{2,1}} & x_{v_{2,2}} \\
y_{v_{1,1}} & y_{v_{1,2}} & y_{v_{2,1}} & y_{v_{2,2}} \\
z_{v_{1,1}} & z_{v_{1,2}} & z_{v_{2,1}} & z_{v_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel Numbe r | Axis |
| :---: | :---: | :---: | :---: | :---: |
| Front left | $\operatorname{VehP}(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis |
| Front right | $\operatorname{VehP}(1,2)$ | 1 | 2 |  |
| $\begin{array}{\|l} \hline \begin{array}{l} \text { Rear } \\ \text { left } \end{array} \\ \hline \end{array}$ | $\operatorname{VehP}(1,3)$ | 2 | 1 |  |
| Rear right | $\operatorname{VehP}(1,4)$ | 2 | 2 |  |
| Front left | $\operatorname{VehP}(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis |
| Front right | $\operatorname{VehP}(2,2)$ | 1 | 2 |  |
| $\begin{array}{\|l} \text { Rear } \\ \text { left } \end{array}$ | $\operatorname{VehP}(2,3)$ | 2 | 1 |  |
| Rear right | $\operatorname{VehP}(2,4)$ | 2 | 2 |  |
| Front left | $\operatorname{VehP}(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis |
| Front right | $\operatorname{VehP}(3,2)$ | 1 | 2 |  |
| $\begin{array}{\|l} \begin{array}{l} \text { Rear } \\ \text { left } \end{array} \\ \hline \end{array}$ | $\operatorname{VehP}(3,3)$ | 2 | 1 |  |
| Rear right | $\operatorname{VehP}(3,4)$ | 2 | 2 |  |

VehV - Vehicle velocity
array
Vehicle velocity at axle a, wheel t along vehicle-fixed coordinate system, in m . Input array dimensions are 3 by the number of wheels on the vehicle.

- $\operatorname{VehV}(1, \ldots)-$ Vehicle velocity at wheel, $x_{v}$, along the vehicle-fixed $x$-axis
- $\operatorname{VehV}(2, \ldots)$ - Vehicle velocity at wheel, $y_{v}$, along the vehicle-fixed $y$-axis
- $\operatorname{VehV}(3, \ldots)-$ Vehicle velocity at wheel, $z_{v}$, along the vehicle-fixed $z$-axis

For example, for a two-axle vehicle with two wheels per axle, the VehV:

- Signal dimensions are [3×4].
- Signal contains 4 velocities according to their axle and wheel locations.

$$
\mathrm{VehV}=\left[\begin{array}{c}
\dot{x}_{v} \\
\dot{y}_{v} \\
\dot{z}_{v}
\end{array}\right]=\left[\begin{array}{llll}
\dot{x}_{v_{1,1}} & \dot{x}_{v_{1,2}} & \dot{x}_{v_{2,1}} & \dot{x}_{v_{2,2}} \\
\dot{y}_{v_{1,1}} & \dot{y}_{v_{1,2}} & \dot{y}_{v_{2,1}} & \dot{y}_{v_{2,2}} \\
\dot{z}_{v_{1,1}} & \dot{z}_{v_{1,2}} & \dot{z}_{v_{2,1}} & \dot{z}_{v_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel Numbe r | Axis |
| :---: | :---: | :---: | :---: | :---: |
| Front left | $\operatorname{VehV}(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis |
| Front right | $\operatorname{VehV}(1,2)$ | 1 | 2 |  |
| Rear left | $\operatorname{VehV}(1,3)$ | 2 | 1 |  |
| Rear right | $\operatorname{VehV}(1,4)$ | 2 | 2 |  |
| Front left | $\operatorname{VehV}(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis |
| Front right | $\operatorname{VehV}(2,2)$ | 1 | 2 |  |
| Rear left | $\operatorname{VehV}(2,3)$ | 2 | 1 |  |
| Rear right | $\operatorname{VehV}(2,4)$ | 2 | 2 |  |
| Front left | $\operatorname{VehV}(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis |
| Front right | $\operatorname{VehV}(3,2)$ | 1 | 2 |  |
| Rear left | $\operatorname{VehV}(3,3)$ | 2 | 1 |  |
| Rear right | $\operatorname{VehV}(3,4)$ | 2 | 2 |  |

StrgAng - Steering angle, optional
array
Optional steering angle for each wheel, $\delta$. Input array dimensions are 1 by the number of steered wheels.

For example, for a two-axle vehicle with two wheels per axle, you can input steering angles for both wheels on the first axle.

- To create the StrgAng port, set Steered axle enable by axle, StrgEnByAxl to [1 0]. The input signal array dimensions are [1x2].
- The StrgAng signal contains two steering angles according to their axle and wheel locations.

$$
\text { StrgAng }=\delta_{\text {steer }}=\left[\delta_{\text {steer }_{1,1}} \delta_{\text {steer }_{1,2}}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | StrgAng (1, 1) | 1 | 1 |
| Front right | StrgAng (1,2) | 1 | 2 |

## Dependencies

To create input port StrgAng, set an element of the Steered axle enable by axle, StrgEnByAxl vector to 1 .

## Output

Info - Bus signal
bus
Bus signal containing block values. The signals are arrays that depend on the wheel location.
For example, here are the indices for a two-axle, two-wheel vehicle. The total number of wheels is four.

- 1D array signal (1-by-4)

| Array Element | Axle | Wheel Number |
| :--- | :--- | :--- |
| $(1,1)$ | 1 | 1 |
| $(1,2)$ | 1 | 2 |
| $(1,3)$ | 2 | 1 |
| $(1,4)$ | 2 | 2 |

- 3D array signal (3-by-4)

| Array Element | Axle | Wheel Number |
| :--- | :--- | :--- |
| $(1,1)$ | 1 | 1 |
| $(1,2)$ | 1 | 2 |
| $(1,3)$ | 2 | 1 |
| $(1,4)$ | 2 | 2 |
| $(2,1)$ | 1 | 1 |
| $(2,2)$ | 1 | 2 |
| $(2,3)$ | 2 | 1 |
| $(2,4)$ | 2 | 2 |
| $(3,1)$ | 1 | 1 |
| $(3,2)$ | 1 | 2 |
| $(3,3)$ | 2 | 1 |
| $(3,4)$ | 2 | 2 |


| Signal | Description | Array Signal | Variable | Units |
| :--- | :--- | :--- | :--- | :--- |
| Camber | Wheel angles according <br> to the axle. | 1 D | WhlAng $[1, \ldots]=\xi=\left[\xi_{a, t}\right]$ | rad |
|  |  |  |  |  |


| Signal | Description | Array Signal | Variable | Units |
| :---: | :---: | :---: | :---: | :---: |
| Caster |  |  | WhlAng $[2, \ldots]=\eta=\left[\eta_{a, t}\right]$ |  |
| Toe |  |  | WhlAng $[3, \ldots]=\zeta=\left[\zeta_{a, t}\right]$ |  |
| Height | Suspension height | 1D | H | m |
| Power | Suspension power dissipation | 1D | $P_{\text {susp }}$ | W |
| Energy | Suspension absorbed energy | 1D | $E_{\text {susp }} \mathrm{J}$ | J |
| VehF | Suspension forces applied to the vehicle | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { VehF }=F_{v}= \\ & {\left[\begin{array}{llll} F_{v x_{1,1}} & F_{v x_{1,2}} & F_{v x_{2,1}} & F_{v x_{2}, 2} \\ F_{v v_{1,1}} & F_{v v_{1,2}} & F_{v y 2,1} & F_{v y 2,2} \\ F_{v z_{1,1}} & F_{v z_{1,2}} & F_{v z_{2,1}} & F_{v z_{2,2}} \end{array}\right.} \end{aligned}$ |  |
| VehM | Suspension moments applied to vehicle | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { VehM }=M_{v}= \\ & {\left[\begin{array}{lllll} M_{v x_{1}, 1} & M_{v x_{1}, 2} & M_{v \chi_{2,1}} & M_{v \times 2} \\ M_{v y_{1}, 1} & M_{v y_{1}, 2} & M_{v y{ }_{2}, 1} & M_{v y 2} \\ M_{v z_{1}, 1} & M_{v z_{1,2}} & M_{v z_{2,1}} & M_{v z_{2}} \end{array}\right.} \end{aligned}$ | $\mathrm{N} \cdot \mathrm{m}$ <br> 2,2 <br> 2,2 <br> 2,2 |


| Signal | Description | Array Signal | Variable | Units |
| :---: | :---: | :---: | :---: | :---: |
| WhlF | Suspension force applied to wheel | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { WhlF }=F_{w}= \\ & {\left[\begin{array}{llll} F_{w x_{1}, 1} & F_{w x_{1,2}} & F_{w x_{2}, 1} & F_{w x_{2}} \\ F_{w y 1,1} & F_{w y_{1,2}} & F_{w y 2,1} & F_{w y_{2}} \\ F_{w z_{1,1}} & F_{w z_{1,2}} & F_{w z_{2,1}} & F_{w z_{2}} \end{array}\right.} \end{aligned}$ |  |
| WhlP | Wheel displacement | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { WhlP }=\left[\begin{array}{l} x_{w} \\ y_{w} \\ z_{w} \end{array}\right]= \\ & {\left[\begin{array}{llll} x_{w_{1,1}} & x_{w_{1,2}} & x_{w_{2,1}} & x_{w_{2}} \\ y_{w_{1,1}} & y_{w_{1,2}} & y_{w_{2,1}} & y_{w y_{2}} \\ z_{w t r_{1,1}} & z_{w t r_{1,2}} & z_{w t r_{2,1}} & z_{w t{ }_{2}} \end{array}\right.} \end{aligned}$ |  |
| Whlv | Wheel velocity | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { WhlV }=\left[\begin{array}{l} \dot{x}_{w} \\ \dot{y}_{w} \\ \dot{z}_{w} \end{array}\right] \\ & = \\ & {\left[\begin{array}{llll} \dot{x}_{w_{1,1}} & \dot{x}_{w_{1,2}} & \dot{x}_{w_{2,1}} & \dot{x}_{w_{2,2}} \\ \dot{y}_{w_{1,1}} & \dot{y}_{w_{1,2}} & \dot{y}_{w_{2,1}} & \dot{y}_{w_{2,2}} \\ \dot{z}_{w_{1,1}} & \dot{z}_{w_{1,2}} & \dot{z}_{w_{2,1}} & \dot{z}_{w_{2,2}} \end{array}\right]} \end{aligned}$ | m/s |


| Signal | Description | Array Signal | Variable | Units |
| :---: | :---: | :---: | :---: | :---: |
| WhlAng | Wheel camber, caster, toe angles | 3D | For a two-axle, two wheels per axle vehicle: | rad |

VehF - Suspension force on vehicle
array
Longitudinal, lateral, and vertical suspension force at axle a, wheel $t$, applied to the vehicle at the suspension connection point, in N. Array dimensions are 3 by the number of wheels on the vehicle.

- $\operatorname{VehF}(1, \ldots)$ - Suspension force applied to vehicle along the vehicle-fixed $x$-axis (longitudinal)
- $\operatorname{VehF}(2, \ldots)$ - Suspension force applied to vehicle along the vehicle-fixed $y$-axis (lateral)
- $\operatorname{VehF}(3, \ldots)$ - Suspension force applied to vehicle along the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the VehF:

- Signal dimensions are [3×4].
- Signal contains suspension forces applied to the vehicle according to the axle and wheel locations.

VehF $=F_{v}=\left[\begin{array}{llll}F_{v x_{1,1}} & F_{v x_{1,2}} & F_{v x_{2,1}} & F_{v x_{2,2}} \\ F_{v v_{1,1}} & F_{v y_{1,2}} & F_{v y_{2,1}} & F_{v y_{2,2}} \\ F_{v z_{1,1}} & F_{v z_{1,2}} & F_{v z_{2,1}} & F_{v z_{2,2}}\end{array}\right]$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | $\operatorname{VehF}(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front <br> right | $\operatorname{VehF}(1,2)$ | 1 | 2 |  |
| Rear <br> left | $\operatorname{VehF}(1,3)$ | 2 | 1 |  |
| Rear <br> right | $\operatorname{VehF}(1,4)$ | 2 | 2 |  |
| Front <br> left | $\operatorname{VehF}(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front <br> right | $\operatorname{VehF}(2,2)$ | 1 | 2 |  |


| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Rear <br> left | VehF $(2,3)$ | 2 | 1 |  |
| Rear <br> right | VehF $(2,4)$ | 2 | 2 |  |
| Front <br> left | $\operatorname{VehF}(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front <br> right | $\operatorname{VehF}(3,2)$ | 1 | 2 |  |
| Rear <br> left | $\operatorname{VehF}(3,3)$ | 2 | 1 |  |
| Rear <br> right | $\operatorname{VehF}(3,4)$ | 2 | 2 |  |

VehM - Suspension moment on vehicle array

Longitudinal, lateral, and vertical suspension moment at axle a, wheel $t$, applied to the vehicle at the suspension connection point, in $\mathrm{N} \cdot \mathrm{m}$. Array dimensions are 3 by the number of wheels on the vehicle.

- VehM(1, ...) - Suspension moment applied to the vehicle about the vehicle-fixed $x$-axis (longitudinal)
- VehM ( $2, \ldots$ ) - Suspension moment applied to the vehicle about the vehicle-fixed $y$-axis (lateral)
- Vehm ( $3, \ldots$ ) - Suspension moment applied to the vehicle about the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the VehM:

- Signal dimensions are [3×4].
- Signal contains suspension moments applied to vehicle according to the axle and wheel locations.

VehM $=M_{v}=\left[\begin{array}{llll}M_{v x_{1,1}} & M_{v x_{1,2}} & M_{v x_{2,1}} & M_{v x_{2,2}} \\ M_{v y 1,1} & M_{v y_{1,2}} & M_{v y_{2,1}} & M_{v y_{2,2}} \\ M_{v z_{1,1}} & M_{v z_{1,2}} & M_{v z_{2,1}} & M_{v z_{2,2}}\end{array}\right]$

| Array Element | Axle | Wheel <br> Number | Moment Axis |
| :--- | :--- | :--- | :--- |
| $\operatorname{VehM}(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| $\operatorname{VehM}(1,2)$ | 1 | 2 |  |
| $\operatorname{VehM}(1,3)$ | 2 | 1 |  |
| $\operatorname{VehM}(1,4)$ | 2 | 2 |  |
| $\operatorname{VehM}(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| $\operatorname{VehM}(2,2)$ | 1 | 2 |  |


| Array Element | Axle | Wheel <br> Number | Moment Axis |
| :--- | :--- | :--- | :--- |
| $\operatorname{VehM}(2,3)$ | 2 | 1 |  |
| $\operatorname{VehM}(2,4)$ | 2 | 2 |  |
| $\operatorname{VehM}(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| $\operatorname{VehM}(3,2)$ | 1 | 2 |  |
| $\operatorname{VehM}(3,3)$ | 2 | 1 |  |
| $\operatorname{VehM}(3,4)$ | 2 | 2 |  |

WhIF - Suspension force on wheel
array
Longitudinal, lateral, and vertical suspension forces at axle a, wheel $t$, applied to the wheel at the axle wheel carrier reference coordinate, in N. Array dimensions are 3 by the number of wheels on the vehicle.

- $\operatorname{WhlF}(1, \ldots)-$ Suspension force on wheel along the vehicle-fixed $x$-axis (longitudinal)
- $\operatorname{WhlF}(2, \ldots)$ - Suspension force on wheel along the vehicle-fixed $y$-axis (lateral)
- WhlF $(3, \ldots)$ - Suspension force on wheel along the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the WhlF:

- Signal dimensions are [3×4].
- Signal contains wheel forces applied to the vehicle according to the axle and wheel locations.

WhlF $=F_{w}=\left[\begin{array}{llll}F_{w x_{1,1}} & F_{w x_{1,2}} & F_{w x_{2,1}} & F_{w x_{2,2}} \\ F_{w y_{1,1}} & F_{w y_{1,2}} & F_{w y_{2,1}} & F_{w y_{2,2}} \\ F_{w z_{1,1}} & F_{w z_{1,2}} & F_{w z_{2,1}} & F_{w z_{2,2}}\end{array}\right]$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | WhlF $(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front <br> right | WhlF $(1,2)$ | 1 | 2 |  |
| Rear <br> left | WhlF $(1,3)$ | 2 | 1 |  |
| Rear <br> right | WhlF $(1,4)$ | 2 | 2 |  |
| Front <br> left | WhlF $(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front <br> right | WhlF $(2,2)$ | 1 | 2 |  |


| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Rear <br> left | WhlF $(2,3)$ | 2 | 1 |  |
| Rear <br> right | WhlF $(2,4)$ | 2 | 2 |  |
| Front <br> left | WhlF $(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front <br> right | WhlF(3,2) | 1 | 2 |  |
| Rear <br> left | WhlF $(3,3)$ | 2 | 1 |  |
| Rear <br> right | WhlF(3,4) | 2 | 2 |  |

WhIV - Wheel velocity
array
Longitudinal, lateral, and vertical wheel velocity at axle a, wheel t , in $\mathrm{m} / \mathrm{s}$. Array dimensions are 3 by the number of wheels on the vehicle.

- WhlV (1, ...) - Wheel velocity along the vehicle-fixed $x$-axis (longitudinal)
- WhlV $(2, \ldots)$ - Wheel velocity along the vehicle-fixed $y$-axis (lateral)
- WhlV $(3, \ldots)-$ Wheel velocity along the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the Whlv:

- Signal dimensions are [3×4].
- Signal contains wheel forces applied to the vehicle according to the axle and wheel locations.

$$
\text { WhlV }=\left[\begin{array}{c}
\dot{x}_{w} \\
\dot{y}_{w} \\
\dot{z}_{w}
\end{array}\right]=\left[\begin{array}{llll}
\dot{x}_{w_{1,1}} & \dot{x}_{w_{1,2}} & \dot{x}_{w_{2,1}} & \dot{x}_{w_{2,2}} \\
\dot{y}_{w_{1,1}} & \dot{y}_{w_{1,2}} & \dot{y}_{w_{2,1}} & \dot{y}_{w_{2,2}} \\
\dot{z}_{w_{1,1}} & \dot{z}_{w_{1,2}} & \dot{z}_{w_{2,1}} & \dot{z}_{w_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | WhlV $(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front <br> right | WhlV $(1,2)$ | 1 | 2 |  |
| Rear <br> left | WhlV $(1,3)$ | 2 | 1 |  |
| Rear <br> right | WhlV $(1,4)$ | 2 | 2 |  |


| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | WhlV $(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front <br> right | WhlV $(2,2)$ | 1 | 2 |  |
| Rear <br> left | WhlV $(2,3)$ | 2 | 1 |  |
| Rear <br> right | WhlV $(2,4)$ | 2 | 2 |  |
| Front <br> left | WhlV $(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front <br> right | WhlV $(3,2)$ | 1 | 2 |  |
| Rear <br> left | WhlV(3,3) | 2 | 1 |  |
| Rear <br> right | WhlV(3,4) | 2 | 2 |  |

WhIAng - Wheel camber, caster, toe angles
array
Camber, caster, and toe angles at axle $a$, wheel $t$, in rad. Array dimensions are 3 by the number of wheels on the vehicle.

- WhlAng(1,...) - Camber angle
- WhlAng (2,...) - Caster angle
- Whlang $(3, \ldots)$ - Toe angle

For example, for a two-axle vehicle with two wheels per axle, the WhlAng:

- Signal dimensions are [3×4].
- Signal contains angles according to the axle and wheel locations.

$$
\text { WhlAng }=\left[\begin{array}{l}
\xi \\
\eta \\
\zeta
\end{array}\right]=\left[\begin{array}{llll}
\xi_{1,1} & \xi_{1,2} & \xi_{2,1} & \xi_{2,2} \\
\eta_{1,1} & \eta_{1,2} & \eta_{2,1} & \eta_{2,2} \\
\zeta_{1,1} & \zeta_{1,2} & \zeta_{2,1} & \zeta_{2,2}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Angle |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | WhlAng (1,1) | 1 | 1 | Camber |
| Front <br> right | WhlAng (1,2) | 1 | 2 |  |


| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Angle |
| :--- | :--- | :--- | :--- | :--- |
| Rear <br> left | WhlAng (1,3) | 2 | 1 |  |
| Rear <br> right | WhlAng (1,4) | 2 | 2 |  |
| Front <br> left | WhlAng (2,1) | 1 | 1 | Caster |
| Front <br> right | WhlAng (2,2) | 1 | 2 |  |
| Rear <br> left | WhlAng (2,3) | 2 | 1 |  |
| Rear <br> right | WhlAng(2,4) | 2 | 2 |  |
| Front <br> left | WhlAng (3,1) | 1 | 1 | Toe |
| Front <br> right | WhlF(3,2) | 1 | 2 |  |
| Rear <br> left | WhlF(3,3) | 2 | 1 |  |
| Rear <br> right | WhlF(3,4) | 2 | 2 |  |

## Parameters

## Axles

## Number of axles, NumAxI - Number of axles

2 (default) | scalar
Number of axles, $N_{a}$, dimensionless.
Number of wheels by axle, NumWhlsByAxI - Number of wheels per axle
[2 2] (default)|vector
Number of wheels per axle, $N t_{a}$, dimensionless. Vector is 1 by the number of vehicle axles, $N_{a}$. For example, [1,2] represents one wheel on axle one and two wheels on axle two.

Steered axle enable by axle, StrgEnByAxI - Boolean vector to enable axle steering
[1 0] (default) |vector
Boolean vector that enables axle steering, $E n_{\text {steer }}$, dimensionless. Vector is 1 by the number of vehicle axles, $N_{a}$. For example:

- [llll-For a two-axle vehicle, enables axle one steering and disables axle two steering
- [1 1]-For a two-axle vehicle, enables axle one and axle two steering


## Dependencies

Setting an element of the Steered axle enable by axle, StrgEnByAxl vector to 1:

- Creates input port StrgAng.
- Creates these parameters
- Toe angle vs steering angle slope, ToeStrgSlp
- Caster angle vs steering angle slope, CasterStrgSlp
- Camber angle vs steering angle slope, CamberStrgSlp
- Suspension height vs steering angle slope, StrgHgtSlp

For example, for a two-axle vehicle with two wheels per axle, you can input steering angles for both wheels on the first axle.

- To create the StrgAng port, set Steered axle enable by axle, StrgEnByAxl to [1 0]. The input signal array dimensions are [1x2].
- The StrgAng signal contains two steering angles according to their axle and wheel locations.

$$
\text { StrgAng }=\delta_{\text {steer }}=\left[\delta_{\text {steer }_{1,1}} \delta_{\text {steer }_{1}, 2}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | StrgAng (1, 1) | 1 | 1 |
| Front right | StrgAng (1,2) | 1 | 2 |

Axle and wheels lumped principal moments of inertia about longitudinal axis, AxIIxx Inertia
300 (default) | vector
Axle and wheels lumped principal moments of inertia about longitudinal axis, AxleIxx $a$, in $\mathrm{kg}^{*} \mathrm{~m} \wedge 2$.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Axle and wheels lumped mass, AxIM - Mass

[2 2] (default)|vector
Axle and wheels lumped mass, $a$, in kg.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

Track hardpoint coordinates relative to axle center, TrackCoords - Point
[0 0 0 0;-1 1 -1 1;0 0 0 0] (default)|array
Track hardpoint coordinates, $T c_{t}$, along the solid axle $x, y$, and $z$-axes, in m .
For example, for a two-axle vehicle with two wheels per axle, the TrackCoords array:

- Dimensions are [3x4].
- Contains four track hardpoint coordinates according to their axle and wheel locations.

$$
T c_{t}=\left[\begin{array}{llll}
x_{w_{1,1}} & x_{w_{1,2}} & x_{w_{2,1}} & x_{w_{2,2}} \\
y_{w_{1,1}} & y_{w_{1,2}} & y_{w_{2,1}} & y_{w_{2,2}} \\
z_{w_{1,1}} & z_{w_{1,2}} & z_{w_{2,1}} & z_{w_{2,2}}
\end{array}\right]
$$

| Array Element | Axle | Wheel Number | Axis |
| :---: | :---: | :---: | :---: |
| TrackCoords(1, 1) | 1 | 1 | Solid axle $x$-axis |
| TrackCoords(1, 2) | 1 | 2 |  |
| ```TrackCoords(1, 3)``` | 2 | 1 |  |
| TrackCoords(1, 4) | 2 | 2 |  |
| TrackCoords(2, 1) | 1 | 1 | Solid axle $y$-axis |
| TrackCoords(2, 2) | 1 | 2 |  |
| TrackCoords(2, 3) | 2 | 1 |  |
| TrackCoords(2, 4) | 2 | 2 |  |
| TrackCoords(3, 1) | 1 | 1 | Solid axle $z$-axis |
| TrackCoords(3, 2) | 1 | 2 |  |
| TrackCoords(3, 3) | 2 | 1 |  |
| TrackCoords(3, <br> 4) | 2 | 2 |  |

## Suspension hardpoint coordinates relative to axle center, SuspCoords - Point

## [0 0 0 0;-1 1-1 1;0 0 0 0] (default)|array

Suspension hardpoint coordinates, $S c_{t}$, along the solid axle $x$-, $y$-, and $z$-axes, in m .
For example, for a two-axle vehicle with two wheels per axle, the SuspCoords array:

- Dimensions are [3×4].
- Contains four track hardpoint coordinates according to their axle and track locations.

$$
S_{c_{t}}=\left[\begin{array}{llll}
x_{s_{1,1}} & x_{s_{1,2}} & x_{s_{2,1}} & x_{s_{2,2}} \\
y_{s_{1,1}} & y_{s_{1,2}} & y_{s_{2,1}} & y_{s_{2,2}} \\
z_{s_{1,1}} & z_{s_{1,2}} & z_{s_{2,1}} & z_{s_{2,2}}
\end{array}\right]
$$

| Array Element | Axle | Track | Axis |
| :---: | :---: | :---: | :---: |
| SuspCoords (1,1 ) | 1 | 1 | Solid axle $x$-axis |
| $\begin{aligned} & \text { SuspCoords(1,2 } \\ & \text { ) } \end{aligned}$ | 1 | 2 |  |
| $\begin{aligned} & \begin{array}{l} \text { SuspCoords (1,3 } \\ \text { ) } \end{array} \\ & \hline \end{aligned}$ | 2 | 1 |  |
| $\begin{aligned} & \begin{array}{l} \text { SuspCoords (1,4 } \\ \text { ) } \end{array} \\ & \hline \end{aligned}$ | 2 | 2 |  |
| SuspCoords(2,1 ) | 1 | 1 | Solid axle $y$-axis |
| $\begin{aligned} & \text { SuspCoords(2,2 } \\ & \text { ) } \end{aligned}$ | 1 | 2 |  |
| SuspCoords(2,3 ) | 2 | 1 |  |
| $\begin{array}{\|l} \hline \begin{array}{l} \text { SuspCoords }(2,4 \\ ) \end{array} \\ \hline \end{array}$ | 2 | 2 |  |
| SuspCoords (3,1 ) | 1 | 1 | Solid axle $z$-axis |
| SuspCoords(3,2 ) | 1 | 2 |  |
| $\begin{aligned} & \begin{array}{l} \text { SuspCoords (3,3 } \\ \text { ) } \end{array} \\ & \hline \end{aligned}$ | 2 | 1 |  |
| $\begin{array}{\|l} \hline \begin{array}{l} \text { SuspCoords }(3,4 \\ ) \end{array} \\ \hline \end{array}$ | 2 | 2 |  |

Wheel and axle interface compliance constant, KzWhIAxI - Spring rate 6437000 (default) | scalar

Wheel and axle interface compliance constant, $k w a_{z}$, in $\mathrm{N} / \mathrm{m}$.
Wheel and axle interface compliance preload, FOzWhIAxI - Spring rate 9810 (default) | scalar

Wheel and axle interface compliance preload, $F w a_{z 0}$, in N .

## Wheel and axle interface damping constant, CzWhIAxI - Damping

10000 (default) | scalar
Wheel and axle interface damping constant, $c w a_{z}$, in $m$.

## Suspension

## Mapped

Axle breakpoints, f_susp_axl_bp - Breakpoints
[1 2] (default)| 1-by-P array
Axle breakpoints, dimensionless.

## Vertical axis suspension height breakpoints, f_susp_dz_bp - Breakpoints

1-by-M array
Vertical axis suspension height breakpoints, in $m$.

## Vertical axis suspension height velocity breakpoints, f_susp_dzdot_bp - Breakpoints

 1-by-N arrayVertical axis suspension height velocity breakpoints, in $\mathrm{m} / \mathrm{s}$.

## Vertical axis suspension force and moment responses, f_susp_fmz - Output array

 zeros (31, 31, 61, 2, 4) (default) | M-by-N-by-0-by-P-by-4 arrayArray of output values as a function of:

- Vertical suspension height, $M$
- Vertical suspension height velocity, $N$
- Steering angle, $O$
- Axle, $P$
- 4 output types
- 1 - Vertical force, in N
- 2 - User-defined
- 3 - Stored energy, in J
- 4-Absorbed power, in W

The array dimensions must match the breakpoint dimensions
Suspension geometry responses, f_susp_geom - Suspension geometry responses zeros (31, 61, 2, 3) (default) | M-by-0-by-P-by-3 array

Array of geometric suspension values as a function of:

- Vertical suspension height, M
- Steering angle, $O$
- Axle, $P$
- 3 output types
- 1 - Camber angle, in rad
- 2 - Caster angle, in rad
- 3-Toe angle, in rad

The array dimensions must match the breakpoint dimensions
Steering angle breakpoints, f_susp_strgdelta_bp - Steering angle breakpoints
1-by-0 array
Steering angle breakpoints, in rad.

## Version History

Introduced in R2018a
R2022b: Parameter name change from NumTracksByAxl to NumWhlsByAxl
Behavior changed in R2022b
The Number of tracks by axle, NumTracksByAxl parameter is renamed to Number of wheels by axle, NumWhlsByAxl.

The block uses the number of wheels per axle to index the input and output block signals.

## References

[1] Gillespie, Thomas. Fundamentals of Vehicle Dynamics. Warrendale, PA: Society of Automotive Engineers, 1992.
[2] Vehicle Dynamics Standards Committee. Vehicle Dynamics Terminology. SAE J670. Warrendale, PA: Society of Automotive Engineers, 2008.
[3] Technical Committee. Road vehicles - Vehicle dynamics and road-holding ability - Vocabulary. ISO 8855:2011. Geneva, Switzerland: International Organization for Standardization, 2011.

## Extended Capabilities

C/C++ Code Generation
Generate C and C++ code using Simulink $\circledR_{\circledR}$ Coder ${ }^{\mathrm{TM}}$.

## See Also

Solid Axle Suspension | Solid Axle Suspension - Coil Spring | Solid Axle Suspension - Leaf Spring

## Solid Axle Suspension

Solid axle suspension for multiple axles


## Libraries:

Vehicle Dynamics Blockset / Suspension

## Description

The Solid Axle Suspension block implements a solid axle suspension for multiple axles with multiple wheels per axle.

The block models the suspension compliance, damping, and geometric effects as functions of the wheel positions and velocities, with axle-specific compliance and damping parameters. Using the wheel position and velocity, the block calculates the vertical wheel position and suspension forces on the vehicle and wheel. The block uses the Z-down (defined in SAE J670) and a solid axle coordinate system. The solid axle coordinate system, shown here, is aligned with the Z-down vehicle coordinate system, with the $x$-axis in the direction of forward vehicle motion.


| For Each | You Can Specify |
| :--- | :--- |
| Axle | • Multiple wheels <br> $\quad$ Suspension parameters |
| Wheel | • Steering angles |

The block contains energy-storing spring elements and energy-dissipating damper elements. The block also stores energy via the axle roll angular acceleration and axle center of mass vertical and lateral acceleration.

This table summarizes the block parameter settings for a vehicle with:

- Two axles
- Two wheels per axle
- Steering angle input for both wheels on the front axle

| Parameter | Setting |
| :--- | :--- |
| Number of axles, NumAxl | 2 |
| Number of wheels by axle, NumWhlsByAxl | $\left[\begin{array}{ll}2 & 2\end{array}\right]$ |
| Steered axle enable by axle, StrgEnByAxl | $\left[\begin{array}{ll}1 & 0\end{array}\right]$ |

The block uses the wheel number, $t$, to index the input and output signals. This table summarizes the wheel, axle, and corresponding wheel number for a vehicle with:

- Two axles
- Two wheels per axle

| Wheel | Axle | Wheel Number |
| :--- | :--- | :--- |
| Front left | Front | 1 |
| Front right | Front | 2 |
| Rear left | Rear | 1 |
| Rear right | Rear | 2 |

## Suspension Compliance and Damping

The block uses a linear spring and damper to model the vertical dynamic effects of the suspension system on the vehicle and wheel. Specifically, the block:

| Uses | To Calculate |
| :--- | :--- |
| -Longitudinal and lateral displacement and <br> velocity of the vehicle. | -Suspension forces applied to the axle center. <br> - <br> Lortical displacements and velocities of the <br> velocity of the wheel. <br> - Vertical wheel forces applied to the vehicle. |
|  | -vehicle and wheel. <br> Longitudinal, lateral and vertical suspension <br> forces and moments applied to the vehicle. <br> Longitudinal, lateral and vertical suspension <br> forces and moments applied to the wheel. |

To calculate the dynamics of the axle, the block implements these equations. The block neglects the effects of:

- Lateral and longitudinal translational velocity.
- Angular velocity about the vertical and lateral axes.

$$
\begin{aligned}
& {\left[\begin{array}{l}
\ddot{x}_{a} \\
\ddot{y}_{a} \\
\ddot{z}_{a}
\end{array}\right]=\frac{1}{M_{a}}\left[\begin{array}{l}
F_{x a} \\
F_{y a} \\
F_{z a}
\end{array}\right]+\left[\begin{array}{l}
\dot{x}_{a} \\
\dot{y}_{a} \\
\dot{z}_{a}
\end{array}\right] \times\left[\begin{array}{l}
p \\
q \\
r
\end{array}\right]=\frac{1}{M_{a}}\left[\begin{array}{c}
0 \\
0 \\
F_{z a}
\end{array}\right]+\left[\begin{array}{c}
0 \\
0 \\
\dot{z}_{a}
\end{array}\right] \times\left[\begin{array}{l}
p \\
0 \\
0
\end{array}\right]+\left[\begin{array}{l}
0 \\
0 \\
g
\end{array}\right]=\left[\begin{array}{c}
0 \\
p \dot{z}_{a} \\
\frac{F_{z a}}{M_{a}}+g
\end{array}\right]} \\
& {\left[\begin{array}{l}
\dot{p} \\
\dot{q} \\
\dot{r}
\end{array}\right]=\left[\left[\begin{array}{l}
M_{x} \\
M_{y} \\
M_{z}
\end{array}\right]-\left[\begin{array}{l}
p \\
q \\
r
\end{array}\right] \times\left[\begin{array}{ccc}
I_{x x} & 0 & 0 \\
0 & I_{y y} & 0 \\
0 & 0 & I_{z z}
\end{array}\right]\left[\begin{array}{c}
p \\
q \\
r
\end{array}\right]\left[\begin{array}{ccc}
I_{x x} & 0 & 0 \\
0 & I_{y y} & 0 \\
0 & 0 & I_{z z}
\end{array}\right]-1\right.} \\
& =\left[\left[\begin{array}{c}
M_{x} \\
0 \\
0
\end{array}\right]-\left[\begin{array}{l}
p \\
q \\
0
\end{array}\right] \times\left[\begin{array}{ccc}
I_{x x} & 0 & 0 \\
0 & I_{y y} & 0 \\
0 & 0 & I_{z z}
\end{array}\right]\left[\begin{array}{c}
p \\
0 \\
0
\end{array}\right]\left[\begin{array}{ccc}
I_{x x} & 0 & 0 \\
0 & I_{y y} & 0 \\
0 & 0 & I_{z z}
\end{array}\right]^{-1}=\left[\begin{array}{c}
\frac{M_{x}}{I_{x x}} \\
0 \\
0
\end{array}\right]\right.
\end{aligned}
$$

The net vertical force on the axle center of mass is the sum of the wheel and suspension forces acting on the axle.

$$
F_{z a}=\sum_{t=1}^{N t a}\left(F_{w z_{a, t}}+F_{z 0_{a}}+k_{z_{a}}\left(z_{v_{a, t}}-z_{s_{a, t}}+m_{h s t e e r_{a}}\left|\delta_{s t e e r_{a, t}}\right|\right)+c_{z_{a}}\left(\dot{z}_{v_{a, t}}-\dot{z}_{s_{a, t}}\right)\right)
$$

The net moment about the roll axis of the solid axle suspension accounts for the hardpoint coordinates of the suspension and wheels.

$$
\begin{aligned}
& M_{x}=\sum_{t=1}^{N t a}\left(F_{w z_{a, t}} y_{w_{t}}+\left(F_{z 0_{a}}+k_{z_{a}}\left(z_{v_{a, t}}-z_{s_{a, t}}+m_{\text {hsteera }} \mid \delta_{\text {steer }}^{a, t}\right.\right.\right. \\
& \\
& \left.\left.+M_{w x_{a, t}} \frac{I_{x x}}{I_{x x}+M_{a} y_{w_{t}}}\right)+c_{z_{a}}\left(\dot{z}_{v_{a, t}}-\dot{z}_{s_{a, t}}\right)\right) y_{s_{t}}
\end{aligned}
$$

Block parameters provide the track and suspension hardpoints coordinates.

$$
\begin{gathered}
T c_{t}=\left[\begin{array}{lll}
x_{w_{1}} & x_{w_{2}} & \cdots \\
y_{w_{1}} & y_{w_{2}} & \cdots \\
z_{w_{1}} & z_{w_{2}} & \cdots
\end{array}\right] \\
S c_{t}=\left[\begin{array}{lll}
x_{s_{1}} & x_{s_{2}} & \cdots \\
y_{s_{1}} & y_{s_{2}} & \cdots \\
z_{s_{1}} & z_{s_{2}} & \cdots
\end{array}\right]
\end{gathered}
$$

The block uses Euler angles to transform the track and suspension displacements, velocities, and accelerations to the vehicle coordinate system.

To calculate the suspension forces applied to the vehicle, the block implements this equation.

$$
F_{v z_{a, t}}=-\left(F_{z 0_{a}}+k_{z_{a}}\left(z_{v_{a, t}}-z_{s_{a, t}}+m_{h s t e e r_{a}}\left|\delta_{\text {steer }_{a, t}}\right|\right)+c_{z_{a}}\left(\dot{z}_{v_{a, t}}-\dot{z}_{s_{a, t}}\right)+F_{z h s t o p_{a, t}}\right)
$$

The suspension forces and moments applied to the vehicle are equal to the suspension forces and moments applied to the wheel.

$$
\begin{aligned}
& F_{v x_{a, t}}=F_{w x_{a, t}} \\
& F_{v y_{a, t}}=F_{w y_{a, t}} \\
& F_{v z_{a, t}}=-F_{w z_{a, t}} \\
& M_{v x_{a, t}}=M_{w x_{a, t}}+F_{w y_{a, t}}\left(R e_{w y_{a, t}}+H_{a, t}\right) \\
& M_{v y_{a, t}}=M_{w y_{a, t}}+F_{w x_{a, t}}\left(R e_{w x_{a, t}}+H_{a, t}\right) \\
& M_{v x_{a, t}}=M_{w z_{a, t}}
\end{aligned}
$$

To calculate the vertical force applied to the suspension at the wheel location, the block implements a stiff spring-damper, shown here.


The block uses this equation.

$$
F_{w z_{a, t}}=-F w a_{z 0}-k w a_{z}\left(z_{w_{a, t}}-z_{s_{a, t}}\right)-c w a_{z}\left(\dot{z}_{w_{a, t}}-\dot{z}_{s_{a, t}}\right)
$$

The equations use these variables.
$F_{w z_{a, t}} M_{w z_{a, t}} \quad$ Suspension force and moment applied to the wheel on axle a, wheel t along wheel-fixed $z$-axis
$F_{w x_{a, t}} M_{w x_{a t t}} \quad$ Suspension force and moment applied to the wheel on axle a, wheel t along wheel-fixed $x$-axis

| $F_{w y_{u, t}} M_{w_{y_{a}, t}}$ | Suspension force and moment applied to the wheel on axle a, wheel $t$ along wheel-fixed $y$-axis |
| :---: | :---: |
| $F_{v z_{a},} M_{v z_{a, t}}$ | Suspension force and moment applied to the vehicle on axle a, wheel t along wheel-fixed $z$-axis |
| $F_{v \chi_{a, t}} M_{v \chi^{\prime}, t}$ | Suspension force and moment applied to the vehicle on axle a, wheel t along wheel-fixed $x$-axis |
| $F_{v y_{a, t}} M_{v y_{a, t}}$ | Suspension force and moment applied to the vehicle on axle a, wheel t along wheel-fixed $y$-axis |
| $F_{z 0_{a}}$ | Vertical suspension spring preload force applied to the wheels on axle a |
| $k_{\chi_{a}}$ | Vertical spring constant applied to wheels on axle a |
| kwa ${ }_{z}$ | Wheel and axle interface compliance constant |
| $m_{\text {hsteer }}$ | Steering angle to vertical force slope applied at wheel carrier for wheels on axle a |
| $\delta_{\text {steer }{ }_{\text {at }}}$ | Steering angle input for axle a, wheel t |
| $C_{z_{a}}$ | Vertical damping constant applied to wheels on axle a |
| cway | Wheel and axle interface damping constant |
| $R e_{w_{a, t}}$ | Effective wheel radius for axle a , wheel t |
| $F_{z h s t o p_{a, t}}$ | Vertical hardstop force at axle a , wheel t , along the vehicle-fixed $z$-axis |
| $F_{\text {zaswy }}^{\text {a }}$, | Vertical anti-sway force at axle a, wheel t , along the vehicle-fixed $z$-axis |
| $F w a_{z 0}$ | Wheel and axle interface compliance constant |
| $z_{v_{a, t}}, \dot{z}_{v_{a, t}}$ | Vehicle displacement and velocity at axle $a$, wheel $t$, along the vehiclefixed $z$-axis |
| $z_{w_{a, t}} \dot{z}_{w_{a}, t}$ | Wheel displacement and velocity at axle a , wheel t , along the vehicle-fixed $z$-axis |
| $\chi_{v_{a, t},} \dot{\chi}_{v_{a, t}}$ | Vehicle displacement and velocity at axle $a$, wheel $t$, along the vehiclefixed $z$-axis |
| $\chi_{w_{a, t},} \dot{x}_{w_{a, t}}$ | Wheel displacement and velocity at axle $a$, wheel $t$, along the vehicle-fixed $z$-axis |
| $y_{v_{a, t}} \dot{y}_{v_{a, t}}$ | Vehicle displacement and velocity at axle a , wheel t , along the vehiclefixed $y$-axis |
| $y_{w_{a, t}} \dot{y}_{w_{a, t}}$ | Wheel displacement and velocity at axle a , wheel t , along the vehicle-fixed $y$-axis |
| $H_{a, t}$ | Suspension height at axle a, wheel t |
| $R e_{w_{a, t}}$ | Effective wheel radius at axle a, wheel t |

## Hardstop Forces

The hardstop feedback force, $F_{\text {zhstopat, }^{\prime}}$ that the block applies depends on whether the suspension is compressing or extending. The block applies the force:

- In compression, when the suspension is compressed more than the maximum distance specified by the Suspension maximum height, Hmax parameter.
- In extension, when the suspension extension is greater than maximum extension specified by the Suspension maximum height, Hmax parameter.

To calculate the force, the block uses a stiffness based on a hyperbolic tangent and exponential scaling.

## Camber, Caster, and Toe Angles

To calculate the camber, caster, and toe angles, block uses linear functions of the suspension height and steering angle.

$$
\begin{aligned}
& \xi_{a, t}=\xi_{0 a}+m_{\text {hcamber }_{a}}\left(z_{w_{a, t}}-z_{v_{a, t}}-m_{\text {hsteer }_{a}}\left|\delta_{\text {steer }_{a, t}}\right|\right)+m_{\text {cambersteer }_{a}}\left|\delta_{\text {steer }_{a, t}}\right| \\
& \eta_{a, t}=\eta_{0 a}+m_{\text {hcaster }_{a}}\left(z_{w_{a, t}}-z_{v_{a, t}}-m_{\text {hsteer }_{a}}\left|\delta_{\text {steer }_{a, t}}\right|\right)+m_{\text {castersteer }_{a}}\left|\delta_{\text {steer }_{a, t}}\right| \\
& \zeta_{a, t}=\zeta_{0 a}+m_{\text {htoe }_{a}}\left(z_{w_{a, t}}-z_{v_{a, t}}-m_{\text {hsteer }_{a}}\left|\delta_{\text {steer }_{a, t}}\right|\right)+m_{\text {toesteer }_{a}}\left|\delta_{\text {steer }_{a}, t}\right|
\end{aligned}
$$

The equations use these variables.

| $\xi_{a, t}$ | Camber angle of wheel on axle $a$, wheel $t$ |
| :---: | :---: |
| $\eta_{a, t}$ | Caster angle of wheel on axle a, wheel t |
| $\zeta_{a, t}$ | Toe angle of wheel on axle a, wheel t |
| $\xi_{0 a}, \eta_{0 a}, \zeta_{0 a}$ | Nominal suspension axle a camber, caster, and toe angles, respectively, at zero steering angle |
| $\begin{aligned} & m_{\text {hcamber }_{a^{\prime}}} m_{\text {hcaster }_{a^{\prime}}} \\ & m_{\text {htoe }^{\prime}} \end{aligned}$ | Camber, caster, and toe angles, respectively, versus suspension height slope for axle a |
| $m_{\text {cambersteer }_{a^{\prime}}} m_{\text {castersteer }_{a^{\prime}}}$ $m_{\text {toesteer }}$ | Camber, caster, and toe angles, respectively, versus steering angle slope for axle a |
| $m_{\text {hsteer }}^{\text {a }}$ | Steering angle versus vertical force slope for axle a |
| $\delta_{\text {stee }}^{\text {at, }}$ | Steering angle input for axle a, wheel t |
| $z_{v_{a t,}}$ | Vehicle displacement at axle a , wheel t , along the vehicle-fixed $z$-axis |
| $z_{w_{\text {at }}}$ | Wheel displacement at axle a , wheel t , along the vehicle-fixed $z$-axis |

## Steering Angles

Optionally, use the Steered axle enable by axle, StrgEnByAxl parameter to input steering angles for the wheels. To calculate the steering angles for the wheels, the block offsets the input steering angles with a linear function of the suspension height.

$$
\delta_{\text {whlsteer }_{a, t}}=\delta_{\text {steer }_{a, t}}+m_{\text {htoe }_{a}}\left(z_{w_{a, t}}-z_{v_{a, t}}-m_{\text {hsteer }_{a}}\left|\delta_{\text {steer }_{a, t}}\right|\right)+m_{\text {toesteer }_{a}}\left|\delta_{\text {steer }_{a, t}}\right|
$$

The equation uses these variables.

| $m_{\text {toesteer }_{a}}$ | Axle a toe angle versus steering angle slope |
| :--- | :--- |
| $m_{\text {hsteer }_{a}}$ | Axle a steering angle versus vertical force slope |
| $m_{\text {htoe }_{a}}$ | Axle a toe angle versus suspension height slope |
| $\delta_{\text {whlster }_{a, t}}$ | Wheel steering angle for axle a, wheel t |
| $\delta_{\text {steer }_{a, t}}$ | Steering angle input for axle a, wheel t |
| $z_{v_{a, t}}$ | Vehicle displacement at axle a, wheel t , along the vehicle-fixed $z$-axis |

$z_{w_{a, t}} \quad$ Wheel displacement at axle $a$, wheel $t$, along the vehicle-fixed $z$-axis

## Power and Energy

The block calculates these suspension characteristics for each axle, $a$, wheel, $t$.

| Calculation | Equation |
| :---: | :---: |
| Dissipated power, $P_{\text {suspot }}$ | $P_{\text {susp }_{a, t}}=F_{w_{z l o o k u p a l ~}}\left(\dot{v}_{v_{a, t}}-\dot{w}_{w_{a, t},} \dot{z}_{v_{a, t}}-\dot{z}_{w_{a, t}} \delta_{\text {steer }_{a, t}}\right)$ |
| Absorbed energy, $E_{\text {susp }}^{\text {at }}$ | $E_{\text {susp }_{a, t}}=F_{w_{z l o o k u p a l}}\left(\dot{v}_{v_{a, t}}-\dot{w}_{w_{a, t}} \dot{z}_{v_{a, t}}-\dot{z}_{w_{a, t}} \delta_{\text {steer }_{a, t}}\right)$ |
| Suspension height, $H_{a, t}$ | $H_{a, t}=-\left(z_{v_{a, t}}-z_{w_{a, t}}+\frac{F_{z 0_{a}}}{k_{z_{a}}}+m_{\text {hsteer }_{a}}\left\|\delta_{\text {steer }_{a, t}}\right\|\right)$ |
| Distance from wheel carrier center to tire/road interface | $z_{w t t_{a, t}}=R e_{w_{a, t}}+H_{a, t}$ |

The equations use these variables.
$m_{h_{s t e e r}^{a}} \quad$ Steering angle to vertical force slope applied at wheel carrier for wheels on axle a
$\delta_{\text {steer }_{a, t}} \quad$ Steering angle input for axle a, wheel t
$R e_{w_{a, t}} \quad$ Axle a, wheel $t$ effective wheel radius from wheel carrier center to tire/road interface
$F_{z 0_{a}} \quad$ Vertical suspension spring preload force applied to the wheels on axle a
$z_{w t r_{a, t}} \quad$ Distance from wheel carrier center to tire/road interface, along the vehicle-fixed $z$ axis
$z_{v_{a, t}}, \dot{z}_{v_{a, t}} \quad$ Vehicle displacement and velocity at axle $a$, wheel $t$, along the vehicle-fixed $z$-axis
$z_{w_{a, t}} \dot{z}_{w_{a, t}} \quad$ Wheel displacement and velocity at axle $a$, wheel $t$, along the vehicle-fixed $z$-axis

## Ports

## Input

WhIPz - Wheel z-axis displacement
array
Wheel displacement, $z_{w}$, along wheel-fixed $z$-axis, in $m$. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlPz:

- Signal array dimensions are [1x4].

$$
\mathrm{WhlPz}=z_{w}=\left[\begin{array}{llll}
z_{w_{1,1}} & z_{w_{1,2}} & z_{w_{2,1}} & z_{w_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlPz $(1,1)$ | 1 | 1 |
| Front right | WhlPz $(1,2)$ | 1 | 2 |


| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Rear left | WhlPz $(1,3)$ | 2 | 1 |
| Rear right | WhlPz $(1,4)$ | 2 | 2 |

WhIRe - Wheel effective radius
array
Effective wheel radius, $R e_{w}$, in m. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlRe:

- Signal array dimensions are [1×4].

$$
\text { WhlRe }=R e_{w}=\left[\begin{array}{ll}
R e_{w_{1,1}} & R e_{w_{1,2}}
\end{array} R e_{w_{2,1}} R e_{w_{2,2}}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlRe $(1,1)$ | 1 | 1 |
| Front right | WhlRe $(1,2)$ | 1 | 2 |
| Rear left | WhlRe $(1,3)$ | 2 | 1 |
| Rear right | WhlRe $(1,4)$ | 2 | 2 |

WhIVz - Wheel z-axis velocity array

Wheel velocity, $\dot{z}_{w}$, along wheel-fixed $z$-axis, in m. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlVz:

- Signal array dimensions are [1×4].

$$
\text { WhlVz }=\dot{z}_{w}=\left[\begin{array}{lll}
\dot{z}_{1,1} & \dot{z}_{w_{1,2}} & \dot{z}_{w_{2,1}} \\
\dot{z}_{w_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlVz $(1,1)$ | 1 | 1 |
| Front right | WhlVz $(1,2)$ | 1 | 2 |
| Rear left | WhlVz $(1,3)$ | 2 | 1 |
| Rear right | WhlVz $(1,4)$ | 2 | 2 |

WhIFx - Longitudinal wheel force on vehicle
array
Longitudinal wheel force applied to vehicle, $F_{w \chi}$, along the vehicle-fixed $x$-axis. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlFx:

- Signal array dimensions are [1×4].

WhlFx $=F_{w x}=\left[F_{w x_{1,1}} F_{w x_{1,2}} F_{w x_{2,1}} F_{w x_{2,2}}\right]$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlFx $(1,1)$ | 1 | 1 |
| Front right | WhlFx $(1,2)$ | 1 | 2 |
| Rear left | WhlFx $(1,3)$ | 2 | 1 |
| Rear right | WhlFx $(1,4)$ | 2 | 2 |

WhIFy - Lateral wheel force on vehicle
array
Lateral wheel force applied to vehicle, $F_{w y}$, along the vehicle-fixed $y$-axis. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlFy:

- Signal array dimensions are [1×4].

WhlFy $=F_{w y}=\left[F_{w y 1,1} F_{w y 1,2} F_{w y 2,1} F_{w y_{2,2}}\right]$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlFy $(1,1)$ | 1 | 1 |
| Front right | WhlFy $(1,2)$ | 1 | 2 |
| Rear left | WhlFy $(1.3)$ | 2 | 1 |
| Rear right | WhlFy $(1,4)$ | 2 | 2 |

WhIM - Suspension moment on wheel
array
Longitudinal, lateral, and vertical suspension moments at axle a, wheel $t$, applied to the wheel at the axle wheel carrier reference coordinate, in $\mathrm{N} \cdot \mathrm{m}$. Input array dimensions are 3 by the number of wheels on the vehicle.

- WhlM (1, . . ) - Suspension moment applied to the wheel about the vehicle-fixed $x$-axis (longitudinal)
- WhlM $(2, \ldots)$ - Suspension moment applied to the wheel about the vehicle-fixed $y$-axis (lateral)
- WhlM $(3, \ldots)$ - Suspension moment applied to the wheel about the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the WhlM:

- Signal dimensions are [3×4].
- Signal contains suspension moments applied to four wheels according to their axle and wheel locations.

$$
\text { WhlM }=M_{w}=\left[\begin{array}{llll}
M_{w x_{1,1}} & M_{w x_{1,2}} & M_{w x_{2,1}} & M_{w x_{2,2}} \\
M_{w y_{1,1}} & M_{w y 1,2} & M_{w y_{2,1}} & M_{w y 2,2} \\
M_{w z_{1,1}} & M_{w z_{1,2}} & M_{w z_{2,1}} & M_{w z 2,2}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Moment Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | WhlM(1,1) | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front <br> right | WhlM(1,2) | 1 | 2 |  |
| Rear <br> left | WhlM(1,3) | 2 | 1 |  |
| Rear <br> right | WhlM(1,4) | 2 | 2 |  |
| Front <br> left | WhlM(2,1) | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front <br> right | WhlM(2,2) | 1 | 2 |  |
| Rear <br> left | WhlM(2,3) | 2 | 1 |  |
| Rear <br> right | WhlM(2,4) | 2 | 2 |  |
| Front <br> left | WhlM(3,1) | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front <br> right | WhlM(3,2) | 1 | 2 |  |
| Rear <br> left | WhlM(3,3) | 2 | 1 |  |
| Rear <br> right | WhlM(3,4) | 2 | 2 |  |

VehP - Vehicle displacement
array
Vehicle displacement from axle a, wheel $t$ along vehicle-fixed coordinate system, in m. Input array dimensions are 3 the number of wheels on the vehicle.

- VehP $(1, \ldots)$ - Vehicle displacement from wheel, $\chi_{v}$, along the vehicle-fixed $x$-axis
- $\operatorname{VehP}(2, \ldots)$ - Vehicle displacement from wheel, $y_{v}$, along the vehicle-fixed $y$-axis
- $\operatorname{VehP}(3, \ldots)-$ Vehicle displacement from wheel, $z_{v}$, along the vehicle-fixed $z$-axis

For example, for a two-axle vehicle with two wheels per axle, the VehP:

- Signal dimensions are [3×4].
- Signal contains four displacements according to their axle and wheel locations.

$$
\text { VehP }=\left[\begin{array}{l}
x_{v} \\
y_{v} \\
z_{v}
\end{array}\right]=\left[\begin{array}{llll}
x_{v_{1,1}} & x_{v_{1,2}} & x_{v_{2,1}} & x_{v_{2,2}} \\
y_{v_{1,1}} & y_{v_{1,2}} & y_{v_{2,1}} & v_{v_{2,2}} \\
z_{v_{1,1}} & z_{v_{1,2}} & z_{v_{2,1}} & z_{v_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel Numbe r | Axis |
| :---: | :---: | :---: | :---: | :---: |
| Front left | $\operatorname{VehP}(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis |
| Front right | $\operatorname{VehP}(1,2)$ | 1 | 2 |  |
| Rear left | $\operatorname{VehP}(1,3)$ | 2 | 1 |  |
| Rear right | $\operatorname{VehP}(1,4)$ | 2 | 2 |  |
| Front left | $\operatorname{VehP}(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis |
| Front right | $\operatorname{VehP}(2,2)$ | 1 | 2 |  |
| $\begin{array}{\|l} \text { Rear } \\ \text { left } \end{array}$ | $\operatorname{VehP}(2,3)$ | 2 | 1 |  |
| Rear right | $\operatorname{VehP}(2,4)$ | 2 | 2 |  |
| Front left | $\operatorname{VehP}(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis |
| Front right | $\operatorname{VehP}(3,2)$ | 1 | 2 |  |
| Rear left | $\operatorname{VehP}(3,3)$ | 2 | 1 |  |
| Rear right | $\operatorname{VehP}(3,4)$ | 2 | 2 |  |

VehV - Vehicle velocity
array
Vehicle velocity at axle a, wheel t along vehicle-fixed coordinate system, in m . Input array dimensions are 3 by the number of wheels on the vehicle.

- $\operatorname{VehV}(1, \ldots)$ - Vehicle velocity at wheel, $x_{v}$, along the vehicle-fixed $x$-axis
- VehV $(2, \ldots)$ - Vehicle velocity at wheel, $y_{v}$, along the vehicle-fixed $y$-axis
- $\operatorname{VehV}(3, \ldots)$ - Vehicle velocity at wheel, $z_{v}$, along the vehicle-fixed $z$-axis

For example, for a two-axle vehicle with two wheels per axle, the VehV:

- Signal dimensions are [3×4].
- Signal contains 4 velocities according to their axle and wheel locations.

$$
\text { VehV }=\left[\begin{array}{l}
\dot{x}_{v} \\
\dot{y}_{v} \\
\dot{z}_{v}
\end{array}\right]=\left[\begin{array}{llll}
\dot{x}_{v_{1,1}} & \dot{x}_{v_{1,2}} & \dot{x}_{v_{2,1}} & \dot{x}_{v_{2,2}} \\
\dot{y}_{v_{1,1}} & \dot{y}_{v_{1,2}} & \dot{y}_{v_{2,1}} & \dot{y}_{v_{2,2}} \\
\dot{z}_{v_{1,1}} & \dot{z}_{v_{1,2}} & \dot{z}_{v_{2,1}} & \dot{z}_{v_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | VehV $(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis |
| Front <br> right | VehV $(1,2)$ | 1 | 2 |  |
| Rear <br> left | VehV $(1,3)$ | 2 | 1 |  |
| Rear <br> right | VehV $(1,4)$ | 2 | 2 |  |
| Front <br> left | VehV $(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis |
| Front <br> right | VehV(2,2) | 1 | 2 |  |
| Rear <br> left | VehV(2,3) | 2 | 1 |  |
| Rear <br> right | VehV(2,4) | 2 | 2 |  |
| Front <br> left | VehV(3,1) | 1 | 1 | Vehicle-fixed $z$-axis |
| Front <br> right | VehV(3,2) | 1 | 2 |  |
| Rear <br> left | VehV(3,3) | 2 | 1 |  |
| Rear <br> right | VehV(3,4) | 2 | 2 |  |

StrgAng - Steering angle, optional
array
Optional steering angle for each wheel, $\delta$. Input array dimensions are 1 by the number of steered wheels.

For example, for a two-axle vehicle with two wheels per axle, you can input steering angles for both wheels on the first axle.

- To create the StrgAng port, set Steered axle enable by axle, StrgEnByAxl to [1 0]. The input signal array dimensions are [1×2].
- The StrgAng signal contains two steering angles according to their axle and wheel locations.

$$
\text { StrgAng }=\delta_{\text {steer }}=\left[\delta_{\text {steer }_{1,1}} \delta_{\text {steer }_{1,2}}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | StrgAng $(1,1)$ | 1 | 1 |
| Front right | StrgAng $(1,2)$ | 1 | 2 |

## Dependencies

To create input port StrgAng, set an element of the Steered axle enable by axle, StrgEnByAxl vector to 1 .

## Output

Info - Bus signal
bus
Bus signal containing block values. The signals are arrays that depend on the wheel location.
For example, here are the indices for a two-axle, two-wheel vehicle. The total number of wheels is four.

- 1D array signal (1-by-4)

| Array Element | Axle | Wheel Number |
| :--- | :--- | :--- |
| $(1,1)$ | 1 | 1 |
| $(1,2)$ | 1 | 2 |
| $(1,3)$ | 2 | 1 |
| $(1,4)$ | 2 | 2 |

- 3D array signal (3-by-4)

| Array Element | Axle | Wheel Number |
| :--- | :--- | :--- |
| $(1,1)$ | 1 | 1 |
| $(1,2)$ | 1 | 2 |
| $(1,3)$ | 2 | 1 |
| $(1,4)$ | 2 | 2 |
| $(2,1)$ | 1 | 1 |
| $(2,2)$ | 1 | 2 |
| $(2,3)$ | 2 | 1 |
| $(2,4)$ | 2 | 2 |
| $(3,1)$ | 1 | 1 |
| $(3,2)$ | 1 | 2 |
| $(3,3)$ | 2 | 1 |
| $(3,4)$ | 2 | 2 |


| Signal | Description | Array Signal | Variable | Units |
| :---: | :---: | :---: | :---: | :---: |
| Camber | Wheel angles according to the axle. | 1D | WhlAng $[1, \ldots]=\xi=\left[\xi_{a, t}\right]$ | rad |
| Caster |  |  | WhlAng $[2, \ldots]=\eta=\left[\eta_{a, t}\right]$ |  |
| Toe |  |  | WhlAng $[3, \ldots]=\zeta=\left[\zeta_{a, t}\right]$ |  |
| Height | Suspension height | 1D | H | m |


| Signal | Description | Array Signal | Variable U | Units |
| :---: | :---: | :---: | :---: | :---: |
| Power | Suspension power dissipation | 1D |  | W |
| Energy | Suspension absorbed energy | 1D | $E_{\text {susp }}$ | J |
| VehF | Suspension forces applied to the vehicle | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { VehF }=F_{v}= \\ & {\left[\begin{array}{llll} F_{v x_{1,1}} & F_{v x_{1,2}} & F_{v x_{2,1}} & F_{v x_{2,2}} \\ F_{v v_{1,1}} & F_{v y_{1,2}} & F_{v v_{2,1}} & F_{v y_{2,2}} \\ F_{v v_{1,1}} & F_{v z_{1,2}} & F_{v z_{2,1}} & F_{v z_{2,2}} \end{array}\right.} \end{aligned}$ | N |
| VehM | Suspension moments applied to vehicle | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { VehM }=M_{v}= \\ & {\left[\begin{array}{llll} M_{v x_{1}, 1} & M_{v x_{1}, 2} & M_{v x_{2,1}} & M_{v \chi_{2},}, \\ M_{v y_{1,1}} & M_{v y_{1,2}} & M_{v y_{2,1}} & M_{v y y_{2},} \\ M_{v \chi_{1,1}} & M_{v z_{1,2}} & M_{v z_{2,1}} & M_{v z_{2},} \end{array}\right.} \end{aligned}$ | $\mathrm{N} \cdot \mathrm{m}$ <br> 2,2 <br> 2,2 <br> 2,2 |


| Signal | Description | Array Signal | Variable | Units |
| :---: | :---: | :---: | :---: | :---: |
| WhlF | Suspension force applied to wheel | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { WhlF }=F_{w}= \\ & {\left[\begin{array}{llll} F_{w x_{1}, 1} & F_{w x_{1,2}} & F_{w x_{2,1}} & F_{w x_{2}} \\ F_{w y 1,1} & F_{w y_{1,2}} & F_{w y 2,1} & F_{w y 2} \\ F_{w z_{1,1}} & F_{w z_{1,2}} & F_{w z 2,1} & F_{w z_{2}} \end{array}\right.} \end{aligned}$ |  |
| WhlP | Wheel displacement | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { WhlP }=\left[\begin{array}{l} x_{w} \\ y_{w} \\ z_{w} \end{array}\right]= \\ & {\left[\begin{array}{cccc} x_{w_{1,1}} & x_{w_{1,2}} & x_{w_{2,1}} & x_{w_{2}} \\ y_{w_{1,1}} & y_{w_{1,2}} & y_{w_{2,1}} & y_{w y} \\ z_{w t r_{1,1}} & z_{w t r_{1,2}} & z_{w t r_{2,1}} & z_{w t r} \end{array}\right.} \end{aligned}$ |  |
| WhlV | Wheel velocity | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { WhlV }=\left[\begin{array}{l} \dot{x}_{w} \\ \dot{y}_{w} \\ \dot{z}_{w} \end{array}\right] \\ & = \\ & {\left[\begin{array}{lll} \dot{x}_{w_{1,1}} & \dot{x}_{w_{1,2}} & \dot{x}_{w_{2,1}} \\ \dot{x}_{w_{2,2}} \\ \dot{y}_{w_{1,1}} & \dot{y}_{w_{1,2}} \dot{y}_{w_{2,1}} & \dot{y}_{w_{2,2}} \\ \dot{z}_{w_{1,1}} & \dot{z}_{w_{1,2}} & \dot{z}_{w_{2,1}} \\ \dot{z}_{w_{2,2}} \end{array}\right]} \end{aligned}$ | m/s |


| Signal | Description | Array Signal | Variable | Units |
| :---: | :---: | :---: | :---: | :---: |
| WhlAng | Wheel camber, caster, toe angles | 3D | For a two-axle, two wheels per axle vehicle: $\left.\begin{array}{l} \text { WhlAng }=\left[\begin{array}{l} \xi \\ \eta \\ \zeta \end{array}\right] \\ =\left[\begin{array}{lll} \xi_{1,1} & \xi_{1,2} & \xi_{2,1} \\ \xi_{2,2} \\ \eta_{1,1} & \eta_{1,2} & \eta_{2,1} \\ \eta_{2,2} \\ \zeta_{1,1} & \zeta_{1,2} & \zeta_{2,1} \end{array} \zeta_{2,2}\right. \end{array}\right] . \begin{aligned} & \eta_{2} \end{aligned}$ | rad |

VehF - Suspension force on vehicle
array
Longitudinal, lateral, and vertical suspension force at axle a, wheel $t$, applied to the vehicle at the suspension connection point, in N. Array dimensions are 3 by the number of wheels on the vehicle.

- $\operatorname{VehF}(1, \ldots)$ - Suspension force applied to vehicle along the vehicle-fixed $x$-axis (longitudinal)
- $\operatorname{VehF}(2, \ldots)$ - Suspension force applied to vehicle along the vehicle-fixed $y$-axis (lateral)
- $\operatorname{VehF}(3, \ldots)$ - Suspension force applied to vehicle along the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the VehF:

- Signal dimensions are [3×4].
- Signal contains suspension forces applied to the vehicle according to the axle and wheel locations.

VehF $=F_{v}=\left[\begin{array}{llll}F_{v x_{1,1}} & F_{v x_{1,2}} & F_{v x_{2,1}} & F_{v x_{2,2}} \\ F_{v v_{1,1}} & F_{v y_{1,2}} & F_{v y_{2,1}} & F_{v y_{2,2}} \\ F_{v z_{1,1}} & F_{v z_{1,2}} & F_{v z_{2,1}} & F_{v z_{2,2}}\end{array}\right]$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | $\operatorname{VehF}(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front <br> right | $\operatorname{VehF}(1,2)$ | 1 | 2 |  |
| Rear <br> left | $\operatorname{VehF}(1,3)$ | 2 | 1 |  |
| Rear <br> right | $\operatorname{VehF}(1,4)$ | 2 | 2 |  |
| Front <br> left | $\operatorname{VehF}(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front <br> right | $\operatorname{VehF}(2,2)$ | 1 | 2 |  |


| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Rear <br> left | VehF $(2,3)$ | 2 | 1 |  |
| Rear <br> right | VehF $(2,4)$ | 2 | 2 |  |
| Front <br> left | $\operatorname{VehF}(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front <br> right | $\operatorname{VehF}(3,2)$ | 1 | 2 |  |
| Rear <br> left | $\operatorname{VehF}(3,3)$ | 2 | 1 |  |
| Rear <br> right | $\operatorname{VehF}(3,4)$ | 2 | 2 |  |

VehM - Suspension moment on vehicle array

Longitudinal, lateral, and vertical suspension moment at axle a, wheel $t$, applied to the vehicle at the suspension connection point, in $\mathrm{N} \cdot \mathrm{m}$. Array dimensions are 3 by the number of wheels on the vehicle.

- VehM(1, ...) - Suspension moment applied to the vehicle about the vehicle-fixed $x$-axis (longitudinal)
- VehM ( $2, \ldots$ ) - Suspension moment applied to the vehicle about the vehicle-fixed $y$-axis (lateral)
- Vehm ( $3, \ldots$ ) - Suspension moment applied to the vehicle about the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the VehM:

- Signal dimensions are [3×4].
- Signal contains suspension moments applied to vehicle according to the axle and wheel locations.

VehM $=M_{v}=\left[\begin{array}{llll}M_{v x_{1,1}} & M_{v x_{1,2}} & M_{v x_{2,1}} & M_{v x_{2,2}} \\ M_{v y 1,1} & M_{v y_{1,2}} & M_{v y_{2,1}} & M_{v y_{2,2}} \\ M_{v z_{1,1}} & M_{v z_{1,2}} & M_{v z_{2,1}} & M_{v z_{2,2}}\end{array}\right]$

| Array Element | Axle | Wheel <br> Number | Moment Axis |
| :--- | :--- | :--- | :--- |
| $\operatorname{VehM}(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| $\operatorname{VehM}(1,2)$ | 1 | 2 |  |
| $\operatorname{VehM}(1,3)$ | 2 | 1 |  |
| $\operatorname{VehM}(1,4)$ | 2 | 2 |  |
| $\operatorname{VehM}(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| $\operatorname{VehM}(2,2)$ | 1 | 2 |  |


| Array Element | Axle | Wheel <br> Number | Moment Axis |
| :--- | :--- | :--- | :--- |
| $\operatorname{VehM}(2,3)$ | 2 | 1 |  |
| $\operatorname{VehM}(2,4)$ | 2 | 2 |  |
| $\operatorname{VehM}(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| $\operatorname{VehM}(3,2)$ | 1 | 2 |  |
| $\operatorname{VehM}(3,3)$ | 2 | 1 |  |
| $\operatorname{VehM}(3,4)$ | 2 | 2 |  |

WhIF - Suspension force on wheel
array
Longitudinal, lateral, and vertical suspension forces at axle a, wheel $t$, applied to the wheel at the axle wheel carrier reference coordinate, in N . Array dimensions are 3 by the number of wheels on the vehicle.

- $\operatorname{WhlF}(1, \ldots)-$ Suspension force on wheel along the vehicle-fixed $x$-axis (longitudinal)
- $\operatorname{WhlF}(2, \ldots)$ - Suspension force on wheel along the vehicle-fixed $y$-axis (lateral)
- WhlF $(3, \ldots)$ - Suspension force on wheel along the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the WhlF:

- Signal dimensions are [3×4].
- Signal contains wheel forces applied to the vehicle according to the axle and wheel locations.

WhlF $=F_{w}=\left[\begin{array}{llll}F_{w x_{1,1}} & F_{w x_{1,2}} & F_{w x_{2,1}} & F_{w x_{2,2}} \\ F_{w y_{1,1}} & F_{w y_{1,2}} & F_{w y_{2,1}} & F_{w y_{2,2}} \\ F_{w z_{1,1}} & F_{w z_{1,2}} & F_{w z_{2,1}} & F_{w z_{2,2}}\end{array}\right]$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | WhlF $(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front <br> right | WhlF $(1,2)$ | 1 | 2 |  |
| Rear <br> left | WhlF $(1,3)$ | 2 | 1 |  |
| Rear <br> right | WhlF $(1,4)$ | 2 | 2 |  |
| Front <br> left | WhlF $(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front <br> right | WhlF $(2,2)$ | 1 | 2 |  |


| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Rear <br> left | WhlF $(2,3)$ | 2 | 1 |  |
| Rear <br> right | WhlF $(2,4)$ | 2 | 2 |  |
| Front <br> left | WhlF $(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front <br> right | WhlF(3,2) | 1 | 2 |  |
| Rear <br> left | WhlF(3,3) | 2 | 1 |  |
| Rear <br> right | WhlF(3,4) | 2 | 2 |  |

Whiv - Wheel velocity
array
Longitudinal, lateral, and vertical wheel velocity at axle a, wheel t , in $\mathrm{m} / \mathrm{s}$. Array dimensions are 3 by the number of wheels on the vehicle.

- WhlV (1, ...) - Wheel velocity along the vehicle-fixed $x$-axis (longitudinal)
- WhlV $(2, \ldots)-$ Wheel velocity along the vehicle-fixed $y$-axis (lateral)
- WhlV $(3, \ldots)-$ Wheel velocity along the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the WhlV:

- Signal dimensions are [3×4].
- Signal contains wheel forces applied to the vehicle according to the axle and wheel locations.

$$
\text { WhlV }=\left[\begin{array}{c}
\dot{x}_{w} \\
\dot{y}_{w} \\
\dot{z}_{w}
\end{array}\right]=\left[\begin{array}{llll}
\dot{x}_{w_{1,1}} & \dot{x}_{w_{1,2}} & \dot{x}_{w_{2,1}} & \dot{x}_{w_{2,2}} \\
\dot{y}_{w_{1,1}} & \dot{y}_{w_{1,2}} & \dot{y}_{w_{2,1}} & \dot{y}_{w_{2,2}} \\
\dot{z}_{w_{1,1}} & \dot{z}_{w_{1,2}} & \dot{z}_{w_{2,1}} & \dot{z}_{w_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | WhlV $(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front <br> right | WhlV $(1,2)$ | 1 | 2 |  |
| Rear <br> left | WhlV $(1,3)$ | 2 | 1 |  |
| Rear <br> right | WhlV $(1,4)$ | 2 | 2 |  |


| Wheel | Array Element | Axie | Wheel Numbe r | Force Axis |
| :---: | :---: | :---: | :---: | :---: |
| Front left | WhlV $(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front right | WhlV (2,2) | 1 | 2 |  |
| Rear left | WhlV (2,3) | 2 | 1 |  |
| Rear right | WhlV $(2,4)$ | 2 | 2 |  |
| Front left | WhlV (3,1) | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front right | WhlV (3,2) | 1 | 2 |  |
| Rear left | WhlV (3,3) | 2 | 1 |  |
| Rear right | WhlV (3,4) | 2 | 2 |  |

WhIAng - Wheel camber, caster, toe angles
array
Camber, caster, and toe angles at axle $a$, wheel $t$, in rad. Array dimensions are 3 by the number of wheels on the vehicle.

- WhlAng(1,...) - Camber angle
- WhlAng ( $2, \ldots$ ) - Caster angle
- Whlang $(3, \ldots)$ - Toe angle

For example, for a two-axle vehicle with two wheels per axle, the WhlAng:

- Signal dimensions are [3×4].
- Signal contains angles according to the axle and wheel locations.

$$
\text { WhlAng }=\left[\begin{array}{l}
\xi \\
\eta \\
\zeta
\end{array}\right]=\left[\begin{array}{llll}
\xi_{1,1} & \xi_{1,2} & \xi_{2,1} & \xi_{2,2} \\
\eta_{1,1} & \eta_{1,2} & \eta_{2,1} & \eta_{2,2} \\
\zeta_{1,1} & \zeta_{1,2} & \zeta_{2,1} & \zeta_{2,2}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Angle |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | WhlAng $(1,1)$ | 1 | 1 | Camber |
| Front <br> right | WhlAng (1,2) | 1 | 2 |  |


| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Angle |
| :--- | :--- | :--- | :--- | :--- |
| Rear <br> left | WhlAng (1,3) | 2 | 1 |  |
| Rear <br> right | WhlAng (1,4) | 2 | 2 |  |
| Front <br> left | WhlAng (2,1) | 1 | 1 | Caster |
| Front <br> right | WhlAng (2,2) | 1 | 2 |  |
| Rear <br> left | WhlAng (2,3) | 2 | 1 |  |
| Rear <br> right | WhlAng(2,4) | 2 | 2 |  |
| Front <br> left | WhlAng (3,1) | 1 | 1 | Toe |
| Front <br> right | WhlF(3,2) | 1 | 2 |  |
| Rear <br> left | WhlF(3,3) | 2 | 1 |  |
| Rear <br> right | WhlF(3,4) | 2 | 2 |  |

## Parameters

## Axles

## Number of axles, NumAxI - Number of axles

2 (default) | scalar
Number of axles, $N_{a}$, dimensionless.
Number of wheels by axle, NumWhlsByAxI - Number of wheels per axle
[2 2] (default)|vector
Number of wheels per axle, $N t_{a}$, dimensionless. Vector is 1 by the number of vehicle axles, $N_{a}$. For example, [1,2] represents one wheel on axle one and two wheels on axle two.

Steered axle enable by axle, StrgEnByAxI - Boolean vector to enable axle steering
[1 0] (default) |vector
Boolean vector that enables axle steering, $E n_{\text {steer }}$, dimensionless. Vector is 1 by the number of vehicle axles, $N_{a}$. For example:

- [llll-For a two-axle vehicle, enables axle one steering and disables axle two steering
- [1 1]-For a two-axle vehicle, enables axle one and axle two steering


## Dependencies

Setting an element of the Steered axle enable by axle, StrgEnByAxl vector to 1:

- Creates input port StrgAng.
- Creates these parameters
- Toe angle vs steering angle slope, ToeStrgSlp
- Caster angle vs steering angle slope, CasterStrgSlp
- Camber angle vs steering angle slope, CamberStrgSlp
- Suspension height vs steering angle slope, StrgHgtSlp

For example, for a two-axle vehicle with two wheels per axle, you can input steering angles for both wheels on the first axle.

- To create the StrgAng port, set Steered axle enable by axle, StrgEnByAxl to [1 0]. The input signal array dimensions are [1x2].
- The StrgAng signal contains two steering angles according to their axle and wheel locations.

$$
\text { StrgAng }=\delta_{\text {steer }}=\left[\delta_{\text {steer }_{1,1}} \delta_{\text {steer }_{1}, 2}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | StrgAng (1, 1) | 1 | 1 |
| Front right | StrgAng (1,2) | 1 | 2 |

Axle and wheels lumped principal moments of inertia about longitudinal axis, Axllxx Inertia
300 (default) | vector
Axle and wheels lumped principal moments of inertia about longitudinal axis, AxleIxx $a$, in $\mathrm{kg}^{*} \mathrm{~m} \wedge 2$.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Axle and wheels lumped mass, AxIM - Mass

[2 2] (default)|vector
Axle and wheels lumped mass, $a$, in kg.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Track hardpoint coordinates relative to axle center, TrackCoords - Point

[0 0 0 0;-1 1 -1 1;0 0 0 0] (default)|array
Track hardpoint coordinates, $T c_{t}$, along the solid axle $x, y$, and $z$-axes, in m .
For example, for a two-axle vehicle with two wheels per axle, the TrackCoords array:

- Dimensions are [3x4].
- Contains four track hardpoint coordinates according to their axle and wheel locations.

$$
T c_{t}=\left[\begin{array}{llll}
x_{w_{1,1}} & x_{w_{1,2}} & x_{w_{2,1}} & x_{w_{2,2}} \\
y_{w_{1,1}} & y_{w_{1,2}} & y_{w_{2,1}} & y_{w_{2,2}} \\
z_{w_{1,1}} & z_{w_{1,2}} & z_{w_{2,1}} & z_{w_{2,2}}
\end{array}\right]
$$

| Array Element | Axle | Wheel Number | Axis |
| :---: | :---: | :---: | :---: |
| TrackCoords(1, 1) | 1 | 1 | Solid axle $x$-axis |
| TrackCoords(1, 2) | 1 | 2 |  |
| ```TrackCoords(1, 3)``` | 2 | 1 |  |
| TrackCoords(1, 4) | 2 | 2 |  |
| TrackCoords(2, 1) | 1 | 1 | Solid axle $y$-axis |
| TrackCoords(2, 2) | 1 | 2 |  |
| TrackCoords(2, 3) | 2 | 1 |  |
| TrackCoords(2, 4) | 2 | 2 |  |
| TrackCoords(3, 1) | 1 | 1 | Solid axle $z$-axis |
| TrackCoords(3, 2) | 1 | 2 |  |
| TrackCoords(3, 3) | 2 | 1 |  |
| TrackCoords(3, <br> 4) | 2 | 2 |  |

## Suspension hardpoint coordinates relative to axle center, SuspCoords - Point

## [0 0 0 0;-1 1-1 1;0 0 0 0] (default)|array

Suspension hardpoint coordinates, $S c_{t}$, along the solid axle $x$-, $y$-, and $z$-axes, in $m$.
For example, for a two-axle vehicle with two wheels per axle, the SuspCoords array:

- Dimensions are [3×4].
- Contains four track hardpoint coordinates according to their axle and track locations.

$$
S c_{t}=\left[\begin{array}{llll}
x_{s_{1,1}} & x_{s_{1,2}} & x_{s_{2,1}} & x_{s_{2,2}} \\
y_{s_{1,1}} & y_{s_{1,2}} & y_{s_{2,1}} & y_{s_{2,2}} \\
z_{s_{1,1}} & z_{s_{1,2}} & z_{s_{2,1}} & z_{s_{2,2}}
\end{array}\right]
$$

| Array Element | Axle | Track | Axis |
| :---: | :---: | :---: | :---: |
| SuspCoords(1,1 ) | 1 | 1 | Solid axle $x$-axis |
| SuspCoords(1,2 ) | 1 | 2 |  |
| $\begin{aligned} & \text { SuspCoords(1,3 } \\ & \text { ) } \end{aligned}$ | 2 | 1 |  |
| SuspCoords(1,4 | 2 | 2 |  |
| $\begin{aligned} & \text { SuspCoords }(2,1 \\ & ) \end{aligned}$ | 1 | 1 | Solid axle $y$-axis |
| SuspCoords(2,2 | 1 | 2 |  |
| SuspCoords(2,3 ) | 2 | 1 |  |
| $\begin{aligned} & \begin{array}{l} \text { SuspCoords }(2,4 \\ ) \\ \hline \end{array} \\ & \hline \end{aligned}$ | 2 | 2 |  |
| SuspCoords (3,1 ) | 1 | 1 | Solid axle $z$-axis |
| SuspCoords (3,2 ) | 1 | 2 |  |
| $\begin{aligned} & \text { SuspCoords }(3,3 \\ & ) \end{aligned}$ | 2 | 1 |  |
| SuspCoords (3,4 ) | 2 | 2 |  |

Wheel and axle interface compliance constant, KzWhIAxI - Spring rate 6437000 (default) | scalar

Wheel and axle interface compliance constant, $k w a_{z}$, in $\mathrm{N} / \mathrm{m}$.
Wheel and axle interface compliance preload, FOzWhIAxI - Spring rate 9810 (default) | scalar

Wheel and axle interface compliance preload, $F w a_{z 0}$, in N .

## Wheel and axle interface damping constant, CzWhIAxI - Damping

10000 (default) | scalar
Wheel and axle interface damping constant, $c w a_{z}$, in $m$.

## Suspension

## Compliance and Damping - Passive

Suspension spring constant, Kz - Suspension spring constant
64370 (default) | scalar | vector
Linear vertical spring constant for independent suspension wheels on axle a, $k_{z_{d}}$, in $\mathrm{N} / \mathrm{m}$.

Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Suspension spring preload, $\mathbf{F O z}$ - Suspension spring preload

9810 (default) | scalar | vector
Vertical preload spring force applied to the wheels on the axle at wheel carrier reference coordinates, $F_{z 0_{a^{\prime}}}$ in N. Positive preload forces:

- Cause the vehicle to lift.
- Point along the negative vehicle-fixed $z$-axis.

Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

Suspension shock damping constant, Cz - Suspension shock damping constant 10000 (default) | scalar | vector

Linear vertical damping constant for independent suspension wheels on axle a, $c_{z_{a^{\prime}}}$ in $\mathrm{Ns} / \mathrm{m}$.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Dependencies

To create this parameter, clear Enable active damping.
Suspension maximum height, Hmax - Height
0.5 (default) | scalar | vector

Maximum suspension extension or minimum suspension compression height, $H_{\text {max }}$, for axle a before the suspension reaches a hardstop, in m .

Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Geometry

Toe angle at steering center, Toe - Toe angle
0.0349 (default) | scalar

Nominal suspension toe angle at zero steering angle, $\zeta_{0 a}$, in rad.
Roll steer vs suspension height slope, RollStrgSIp - Steer angle suspension slope -0. 2269 (default) | scalar | vector

Roll steer angle versus suspension height, $m_{\text {htoe }}^{a_{a}}$, in $\mathrm{rad} / \mathrm{m}$.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

Toe angle vs steering angle slope, ToeStrgSIp - Toe angle steering slope
0.01 (default) | scalar | vector

Toe angle versus steering angle slope, $m_{\text {toesteer }_{d^{\prime}}}$ dimensionless.

Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Dependencies

To create input port StrgAng, set an element of the Steered axle enable by axle, StrgEnByAxl vector to 1 .

Caster angle at steering center, Caster - Caster angle at steering center 0.0698 (default) | scalar

Nominal suspension caster angle at zero steering angle, $\eta_{0 a}$, in rad.
Caster angle vs suspension height slope, CasterHslp - Caster angle versus suspension height slope
-0. 2269 (default) | scalar | vector
Caster angle versus suspension height, $m_{\text {hcaster }_{a^{\prime}}}$ in rad $/ \mathrm{m}$.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

Caster angle vs steering angle slope, CasterStrgSIp - Caster angle versus steering angle slope 0.01 (default) | scalar | vector

Caster angle versus steering angle slope, $m_{\text {castersteer }_{d^{\prime}}}$ dimensionless.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Dependencies

To create input port StrgAng, set an element of the Steered axle enable by axle, StrgEnByAxl vector to 1 .

Camber angle at steering center, Camber - Camber angle at steering center 0.0698 (default) | scalar

Nominal suspension camber angle at zero steering angle, $\xi_{0 a}$, in rad.
Camber angle vs suspension height slope, CamberHslp - Camber angle versus suspension height slope
-0.2269 (default) | scalar | vector
Camber angle versus suspension height, $m_{\text {hcamber }}$, in rad $/ \mathrm{m}$.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

Camber angle vs steering angle slope, CamberStrgSIp - Camber angle versus steering angle slope
0.01 (default) | scalar | vector

Camber angle versus steering angle slope, $m_{\text {cambersteer }{ }_{a}}{ }^{\text {d }}$ dimensionless.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Dependencies

To create input port StrgAng, set an element of the Steered axle enable by axle, StrgEnByAxl vector to 1 .

Suspension height vs steering angle slope, StrgHgtSIp - Suspension height versus steering angle slope
0.1432 (default) | scalar | vector

Steering angle to vertical force slope applied at suspension wheel carrier reference point, $m_{\text {hsteer }}$, in $\mathrm{m} / \mathrm{rad}$.

Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Dependencies

To create input port StrgAng, set an element of the Steered axle enable by axle, StrgEnByAxl vector to 1 .

## Version History <br> Introduced in R2018a

## R2022b: Parameter name change from NumTracksByAxl to NumWhlsByAxl

Behavior changed in R2022b
The Number of tracks by axle, NumTracksByAxl parameter is renamed to Number of wheels by axle, NumWhlsByAxl.

The block uses the number of wheels per axle to index the input and output block signals.

## References

[1] Gillespie, Thomas. Fundamentals of Vehicle Dynamics. Warrendale, PA: Society of Automotive Engineers, 1992.
[2] Vehicle Dynamics Standards Committee. Vehicle Dynamics Terminology. SAE J670. Warrendale, PA: Society of Automotive Engineers, 2008.
[3] Technical Committee. Road vehicles - Vehicle dynamics and road-holding ability - Vocabulary. ISO 8855:2011. Geneva, Switzerland: International Organization for Standardization, 2011.

## Extended Capabilities

## C/C++ Code Generation

Generate C and C++ code using Simulink® Coder ${ }^{\mathrm{TM}}$.

## See Also

Solid Axle Suspension - Coil Spring | Solid Axle Suspension - Leaf Spring | Solid Axle Suspension Mapped

## Solid Axle Suspension - Coil Spring

Solid axle suspension with coil spring


## Libraries:

Vehicle Dynamics Blockset / Suspension

## Description

The Solid Axle Suspension - Coil Spring block implements a solid axle suspension with a coil spring for multiple axles with multiple wheels per axle.

The block models the suspension compliance, damping, and geometric effects as functions of the wheel positions and velocities, with axle-specific compliance and damping parameters. Using the wheel position and velocity, the block calculates the vertical wheel position and suspension forces on the vehicle and wheel. The block uses the Z-down (defined in SAE J670) and a solid axle coordinate system. The solid axle coordinate system, shown here, is aligned with the Z-down vehicle coordinate system, with the $x$-axis in the direction of forward vehicle motion.


| For Each | You Can Specify |
| :--- | :--- |
| Axle | $\bullet \quad$ Multiple wheels |
|  | $\bullet \quad$ Suspension parameters |
| Wheel | $\bullet$ Steering angles |

The block contains energy-storing spring elements and energy-dissipating damper elements. The block also stores energy via the axle roll angular acceleration and axle center of mass vertical and lateral acceleration.

This table summarizes the block parameter settings for a vehicle with:

- Two axles
- Two wheels per axle
- Steering angle input for both wheels on the front axle

| Parameter | Setting |
| :--- | :--- |
| Number of axles, NumAxl | 2 |
| Number of wheels by axle, NumWhlsByAxl | $\left[\begin{array}{ll}2 & 2\end{array}\right]$ |
| Steered axle enable by axle, StrgEnByAxl | $\left[\begin{array}{ll}1 & 0\end{array}\right]$ |

The block uses the wheel number, $t$, to index the input and output signals. This table summarizes the wheel, axle, and corresponding wheel number for a vehicle with:

- Two axles
- Two wheels per axle

| Wheel | Axle | Wheel Number |
| :--- | :--- | :--- |
| Front left | Front | 1 |
| Front right | Front | 2 |
| Rear left | Rear | 1 |
| Rear right | Rear | 2 |

## Suspension Compliance and Damping

The block uses a linear spring and damper to model the vertical dynamic effects of the suspension system on the vehicle and wheel. Specifically, the block:

| Uses | To Calculate |
| :--- | :--- |
| -Longitudinal and lateral displacement and <br> velocity of the vehicle. | -Suspension forces applied to the axle center. <br> - <br> Lortical displacements and velocities of the <br> velocity of the wheel. <br> - Vertical wheel forces applied to the vehicle. |
|  | -vehicle and wheel. <br> Longitudinal, lateral and vertical suspension <br> forces and moments applied to the vehicle. <br> Longitudinal, lateral and vertical suspension <br> forces and moments applied to the wheel. |

To calculate the dynamics of the axle, the block implements these equations. The block neglects the effects of:

- Lateral and longitudinal translational velocity.
- Angular velocity about the vertical and lateral axes.

$$
\begin{aligned}
& {\left[\begin{array}{l}
\ddot{x}_{a} \\
\ddot{y}_{a} \\
\ddot{z}_{a}
\end{array}\right]=\frac{1}{M_{a}}\left[\begin{array}{l}
F_{x a} \\
F_{y a} \\
F_{z a}
\end{array}\right]+\left[\begin{array}{l}
\dot{x}_{a} \\
\dot{y}_{a} \\
\dot{z}_{a}
\end{array}\right] \times\left[\begin{array}{l}
p \\
q \\
r
\end{array}\right]=\frac{1}{M_{a}}\left[\begin{array}{c}
0 \\
0 \\
F_{z a}
\end{array}\right]+\left[\begin{array}{c}
0 \\
0 \\
\dot{z}_{a}
\end{array}\right] \times\left[\begin{array}{l}
p \\
0 \\
0
\end{array}\right]+\left[\begin{array}{l}
0 \\
0 \\
g
\end{array}\right]=\left[\begin{array}{c}
0 \\
p \dot{z}_{a} \\
\frac{F_{z a}}{M_{a}}+g
\end{array}\right]} \\
& {\left[\begin{array}{c}
\dot{p} \\
\dot{q} \\
\dot{r}
\end{array}\right]=\left[\left[\begin{array}{l}
M_{x} \\
M_{y} \\
M_{z}
\end{array}\right]-\left[\begin{array}{c}
p \\
q \\
r
\end{array}\right] \times\left[\begin{array}{ccc}
I_{x x} & 0 & 0 \\
0 & I_{y y} & 0 \\
0 & 0 & I_{z z}
\end{array}\right]\left[\begin{array}{c}
p \\
q \\
r
\end{array}\right]\left[\begin{array}{ccc}
I_{x x} & 0 & 0 \\
0 & I_{y y} & 0 \\
0 & 0 & I_{z z}
\end{array}\right]-1\right.} \\
& =\left[\left[\begin{array}{c}
M_{x} \\
0 \\
0
\end{array}\right]-\left[\begin{array}{c}
p \\
q \\
0
\end{array}\right] \times\left[\begin{array}{ccc}
I_{x x} & 0 & 0 \\
0 & I_{y y} & 0 \\
0 & 0 & I_{z z}
\end{array}\right]\left[\begin{array}{l}
p \\
0 \\
0
\end{array}\right]\left[\begin{array}{ccc}
I_{x x} & 0 & 0 \\
0 & I_{y y} & 0 \\
0 & 0 & I_{z z}
\end{array}\right]^{-1}=\left[\begin{array}{c}
M_{x} \\
\frac{I_{x x}}{} \\
0 \\
0
\end{array}\right]\right.
\end{aligned}
$$

The net vertical force on the axle center of mass is the sum of the wheel and suspension forces acting on the axle.

$$
F_{z a}=\sum_{t=1}^{N t a}\left(F_{w z_{a, t}}+F_{z 0_{a}}+k_{z_{a}}\left(z_{v_{a, t}}-z_{s_{a, t}}+m_{\text {hsteera }}\left|\delta_{s t e e r_{a, t}}\right|\right)+c_{z_{a}}\left(\dot{z}_{v_{a, t}}-\dot{z}_{s_{a, t}}\right)\right)
$$

The net moment about the roll axis of the solid axle suspension accounts for the hardpoint coordinates of the suspension and wheels.

$$
\begin{aligned}
& M_{x}=\sum_{t=1}^{N t a}\left(F_{w z_{a, t}} y_{w_{t}}+\left(F_{z 0_{a}}+k_{z_{a}}\left(z_{v_{a, t}}-z_{s_{a, t}}+m_{h s t e e r_{a}} \mid \delta_{\text {steer }}^{a, t}\right.\right.\right. \\
& \left.\left.+M_{w x_{a, t}} \frac{I_{x x}}{I_{x x}+M_{a} y_{w_{t}}}\right)+c_{z_{a}}\left(\dot{z}_{v_{a, t}}-\dot{z}_{s_{a, t}}\right)\right) y_{s_{t}} \\
&
\end{aligned}
$$

Block parameters provide the track and suspension hardpoints coordinates.

$$
\begin{gathered}
T c_{t}=\left[\begin{array}{lll}
x_{w_{1}} & x_{w_{2}} & \cdots \\
y_{w_{1}} & y_{w_{2}} & \cdots \\
z_{w_{1}} & z_{w_{2}} & \cdots
\end{array}\right] \\
S c_{t}=\left[\begin{array}{lll}
x_{s_{1}} & x_{s_{2}} & \cdots \\
y_{s_{1}} & y_{s_{2}} & \cdots \\
z_{s_{1}} & z_{s_{2}} & \cdots
\end{array}\right]
\end{gathered}
$$

The block uses Euler angles to transform the track and suspension displacements, velocities, and accelerations to the vehicle coordinate system.

To calculate the suspension forces applied to the vehicle, the block implements this equation.

$$
F_{v z_{a, t}}=-\left(F_{z 0_{a}}+k_{z_{a}}\left(z_{v_{a, t}}-z_{s_{a, t}}+m_{h s t e e r_{a}}\left|\delta_{\text {steer }_{a, t}}\right|\right)+c_{z_{a}}\left(\dot{z}_{v_{a, t}}-\dot{z}_{s_{a, t}}\right)+F_{z h s t o p_{a, t}}\right)
$$

The suspension forces and moments applied to the vehicle are equal to the suspension forces and moments applied to the wheel.

$$
\begin{aligned}
& F_{v x_{a, t}}=F_{w x_{a, t}} \\
& F_{v y_{a, t}}=F_{w y_{a, t}} \\
& F_{v x_{a, t}}=-F_{w z_{a, t}} \\
& M_{v x_{a, t}}=M_{w x_{a, t}}+F_{w y_{a, t}}\left(R e_{w y_{a, t}}+H_{a, t}\right) \\
& M_{v y_{a, t}}=M_{w y_{a, t}}+F_{w x_{a, t}}\left(R e_{w x_{a, t}}+H_{a, t}\right) \\
& M_{v x_{a, t}}=M_{w x_{a, t}}
\end{aligned}
$$

To calculate the vertical force applied to the suspension at the wheel location, the block implements a stiff spring-damper, shown here.


The block uses this equation.

$$
F_{w z_{a, t}}=-F w a_{z 0}-k w a_{z}\left(z_{w_{a, t}}-z_{s_{a, t}}\right)-c w a_{z}\left(\dot{z}_{w_{a, t}}-\dot{z}_{s_{a, t}}\right)
$$

The equations use these variables.
$F_{w z_{a}, t} M_{w z_{a, t}} \quad$ Suspension force and moment applied to the wheel on axle a, wheel t along wheel-fixed $z$-axis
$F_{w x_{a, t}} M_{w x_{a t}}$
Suspension force and moment applied to the wheel on axle a, wheel $t$ along wheel-fixed $x$-axis

| $F_{w y_{y_{a},}} M_{w y_{a, t}}$ | Suspension force and moment applied to the wheel on axle a, wheel $t$ along wheel-fixed $y$-axis |
| :---: | :---: |
| $F_{v z_{a, t}} M_{v z_{\text {a }}, t}$ | Suspension force and moment applied to the vehicle on axle a, wheel t along wheel-fixed $z$-axis |
| $F_{v x_{a, t}} M_{v x^{\prime}, t}$ | Suspension force and moment applied to the vehicle on axle a, wheel t along wheel-fixed $x$-axis |
| $F_{v y_{a, t}} M_{v y^{\prime}, t}$ | Suspension force and moment applied to the vehicle on axle a, wheel t along wheel-fixed $y$-axis |
| $F_{z 0_{a}}$ | Vertical suspension spring preload force applied to the wheels on axle a |
| $k_{z_{a}}$ | Vertical spring constant applied to wheels on axle a |
| kwa ${ }_{z}$ | Wheel and axle interface compliance constant |
| $m_{\text {hsteer }}$ | Steering angle to vertical force slope applied at wheel carrier for wheels on axle a |
| $\delta_{\text {steer }}^{\text {a }}$ ${ }_{\text {a }}$ | Steering angle input for axle a, wheel t |
| $C_{z_{a}}$ | Vertical damping constant applied to wheels on axle a |
| cwa ${ }_{z}$ | Wheel and axle interface damping constant |
| $R e_{w_{a, t}}$ | Effective wheel radius for axle $a$, wheel $t$ |
| $F_{z h s t o p a t}$ | Vertical hardstop force at axle a , wheel t , along the vehicle-fixed $z$-axis |
| $F_{\text {zaswy }}^{\text {a }}$, | Vertical anti-sway force at axle a, wheel t , along the vehicle-fixed $z$-axis |
| $F w a_{z 0}$ | Wheel and axle interface compliance constant |
| $z_{v_{a, t}}, \dot{z}_{v_{a, t}}$ | Vehicle displacement and velocity at axle $a$, wheel $t$, along the vehiclefixed $z$-axis |
| $z_{w_{a, t}} \dot{z}_{w_{a}, t}$ | Wheel displacement and velocity at axle $a$, wheel $t$, along the vehicle-fixed $z$-axis |
| $\chi_{v_{a, t}} \dot{\chi}_{v_{a, t}}$ | Vehicle displacement and velocity at axle $a$, wheel $t$, along the vehiclefixed $z$-axis |
| $\chi_{w_{a, t}} \dot{\chi}_{w_{a, t}}$ | Wheel displacement and velocity at axle $a$, wheel t , along the vehicle-fixed $z$-axis |
| $y_{v_{a, t}} \dot{y}_{v_{a, t}}$ | Vehicle displacement and velocity at axle $a$, wheel $t$, along the vehiclefixed $y$-axis |
| $y_{w_{a, t}} \dot{y}_{w_{a, t}}$ | Wheel displacement and velocity at axle $a$, wheel $t$, along the vehicle-fixed $y$-axis |
| $H_{a, t}$ | Suspension height at axle a, wheel t |
| $R e_{w_{a, t}}$ | Effective wheel radius at axle a, wheel t |

## Hardstop Forces

The hardstop feedback force, $F_{\text {zhstop }_{a},}$, that the block applies depends on whether the suspension is compressing or extending. The block applies the force:

- In compression, when the suspension is compressed more than the maximum distance specified by the Suspension maximum height, Hmax parameter.
- In extension, when the suspension extension is greater than maximum extension specified by the Suspension maximum height, Hmax parameter.

To calculate the force, the block uses a stiffness based on a hyperbolic tangent and exponential scaling.

## Camber, Caster, and Toe Angles

To calculate the camber, caster, and toe angles, block uses linear functions of the suspension height and steering angle.

$$
\begin{aligned}
& \xi_{a, t}=\xi_{0 a}+m_{\text {hcamber }_{a}}\left(z_{w_{a, t}}-z_{v_{a, t}}-m_{\text {hsteer }_{a}}\left|\delta_{\text {steer }_{a, t}}\right|\right)+m_{\text {cambersteer }_{a}}\left|\delta_{\text {steer }_{a, t}}\right| \\
& \eta_{a, t}=\eta_{0 a}+m_{\text {hcaster }_{a}}\left(z_{w_{a, t}}-z_{v_{a, t}}-m_{\text {hsteer }_{a}}\left|\delta_{\text {steer }_{a, t}}\right|\right)+m_{\text {castersteer }_{a}}\left|\delta_{\text {steer }_{a, t}}\right| \\
& \zeta_{a, t}=\zeta_{0 a}+m_{\text {htee }_{a}}\left(z_{w_{a, t}}-z_{v_{a, t}}-m_{\text {hsteer }_{a}}\left|\delta_{\text {steer }_{a, t}}\right|\right)+m_{\text {toesteer }_{a}}\left|\delta_{\text {steer }_{a, t}}\right|
\end{aligned}
$$

The equations use these variables.

| $\xi_{a, t}$ | Camber angle of wheel on axle a, wheel t |
| :---: | :---: |
| $\eta_{a, t}$ | Caster angle of wheel on axle a, wheel t |
| $\zeta_{a, t}$ | Toe angle of wheel on axle $a$, wheel $t$ |
| $\xi_{0 a}, \eta_{0 a}, \zeta_{0 a}$ | Nominal suspension axle a camber, caster, and toe angles, respectively, at zero steering angle |
| $m_{\text {hcamber }_{a^{\prime}}} m_{\text {hcaster }_{a^{\prime}}}$ $m_{\text {htoe }_{a}}$ | Camber, caster, and toe angles, respectively, versus suspension height slope for axle a |
| $m_{\text {camberster }_{a^{\prime}}} m_{\text {castersteer }_{a^{\prime}}}$ <br> $m_{\text {toesteer }}$ | Camber, caster, and toe angles, respectively, versus steering angle slope for axle a |
| $m_{\text {hsteer }}$ | Steering angle versus vertical force slope for axle a |
| $\delta_{\text {stee }}^{\text {at, }}$ | Steering angle input for axle a, wheel t |
| $z_{v_{a t}}$ | Vehicle displacement at axle a , wheel t , along the vehicle-fixed $z$-axis |
| $z_{w_{a, t}}$ | Wheel displacement at axle a , wheel t , along the vehicle-fixed $z$-axis |

## Steering Angles

Optionally, use the Steered axle enable by axle, StrgEnByAxl parameter to input steering angles for the wheels. To calculate the steering angles for the wheels, the block offsets the input steering angles with a linear function of the suspension height.

$$
\delta_{\text {whlsteer }_{a, t}}=\delta_{\text {steer }_{a, t}}+m_{\text {htoe }_{a}}\left(z_{w_{a, t}}-z_{v_{a, t}}-m_{\text {hsteer }_{a}}\left|\delta_{\text {steer }_{a, t}}\right|\right)+m_{\text {toesteer }_{a}}\left|\delta_{\text {steer }_{a, t}}\right|
$$

The equation uses these variables.

| $m_{\text {toesteer }_{a}}$ | Axle a toe angle versus steering angle slope |
| :--- | :--- |
| $m_{\text {hsteer }_{a}}$ | Axle a steering angle versus vertical force slope |
| $m_{\text {htoe }_{a}}$ | Axle a toe angle versus suspension height slope |
| $\delta_{\text {whlster }_{a, t}}$ | Wheel steering angle for axle a, wheel t |
| $\delta_{\text {steer }_{a, t}}$ | Steering angle input for axle a, wheel t |
| $z_{v_{a, t}}$ | Vehicle displacement at axle a, wheel t, along the vehicle-fixed $z$-axis |

$z_{w_{a, t}} \quad$ Wheel displacement at axle a , wheel t , along the vehicle-fixed $z$-axis

## Power and Energy

The block calculates these suspension characteristics for each axle, $a$, wheel, $t$.

| Calculation | Equation |
| :---: | :---: |
| Dissipated power, $P_{\text {susp }_{a, t}}$ | $P_{\text {susp }_{a, t}}=F_{\text {wzlookup }}\left(\dot{z}_{v_{a, t}}-\dot{z}_{w_{a, t} t^{\prime}} \dot{z}_{v_{a, t}}-\dot{z}_{w_{a, t^{\prime}}} \delta_{\text {steer }_{a, t}}\right)$ |
| Absorbed energy, $E_{\text {susp }_{\text {a,t }}}$ | $E_{\text {susp }_{a, t}}=F_{\text {wzlookup }}\left(\dot{z}_{v_{a, t}}-\dot{z}_{w_{a, t}} \dot{z}_{v_{a, t}}-\dot{z}_{w_{a, t^{\prime}}} \delta_{\text {steer }}^{a, t}\right.$ $)$ |
| Suspension height, $H_{a, t}$ | $H_{a, t}=-\left(z_{v_{a, t}}-z_{w_{a, t}}+\frac{F_{z 0_{a}}}{k_{z_{a}}}+m_{\text {hsteer }_{a}}\left\|\delta_{\text {steer }_{a, t}}\right\|\right)$ |
| Distance from wheel carrier center to tire/road interface | $z_{w t r_{a, t}}=R e_{w_{a, t}}+H_{a, t}$ |

The equations use these variables.

| $m_{h s t e e r_{a}}$ | Steering angle to vertical force slope applied at wheel carrier for wheels on axle a |
| :--- | :--- |
| $\delta_{s t e e r_{a, t}}$ | Steering angle input for axle a, wheel t |
| $R e_{w_{a, t}}$ | Axle a, wheel t effective wheel radius from wheel carrier center to tire/road <br> interface |
| $F_{z 0_{a}}$ | Vertical suspension spring preload force applied to the wheels on axle a |
| $z_{w t r_{a, t}}$ | Distance from wheel carrier center to tire/road interface, along the vehicle-fixed $z$ - <br> axis |
| $z_{v_{a, t}}, \dot{z}_{v_{a, t}}$ | Vehicle displacement and velocity at axle a, wheel $t$, along the vehicle-fixed $z$-axis <br> $z_{w_{a, t}}$ |
| $\dot{z}_{w_{a, t}}$ | Wheel displacement and velocity at axle a, wheel $t$, along the vehicle-fixed $z$-axis |

## Ports

## Input

WhIPz - Wheel z-axis displacement
array
Wheel displacement, $z_{w}$, along wheel-fixed $z$-axis, in $m$. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlPz:

- Signal array dimensions are [1x4].

$$
\mathrm{WhlPz}=z_{w}=\left[\begin{array}{llll}
z_{w_{1,1}} & z_{w_{1,2}} & z_{w_{2,1}} & z_{w_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlPz $(1,1)$ | 1 | 1 |
| Front right | WhlPz $(1,2)$ | 1 | 2 |


| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Rear left | WhlPz $(1,3)$ | 2 | 1 |
| Rear right | WhlPz $(1,4)$ | 2 | 2 |

WhIRe - Wheel effective radius
array
Effective wheel radius, $R e_{w}$, in m. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlRe:

- Signal array dimensions are [1×4].

$$
\text { WhlRe }=R e_{w}=\left[\begin{array}{ll}
R e_{w_{1,1}} & R e_{w_{1,2}}
\end{array} R e_{w_{2,1}} R e_{w_{2,2}}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlRe $(1,1)$ | 1 | 1 |
| Front right | WhlRe $(1,2)$ | 1 | 2 |
| Rear left | WhlRe $(1,3)$ | 2 | 1 |
| Rear right | WhlRe $(1,4)$ | 2 | 2 |

WhIVz - Wheel z-axis velocity array

Wheel velocity, $\dot{z}_{w}$, along wheel-fixed $z$-axis, in m. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlVz:

- Signal array dimensions are [1×4].

$$
\text { WhlVz }=\dot{z}_{w}=\left[\begin{array}{lll}
\dot{z}_{1,1} & \dot{z}_{w_{1,2}} & \dot{z}_{w_{2,1}} \\
\dot{z}_{w_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlVz $(1,1)$ | 1 | 1 |
| Front right | WhlVz $(1,2)$ | 1 | 2 |
| Rear left | WhlVz $(1,3)$ | 2 | 1 |
| Rear right | WhlVz $(1,4)$ | 2 | 2 |

WhIFx - Longitudinal wheel force on vehicle
array
Longitudinal wheel force applied to vehicle, $F_{w x}$, along the vehicle-fixed $x$-axis. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlFx:

- Signal array dimensions are [1×4].

WhlFx $=F_{w x}=\left[F_{w x_{1,1}} F_{w x_{1,2}} F_{w x_{2,1}} F_{w x_{2,2}}\right]$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlFx $(1,1)$ | 1 | 1 |
| Front right | WhlFx $(1,2)$ | 1 | 2 |
| Rear left | WhlFx $(1,3)$ | 2 | 1 |
| Rear right | WhlFx $(1,4)$ | 2 | 2 |

WhIFy - Lateral wheel force on vehicle
array
Lateral wheel force applied to vehicle, $F_{w y}$, along the vehicle-fixed $y$-axis. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlFy:

- Signal array dimensions are [1×4].

WhlFy $=F_{w y}=\left[F_{w y 1,1} F_{w y 1,2} F_{w y 2,1} F_{w y_{2,2}}\right]$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlFy $(1,1)$ | 1 | 1 |
| Front right | WhlFy $(1,2)$ | 1 | 2 |
| Rear left | WhlFy $(1.3)$ | 2 | 1 |
| Rear right | WhlFy $(1,4)$ | 2 | 2 |

WhIM - Suspension moment on wheel
array
Longitudinal, lateral, and vertical suspension moments at axle a, wheel $t$, applied to the wheel at the axle wheel carrier reference coordinate, in $\mathrm{N} \cdot \mathrm{m}$. Input array dimensions are 3 by the number of wheels on the vehicle.

- WhlM (1, . . ) - Suspension moment applied to the wheel about the vehicle-fixed $x$-axis (longitudinal)
- WhlM ( $2, \ldots$ ) - Suspension moment applied to the wheel about the vehicle-fixed $y$-axis (lateral)
- WhlM $(3, \ldots)$ - Suspension moment applied to the wheel about the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the WhlM:

- Signal dimensions are [3×4].
- Signal contains suspension moments applied to four wheels according to their axle and wheel locations.

$$
\text { WhlM }=M_{w}=\left[\begin{array}{lllll}
M_{w x_{1,1}} & M_{w x_{1}, 2} & M_{w x_{2}, 1} & M_{w x_{2,2}} \\
M_{w y_{1,1}} & M_{w y_{1,2}} & M_{w y 2,1} & M_{w y 2,2} \\
M_{w z_{1,1}} & M_{w z_{1,2}} & M_{w z_{2,1}} & M_{w z_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Moment Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | WhlM(1,1) | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front <br> right | WhlM(1,2) | 1 | 2 |  |
| Rear <br> left | WhlM(1,3) | 2 | 1 |  |
| Rear <br> right | WhlM(1,4) | 2 | 2 |  |
| Front <br> left | WhlM(2,1) | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front <br> right | WhlM(2,2) | 1 | 2 |  |
| Rear <br> left | WhlM(2,3) | 2 | 1 |  |
| Rear <br> right | WhlM(2,4) | 2 | 2 |  |
| Front <br> left | WhlM(3,1) | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front <br> right | WhlM(3,2) | 1 | 2 |  |
| Rear <br> left | WhlM(3,3) | 2 | 1 |  |
| Rear <br> right | WhlM(3,4) | 2 | 2 |  |

VehP - Vehicle displacement
array
Vehicle displacement from axle a, wheel $t$ along vehicle-fixed coordinate system, in m. Input array dimensions are 3 the number of wheels on the vehicle.

- $\operatorname{VehP}(1, \ldots)$ - Vehicle displacement from wheel, $x_{v}$, along the vehicle-fixed $x$-axis
- $\operatorname{VehP}(2, \ldots)$ - Vehicle displacement from wheel, $y_{v}$, along the vehicle-fixed $y$-axis
- $\operatorname{VehP}(3, \ldots)-$ Vehicle displacement from wheel, $z_{v}$, along the vehicle-fixed $z$-axis

For example, for a two-axle vehicle with two wheels per axle, the VehP:

- Signal dimensions are [3×4].
- Signal contains four displacements according to their axle and wheel locations.

$$
\text { VehP }=\left[\begin{array}{l}
x_{v} \\
y_{v} \\
z_{v}
\end{array}\right]=\left[\begin{array}{llll}
x_{v_{1,1}} & x_{v_{1,2}} & x_{v_{2,1}} & x_{v_{2,2}} \\
y_{v_{1,1}} & y_{v_{1,2}} & v_{v_{2,1}} & v_{v_{2,2}} \\
z_{v_{1,1}} & z_{v_{1,2}} & z_{v_{2,1}} & z_{v_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | VehP $(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis |
| Front <br> right | VehP $(1,2)$ | 1 | 2 |  |
| Rear <br> left | VehP $(1,3)$ | 2 | 1 |  |
| Rear <br> right | VehP(1,4) | 2 | 2 |  |
| Front <br> left | VehP $(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis |
| Front <br> right | VehP $(2,2)$ | 1 | 2 |  |
| Rear <br> left | VehP $(2,3)$ | 2 | 1 |  |
| Rear <br> right | $\operatorname{VehP}(2,4)$ | 2 | 2 |  |
| Front <br> left | $\operatorname{VehP}(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis |
| Front <br> right | $\operatorname{VehP}(3,2)$ | 1 | 2 |  |
| Rear <br> left | $\operatorname{VehP}(3,3)$ | 2 | 1 |  |
| Rear <br> right | $\operatorname{VehP}(3,4)$ | 2 | 2 |  |

VehV - Vehicle velocity
array
Vehicle velocity at axle $a$, wheel $t$ along vehicle-fixed coordinate system, in $m$. Input array dimensions are 3 by the number of wheels on the vehicle.

- VehV $(1, \ldots)$ - Vehicle velocity at wheel, $x_{v}$, along the vehicle-fixed $x$-axis
- VehV $(2, \ldots)$ - Vehicle velocity at wheel, $y_{v}$, along the vehicle-fixed $y$-axis
- $\operatorname{VehV}(3, \ldots)-$ Vehicle velocity at wheel, $z_{v}$, along the vehicle-fixed $z$-axis

For example, for a two-axle vehicle with two wheels per axle, the VehV:

- Signal dimensions are [3×4].
- Signal contains 4 velocities according to their axle and wheel locations.

$$
\text { VehV }=\left[\begin{array}{l}
\dot{x}_{v} \\
\dot{y}_{v} \\
\dot{z}_{v}
\end{array}\right]=\left[\begin{array}{llll}
\dot{x}_{v_{1,1}} & \dot{x}_{v_{1,2}} & \dot{x}_{v_{2,1}} & \dot{x}_{v_{2,2}} \\
\dot{y}_{v_{1,1}} & \dot{y}_{v_{1,2}} & \dot{y}_{v_{2,1}} & \dot{y}_{v_{2,2}} \\
\dot{z}_{v_{1,1}} & \dot{z}_{v_{1,2}} & \dot{z}_{v_{2,1}} & \dot{z}_{v_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel Numbe r | Axis |
| :---: | :---: | :---: | :---: | :---: |
| Front left | $\operatorname{VehV}(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis |
| Front right | $\operatorname{VehV}(1,2)$ | 1 | 2 |  |
| Rear left | $\operatorname{VehV}(1,3)$ | 2 | 1 |  |
| Rear right | $\operatorname{VehV}(1,4)$ | 2 | 2 |  |
| Front left | $\operatorname{VehV}(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis |
| Front right | $\operatorname{VehV}(2,2)$ | 1 | 2 |  |
| $\begin{array}{\|l} \begin{array}{l} \text { Rear } \\ \text { left } \end{array} \\ \hline \end{array}$ | $\operatorname{VehV}(2,3)$ | 2 | 1 |  |
| Rear right | $\operatorname{VehV}(2,4)$ | 2 | 2 |  |
| Front left | $\operatorname{VehV}(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis |
| Front right | $\operatorname{VehV}(3,2)$ | 1 | 2 |  |
| Rear left | $\operatorname{VehV}(3,3)$ | 2 | 1 |  |
| Rear right | $\operatorname{VehV}(3,4)$ | 2 | 2 |  |

StrgAng - Steering angle, optional
array
Optional steering angle for each wheel, $\delta$. Input array dimensions are 1 by the number of steered wheels.

For example, for a two-axle vehicle with two wheels per axle, you can input steering angles for both wheels on the first axle.

- To create the StrgAng port, set Steered axle enable by axle, StrgEnByAxl to [1 0]. The input signal array dimensions are [1×2].
- The StrgAng signal contains two steering angles according to their axle and wheel locations.

$$
\text { StrgAng }=\delta_{\text {steer }}=\left[\delta_{\text {steer }_{1,1}} \delta_{\text {steer }_{1,2}}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | StrgAng $(1,1)$ | 1 | 1 |
| Front right | StrgAng $(1,2)$ | 1 | 2 |

## Dependencies

To create input port StrgAng, set an element of the Steered axle enable by axle, StrgEnByAxl vector to 1 .

## Output

Info - Bus signal
bus
Bus signal containing block values. The signals are arrays that depend on the wheel location.
For example, here are the indices for a two-axle, two-wheel vehicle. The total number of wheels is four.

- 1D array signal (1-by-4)

| Array Element | Axle | Wheel Number |
| :--- | :--- | :--- |
| $(1,1)$ | 1 | 1 |
| $(1,2)$ | 1 | 2 |
| $(1,3)$ | 2 | 1 |
| $(1,4)$ | 2 | 2 |

- 3D array signal (3-by-4)

| Array Element | Axle | Wheel Number |
| :--- | :--- | :--- |
| $(1,1)$ | 1 | 1 |
| $(1,2)$ | 1 | 2 |
| $(1,3)$ | 2 | 1 |
| $(1,4)$ | 2 | 2 |
| $(2,1)$ | 1 | 1 |
| $(2,2)$ | 1 | 2 |
| $(2,3)$ | 2 | 1 |
| $(2,4)$ | 2 | 2 |
| $(3,1)$ | 1 | 1 |
| $(3,2)$ | 1 | 2 |
| $(3,3)$ | 2 | 1 |
| $(3,4)$ | 2 | 2 |


| Signal | Description | Array Signal | Variable | Units |
| :---: | :---: | :---: | :---: | :---: |
| Camber | Wheel angles according to the axle. | 1D | WhlAng $[1, \ldots]=\xi=\left[\xi_{a, t}\right]$ | rad |
| Caster |  |  | WhlAng $[2, \ldots]=\eta=\left[\eta_{a, t}\right]$ |  |
| Toe |  |  | WhlAng $[3, \ldots]=\zeta=\left[\zeta_{a, t}\right]$ |  |
| Height | Suspension height | 1D | H | m |


| Signal | Description | Array Signal | Variable | Units |
| :---: | :---: | :---: | :---: | :---: |
| Power | Suspension power dissipation | 1D | $P_{\text {susp }}$ | W |
| Energy | Suspension absorbed energy | 1D | $E_{\text {susp }} \mathrm{J}$ | J |
| VehF | Suspension forces applied to the vehicle | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { VehF }=F_{v}= \\ & {\left[\begin{array}{llll} F_{v x_{1,1}} & F_{v x_{1,2}} & F_{v x_{2,1}} & F_{v x_{2}, 2} \\ F_{v v_{1,1}} & F_{v v_{1,2}} & F_{v v_{2,1}} & F_{v y_{2,2}} \\ F_{v z 1,1} & F_{v z_{1,2}} & F_{v z_{2,1}} & F_{v z_{2,2}} \end{array}\right.} \end{aligned}$ | $\mathrm{N}$ |
| VehM | Suspension moments applied to vehicle | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { VehM }=M_{v}= \\ & {\left[\begin{array}{lllll} M_{v x_{1}, 1} & M_{v x_{1}, 2} & M_{v x_{2}, 1} & M_{v \times 2} \\ M_{v y_{1}, 1} & M_{v y_{1}, 2} & M_{v y 2,1} & M_{v y 2} \\ M_{v z_{1,1}} & M_{v z_{1,2}} & M_{v z_{2,1}} & M_{v z_{2}} \end{array}\right.} \end{aligned}$ | $\mathrm{N} \cdot \mathrm{~m}$ <br> 2,2 <br> 2,2 <br> 2,2 |


| Signal | Description | Array Signal | Variable | Units |
| :---: | :---: | :---: | :---: | :---: |
| WhlF | Suspension force applied to wheel | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { WhlF }=F_{w}= \\ & {\left[\begin{array}{llll} F_{w x_{1}, 1} & F_{w x_{1,2}} & F_{w x_{2,1}} & F_{w x_{2}} \\ F_{w y 1,1} & F_{w y_{1,2}} & F_{w y 2,1} & F_{w y 2} \\ F_{w z_{1,1}} & F_{w z_{1,2}} & F_{w z 2,1} & F_{w z_{2}} \end{array}\right.} \end{aligned}$ |  |
| WhlP | Wheel displacement | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { WhlP }=\left[\begin{array}{l} x_{w} \\ y_{w} \\ z_{w} \end{array}\right]= \\ & {\left[\begin{array}{cccc} x_{w_{1,1}} & x_{w_{1,2}} & x_{w_{2,1}} & x_{w_{2}} \\ y_{w_{1,1}} & y_{w_{1,2}} & y_{w_{2,1}} & y_{w y} \\ z_{w t r_{1,1}} & z_{w t r_{1,2}} & z_{w t r_{2,1}} & z_{w t r} \end{array}\right.} \end{aligned}$ |  |
| WhlV | Wheel velocity | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { WhlV }=\left[\begin{array}{l} \dot{x}_{w} \\ \dot{y}_{w} \\ \dot{z}_{w} \end{array}\right] \\ & = \\ & {\left[\begin{array}{lll} \dot{x}_{w_{1,1}} & \dot{x}_{w_{1,2}} & \dot{x}_{w_{2,1}} \\ \dot{x}_{w_{2,2}} \\ \dot{y}_{w_{1,1}} & \dot{y}_{w_{1,2}} \dot{y}_{w_{2,1}} & \dot{y}_{w_{2,2}} \\ \dot{z}_{w_{1,1}} & \dot{z}_{w_{1,2}} & \dot{z}_{w_{2,1}} \\ \dot{z}_{w_{2,2}} \end{array}\right]} \end{aligned}$ | m/s |


| Signal | Description | Array Signal | Variable | Units |
| :---: | :---: | :---: | :---: | :---: |
| WhlAng | Wheel camber, caster toe angles | 3D | For a two-axle, two wheels per axle vehicle: $\left.\begin{array}{l} \text { WhlAng }=\left[\begin{array}{l} \xi \\ \eta \\ \zeta \end{array}\right] \\ =\left[\begin{array}{lll} \xi_{1,1} & \xi_{1,2} & \xi_{2,1} \\ \xi_{2,2} \\ \eta_{1,1} & \eta_{1,2} & \eta_{2,1} \\ \eta_{2,2} \\ \zeta_{1,1} & \zeta_{1,2} & \zeta_{2,1} \end{array} \zeta_{2,2}\right. \end{array}\right] . \begin{aligned} & \eta_{2} \end{aligned}$ | rad |

## VehF - Suspension force on vehicle

array
Longitudinal, lateral, and vertical suspension force at axle a, wheel $t$, applied to the vehicle at the suspension connection point, in N . Array dimensions are 3 by the number of wheels on the vehicle.

- $\operatorname{VehF}(1, \ldots)$ - Suspension force applied to vehicle along the vehicle-fixed $x$-axis (longitudinal)
- $\operatorname{VehF}(2, \ldots)$ - Suspension force applied to vehicle along the vehicle-fixed $y$-axis (lateral)
- $\operatorname{VehF}(3, \ldots)$ - Suspension force applied to vehicle along the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the VehF:

- Signal dimensions are [3×4].
- Signal contains suspension forces applied to the vehicle according to the axle and wheel locations.

$$
\text { VehF }=F_{v}=\left[\begin{array}{lllll}
F_{v x_{1,1}} & F_{v x_{1,2}} & F_{v x_{2,1}} & F_{v x_{2,2}} \\
F_{v y_{1,1}} & F_{v y_{1,2}} & F_{v y_{2,1}} & F_{v y_{2,2}} \\
F_{v z_{1,1}} & F_{v z_{1,2}} & F_{v z_{2,1}} & F_{v z_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | $\operatorname{VehF}(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front <br> right | $\operatorname{VehF}(1,2)$ | 1 | 2 |  |
| Rear <br> left | $\operatorname{VehF}(1,3)$ | 2 | 1 |  |
| Rear <br> right | $\operatorname{VehF}(1,4)$ | 2 | 2 |  |
| Front <br> left | $\operatorname{VehF}(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front <br> right | $\operatorname{VehF}(2,2)$ | 1 | 2 |  |


| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Rear <br> left | $\operatorname{VehF}(2,3)$ | 2 | 1 |  |
| Rear <br> right | $\operatorname{VehF}(2,4)$ | 2 | 2 |  |
| Front <br> left | $\operatorname{VehF}(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front <br> right | $\operatorname{VehF}(3,2)$ | 1 | 2 |  |
| Rear <br> left | $\operatorname{VehF}(3,3)$ | 2 | 1 |  |
| Rear <br> right | $\operatorname{VehF}(3,4)$ | 2 | 2 |  |

VehM - Suspension moment on vehicle array

Longitudinal, lateral, and vertical suspension moment at axle a, wheel $t$, applied to the vehicle at the suspension connection point, in $\mathrm{N} \cdot \mathrm{m}$. Array dimensions are 3 by the number of wheels on the vehicle.

- VehM (1, ...) - Suspension moment applied to the vehicle about the vehicle-fixed $x$-axis (longitudinal)
- VehM ( $2, \ldots$ ) - Suspension moment applied to the vehicle about the vehicle-fixed $y$-axis (lateral)
- Vehm ( $3, \ldots$ ) - Suspension moment applied to the vehicle about the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the VehM:

- Signal dimensions are [3×4].
- Signal contains suspension moments applied to vehicle according to the axle and wheel locations.

VehM $=M_{v}=\left[\begin{array}{lllll}M_{v x_{1,1}} & M_{v x_{1,2}} & M_{v x_{2,1}} & M_{v x_{2,2}} \\ M_{v y_{1,1}} & M_{v y_{1,2}} & M_{v y_{2,1}} & M_{v y_{2,2}} \\ M_{v z_{1,1}} & M_{v z_{1,2}} & M_{v z_{2,1}} & M_{v z_{2,2}}\end{array}\right]$

| Array Element | Axle | Wheel <br> Number | Moment Axis |
| :--- | :--- | :--- | :--- |
| $\operatorname{VehM}(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| $\operatorname{VehM}(1,2)$ | 1 | 2 |  |
| $\operatorname{VehM}(1,3)$ | 2 | 1 |  |
| $\operatorname{VehM}(1,4)$ | 2 | 2 |  |
| $\operatorname{VehM}(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| $\operatorname{VehM}(2,2)$ | 1 | 2 |  |


| Array Element | Axle | Wheel <br> Number | Moment Axis |
| :--- | :--- | :--- | :--- |
| $\operatorname{VehM}(2,3)$ | 2 | 1 |  |
| $\operatorname{VehM}(2,4)$ | 2 | 2 |  |
| $\operatorname{VehM}(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| $\operatorname{VehM}(3,2)$ | 1 | 2 |  |
| $\operatorname{VehM}(3,3)$ | 2 | 1 |  |
| $\operatorname{VehM}(3,4)$ | 2 | 2 |  |

WhIF - Suspension force on wheel
array
Longitudinal, lateral, and vertical suspension forces at axle a, wheel $t$, applied to the wheel at the axle wheel carrier reference coordinate, in N . Array dimensions are 3 by the number of wheels on the vehicle.

- $\operatorname{WhlF}(1, \ldots)$ - Suspension force on wheel along the vehicle-fixed $x$-axis (longitudinal)
- $\operatorname{WhlF}(2, \ldots)$ - Suspension force on wheel along the vehicle-fixed $y$-axis (lateral)
- WhlF $(3, \ldots)$ - Suspension force on wheel along the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the WhlF:

- Signal dimensions are [3×4].
- Signal contains wheel forces applied to the vehicle according to the axle and wheel locations.

WhlF $=F_{w}=\left[\begin{array}{lllll}F_{w x_{1,1}} & F_{w x_{1,2}} & F_{w x_{2,1}} & F_{w x_{2,2}} \\ F_{w y_{1,1}} & F_{w y_{1,2}} & F_{w y_{2,1}} & F_{w y_{2,2}} \\ F_{w z_{1,1}} & F_{w z_{1,2}} & F_{w z_{2,1}} & F_{w z_{2,2}}\end{array}\right]$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | WhlF $(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front <br> right | WhlF $(1,2)$ | 1 | 2 |  |
| Rear <br> left | WhlF $(1,3)$ | 2 | 1 |  |
| Rear <br> right | WhlF $(1,4)$ | 2 | 2 |  |
| Front <br> left | WhlF $(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front <br> right | WhlF $(2,2)$ | 1 | 2 |  |


| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Rear <br> left | WhlF $(2,3)$ | 2 | 1 |  |
| Rear <br> right | WhlF $(2,4)$ | 2 | 2 |  |
| Front <br> left | WhlF (3,1) | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front <br> right | WhlF (3,2) | 1 | 2 |  |
| Rear <br> left | WhlF $(3,3)$ | 2 | 1 |  |
| Rear <br> right | WhlF (3,4) | 2 | 2 |  |

WhIV - Wheel velocity
array
Longitudinal, lateral, and vertical wheel velocity at axle a, wheel t , in $\mathrm{m} / \mathrm{s}$. Array dimensions are 3 by the number of wheels on the vehicle.

- WhlV $(1, \ldots)$ - Wheel velocity along the vehicle-fixed $x$-axis (longitudinal)
- WhlV $(2, \ldots)$ - Wheel velocity along the vehicle-fixed $y$-axis (lateral)
- WhlV $(3, \ldots)-$ Wheel velocity along the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the Whlv:

- Signal dimensions are [3×4].
- Signal contains wheel forces applied to the vehicle according to the axle and wheel locations.

$$
\text { WhlV }=\left[\begin{array}{l}
\dot{x}_{w} \\
\dot{y}_{w} \\
\dot{z}_{w}
\end{array}\right]=\left[\begin{array}{llll}
\dot{x}_{w_{1,1}} & \dot{x}_{w_{1,2}} & \dot{x}_{w_{2,1}} & \dot{x}_{w_{2,2}} \\
\dot{y}_{w_{1,1}} & \dot{y}_{w_{1,2}} & \dot{y}_{w_{2,1}} & \dot{y}_{w_{2,2}} \\
\dot{z}_{w_{1,1}} & \dot{z}_{w_{1,2}} & \dot{z}_{w_{2,1}} & \dot{z}_{w_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | WhlV $(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front <br> right | WhlV $(1,2)$ | 1 | 2 |  |
| Rear <br> left | WhlV $(1,3)$ | 2 | 1 |  |
| Rear <br> right | WhlV $(1,4)$ | 2 | 2 |  |


| Wheel | Array Element | Axle | Wheel Numbe r | Force Axis |
| :---: | :---: | :---: | :---: | :---: |
| Front left | WhlV (2,1) | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front right | WhlV (2,2) | 1 | 2 |  |
| Rear left | WhlV (2,3) | 2 | 1 |  |
| Rear right | WhlV (2,4) | 2 | 2 |  |
| Front left | WhlV (3,1) | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front right | WhlV (3,2) | 1 | 2 |  |
| Rear left | WhlV (3, 3) | 2 | 1 |  |
| Rear right | WhlV(3,4) | 2 | 2 |  |

WhIAng - Wheel camber, caster, toe angles
array
Camber, caster, and toe angles at axle $a$, wheel $t$, in rad. Array dimensions are 3 by the number of wheels on the vehicle.

- WhlAng (1,...) - Camber angle
- WhlAng ( $2, \ldots$ ) - Caster angle
- Whlang $(3, \ldots)$ - Toe angle

For example, for a two-axle vehicle with two wheels per axle, the WhlAng:

- Signal dimensions are [3×4].
- Signal contains angles according to the axle and wheel locations.

$$
\text { WhlAng }=\left[\begin{array}{l}
\xi \\
\eta \\
\zeta
\end{array}\right]=\left[\begin{array}{llll}
\xi_{1,1} & \xi_{1,2} & \xi_{2,1} & \xi_{2,2} \\
\eta_{1,1} & \eta_{1,2} & \eta_{2,1} & \eta_{2,2} \\
\zeta_{1,1} & \zeta_{1,2} & \zeta_{2,1} & \zeta_{2,2}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Angle |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | WhlAng (1,1) | 1 | 1 | Camber |
| Front <br> right | WhlAng (1,2) | 1 | 2 |  |


| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Angle |
| :--- | :--- | :--- | :--- | :--- |
| Rear <br> left | WhlAng (1,3) | 2 | 1 |  |
| Rear <br> right | WhlAng (1,4) | 2 | 2 |  |
| Front <br> left | WhlAng (2,1) | 1 | 1 | Caster |
| Front <br> right | WhlAng (2,2) | 1 | 2 |  |
| Rear <br> left | WhlAng (2,3) | 2 | 1 |  |
| Rear <br> right | WhlAng(2,4) | 2 | 2 |  |
| Front <br> left | WhlAng(3,1) | 1 | 1 | Toe |
| Front <br> right | WhlF(3,2) | 1 | 2 |  |
| Rear <br> left | WhlF(3,3) | 2 | 1 |  |
| Rear <br> right | WhlF(3,4) | 2 | 2 |  |

## Parameters

## Axles

Number of axles, NumAxI - Number of axles
2 (default) | scalar
Number of axles, $N_{a}$, dimensionless.
Number of wheels by axle, NumWhlsByAxI - Number of wheels per axle
[2 2] (default)|vector
Number of wheels per axle, $N t_{a}$, dimensionless. Vector is 1 by the number of vehicle axles, $N_{a}$. For example, [1,2] represents one wheel on axle one and two wheels on axle two.

Steered axle enable by axle, StrgEnByAxI - Boolean vector to enable axle steering
[1 0] (default) | vector
Boolean vector that enables axle steering, $E n_{\text {steer }}$, dimensionless. Vector is 1 by the number of vehicle axles, $N_{a}$. For example:

- [llllle $\left.\begin{array}{l}1 \\ \hline\end{array}\right]$ For a two-axle vehicle, enables axle one steering and disables axle two steering
- [1 1]-For a two-axle vehicle, enables axle one and axle two steering


## Dependencies

Setting an element of the Steered axle enable by axle, StrgEnByAxl vector to 1:

- Creates input port StrgAng.
- Creates these parameters
- Toe angle vs steering angle slope, ToeStrgSlp
- Caster angle vs steering angle slope, CasterStrgSlp
- Camber angle vs steering angle slope, CamberStrgSlp
- Suspension height vs steering angle slope, StrgHgtSlp

For example, for a two-axle vehicle with two wheels per axle, you can input steering angles for both wheels on the first axle.

- To create the StrgAng port, set Steered axle enable by axle, StrgEnByAxl to [1 0]. The input signal array dimensions are [1x2].
- The StrgAng signal contains two steering angles according to their axle and wheel locations.

$$
\text { StrgAng }=\delta_{\text {steer }}=\left[\delta_{\text {steer }_{1,1}} \delta_{\text {steer }_{1}, 2}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | StrgAng (1, 1) | 1 | 1 |
| Front right | StrgAng (1,2) | 1 | 2 |

Axle and wheels lumped principal moments of inertia about longitudinal axis, AxIIxx Inertia
300 (default) | vector
Axle and wheels lumped principal moments of inertia about longitudinal axis, AxleIxx $a$, in $\mathrm{kg}^{*} \mathrm{~m} \wedge 2$.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Axle and wheels lumped mass, AxIM - Mass

[2 2] (default)|vector
Axle and wheels lumped mass, $a$, in kg.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Track hardpoint coordinates relative to axle center, TrackCoords - Point

[0 0 0 0;-1 1 -1 1;0 0 0 0] (default)|array
Track hardpoint coordinates, $T c_{t}$, along the solid axle $x, y$, and $z$-axes, in m .
For example, for a two-axle vehicle with two wheels per axle, the TrackCoords array:

- Dimensions are [3x4].
- Contains four track hardpoint coordinates according to their axle and wheel locations.

$$
T c_{t}=\left[\begin{array}{llll}
x_{w_{1,1}} & x_{w_{1,2}} & x_{w_{2,1}} & x_{w_{2,2}} \\
y_{w_{1,1}} & y_{w_{1,2}} & y_{w_{2,1}} & y_{w_{2,2}} \\
z_{w_{1,1}} & z_{w_{1,2}} & z_{w_{2,1}} & z_{w_{2,2}}
\end{array}\right]
$$

| Array Element | Axle | Wheel Number | Axis |
| :---: | :---: | :---: | :---: |
| TrackCoords(1, 1) | 1 | 1 | Solid axle $x$-axis |
| TrackCoords(1, 2) | 1 | 2 |  |
| TrackCoords(1, 3) | 2 | 1 |  |
| TrackCoords(1, 4) | 2 | 2 |  |
| TrackCoords(2, 1) | 1 | 1 | Solid axle $y$-axis |
| TrackCoords(2, 2) | 1 | 2 |  |
| TrackCoords(2, 3) | 2 | 1 |  |
| TrackCoords(2, 4) | 2 | 2 |  |
| TrackCoords(3, 1) | 1 | 1 | Solid axle $z$-axis |
| TrackCoords(3, 2) | 1 | 2 |  |
| TrackCoords(3, 3) | 2 | 1 |  |
| TrackCoords(3, 4) | 2 | 2 |  |

## Suspension hardpoint coordinates relative to axle center, SuspCoords - Point

## [0 0 0 0;-1 1-1 1;0 0 0 0] (default)|array

Suspension hardpoint coordinates, $S c_{t}$, along the solid axle $x$-, $y$-, and $z$-axes, in $m$.
For example, for a two-axle vehicle with two wheels per axle, the SuspCoords array:

- Dimensions are [3×4].
- Contains four track hardpoint coordinates according to their axle and track locations.

$$
S_{c_{t}}=\left[\begin{array}{llll}
x_{s_{1,1}} & x_{s_{1,2}} & x_{s_{2,1}} & x_{s_{2,2}} \\
y_{s_{1,1}} & y_{s_{1,2}} & y_{s_{2,1}} & y_{s_{2,2}} \\
z_{s_{1,1}} & z_{s_{1,2}} & z_{s_{2,1}} & z_{s_{2,2}}
\end{array}\right]
$$

| Array Element | Axle | Track | Axis |
| :---: | :---: | :---: | :---: |
| SuspCoords(1,1 ) | 1 | 1 | Solid axle $x$-axis |
| SuspCoords(1,2 | 1 | 2 |  |
| SuspCoords(1,3 | 2 | 1 |  |
| $\begin{aligned} & \begin{array}{l} \text { SuspCoords (1,4 } \\ ) \end{array} \\ & \hline \end{aligned}$ | 2 | 2 |  |
| SuspCoords(2,1 ) | 1 | 1 | Solid axle $y$-axis |
| SuspCoords(2,2 ) | 1 | 2 |  |
| SuspCoords(2,3 ) | 2 | 1 |  |
| SuspCoords (2,4 ) | 2 | 2 |  |
| SuspCoords(3,1 ) | 1 | 1 | Solid axle $z$-axis |
| SuspCoords(3,2 ) | 1 | 2 |  |
| $\begin{aligned} & \begin{array}{l} \text { SuspCoords }(3,3 \\ ) \\ \hline \end{array} \\ & \hline \end{aligned}$ | 2 | 1 |  |
| SuspCoords (3,4 ) | 2 | 2 |  |

Wheel and axle interface compliance constant, KzWhIAxI - Spring rate 6437000 (default) | scalar

Wheel and axle interface compliance constant, $k w a_{z}$, in $\mathrm{N} / \mathrm{m}$.
Wheel and axle interface compliance preload, FOzWhIAxI - Spring rate 9810 (default) | scalar

Wheel and axle interface compliance preload, $F w a_{z 0}$, in N .

## Wheel and axle interface damping constant, CzWhIAxI - Damping

10000 (default) | scalar
Wheel and axle interface damping constant, $c w a_{z}$, in $m$.

## Suspension

## Compliance and Damping - Passive

Suspension spring constant, Kz - Suspension spring constant
64370 (default) | scalar | vector
Linear vertical spring constant for independent suspension wheels on axle a, $k_{z_{d}}$, in $\mathrm{N} / \mathrm{m}$.

Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Suspension spring preload, $\mathbf{F O z}$ - Suspension spring preload

9810 (default) | scalar | vector
Vertical preload spring force applied to the wheels on the axle at wheel carrier reference coordinates, $F_{z 0_{a^{\prime}}}$ in N. Positive preload forces:

- Cause the vehicle to lift.
- Point along the negative vehicle-fixed $z$-axis.

Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

Suspension shock damping constant, Cz - Suspension shock damping constant 10000 (default) | scalar | vector

Linear vertical damping constant for independent suspension wheels on axle a, $c_{z_{a^{\prime}}}$ in $\mathrm{Ns} / \mathrm{m}$.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Dependencies

To create this parameter, clear Enable active damping.
Suspension maximum height, Hmax - Height
0.5 (default) | scalar | vector

Maximum suspension extension or minimum suspension compression height, $H_{\text {max }}$, for axle a before the suspension reaches a hardstop, in m .

Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Geometry

Toe angle at steering center, Toe - Toe angle
0.0349 (default) | scalar

Nominal suspension toe angle at zero steering angle, $\zeta_{0 a}$, in rad.
Roll steer vs suspension height slope, RollStrgSIp - Steer angle suspension slope -0. 2269 (default) | scalar | vector

Roll steer angle versus suspension height, $m_{\text {htoe }}^{a^{\prime}}$ in $\mathrm{rad} / \mathrm{m}$.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

Toe angle vs steering angle slope, ToeStrgSIp - Toe angle steering slope
0.01 (default) | scalar | vector

Toe angle versus steering angle slope, $m_{\text {toesteer }_{d^{\prime}}}$ dimensionless.

Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Dependencies

To create input port StrgAng, set an element of the Steered axle enable by axle, StrgEnByAxl vector to 1 .

Caster angle at steering center, Caster - Caster angle at steering center 0.0698 (default) | scalar

Nominal suspension caster angle at zero steering angle, $\eta_{0 a}$, in rad.
Caster angle vs suspension height slope, CasterHslp - Caster angle versus suspension height slope
-0. 2269 (default) | scalar | vector
Caster angle versus suspension height, $m_{\text {hcaster }_{a^{\prime}}}$ in rad $/ \mathrm{m}$.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

Caster angle vs steering angle slope, CasterStrgSIp - Caster angle versus steering angle slope 0.01 (default) | scalar | vector

Caster angle versus steering angle slope, $m_{\text {castersteer }_{a^{\prime}}}$ dimensionless.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Dependencies

To create input port StrgAng, set an element of the Steered axle enable by axle, StrgEnByAxl vector to 1 .

Camber angle at steering center, Camber - Camber angle at steering center 0.0698 (default) | scalar

Nominal suspension camber angle at zero steering angle, $\xi_{0 a}$, in rad.
Camber angle vs suspension height slope, CamberHslp - Camber angle versus suspension height slope
-0.2269 (default) | scalar | vector
Camber angle versus suspension height, $m_{\text {hcamber }}{ }^{\prime}$ in rad $/ \mathrm{m}$.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

Camber angle vs steering angle slope, CamberStrgSIp - Camber angle versus steering angle slope
0.01 (default) | scalar | vector

Camber angle versus steering angle slope, $m_{\text {cambersteer }{ }_{a}}{ }^{\text {d }}$ dimensionless.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Dependencies

To create input port StrgAng, set an element of the Steered axle enable by axle, StrgEnByAxl vector to 1.

Suspension height vs steering angle slope, StrgHgtSIp - Suspension height versus steering angle slope
0.1432 (default) | scalar | vector

Steering angle to vertical force slope applied at suspension wheel carrier reference point, $m_{\text {hsteer }_{a^{\prime}} \text {, }}$ in m/rad.

Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Dependencies

To create input port StrgAng, set an element of the Steered axle enable by axle, StrgEnByAxl vector to 1.

## Version History

## Introduced in R2018a

## R2022b: Parameter name change from NumTracksByAxl to NumWhlsByAxl

Behavior changed in R2022b
The Number of tracks by axle, NumTracksByAxl parameter is renamed to Number of wheels by axle, NumWhlsByAxl.

The block uses the number of wheels per axle to index the input and output block signals.

## References

[1] Gillespie, Thomas. Fundamentals of Vehicle Dynamics. Warrendale, PA: Society of Automotive Engineers, 1992.
[2] Vehicle Dynamics Standards Committee. Vehicle Dynamics Terminology. SAE J670. Warrendale, PA: Society of Automotive Engineers, 2008.
[3] Technical Committee. Road vehicles - Vehicle dynamics and road-holding ability - Vocabulary. ISO 8855:2011. Geneva, Switzerland: International Organization for Standardization, 2011.

## Extended Capabilities

C/C++ Code Generation
Generate C and $\mathrm{C}++$ code using Simulink ${ }^{\circledR}$ Coder $^{\mathrm{TM}}$.

## See Also

Solid Axle Suspension | Solid Axle Suspension - Leaf Spring | Solid Axle Suspension - Mapped

## Solid Axle Suspension - Leaf Spring

Solid axle suspension with leaf spring


## Libraries:

Vehicle Dynamics Blockset / Suspension

## Description

The Solid Axle Suspension - Leaf Spring block implements a solid axle suspension with a leaf spring for multiple axles with multiple wheels per axle.

The block models the suspension compliance, damping, and geometric effects as functions of the wheel positions and velocities, with axle-specific compliance and damping parameters. Using the wheel position and velocity, the block calculates the vertical wheel position and suspension forces on the vehicle and wheel. The block uses the Z-down (defined in SAE J670) and a solid axle coordinate system. The solid axle coordinate system, shown here, is aligned with the Z-down vehicle coordinate system, with the $x$-axis in the direction of forward vehicle motion.


| For Each | You Can Specify |
| :--- | :--- |
| Axle | • Multiple wheels |
|  | - Suspension parameters |
| Wheel | • Steering angles |

The block contains energy-storing spring elements and energy-dissipating damper elements. The block also stores energy via the axle roll angular acceleration and axle center of mass vertical and lateral acceleration.

This table summarizes the block parameter settings for a vehicle with:

- Two axles
- Two wheels per axle
- Steering angle input for both wheels on the front axle

| Parameter | Setting |
| :--- | :--- |
| Number of axles, NumAxl | 2 |
| Number of wheels by axle, NumWhlsByAxl | $\left[\begin{array}{ll}2 & 2\end{array}\right]$ |
| Steered axle enable by axle, StrgEnByAxl | $\left[\begin{array}{ll}1 & 0\end{array}\right]$ |

The block uses the wheel number, $t$, to index the input and output signals. This table summarizes the wheel, axle, and corresponding wheel number for a vehicle with:

- Two axles
- Two wheels per axle

| Wheel | Axle | Wheel Number |
| :--- | :--- | :--- |
| Front left | Front | 1 |
| Front right | Front | 2 |
| Rear left | Rear | 1 |
| Rear right | Rear | 2 |

## Suspension Compliance and Damping

The block uses a linear spring and damper to model the vertical dynamic effects of the suspension system on the vehicle and wheel. Specifically, the block:

| Uses | To Calculate |
| :--- | :--- |
| -Longitudinal and lateral displacement and <br> velocity of the vehicle. | -Suspension forces applied to the axle center. <br> - <br> Lortical displacements and velocities of the <br> velocity of the wheel. <br> - Vertical wheel forces applied to the vehicle. |
|  | -vehicle and wheel. <br> Longitudinal, lateral and vertical suspension <br> forces and moments applied to the vehicle. <br> Longitudinal, lateral and vertical suspension <br> forces and moments applied to the wheel. |

To calculate the dynamics of the axle, the block implements these equations. The block neglects the effects of:

- Lateral and longitudinal translational velocity.
- Angular velocity about the vertical and lateral axes.

$$
\begin{aligned}
& {\left[\begin{array}{l}
\ddot{x}_{a} \\
\ddot{y}_{a} \\
\ddot{z}_{a}
\end{array}\right]=\frac{1}{M_{a}}\left[\begin{array}{l}
F_{x a} \\
F_{y a} \\
F_{z a}
\end{array}\right]+\left[\begin{array}{l}
\dot{x}_{a} \\
\dot{y}_{a} \\
\dot{z}_{a}
\end{array}\right] \times\left[\begin{array}{l}
p \\
q \\
r
\end{array}\right]=\frac{1}{M_{a}}\left[\begin{array}{c}
0 \\
0 \\
F_{z a}
\end{array}\right]+\left[\begin{array}{c}
0 \\
0 \\
\dot{z}_{a}
\end{array}\right] \times\left[\begin{array}{l}
p \\
0 \\
0
\end{array}\right]+\left[\begin{array}{l}
0 \\
0 \\
g
\end{array}\right]=\left[\begin{array}{c}
0 \\
p \dot{z}_{a} \\
\frac{F_{z a}}{M_{a}}+g
\end{array}\right]} \\
& {\left[\begin{array}{l}
\dot{p} \\
\dot{q} \\
\dot{r}
\end{array}\right]=\left[\left[\begin{array}{l}
M_{x} \\
M_{y} \\
M_{z}
\end{array}\right]-\left[\begin{array}{l}
p \\
q \\
r
\end{array}\right] \times\left[\begin{array}{ccc}
I_{x x} & 0 & 0 \\
0 & I_{y y} & 0 \\
0 & 0 & I_{z z}
\end{array}\right]\left[\begin{array}{c}
p \\
q \\
r
\end{array}\right]\left[\begin{array}{ccc}
I_{x x} & 0 & 0 \\
0 & I_{y y} & 0 \\
0 & 0 & I_{z z}
\end{array}\right]-1\right.} \\
& =\left[\left[\begin{array}{c}
M_{x} \\
0 \\
0
\end{array}\right]-\left[\begin{array}{l}
p \\
q \\
0
\end{array}\right] \times\left[\begin{array}{ccc}
I_{x x} & 0 & 0 \\
0 & I_{y y} & 0 \\
0 & 0 & I_{z z}
\end{array}\right]\left[\begin{array}{c}
p \\
0 \\
0
\end{array}\right]\left[\begin{array}{ccc}
I_{x x} & 0 & 0 \\
0 & I_{y y} & 0 \\
0 & 0 & I_{z z}
\end{array}\right]^{-1}=\left[\begin{array}{c}
\frac{M_{x}}{I_{x x}} \\
0 \\
0
\end{array}\right]\right.
\end{aligned}
$$

The net vertical force on the axle center of mass is the sum of the wheel and suspension forces acting on the axle.

$$
F_{z a}=\sum_{t=1}^{N t a}\left(F_{w z_{a, t}}+F_{z 0_{a}}+k_{z_{a}}\left(z_{v_{a, t}}-z_{s_{a, t}}+m_{h s t e e r_{a}}\left|\delta_{s t e e r_{a, t}}\right|\right)+c_{z_{a}}\left(\dot{z}_{v_{a, t}}-\dot{z}_{s_{a, t}}\right)\right)
$$

The net moment about the roll axis of the solid axle suspension accounts for the hardpoint coordinates of the suspension and wheels.

$$
\begin{aligned}
& M_{x}=\sum_{t=1}^{N t a}\left(F_{w z_{a, t}} y_{w_{t}}+\left(F_{z 0_{a}}+k_{z_{a}}\left(z_{v_{a, t}}-z_{s_{a, t}}+m_{\text {hsteera }} \mid \delta_{\text {steer }}^{a, t}\right.\right.\right. \\
& \\
& \left.\left.+M_{w x_{a, t}} \frac{I_{x x}}{I_{x x}+M_{a} y_{w_{t}}}\right)+c_{z_{a}}\left(\dot{z}_{v_{a, t}}-\dot{z}_{s_{a, t}}\right)\right) y_{s_{t}}
\end{aligned}
$$

Block parameters provide the track and suspension hardpoints coordinates.

$$
\begin{gathered}
T c_{t}=\left[\begin{array}{lll}
x_{w_{1}} & x_{w_{2}} & \cdots \\
y_{w_{1}} & y_{w_{2}} & \cdots \\
z_{w_{1}} & z_{w_{2}} & \cdots
\end{array}\right] \\
S c_{t}=\left[\begin{array}{lll}
x_{s_{1}} & x_{s_{2}} & \cdots \\
y_{s_{1}} & y_{s_{2}} & \cdots \\
z_{s_{1}} & z_{s_{2}} & \cdots
\end{array}\right]
\end{gathered}
$$

The block uses Euler angles to transform the track and suspension displacements, velocities, and accelerations to the vehicle coordinate system.

To calculate the suspension forces applied to the vehicle, the block implements this equation.

$$
F_{v z_{a, t}}=-\left(F_{z 0_{a}}+k_{z_{a}}\left(z_{v_{a, t}}-z_{s_{a, t}}+m_{h s t e e r_{a}}\left|\delta_{\text {steer }_{a, t}}\right|\right)+c_{z_{a}}\left(\dot{z}_{v_{a, t}}-\dot{z}_{s_{a, t}}\right)+F_{z h s t o p_{a, t}}\right)
$$

The suspension forces and moments applied to the vehicle are equal to the suspension forces and moments applied to the wheel.

$$
\begin{aligned}
& F_{v x_{a, t}}=F_{w x_{a, t}} \\
& F_{v y_{a, t}}=F_{w y_{a, t}} \\
& F_{v x_{a, t}}=-F_{w z_{a, t}} \\
& M_{v x_{a, t}}=M_{w x_{a, t}}+F_{w y_{a, t}}\left(R e_{w y_{a, t}}+H_{a, t}\right) \\
& M_{v y_{a, t}}=M_{w y_{a, t}}+F_{w x_{a, t}}\left(R e_{w x_{a, t}}+H_{a, t}\right) \\
& M_{v x_{a, t}}=M_{w z_{a, t}}
\end{aligned}
$$

To calculate the vertical force applied to the suspension at the wheel location, the block implements a stiff spring-damper, shown here.


The block uses this equation.

$$
F_{w z_{a, t}}=-F w a_{z 0}-k w a_{z}\left(z_{w_{a, t}}-z_{s_{a, t}}\right)-c w a_{z}\left(\dot{z}_{w_{a, t}}-\dot{z}_{s_{a, t}}\right)
$$

The equations use these variables.
$F_{w z_{a}, t} M_{w z_{a, t}} \quad$ Suspension force and moment applied to the wheel on axle a, wheel t along wheel-fixed $z$-axis
$F_{w x_{a, t}} M_{w x_{a t t}} \quad$ Suspension force and moment applied to the wheel on axle a, wheel t along wheel-fixed $x$-axis

| $F_{w y_{0, t}} M_{w y_{a, t}}$ | Suspension force and moment applied to the wheel on axle a, wheel $t$ along wheel-fixed $y$-axis |
| :---: | :---: |
| $F_{v z_{a, t}} M_{v z_{a}, t}$ | Suspension force and moment applied to the vehicle on axle a, wheel t along wheel-fixed $z$-axis |
| $F_{v x_{a, t}} M_{V x^{\prime}, t}$ | Suspension force and moment applied to the vehicle on axle a, wheel t along wheel-fixed $x$-axis |
| $F_{v y_{a, t}} M_{v y_{a, t}}$ | Suspension force and moment applied to the vehicle on axle a, wheel t along wheel-fixed $y$-axis |
| $F_{z 0_{a}}$ | Vertical suspension spring preload force applied to the wheels on axle a |
| $k_{\chi_{a}}$ | Vertical spring constant applied to wheels on axle a |
| kwa ${ }_{z}$ | Wheel and axle interface compliance constant |
| $m_{\text {hsteer }}$ | Steering angle to vertical force slope applied at wheel carrier for wheels on axle a |
| $\delta_{\text {steer }}^{\text {a }}$ | Steering angle input for axle a, wheel t |
| $C_{z_{a}}$ | Vertical damping constant applied to wheels on axle a |
| cwa ${ }_{z}$ | Wheel and axle interface damping constant |
| $R e_{w_{a t t}}$ | Effective wheel radius for axle a, wheel t |
| $F_{\text {zhstop }{ }_{\text {at }}}$ | Vertical hardstop force at axle a , wheel t , along the vehicle-fixed $z$-axis |
| $F_{\text {zaswy }}{ }_{\text {a }}$ | Vertical anti-sway force at axle a, wheel t , along the vehicle-fixed $z$-axis |
| $\mathrm{Fwa}_{z 0}$ | Wheel and axle interface compliance constant |
| $z_{v_{a, t}}, \dot{z}_{v_{a, t}}$ | Vehicle displacement and velocity at axle a , wheel t , along the vehiclefixed $z$-axis |
| $z_{w_{a, t}} \dot{z}_{w_{a, t}}$ | Wheel displacement and velocity at axle $a$, wheel $t$, along the vehicle-fixed $z$-axis |
| $\chi_{v_{a, t}} \dot{\chi}_{v_{a, t}}$ | Vehicle displacement and velocity at axle $a$, wheel $t$, along the vehiclefixed $z$-axis |
| $\chi_{w_{a, t},} \dot{\chi}_{w_{a, t}}$ | Wheel displacement and velocity at axle $a$, wheel $t$, along the vehicle-fixed $z$-axis |
| $y_{v_{a, t}} \dot{y}_{v_{a, t}}$ | Vehicle displacement and velocity at axle a , wheel t , along the vehiclefixed $y$-axis |
| $y_{w_{a, t}} \dot{y}_{w_{a, t}}$ | Wheel displacement and velocity at axle a , wheel t , along the vehicle-fixed $y$-axis |
| $H_{a, t}$ | Suspension height at axle a, wheel t |
| $R e_{w_{a, t}}$ | Effective wheel radius at axle a, wheel t |

## Hardstop Forces

The hardstop feedback force, $F_{\text {zhstopat, }^{\prime}}$ that the block applies depends on whether the suspension is compressing or extending. The block applies the force:

- In compression, when the suspension is compressed more than the maximum distance specified by the Suspension maximum height, Hmax parameter.
- In extension, when the suspension extension is greater than maximum extension specified by the Suspension maximum height, Hmax parameter.

To calculate the force, the block uses a stiffness based on a hyperbolic tangent and exponential scaling.

## Camber, Caster, and Toe Angles

To calculate the camber, caster, and toe angles, block uses linear functions of the suspension height and steering angle.

$$
\begin{aligned}
& \xi_{a, t}=\xi_{0 a}+m_{\text {hcamber }_{a}}\left(z_{w_{a, t}}-z_{v_{a, t}}-m_{\text {hsteer }_{a}}\left|\delta_{\text {steer }_{a, t}}\right|\right)+m_{\text {cambersteer }_{a}}\left|\delta_{\text {steer }_{a}, t}\right| \\
& \eta_{a, t}=\eta_{0 a}+m_{\text {hcaster }_{a}}\left(z_{w_{a, t}}-z_{v_{a, t}}-m_{\text {hsteer }_{a}}\left|\delta_{\text {steer }_{a, t}}\right|\right)+m_{\text {castersteer }_{a}}\left|\delta_{\text {steer }_{a, t}}\right| \\
& \zeta_{a, t}=\zeta_{0 a}+m_{\text {htoe }_{a}}\left(z_{w_{a, t}}-z_{v_{a, t}}-m_{\text {hsteer }_{a}}\left|\delta_{\text {steer }_{a, t}}\right|\right)+m_{\text {toesteer }_{a}}\left|\delta_{\text {steer }_{a} t}\right|
\end{aligned}
$$

The equations use these variables.

| $\xi_{a, t}$ | Camber angle of wheel on axle $a$, wheel $t$ |
| :---: | :---: |
| $\eta_{a, t}$ | Caster angle of wheel on axle a, wheel t |
| $\zeta_{a, t}$ | Toe angle of wheel on axle $a$, wheel $t$ |
| $\xi_{0 a}, \eta_{0 a}, \zeta_{0 a}$ | Nominal suspension axle a camber, caster, and toe angles, respectively, at zero steering angle |
| $\begin{aligned} & m_{\text {hcamber }_{a^{\prime}}} m_{\text {hcaster }_{a^{\prime}}} \\ & m_{\text {htoe }_{a}} \end{aligned}$ | Camber, caster, and toe angles, respectively, versus suspension height slope for axle a |
| $m_{\text {cambersteer }_{\alpha^{\prime}}} m_{\text {castersteer }_{a^{\prime}}}$ $m_{\text {toesteer }_{a}}$ | Camber, caster, and toe angles, respectively, versus steering angle slope for axle a |
| $m_{\text {hsteer }}$ | Steering angle versus vertical force slope for axle a |
| $\delta_{\text {stee }}^{\text {at, }}$ | Steering angle input for axle a, wheel t |
| $z_{v_{a t, t}}$ | Vehicle displacement at axle a , wheel t , along the vehicle-fixed $z$-axis |
| $z_{w_{\text {a }}, t}$ | Wheel displacement at axle a , wheel t , along the vehicle-fixed $z$-axis |

## Steering Angles

Optionally, use the Steered axle enable by axle, StrgEnByAxl parameter to input steering angles for the wheels. To calculate the steering angles for the wheels, the block offsets the input steering angles with a linear function of the suspension height.

$$
\delta_{\text {whlsteer }_{a, t}}=\delta_{\text {steer }_{a, t}}+m_{\text {htoe }_{a}}\left(z_{w_{a, t}}-z_{v_{a, t}}-m_{\text {hsteer }_{a}}\left|\delta_{\text {steer }_{a, t}}\right|\right)+m_{\text {toesteer }_{a}}\left|\delta_{\text {steer }_{a, t}}\right|
$$

The equation uses these variables.

| $m_{\text {toester }_{a}}$ | Axle a toe angle versus steering angle slope |
| :--- | :--- |
| $m_{\text {hsteer }_{a}}$ | Axle a steering angle versus vertical force slope |
| $m_{\text {htoe }}^{a}$ | Axle a toe angle versus suspension height slope |
| $\delta_{\text {whlsteer }_{a, t}}$ | Wheel steering angle for axle a, wheel t |
| $\delta_{\text {stee }_{a, t}}$ | Steering angle input for axle a, wheel t |
| $z_{v_{a, t}}$ | Vehicle displacement at axle a, wheel t, along the vehicle-fixed $z$-axis |

$z_{w_{a, t}} \quad$ Wheel displacement at axle $a$, wheel $t$, along the vehicle-fixed $z$-axis

## Power and Energy

The block calculates these suspension characteristics for each axle, $a$, wheel, $t$.

| Calculation | Equation |
| :---: | :---: |
| Dissipated power, $P_{\text {suspot }}$ | $P_{\text {susp }_{a, t}}=F_{w_{z l o o k u p a l ~}}\left(\dot{v}_{v_{a, t}}-\dot{w}_{w_{a, t},} \dot{z}_{v_{a, t}}-\dot{z}_{w_{a, t}} \delta_{\text {steer }_{a, t}}\right)$ |
| Absorbed energy, $E_{\text {susp }}^{\text {at }}$ | $E_{\text {susp }_{a, t}}=F_{w_{z l o o k u p a l}}\left(\dot{v}_{v_{a, t}}-\dot{w}_{w_{a, t}} \dot{z}_{v_{a, t}}-\dot{z}_{w_{a, t}} \delta_{\text {steer }_{a, t}}\right)$ |
| Suspension height, $H_{a, t}$ | $H_{a, t}=-\left(z_{v_{a, t}}-z_{w_{a, t}}+\frac{F_{z 0_{a}}}{k_{z_{a}}}+m_{\text {hsteer }_{a}}\left\|\delta_{\text {steer }_{a, t}}\right\|\right)$ |
| Distance from wheel carrier center to tire/road interface | $z_{w t t_{a, t}}=R e_{w_{a, t}}+H_{a, t}$ |

The equations use these variables.
$m_{\text {hsteer }_{a}} \quad$ Steering angle to vertical force slope applied at wheel carrier for wheels on axle a
$\delta_{\text {steer }_{a, t}} \quad$ Steering angle input for axle a, wheel t
$R e_{w_{a, t}} \quad$ Axle a, wheel $t$ effective wheel radius from wheel carrier center to tire/road interface
$F_{z 0_{a}} \quad$ Vertical suspension spring preload force applied to the wheels on axle a
$z_{w t r_{a, t}} \quad$ Distance from wheel carrier center to tire/road interface, along the vehicle-fixed $z$ axis
$z_{v_{a, t}}, \dot{z}_{v_{a, t}} \quad$ Vehicle displacement and velocity at axle $a$, wheel $t$, along the vehicle-fixed $z$-axis
$z_{w_{a, t}} \dot{z}_{w_{a, t}} \quad$ Wheel displacement and velocity at axle $a$, wheel $t$, along the vehicle-fixed $z$-axis

## Ports

## Input

WhIPz - Wheel z-axis displacement
array
Wheel displacement, $z_{w}$, along wheel-fixed $z$-axis, in $m$. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlPz:

- Signal array dimensions are [1x4].

$$
\mathrm{WhlPz}=z_{w}=\left[\begin{array}{llll}
z_{w_{1,1}} & z_{w_{1,2}} & z_{w_{2,1}} & z_{w_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlPz $(1,1)$ | 1 | 1 |
| Front right | WhlPz $(1,2)$ | 1 | 2 |


| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Rear left | WhlPz $(1,3)$ | 2 | 1 |
| Rear right | WhlPz $(1,4)$ | 2 | 2 |

WhIRe - Wheel effective radius
array
Effective wheel radius, $R e_{w}$, in m. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlRe:

- Signal array dimensions are [1×4].

$$
\text { WhlRe }=R e_{w}=\left[\begin{array}{ll}
R e_{w_{1,1}} & R e_{w_{1,2}}
\end{array} R e_{w_{2,1}} R e_{w_{2,2}}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlRe $(1,1)$ | 1 | 1 |
| Front right | WhlRe $(1,2)$ | 1 | 2 |
| Rear left | WhlRe $(1,3)$ | 2 | 1 |
| Rear right | WhlRe $(1,4)$ | 2 | 2 |

WhIVz - Wheel z-axis velocity array

Wheel velocity, $\dot{z}_{w}$, along wheel-fixed $z$-axis, in m. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlVz:

- Signal array dimensions are [1×4].

$$
\text { WhlVz }=\dot{z}_{w}=\left[\begin{array}{lll}
\dot{z}_{1,1} & \dot{z}_{w_{1,2}} & \dot{z}_{w_{2,1}} \\
\dot{z}_{w_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlVz $(1,1)$ | 1 | 1 |
| Front right | WhlVz $(1,2)$ | 1 | 2 |
| Rear left | WhlVz $(1,3)$ | 2 | 1 |
| Rear right | WhlVz $(1,4)$ | 2 | 2 |

WhIFx - Longitudinal wheel force on vehicle
array
Longitudinal wheel force applied to vehicle, $F_{w x}$, along the vehicle-fixed $x$-axis. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlFx:

- Signal array dimensions are [1×4].

WhlFx $=F_{w x}=\left[F_{w x_{1,1}} F_{w x_{1,2}} F_{w x_{2,1}} F_{w x_{2,2}}\right]$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlFx $(1,1)$ | 1 | 1 |
| Front right | WhlFx $(1,2)$ | 1 | 2 |
| Rear left | WhlFx $(1,3)$ | 2 | 1 |
| Rear right | WhlFx $(1,4)$ | 2 | 2 |

WhIFy - Lateral wheel force on vehicle
array
Lateral wheel force applied to vehicle, $F_{w y}$, along the vehicle-fixed $y$-axis. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlFy:

- Signal array dimensions are [1×4].

WhlFy $=F_{w y}=\left[F_{w y 1,1} F_{w y 1,2} F_{w y 2,1} F_{w y_{2,2}}\right]$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlFy $(1,1)$ | 1 | 1 |
| Front right | WhlFy $(1,2)$ | 1 | 2 |
| Rear left | WhlFy $(1.3)$ | 2 | 1 |
| Rear right | WhlFy $(1,4)$ | 2 | 2 |

WhIM - Suspension moment on wheel
array
Longitudinal, lateral, and vertical suspension moments at axle a, wheel $t$, applied to the wheel at the axle wheel carrier reference coordinate, in $\mathrm{N} \cdot \mathrm{m}$. Input array dimensions are 3 by the number of wheels on the vehicle.

- WhlM (1, . . ) - Suspension moment applied to the wheel about the vehicle-fixed $x$-axis (longitudinal)
- WhlM $(2, \ldots)$ - Suspension moment applied to the wheel about the vehicle-fixed $y$-axis (lateral)
- WhlM $(3, \ldots)$ - Suspension moment applied to the wheel about the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the WhlM:

- Signal dimensions are [3×4].
- Signal contains suspension moments applied to four wheels according to their axle and wheel locations.

$$
\text { WhlM }=M_{w}=\left[\begin{array}{llll}
M_{w x_{1,1}} & M_{w x_{1,2}} & M_{w x_{2,1}} & M_{w x_{2,2}} \\
M_{w y_{1,1}} & M_{w y 1,2} & M_{w y_{2,1}} & M_{w y 2,2} \\
M_{w z_{1,1}} & M_{w z_{1,2}} & M_{w z_{2,1}} & M_{w z 2,2}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Moment Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | WhlM $(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front <br> right | WhlM(1,2) | 1 | 2 |  |
| Rear <br> left | WhlM(1,3) | 2 | 1 |  |
| Rear <br> right | WhlM(1,4) | 2 | 2 |  |
| Front <br> left | WhlM(2,1) | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front <br> right | WhlM(2,2) | 1 | 2 |  |
| Rear <br> left | WhlM(2,3) | 2 | 1 |  |
| Rear <br> right | WhlM(2,4) | 2 | 2 |  |
| Front <br> left | WhlM(3,1) | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front <br> right | WhlM(3,2) | 1 | 2 |  |
| Rear <br> left | WhlM(3,3) | 2 | 1 |  |
| Rear <br> right | WhlM(3,4) | 2 | 2 |  |

VehP - Vehicle displacement
array
Vehicle displacement from axle a, wheel $t$ along vehicle-fixed coordinate system, in m. Input array dimensions are 3 the number of wheels on the vehicle.

- VehP (1, ...) - Vehicle displacement from wheel, $\chi_{v}$, along the vehicle-fixed $x$-axis
- $\operatorname{VehP}(2, \ldots)$ - Vehicle displacement from wheel, $y_{v}$, along the vehicle-fixed $y$-axis
- $\operatorname{VehP}(3, \ldots)-$ Vehicle displacement from wheel, $z_{v}$, along the vehicle-fixed $z$-axis

For example, for a two-axle vehicle with two wheels per axle, the VehP:

- Signal dimensions are [3x4].
- Signal contains four displacements according to their axle and wheel locations.

$$
\text { VehP }=\left[\begin{array}{l}
x_{v} \\
y_{v} \\
z_{v}
\end{array}\right]=\left[\begin{array}{llll}
x_{v_{1,1}} & x_{v_{1,2}} & x_{v_{2,1}} & x_{v_{2,2}} \\
y_{v_{1,1}} & y_{v_{1,2}} & y_{v_{2,1}} & y_{v_{2,2}} \\
z_{v_{1,1}} & z_{v_{1,2}} & z_{v_{2,1}} & z_{v_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel Numbe r | Axis |
| :---: | :---: | :---: | :---: | :---: |
| Front left | $\operatorname{VehP}(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis |
| Front right | $\operatorname{VehP}(1,2)$ | 1 | 2 |  |
| Rear left | $\operatorname{VehP}(1,3)$ | 2 | 1 |  |
| Rear right | $\operatorname{VehP}(1,4)$ | 2 | 2 |  |
| Front left | $\operatorname{VehP}(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis |
| Front right | $\operatorname{VehP}(2,2)$ | 1 | 2 |  |
| $\begin{array}{\|l} \text { Rear } \\ \text { left } \end{array}$ | $\operatorname{VehP}(2,3)$ | 2 | 1 |  |
| Rear right | $\operatorname{VehP}(2,4)$ | 2 | 2 |  |
| Front left | $\operatorname{VehP}(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis |
| Front right | $\operatorname{VehP}(3,2)$ | 1 | 2 |  |
| Rear left | $\operatorname{VehP}(3,3)$ | 2 | 1 |  |
| Rear right | $\operatorname{VehP}(3,4)$ | 2 | 2 |  |

VehV - Vehicle velocity
array
Vehicle velocity at axle $a$, wheel $t$ along vehicle-fixed coordinate system, in $m$. Input array dimensions are 3 by the number of wheels on the vehicle.

- $\operatorname{VehV}(1, \ldots)$ - Vehicle velocity at wheel, $x_{v}$, along the vehicle-fixed $x$-axis
- VehV $(2, \ldots)$ - Vehicle velocity at wheel, $y_{v}$, along the vehicle-fixed $y$-axis
- $\operatorname{VehV}(3, \ldots)-$ Vehicle velocity at wheel, $z_{v}$, along the vehicle-fixed $z$-axis

For example, for a two-axle vehicle with two wheels per axle, the VehV:

- Signal dimensions are [3×4].
- Signal contains 4 velocities according to their axle and wheel locations.

$$
\text { VehV }=\left[\begin{array}{l}
\dot{x}_{v} \\
\dot{y}_{v} \\
\dot{z}_{v}
\end{array}\right]=\left[\begin{array}{lllll}
\dot{x}_{v_{1,1}} & \dot{x}_{v_{1,2}} & \dot{x}_{v_{2,1}} & \dot{x}_{v_{2,2}} \\
\dot{y}_{v_{1,1}} & \dot{y}_{v_{1,2}} & \dot{y}_{v_{2,1}} & \dot{y}_{v_{2,2}} \\
\dot{z}_{v_{1,1}} & \dot{z}_{v_{1,2}} & \dot{z}_{v_{2,1}} & \dot{z}_{v_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel Numbe r | Axis |
| :---: | :---: | :---: | :---: | :---: |
| Front left | $\operatorname{VehV}(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis |
| Front right | $\operatorname{VehV}(1,2)$ | 1 | 2 |  |
| Rear <br> left | $\operatorname{VehV}(1,3)$ | 2 | 1 |  |
| Rear right | $\operatorname{VehV}(1,4)$ | 2 | 2 |  |
| Front left | $\operatorname{VehV}(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis |
| Front right | $\operatorname{VehV}(2,2)$ | 1 | 2 |  |
| $\begin{array}{\|l} \text { Rear } \\ \text { left } \end{array}$ | $\operatorname{VehV}(2,3)$ | 2 | 1 |  |
| Rear right | $\operatorname{VehV}(2,4)$ | 2 | 2 |  |
| Front left | $\operatorname{VehV}(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis |
| Front right | $\operatorname{VehV}(3,2)$ | 1 | 2 |  |
| $\begin{aligned} & \text { Rear } \\ & \text { left } \end{aligned}$ | $\operatorname{VehV}(3,3)$ | 2 | 1 |  |
| Rear right | $\operatorname{VehV}(3,4)$ | 2 | 2 |  |

StrgAng - Steering angle, optional
array
Optional steering angle for each wheel, $\delta$. Input array dimensions are 1 by the number of steered wheels.

For example, for a two-axle vehicle with two wheels per axle, you can input steering angles for both wheels on the first axle.

- To create the StrgAng port, set Steered axle enable by axle, StrgEnByAxl to [1 0]. The input signal array dimensions are [1×2].
- The StrgAng signal contains two steering angles according to their axle and wheel locations.

$$
\operatorname{StrgAng}=\delta_{\text {steer }}=\left[\delta_{\text {steer }_{1,1}} \delta_{\text {steer }_{1,2}}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | StrgAng $(1,1)$ | 1 | 1 |
| Front right | StrgAng $(1,2)$ | 1 | 2 |

## Dependencies

To create input port StrgAng, set an element of the Steered axle enable by axle, StrgEnByAxl vector to 1 .

## Output

Info - Bus signal
bus
Bus signal containing block values. The signals are arrays that depend on the wheel location.
For example, here are the indices for a two-axle, two-wheel vehicle. The total number of wheels is four.

- 1D array signal (1-by-4)

| Array Element | Axle | Wheel Number |
| :--- | :--- | :--- |
| $(1,1)$ | 1 | 1 |
| $(1,2)$ | 1 | 2 |
| $(1,3)$ | 2 | 1 |
| $(1,4)$ | 2 | 2 |

- 3D array signal (3-by-4)

| Array Element | Axle | Wheel Number |
| :--- | :--- | :--- |
| $(1,1)$ | 1 | 1 |
| $(1,2)$ | 1 | 2 |
| $(1,3)$ | 2 | 1 |
| $(1,4)$ | 2 | 2 |
| $(2,1)$ | 1 | 1 |
| $(2,2)$ | 1 | 2 |
| $(2,3)$ | 2 | 1 |
| $(2,4)$ | 2 | 2 |
| $(3,1)$ | 1 | 1 |
| $(3,2)$ | 1 | 2 |
| $(3,3)$ | 2 | 1 |
| $(3,4)$ | 2 | 2 |


| Signal | Description | Array Signal | Variable | Units |
| :---: | :---: | :---: | :---: | :---: |
| Camber | Wheel angles according to the axle. | 1D | WhlAng $[1, \ldots]=\xi=\left[\xi_{a, t}\right]$ | rad |
| Caster |  |  | WhlAng $[2, \ldots]=\eta=\left[\eta_{a, t}\right]$ |  |
| Toe |  |  | WhlAng $[3, \ldots]=\zeta=\left[\zeta_{a, t}\right]$ |  |
| Height | Suspension height | 1D | H | m |


| Signal | Description | Array Signal | Variable U | Units |
| :---: | :---: | :---: | :---: | :---: |
| Power | Suspension power dissipation | 1D |  | W |
| Energy | Suspension absorbed energy | 1D | $E_{\text {susp }}$ | J |
| VehF | Suspension forces applied to the vehicle | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { VehF }=F_{v}= \\ & {\left[\begin{array}{llll} F_{v x_{1,1}} & F_{v x_{1,2}} & F_{v x_{2,1}} & F_{v x_{2,2}} \\ F_{v v_{1,1}} & F_{v y_{1,2}} & F_{v v_{2,1}} & F_{v y_{2,2}} \\ F_{v v_{1,1}} & F_{v z_{1,2}} & F_{v z_{2,1}} & F_{v z_{2,2}} \end{array}\right.} \end{aligned}$ | N |
| VehM | Suspension moments applied to vehicle | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { VehM }=M_{v}= \\ & {\left[\begin{array}{llll} M_{v x_{1}, 1} & M_{v x_{1}, 2} & M_{v x_{2,1}} & M_{v \chi_{2},}, \\ M_{v y_{1,1}} & M_{v y_{1,2}} & M_{v y_{2,1}} & M_{v y y_{2},} \\ M_{v \chi_{1,1}} & M_{v z_{1,2}} & M_{v z_{2,1}} & M_{v z_{2},} \end{array}\right.} \end{aligned}$ | $\mathrm{N} \cdot \mathrm{m}$ <br> 2,2 <br> 2,2 <br> 2,2 |


| Signal | Description | Array Signal | Variable | Units |
| :---: | :---: | :---: | :---: | :---: |
| WhlF | Suspension force applied to wheel | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { WhlF }=F_{w}= \\ & {\left[\begin{array}{llll} F_{w x_{1}, 1} & F_{w x_{1,2}} & F_{w x_{2}, 1} & F_{w x_{2}} \\ F_{w y 1,1} & F_{w y_{1,2}} & F_{w y 2,1} & F_{w y_{2}} \\ F_{w z_{1,1}} & F_{w z_{1,2}} & F_{w z_{2,1}} & F_{w z_{2}} \end{array}\right.} \end{aligned}$ |  |
| WhlP | Wheel displacement | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { WhlP }=\left[\begin{array}{l} x_{w} \\ y_{w} \\ z_{w} \end{array}\right]= \\ & {\left[\begin{array}{llll} x_{w_{1,1}} & x_{w_{1,2}} & x_{w_{2,1}} & x_{w_{2}} \\ y_{w_{1,1}} & y_{w_{1,2}} & y_{w_{2,1}} & y_{w y_{2}} \\ z_{w t r_{1,1}} & z_{w t r_{1,2}} & z_{w t r_{2,1}} & z_{w t{ }_{2}} \end{array}\right.} \end{aligned}$ |  |
| Whlv | Wheel velocity | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { WhlV }=\left[\begin{array}{l} \dot{x}_{w} \\ \dot{y}_{w} \\ \dot{z}_{w} \end{array}\right] \\ & = \\ & {\left[\begin{array}{llll} \dot{x}_{w_{1,1}} & \dot{x}_{w_{1,2}} & \dot{x}_{w_{2,1}} & \dot{x}_{w_{2,2}} \\ \dot{y}_{w_{1,1}} & \dot{y}_{w_{1,2}} & \dot{y}_{w_{2,1}} & \dot{y}_{w_{2,2}} \\ \dot{z}_{w_{1,1}} & \dot{z}_{w_{1,2}} & \dot{z}_{w_{2,1}} & \dot{z}_{w_{2,2}} \end{array}\right]} \end{aligned}$ | m/s |


| Signal | Description | Array Signal | Variable | Units |
| :---: | :---: | :---: | :---: | :---: |
| WhlAng | Wheel camber, caster, toe angles | 3D | For a two-axle, two wheels per axle vehicle: | rad |

VehF - Suspension force on vehicle
array
Longitudinal, lateral, and vertical suspension force at axle a, wheel $t$, applied to the vehicle at the suspension connection point, in N. Array dimensions are 3 by the number of wheels on the vehicle.

- $\operatorname{VehF}(1, \ldots)$ - Suspension force applied to vehicle along the vehicle-fixed $x$-axis (longitudinal)
- $\operatorname{VehF}(2, \ldots)$ - Suspension force applied to vehicle along the vehicle-fixed $y$-axis (lateral)
- $\operatorname{VehF}(3, \ldots)$ - Suspension force applied to vehicle along the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the VehF:

- Signal dimensions are [3×4].
- Signal contains suspension forces applied to the vehicle according to the axle and wheel locations.

VehF $=F_{v}=\left[\begin{array}{llll}F_{v x_{1,1}} & F_{v x_{1,2}} & F_{v x_{2,1}} & F_{v x_{2,2}} \\ F_{v v_{1,1}} & F_{v y_{1,2}} & F_{v y_{2,1}} & F_{v y_{2,2}} \\ F_{v z_{1,1}} & F_{v z_{1,2}} & F_{v z_{2,1}} & F_{v z_{2,2}}\end{array}\right]$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | $\operatorname{VehF}(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front <br> right | $\operatorname{VehF}(1,2)$ | 1 | 2 |  |
| Rear <br> left | $\operatorname{VehF}(1,3)$ | 2 | 1 |  |
| Rear <br> right | $\operatorname{VehF}(1,4)$ | 2 | 2 |  |
| Front <br> left | $\operatorname{VehF}(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front <br> right | $\operatorname{VehF}(2,2)$ | 1 | 2 |  |


| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Rear <br> left | VehF $(2,3)$ | 2 | 1 |  |
| Rear <br> right | VehF $(2,4)$ | 2 | 2 |  |
| Front <br> left | $\operatorname{VehF}(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front <br> right | $\operatorname{VehF}(3,2)$ | 1 | 2 |  |
| Rear <br> left | $\operatorname{VehF}(3,3)$ | 2 | 1 |  |
| Rear <br> right | $\operatorname{VehF}(3,4)$ | 2 | 2 |  |

VehM - Suspension moment on vehicle array

Longitudinal, lateral, and vertical suspension moment at axle a, wheel $t$, applied to the vehicle at the suspension connection point, in $\mathrm{N} \cdot \mathrm{m}$. Array dimensions are 3 by the number of wheels on the vehicle.

- VehM (1, ...) - Suspension moment applied to the vehicle about the vehicle-fixed $x$-axis (longitudinal)
- VehM ( $2, \ldots$ ) - Suspension moment applied to the vehicle about the vehicle-fixed $y$-axis (lateral)
- Vehm ( $3, \ldots$ ) - Suspension moment applied to the vehicle about the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the VehM:

- Signal dimensions are [3×4].
- Signal contains suspension moments applied to vehicle according to the axle and wheel locations.

VehM $=M_{v}=\left[\begin{array}{llll}M_{v x_{1,1}} & M_{v x_{1,2}} & M_{v x_{2,1}} & M_{v x_{2,2}} \\ M_{v y 1,1} & M_{v y_{1,2}} & M_{v y_{2,1}} & M_{v y_{2,2}} \\ M_{v z_{1,1}} & M_{v z_{1,2}} & M_{v z_{2,1}} & M_{v z_{2,2}}\end{array}\right]$

| Array Element | Axle | Wheel <br> Number | Moment Axis |
| :--- | :--- | :--- | :--- |
| $\operatorname{VehM}(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| $\operatorname{VehM}(1,2)$ | 1 | 2 |  |
| $\operatorname{VehM}(1,3)$ | 2 | 1 |  |
| $\operatorname{VehM}(1,4)$ | 2 | 2 |  |
| $\operatorname{VehM}(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| $\operatorname{VehM}(2,2)$ | 1 | 2 |  |


| Array Element | Axle | Wheel <br> Number | Moment Axis |
| :--- | :--- | :--- | :--- |
| $\operatorname{VehM}(2,3)$ | 2 | 1 |  |
| $\operatorname{VehM}(2,4)$ | 2 | 2 |  |
| $\operatorname{VehM}(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| $\operatorname{VehM}(3,2)$ | 1 | 2 |  |
| $\operatorname{VehM}(3,3)$ | 2 | 1 |  |
| $\operatorname{VehM}(3,4)$ | 2 | 2 |  |

WhIF - Suspension force on wheel
array
Longitudinal, lateral, and vertical suspension forces at axle a, wheel $t$, applied to the wheel at the axle wheel carrier reference coordinate, in N . Array dimensions are 3 by the number of wheels on the vehicle.

- $\operatorname{WhlF}(1, \ldots)-$ Suspension force on wheel along the vehicle-fixed $x$-axis (longitudinal)
- $\operatorname{WhlF}(2, \ldots)$ - Suspension force on wheel along the vehicle-fixed $y$-axis (lateral)
- WhlF $(3, \ldots)$ - Suspension force on wheel along the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the WhlF:

- Signal dimensions are [3×4].
- Signal contains wheel forces applied to the vehicle according to the axle and wheel locations.

WhlF $=F_{w}=\left[\begin{array}{llll}F_{w x_{1,1}} & F_{w x_{1,2}} & F_{w x_{2,1}} & F_{w x_{2,2}} \\ F_{w y_{1,1}} & F_{w y_{1,2}} & F_{w y_{2,1}} & F_{w y_{2,2}} \\ F_{w z_{1,1}} & F_{w z_{1,2}} & F_{w z_{2,1}} & F_{w z_{2,2}}\end{array}\right]$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | WhlF $(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front <br> right | WhlF $(1,2)$ | 1 | 2 |  |
| Rear <br> left | WhlF $(1,3)$ | 2 | 1 |  |
| Rear <br> right | WhlF $(1,4)$ | 2 | 2 |  |
| Front <br> left | WhlF $(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front <br> right | WhlF $(2,2)$ | 1 | 2 |  |


| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Rear <br> left | WhlF $(2,3)$ | 2 | 1 |  |
| Rear <br> right | WhlF $(2,4)$ | 2 | 2 |  |
| Front <br> left | WhlF $(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front <br> right | WhlF(3,2) | 1 | 2 |  |
| Rear <br> left | WhlF $(3,3)$ | 2 | 1 |  |
| Rear <br> right | WhlF(3,4) | 2 | 2 |  |

WhIV - Wheel velocity
array
Longitudinal, lateral, and vertical wheel velocity at axle a, wheel t , in $\mathrm{m} / \mathrm{s}$. Array dimensions are 3 by the number of wheels on the vehicle.

- WhlV (1, ...) - Wheel velocity along the vehicle-fixed $x$-axis (longitudinal)
- WhlV $(2, \ldots)$ - Wheel velocity along the vehicle-fixed $y$-axis (lateral)
- WhlV $(3, \ldots)-$ Wheel velocity along the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the Whlv:

- Signal dimensions are [3×4].
- Signal contains wheel forces applied to the vehicle according to the axle and wheel locations.

$$
\text { WhlV }=\left[\begin{array}{c}
\dot{x}_{w} \\
\dot{y}_{w} \\
\dot{z}_{w}
\end{array}\right]=\left[\begin{array}{llll}
\dot{x}_{w_{1,1}} & \dot{x}_{w_{1,2}} & \dot{x}_{w_{2,1}} & \dot{x}_{w_{2,2}} \\
\dot{y}_{w_{1,1}} & \dot{y}_{w_{1,2}} & \dot{y}_{w_{2,1}} & \dot{y}_{w_{2,2}} \\
\dot{z}_{w_{1,1}} & \dot{z}_{w_{1,2}} & \dot{z}_{w_{2,1}} & \dot{z}_{w_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | WhlV $(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front <br> right | WhlV $(1,2)$ | 1 | 2 |  |
| Rear <br> left | WhlV $(1,3)$ | 2 | 1 |  |
| Rear <br> right | WhlV $(1,4)$ | 2 | 2 |  |


| Wheel | Array Element | Axie | Wheel Numbe r | Force Axis |
| :---: | :---: | :---: | :---: | :---: |
| Front left | WhlV $(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front right | WhlV (2,2) | 1 | 2 |  |
| Rear left | WhlV (2,3) | 2 | 1 |  |
| Rear right | WhlV $(2,4)$ | 2 | 2 |  |
| Front left | WhlV (3,1) | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front right | WhlV (3,2) | 1 | 2 |  |
| Rear left | WhlV (3,3) | 2 | 1 |  |
| Rear right | WhlV (3,4) | 2 | 2 |  |

WhIAng - Wheel camber, caster, toe angles
array
Camber, caster, and toe angles at axle $a$, wheel $t$, in rad. Array dimensions are 3 by the number of wheels on the vehicle.

- WhlAng(1,...) - Camber angle
- WhlAng $(2, \ldots)$ - Caster angle
- Whlang $(3, \ldots)$ - Toe angle

For example, for a two-axle vehicle with two wheels per axle, the WhlAng:

- Signal dimensions are [3×4].
- Signal contains angles according to the axle and wheel locations.

$$
\text { WhlAng }=\left[\begin{array}{l}
\xi \\
\eta \\
\zeta
\end{array}\right]=\left[\begin{array}{llll}
\xi_{1,1} & \xi_{1,2} & \xi_{2,1} & \xi_{2,2} \\
\eta_{1,1} & \eta_{1,2} & \eta_{2,1} & \eta_{2,2} \\
\zeta_{1,1} & \zeta_{1,2} & \zeta_{2,1} & \zeta_{2,2}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> $\mathbf{r}$ | Angle |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | WhlAng (1,1) | 1 | 1 | Camber |
| Front <br> right | WhlAng (1,2) | 1 | 2 |  |


| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Angle |
| :--- | :--- | :--- | :--- | :--- |
| Rear <br> left | WhlAng (1,3) | 2 | 1 |  |
| Rear <br> right | WhlAng (1,4) | 2 | 2 |  |
| Front <br> left | WhlAng (2,1) | 1 | 1 | Caster |
| Front <br> right | WhlAng (2,2) | 1 | 2 |  |
| Rear <br> left | WhlAng (2,3) | 2 | 1 |  |
| Rear <br> right | WhlAng(2,4) | 2 | 2 |  |
| Front <br> left | WhlAng (3,1) | 1 | 1 | Toe |
| Front <br> right | WhlF(3,2) | 1 | 2 |  |
| Rear <br> left | WhlF(3,3) | 2 | 1 |  |
| Rear <br> right | WhlF(3,4) | 2 | 2 |  |

## Parameters

## Axles

## Number of axles, NumAxI - Number of axles

2 (default) | scalar
Number of axles, $N_{a}$, dimensionless.
Number of wheels by axle, NumWhlsByAxI - Number of wheels per axle
[2 2] (default)|vector
Number of wheels per axle, $N t_{a}$, dimensionless. Vector is 1 by the number of vehicle axles, $N_{a}$. For example, [1,2] represents one wheel on axle one and two wheels on axle two.

Steered axle enable by axle, StrgEnByAxI - Boolean vector to enable axle steering
[1 0] (default) |vector
Boolean vector that enables axle steering, $E n_{\text {steer }}$, dimensionless. Vector is 1 by the number of vehicle axles, $N_{a}$. For example:

- [llll-For a two-axle vehicle, enables axle one steering and disables axle two steering
- [11 1]-For a two-axle vehicle, enables axle one and axle two steering


## Dependencies

Setting an element of the Steered axle enable by axle, StrgEnByAxl vector to 1:

- Creates input port StrgAng.
- Creates these parameters
- Toe angle vs steering angle slope, ToeStrgSlp
- Caster angle vs steering angle slope, CasterStrgSlp
- Camber angle vs steering angle slope, CamberStrgSlp
- Suspension height vs steering angle slope, StrgHgtSlp

For example, for a two-axle vehicle with two wheels per axle, you can input steering angles for both wheels on the first axle.

- To create the StrgAng port, set Steered axle enable by axle, StrgEnByAxl to [1 0]. The input signal array dimensions are [1x2].
- The StrgAng signal contains two steering angles according to their axle and wheel locations.

$$
\text { StrgAng }=\delta_{\text {steer }}=\left[\delta_{\text {steer }_{1,1}} \delta_{\text {steer }_{1}, 2}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | StrgAng (1, 1) | 1 | 1 |
| Front right | StrgAng (1,2) | 1 | 2 |

Axle and wheels lumped principal moments of inertia about longitudinal axis, Axllxx Inertia
300 (default) | vector
Axle and wheels lumped principal moments of inertia about longitudinal axis, AxleIxx $a$, in $\mathrm{kg}^{*} \mathrm{~m} \wedge 2$.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Axle and wheels lumped mass, AxIM - Mass

[2 2] (default)|vector
Axle and wheels lumped mass, $a$, in kg.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

Track hardpoint coordinates relative to axle center, TrackCoords - Point
[0 0 0 0;-1 1 -1 1;0 0 0 0] (default)|array
Track hardpoint coordinates, $T c_{t}$, along the solid axle $x, y$, and $z$-axes, in m .
For example, for a two-axle vehicle with two wheels per axle, the TrackCoords array:

- Dimensions are [3x4].
- Contains four track hardpoint coordinates according to their axle and wheel locations.

$$
T c_{t}=\left[\begin{array}{llll}
x_{w_{1,1}} & x_{w_{1,2}} & x_{w_{2,1}} & x_{w_{2,2}} \\
y_{w_{1,1}} & y_{w_{1,2}} & y_{w_{2,1}} & y_{w_{2,2}} \\
z_{w_{1,1}} & z_{w_{1,2}} & z_{w_{2,1}} & z_{w_{2,2}}
\end{array}\right]
$$

| Array Element | Axle | Wheel Number | Axis |
| :---: | :---: | :---: | :---: |
| TrackCoords(1, 1) | 1 | 1 | Solid axle $x$-axis |
| TrackCoords(1, 2) | 1 | 2 |  |
| ```TrackCoords(1, 3)``` | 2 | 1 |  |
| TrackCoords(1, 4) | 2 | 2 |  |
| TrackCoords(2, 1) | 1 | 1 | Solid axle $y$-axis |
| TrackCoords(2, 2) | 1 | 2 |  |
| TrackCoords(2, 3) | 2 | 1 |  |
| TrackCoords(2, 4) | 2 | 2 |  |
| TrackCoords(3, 1) | 1 | 1 | Solid axle $z$-axis |
| TrackCoords(3, 2) | 1 | 2 |  |
| TrackCoords(3, 3) | 2 | 1 |  |
| TrackCoords(3, <br> 4) | 2 | 2 |  |

## Suspension hardpoint coordinates relative to axle center, SuspCoords - Point

## [0 0 0 0;-1 1-1 1;0 0 0 0] (default)|array

Suspension hardpoint coordinates, $S c_{t}$, along the solid axle $x$-, $y$-, and $z$-axes, in m .
For example, for a two-axle vehicle with two wheels per axle, the SuspCoords array:

- Dimensions are [3×4].
- Contains four track hardpoint coordinates according to their axle and track locations.

$$
S_{c_{t}}=\left[\begin{array}{llll}
x_{s_{1,1}} & x_{s_{1,2}} & x_{s_{2,1}} & x_{s_{2,2}} \\
y_{s_{1,1}} & y_{s_{1,2}} & y_{s_{2,1}} & y_{s_{2,2}} \\
z_{s_{1,1}} & z_{s_{1,2}} & z_{s_{2,1}} & z_{s_{2,2}}
\end{array}\right]
$$

| Array Element | Axle | Track | Axis |
| :---: | :---: | :---: | :---: |
| SuspCoords(1,1 ) | 1 | 1 | Solid axle $x$-axis |
| SuspCoords(1,2 ) | 1 | 2 |  |
| $\begin{aligned} & \text { SuspCoords(1,3 } \\ & \text { ) } \end{aligned}$ | 2 | 1 |  |
| SuspCoords(1,4 | 2 | 2 |  |
| $\begin{aligned} & \text { SuspCoords }(2,1 \\ & ) \end{aligned}$ | 1 | 1 | Solid axle $y$-axis |
| SuspCoords(2,2 | 1 | 2 |  |
| SuspCoords(2,3 ) | 2 | 1 |  |
| $\begin{aligned} & \begin{array}{l} \text { SuspCoords }(2,4 \\ ) \\ \hline \end{array} \\ & \hline \end{aligned}$ | 2 | 2 |  |
| SuspCoords (3,1 ) | 1 | 1 | Solid axle $z$-axis |
| SuspCoords (3,2 ) | 1 | 2 |  |
| $\begin{aligned} & \text { SuspCoords }(3,3 \\ & ) \end{aligned}$ | 2 | 1 |  |
| SuspCoords (3,4 ) | 2 | 2 |  |

Wheel and axle interface compliance constant, KzWhIAxI - Spring rate 6437000 (default) | scalar

Wheel and axle interface compliance constant, $k w a_{z}$, in $\mathrm{N} / \mathrm{m}$.
Wheel and axle interface compliance preload, FOzWhIAxI - Spring rate 9810 (default) | scalar

Wheel and axle interface compliance preload, $F w a_{z 0}$, in N .

## Wheel and axle interface damping constant, CzWhIAxI - Damping

10000 (default) | scalar
Wheel and axle interface damping constant, $c w a_{z}$, in $m$.

## Suspension

## Compliance and Damping - Passive

Suspension spring constant, Kz - Suspension spring constant
64370 (default) | scalar | vector
Linear vertical spring constant for independent suspension wheels on axle a, $k_{z_{d}}$, in $\mathrm{N} / \mathrm{m}$.

Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Suspension spring preload, $\mathbf{F O z}$ - Suspension spring preload

9810 (default) | scalar | vector
Vertical preload spring force applied to the wheels on the axle at wheel carrier reference coordinates, $F_{z 0_{a^{\prime}}}$ in N. Positive preload forces:

- Cause the vehicle to lift.
- Point along the negative vehicle-fixed $z$-axis.

Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

Suspension shock damping constant, Cz - Suspension shock damping constant 10000 (default) | scalar | vector

Linear vertical damping constant for independent suspension wheels on axle a, $c_{z_{a^{\prime}}}$ in $\mathrm{Ns} / \mathrm{m}$.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Dependencies

To create this parameter, clear Enable active damping.
Suspension maximum height, Hmax - Height
0.5 (default) | scalar | vector

Maximum suspension extension or minimum suspension compression height, $H_{\text {max }}$, for axle a before the suspension reaches a hardstop, in m .

Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Geometry

Toe angle at steering center, Toe - Toe angle
0.0349 (default) | scalar

Nominal suspension toe angle at zero steering angle, $\zeta_{0 a}$, in rad.
Roll steer vs suspension height slope, RollStrgSIp - Steer angle suspension slope -0. 2269 (default) | scalar | vector

Roll steer angle versus suspension height, $m_{\text {htoe }}^{a_{a}}$, in $\mathrm{rad} / \mathrm{m}$.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

Toe angle vs steering angle slope, ToeStrgSIp - Toe angle steering slope
0.01 (default) | scalar | vector

Toe angle versus steering angle slope, $m_{\text {toesteer }_{d^{\prime}}}$ dimensionless.

Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Dependencies

To create input port StrgAng, set an element of the Steered axle enable by axle, StrgEnByAxl vector to 1.

Caster angle at steering center, Caster - Caster angle at steering center 0.0698 (default) | scalar

Nominal suspension caster angle at zero steering angle, $\eta_{0 a}$, in rad.
Caster angle vs suspension height slope, CasterHslp - Caster angle versus suspension height slope
-0. 2269 (default) | scalar | vector
Caster angle versus suspension height, $m_{\text {hcaster }_{a^{\prime}}}$ in $\mathrm{rad} / \mathrm{m}$.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

Caster angle vs steering angle slope, CasterStrgSIp - Caster angle versus steering angle slope 0.01 (default) | scalar | vector

Caster angle versus steering angle slope, $m_{\text {castersteer }_{a^{\prime}}}$ dimensionless.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Dependencies

To create input port StrgAng, set an element of the Steered axle enable by axle, StrgEnByAxl vector to 1.

Camber angle at steering center, Camber - Camber angle at steering center 0.0698 (default) | scalar

Nominal suspension camber angle at zero steering angle, $\xi_{0 a}$, in rad.
Camber angle vs suspension height slope, CamberHslp - Camber angle versus suspension height slope
-0. 2269 (default) | scalar | vector
Camber angle versus suspension height, $m_{\text {hcamber }_{a}}$, in $\mathrm{rad} / \mathrm{m}$.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

Camber angle vs steering angle slope, CamberStrgSIp - Camber angle versus steering angle slope
0.01 (default) | scalar | vector

Camber angle versus steering angle slope, $m_{\text {cambersteer }_{a^{\prime}}}$ dimensionless.
Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Dependencies

To create input port StrgAng, set an element of the Steered axle enable by axle, StrgEnByAxl vector to 1 .

Suspension height vs steering angle slope, StrgHgtSIp - Suspension height versus steering angle slope
0.1432 (default) | scalar | vector

Steering angle to vertical force slope applied at suspension wheel carrier reference point, $m_{\text {hsteer }}$, in $\mathrm{m} / \mathrm{rad}$.

Vector is 1 by the number of vehicle axles, $N_{a}$. If you provide a scalar value, the block uses that value for all axles.

## Dependencies

To create input port StrgAng, set an element of the Steered axle enable by axle, StrgEnByAxl vector to 1 .

## Version History

## Introduced in R2018a

## R2022b: Parameter name change from NumTracksByAxl to NumWhlsByAxl

Behavior changed in R2022b
The Number of tracks by axle, NumTracksByAxl parameter is renamed to Number of wheels by axle, NumWhlsByAxl.

The block uses the number of wheels per axle to index the input and output block signals.

## References

[1] Gillespie, Thomas. Fundamentals of Vehicle Dynamics. Warrendale, PA: Society of Automotive Engineers, 1992.
[2] Vehicle Dynamics Standards Committee. Vehicle Dynamics Terminology. SAE J670. Warrendale, PA: Society of Automotive Engineers, 2008.
[3] Technical Committee. Road vehicles - Vehicle dynamics and road-holding ability - Vocabulary. ISO 8855:2011. Geneva, Switzerland: International Organization for Standardization, 2011.

## Extended Capabilities

C/C++ Code Generation
Generate C and C++ code using Simulink ${ }^{\circledR}$ Coder ${ }^{\mathrm{TM}}$.

## See Also

Solid Axle Suspension | Solid Axle Suspension - Coil Spring | Solid Axle Suspension - Mapped

## Independent Suspension - K and C

Independent kinematics and compliance test suspension


## Libraries:

Vehicle Dynamics Blockset / Suspension

## Description

In the Vehicle Dynamics Blockset ${ }^{\text {TM }}$ library, there are two types of suspension blocks that implement the kinematics and compliance ( K and C ) test suspension characteristics measured from simulated or actual laboratory suspension tests.



## $K$ and C Effects on Suspension

To determine the overall suspension forces and geometric effects on the vehicle and wheels, the block adds the individual effects from kinematic (bounce, roll, steering) and compliance (longitudinal and lateral forces, aligning moments) inputs. Specifically, the block multiplies the suspension geometry states by either gradient or table values to determine the K and C effects on wheel orientation and suspension forces.

## Wheel orientation:

- Camber, caster, and steer angles
- Lateral wheel center displacement
- Longitudinal wheel center displacement

Vertical suspension forces:

- Anti-sway bar
- Shock force
- Wheel rate
- Contact patch swing arm (CPSA) force
- Longitudinal side view swing arm (SVSA) anti-effects


## Camber, Caster, and Steer Angles

The block uses these parameters to account for the K and C effects on the camber, caster, and steer angles.

- Bounce test- Independent suspension
- Roll test- Independent suspension
- Steer test
- Longitudinal compliance test
- Lateral compliance-opposed test
- Aligning torque compliance-opposed test

Use the Static alignment settings parameters to set the initial state of the suspension.

## Lateral Wheel Center Displacement

The block uses these parameters to account for the K and C effects the lateral wheel center displacement.

- Bounce test
- Longitudinal compliance test
- Lateral compliance-opposed test


## Longitudinal Wheel Center Displacement

The block uses these parameters to account for the K and C effects on the longitudinal wheel center displacement.

- Bounce test
- Longitudinal compliance test


## Shock Force

The block uses the Shock force parameters to calculate the shock force effect on the vertical suspension force. You can specify table-based or constant parameter values.

## Wheel Rate

The block uses the Bounce test parameters to calculate the wheel rate effect on the vertical suspension force.

## Contact Patch Swing Arm

The block uses these equations to calculate the effect of the contact patch swing arm (CPSA) forces on vertical suspension force.

$$
\begin{aligned}
& \tan \left(\theta_{C P S A}\right)=f\left(Z_{w}\right) \\
& F_{z C P S A}=F_{y} \tan \left(\theta_{C P S A}\right)
\end{aligned}
$$

The block also uses the Static loaded radius of wheels parameter in the CPSA force calculation.
The equations use these variables.
$\theta_{\text {CPSA }} \quad$ Contact patch swing arm angle
$F_{y} \quad$ Lateral suspension force
$F_{z C P S A} \quad$ CPSA effect on vertical suspension force
$z_{w} \quad$ Wheel displacement

## Longitudinal Side View Swing Arm Anti-Effects

The block uses these equations to calculate the effect of the side view swing arm (SVSA) forces on vertical suspension force during acceleration and braking.

$$
\begin{aligned}
& \tan \left(\theta_{S V S A}\right)=f\left(Z_{w}\right) \\
& F_{z S V S A}=F_{\chi} \tan \left(\theta_{S V S A}\right)
\end{aligned}
$$

Use the Drivetrain type parameter to ensure that the block applies the acceleration anti-effects to the correct wheels.

The equations use these variables.

| $\theta_{S V S A}$ | Contact patch swing arm angle |
| :--- | :--- |
| $F_{x}$ | Longitudinal wheel force |
| $F_{z S V S A}$ | SVSA effect on vertical suspension force |
| $z_{w}$ | Wheel displacement |

## Anti-Sway Bar

Optionally, use the Anti-sway axle enable by axle, AntiSwayEnByAxl parameter to implement antisway bar reaction forces by axle.

If you enable an anti-sway bar on the axle, the anti-sway bar stiffness is the difference between the anti-sway bar torque parameter, Suspension roll stiffness with anti-roll bar, RollStiffArb, and the roll stiffness parameter measured with no anti-sway bar present Suspension roll stiffness without anti-roll bar, RollStiffNoArb.

If you do not enable an anti-sway bar, the roll stiffness is 0 .

## Ports

The block uses the wheel number, $t$, to index the input and output signals. This table summarizes the wheel, axle, and corresponding wheel number for a vehicle with:

- Two axles
- Two wheels per axle

| Wheel | Axle | Wheel Number |
| :--- | :--- | :--- |
| Front left | Front | 1 |
| Front right | Front | 2 |
| Rear left | Rear | 1 |
| Rear right | Rear | 2 |

## Input

WhIPz - Wheel z-axis displacement
array
Wheel displacement, $z_{w}$, along wheel-fixed $z$-axis, in $m$. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlPz:

- Signal array dimensions are [1×4].

$$
\text { WhlPz }=z_{w}=\left[\begin{array}{llll}
z_{w_{1,1}} & z_{w_{1,2}} & z_{w_{2,1}} & z_{w_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlPz $(1,1)$ | 1 | 1 |
| Front right | WhlPz $(1,2)$ | 1 | 2 |
| Rear left | WhlPz $(1,3)$ | 2 | 1 |
| Rear right | WhlPz $(1,4)$ | 2 | 2 |

WhIRe - Wheel effective radius
array
Effective wheel radius, $R e_{w}$, in m. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlRe:

- Signal array dimensions are [1×4].

$$
\text { WhlRe }=R e_{w}=\left[\begin{array}{lll}
R e_{w_{1,1}} & R e_{w_{1,2}} & R e_{w_{2,1}}
\end{array} R e_{w_{2,2}}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlRe $(1,1)$ | 1 | 1 |
| Front right | WhlRe $(1,2)$ | 1 | 2 |
| Rear left | WhlRe $(1,3)$ | 2 | 1 |
| Rear right | WhlRe $(1,4)$ | 2 | 2 |

WhIVz - Wheel z-axis velocity array

Wheel velocity, $\dot{z}_{w}$, along wheel-fixed $z$-axis, in m. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlVz:

- Signal array dimensions are [1×4].

WhlVz $=\dot{z}_{w}=\left[\begin{array}{lll}\dot{z}_{w_{1,1}} & \dot{z}_{w_{1,2}} & \dot{z}_{w_{2,1}}\end{array} \dot{z}_{w_{2,2}}\right]$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlVz $(1,1)$ | 1 | 1 |
| Front right | WhlVz $(1,2)$ | 1 | 2 |
| Rear left | WhlVz $(1,3)$ | 2 | 1 |
| Rear right | WhlVz $(1,4)$ | 2 | 2 |

WhIFx - Longitudinal wheel force on vehicle
array

Longitudinal wheel force applied to vehicle, $F_{w x}$, along the vehicle-fixed $x$-axis. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlFx:

- Signal array dimensions are [1×4].

$$
\mathrm{WhlFx}=F_{w x}=\left[\begin{array}{ll}
F_{w x_{1,1}} & F_{w x_{1,2}} \\
F_{w x_{2,1}} & F_{w x_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlFx $(1,1)$ | 1 | 1 |
| Front right | WhlFx $(1,2)$ | 1 | 2 |
| Rear left | WhlFx $(1,3)$ | 2 | 1 |
| Rear right | WhlFx $(1,4)$ | 2 | 2 |

WhIFy - Lateral wheel force on vehicle
array
Lateral wheel force applied to vehicle, $F_{w y}$, along the vehicle-fixed $y$-axis. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlFy:

- Signal array dimensions are [1x4].

$$
\text { WhlFy }=F_{w y}=\left[F_{w y_{1,1}} F_{w y_{1,2}} F_{w y_{2,1}} F_{w y_{2,2}}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlFy $(1,1)$ | 1 | 1 |
| Front right | WhlFy $(1,2)$ | 1 | 2 |
| Rear left | WhlFy $(1.3)$ | 2 | 1 |
| Rear right | WhlFy $(1,4)$ | 2 | 2 |

WhIM - Suspension moment on wheel
array
Longitudinal, lateral, and vertical suspension moments at axle a, wheel $t$, applied to the wheel at the axle wheel carrier reference coordinate, in $N \cdot m$. Input array dimensions are 3 by the number of wheels on the vehicle.

- WhlM (1, ...) - Suspension moment applied to the wheel about the vehicle-fixed $x$-axis (longitudinal)
- WhlM ( $2, \ldots$ ) - Suspension moment applied to the wheel about the vehicle-fixed $y$-axis (lateral)
- WhlM ( $3, \ldots$ ) - Suspension moment applied to the wheel about the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the WhlM:

- Signal dimensions are [3×4].
- Signal contains suspension moments applied to four wheels according to their axle and wheel locations.

$$
\text { WhlM }=M_{w}=\left[\begin{array}{llll}
M_{w x_{1,1}} & M_{w x_{1,2}} & M_{w x_{2,1}} & M_{w x_{2,2}} \\
M_{w y_{1,1}} & M_{w y_{1,2}} & M_{w y_{2,1}} & M_{w y 2,2} \\
M_{w z_{1,1}} & M_{w z_{1,2}} & M_{w z_{2,1}} & M_{w z_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Moment Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | WhlM(1,1) | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front <br> right | WhlM(1,2) | 1 | 2 |  |
| Rear <br> left | WhlM(1,3) | 2 | 1 |  |
| Rear <br> right | WhlM(1,4) | 2 | 2 |  |
| Front <br> left | WhlM(2,1) | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front <br> right | WhlM(2,2) | 1 | 2 |  |
| Rear <br> left | WhlM(2,3) | 2 | 1 |  |
| Rear <br> right | WhlM(2,4) | 2 | 2 |  |
| Front <br> left | WhlM(3,1) | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front <br> right | WhlM(3,2) | 1 | 2 |  |
| Rear <br> left | WhlM(3,3) | 2 | 1 |  |
| Rear <br> right | WhlM(3,4) | 2 | 2 |  |

VehP - Vehicle displacement
array
Vehicle displacement from axle a, wheel $t$ along vehicle-fixed coordinate system, in m. Input array dimensions are 3 the number of wheels on the vehicle.

- VehP $(1, \ldots)$ - Vehicle displacement from wheel, $\chi_{v}$, along the vehicle-fixed $x$-axis
- $\operatorname{VehP}(2, \ldots)$ - Vehicle displacement from wheel, $y_{v}$, along the vehicle-fixed $y$-axis
- $\operatorname{VehP}(3, \ldots)-$ Vehicle displacement from wheel, $z_{v}$, along the vehicle-fixed $z$-axis

For example, for a two-axle vehicle with two wheels per axle, the VehP:

- Signal dimensions are [3x4].
- Signal contains four displacements according to their axle and wheel locations.

$$
\text { VehP }=\left[\begin{array}{l}
x_{v} \\
y_{v} \\
z_{v}
\end{array}\right]=\left[\begin{array}{llll}
x_{v_{1,1}} & x_{v_{1,2}} & x_{v_{2,1}} & x_{v_{2,2}} \\
y_{v_{1,1}} & y_{v_{1,2}} & y_{v_{2,1}} & y_{v_{2,2}} \\
z_{v_{1,1}} & z_{v_{1,2}} & z_{v_{2,1}} & z_{v_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel Numbe r | Axis |
| :---: | :---: | :---: | :---: | :---: |
| Front left | $\operatorname{VehP}(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis |
| Front right | $\operatorname{VehP}(1,2)$ | 1 | 2 |  |
| $\begin{array}{\|l} \hline \begin{array}{l} \text { Rear } \\ \text { left } \end{array} \\ \hline \end{array}$ | $\operatorname{VehP}(1,3)$ | 2 | 1 |  |
| Rear right | $\operatorname{VehP}(1,4)$ | 2 | 2 |  |
| Front left | $\operatorname{VehP}(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis |
| Front right | $\operatorname{VehP}(2,2)$ | 1 | 2 |  |
| $\begin{array}{\|l} \text { Rear } \\ \text { left } \end{array}$ | $\operatorname{VehP}(2,3)$ | 2 | 1 |  |
| Rear right | $\operatorname{VehP}(2,4)$ | 2 | 2 |  |
| Front left | $\operatorname{VehP}(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis |
| Front right | $\operatorname{VehP}(3,2)$ | 1 | 2 |  |
| $\begin{array}{\|l} \begin{array}{l} \text { Rear } \\ \text { left } \end{array} \\ \hline \end{array}$ | $\operatorname{VehP}(3,3)$ | 2 | 1 |  |
| Rear right | $\operatorname{VehP}(3,4)$ | 2 | 2 |  |

VehV - Vehicle velocity
array
Vehicle velocity at axle a, wheel t along vehicle-fixed coordinate system, in m . Input array dimensions are 3 by the number of wheels on the vehicle.

- $\operatorname{VehV}(1, \ldots)-$ Vehicle velocity at wheel, $x_{v}$, along the vehicle-fixed $x$-axis
- $\operatorname{VehV}(2, \ldots)$ - Vehicle velocity at wheel, $y_{v}$, along the vehicle-fixed $y$-axis
- $\operatorname{VehV}(3, \ldots)-$ Vehicle velocity at wheel, $z_{v}$, along the vehicle-fixed $z$-axis

For example, for a two-axle vehicle with two wheels per axle, the VehV:

- Signal dimensions are [3×4].
- Signal contains 4 velocities according to their axle and wheel locations.

$$
\text { VehV }=\left[\begin{array}{c}
\dot{x}_{v} \\
\dot{y}_{v} \\
\dot{z}_{v}
\end{array}\right]=\left[\begin{array}{llll}
\dot{x}_{v_{1,1}} & \dot{x}_{v_{1,2}} & \dot{x}_{v_{2,1}} & \dot{x}_{v_{2,2}} \\
\dot{y}_{v_{1,1}} & \dot{y}_{v_{1,2}} & \dot{y}_{v_{2,1}} & \dot{v}_{v_{2,2}} \\
\dot{z}_{v_{1,1}} & \dot{z}_{v_{1,2}} & \dot{z}_{v_{2,1}} & \dot{z}_{v_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel Numbe r | Axis |
| :---: | :---: | :---: | :---: | :---: |
| Front left | $\operatorname{VehV}(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis |
| Front right | $\operatorname{VehV}(1,2)$ | 1 | 2 |  |
| $\begin{array}{\|l} \hline \begin{array}{l} \text { Rear } \\ \text { left } \end{array} \\ \hline \end{array}$ | $\operatorname{VehV}(1,3)$ | 2 | 1 |  |
| Rear right | $\operatorname{VehV}(1,4)$ | 2 | 2 |  |
| Front left | $\operatorname{VehV}(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis |
| Front right | $\operatorname{VehV}(2,2)$ | 1 | 2 |  |
| Rear <br> left | $\operatorname{VehV}(2,3)$ | 2 | 1 |  |
| Rear right | $\operatorname{VehV}(2,4)$ | 2 | 2 |  |
| Front left | $\operatorname{VehV}(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis |
| Front right | $\operatorname{VehV}(3,2)$ | 1 | 2 |  |
| Rear left | $\operatorname{VehV}(3,3)$ | 2 | 1 |  |
| Rear right | $\operatorname{VehV}(3,4)$ | 2 | 2 |  |

StrgAng - Steering angle, optional
array
Optional steering angle for each wheel, $\delta$. Input array dimensions are 1 by the number of steered wheels.

For example, for a two-axle vehicle with two wheels per axle, you can input steering angles for both wheels on the first axle.

- To create the StrgAng port, set Steered axle enable by axle, StrgEnByAxl to [1 0]. The input signal array dimensions are [1×2].
- The StrgAng signal contains two steering angles according to their axle and wheel locations.

$$
\text { StrgAng }=\delta_{\text {steer }}=\left[\delta_{\text {steer }_{1,1}} \delta_{\text {steer }_{1,2}}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | StrgAng $(1,1)$ | 1 | 1 |
| Front right | StrgAng $(1,2)$ | 1 | 2 |

## Dependencies

To create input port StrgAng, set an element of the Steered axle enable by axle, StrgEnByAxl vector to 1 .

Phi - Vehicle pitch angle
scalar
Vehicle pitch angle about earth-fixed $Y$-axis, in rad.
TrckWdth - Track width
array
Distance between wheels on each axle. Input array dimensions are 1-by-2.

| Array Element | Description |
| :--- | :--- |
| TrckWdth $(1,1)$ | Distance between wheels on front axle |
| TrckWdth $(1,2)$ | Distance between wheels on rear axle |

## Output

Info - Bus signal
bus
Bus signal containing block values. The signals are arrays that depend on the wheel location.
For example, here are the indices for a two-axle, two-wheel vehicle. The total number of wheels is four.

- 1D array signal (1-by-4)

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | $(1,1)$ | 1 | 1 |
| Front right | $(1,2)$ | 1 | 2 |
| Rear left | $(1,3)$ | 2 | 1 |
| Rear right | $(1,4)$ | 2 | 2 |

- 3D array signal (3-by-4)

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | $(1,1)$ | 1 | 1 |
| Front right | $(1,2)$ | 1 | 2 |
| Rear left | $(1,3)$ | 2 | 1 |
| Rear right | $(1,4)$ | 2 | 2 |
| Front left | $(2,1)$ | 1 | 1 |


| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front right | $(2,2)$ | 1 | 2 |
| Rear left | $(2,3)$ | 2 | 1 |
| Rear right | $(2,4)$ | 2 | 2 |
| Front left | $(3,1)$ | 1 | 1 |
| Front right | $(3,2)$ | 1 | 2 |
| Rear left | $(3,3)$ | 2 | 1 |
| Rear right | $(3,4)$ | 2 | 2 |


| Signal | Description | Array Signal | Variable | Units |
| :---: | :---: | :---: | :---: | :---: |
| Camber | Wheel angles according to the axle and wheel location. | 1D | WhlAng $[1, \ldots]=\xi=\left[\xi_{a, t}\right]$ | rad |
| Caster |  |  | WhlAng $[2, \ldots]=\eta=\left[\eta_{a, t}\right]$ |  |
| Toe |  |  | WhlAng $[3, \ldots]=\zeta=\left[\zeta_{a, t}\right]$ |  |
| Height | Suspension height | 1D | H | m |
| Power | Suspension power dissipation | 1D | $P_{\text {susp }}$ | W |
| Energy | Suspension absorbed energy | 1D | $E_{\text {susp }}$ | J |
| VehF | Suspension forces applied to the vehicle | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { VehF }=F_{v}= \\ & {\left[\begin{array}{llll} F_{v x_{1,1}} & F_{v x_{1,2}} & F_{v x_{2,1}} & F_{v x_{2}, 2} \\ F_{v y 1,1} & F_{v x_{1,2}} & F_{v v_{2,1}} & F_{v y 2,2} \\ F_{v x_{1,1}} & F_{v x_{1,2}} & F_{v z_{2,1}} & F_{v z_{2,2}} \end{array}\right.} \end{aligned}$ | N |


| Signal | Description | Array Signal | Variable Units |
| :---: | :---: | :---: | :---: |
| VehM | Suspension moments applied to vehicle | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { VehM }=M_{v}= \\ & {\left[\begin{array}{lllll} M_{v x_{1}, 1} & M_{v x_{1}, 2} & M_{v x_{2,1}} & M_{v \times 2,2} \\ M_{v y_{1,1}} & M_{v y_{1,2}} & M_{v y 2,1} & M_{v y 2,2} \\ M_{v z_{1,1}} & M_{v z_{1,2}} & M_{v z_{2,1}} & M_{v \chi_{2,2}} \end{array}\right.} \end{aligned}$ |
| WhlF | Suspension force applied to wheel | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { WhlF }=F_{w}= \\ & {\left[\begin{array}{llll} F_{w x_{1}, 1} & F_{w x_{1,2}} & F_{w x_{2,1}} & F_{w x_{2}, 2} \\ F_{w y_{1,1}} & F_{w y_{1,2}} & F_{w y 2,1} & F_{w y_{2,2}} \\ F_{w z_{1,1}} & F_{w z_{1,2}} & F_{w z_{2,1}} & F_{w z_{2,2}} \end{array}\right.} \end{aligned}$ |
| WhlP | Wheel displacement | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { WhlP }=\left[\begin{array}{l} x_{w} \\ y_{w} \\ z_{w} \end{array}\right]= \\ & {\left[\begin{array}{llll} x_{w_{1,1}} & x_{w_{1,2}} & x_{w_{2,1}} & x_{w_{2,2}} \\ y_{w_{1,1}} & y_{w_{1,2}} & y_{w_{2,1}} & y_{w \not{ }_{2,2}} \\ z_{w t r_{1,1}} & z_{w t r_{1,2}} & z_{w t r_{2,1}} & z_{w t t_{2,2}} \end{array}\right.} \end{aligned}$ |


| Signal | Description | Array Signal | Variable | Units |
| :---: | :---: | :---: | :---: | :---: |
| WhlV | Wheel velocity | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { WhlV }=\left[\begin{array}{l} \dot{x}_{w} \\ \dot{y}_{w} \\ \dot{z}_{w} \end{array}\right] \\ & = \\ & {\left[\begin{array}{llll} \dot{x}_{w_{1,1}} & \dot{x}_{w_{1,2}} & \dot{x}_{w_{2,1}} & \dot{x}_{w_{2,2}} \\ \dot{y}_{w_{1,1}} & \dot{y}_{w_{1,2}} & \dot{y}_{w_{2,1}} & \dot{y}_{w_{2,2}} \\ \dot{z}_{w_{1,1}} & \dot{z}_{w_{1,2}} & \dot{z}_{w_{2,1}} & \dot{z}_{w_{2,2}} \end{array}\right]} \end{aligned}$ | $\mathrm{m} / \mathrm{s}$ |
| WhlAng | Wheel camber, caster, toe angles | 3D | For a two-axle, two wheels per axle vehicle: $\left.\begin{array}{l} \text { WhlAng }=\left[\begin{array}{l} \xi \\ \eta \\ \zeta \end{array}\right] \\ =\left[\begin{array}{lll} \xi_{1,1} & \xi_{1,2} & \xi_{2,1} \\ \xi_{2,2} \\ \eta_{1,1} & \eta_{1,2} & \eta_{2,1} \\ \zeta_{2,2} \\ \zeta_{1,1} & \zeta_{1,2} & \zeta_{2,1} \end{array} \zeta_{2,2}\right. \end{array}\right] .$ | rad |

## VehF - Suspension force on vehicle array

Longitudinal, lateral, and vertical suspension force at axle a, wheel $t$, applied to the vehicle at the suspension connection point, in N. Array dimensions are 3 by the number of wheels on the vehicle.

- $\operatorname{VehF}(1, \ldots)$ - Suspension force applied to vehicle along the vehicle-fixed $x$-axis (longitudinal)
- $\operatorname{VehF}(2, \ldots)$ - Suspension force applied to vehicle along the vehicle-fixed $y$-axis (lateral)
- $\operatorname{VehF}(3, \ldots)$ - Suspension force applied to vehicle along the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the VehF:

- Signal dimensions are [3×4].
- Signal contains suspension forces applied to the vehicle according to the axle and wheel locations.

$$
\text { VehF }=F_{v}=\left[\begin{array}{lllll}
F_{v x_{1,1}} & F_{v x_{1,2}} & F_{v x_{2,1}} & F_{v x_{2,2}} \\
F_{v y 1,1} & F_{v y_{1,2}} & F_{v y_{2,1}} & F_{v y_{2,2}} \\
F_{v z_{1,1}} & F_{v z_{1,2}} & F_{v z_{2,1}} & F_{v z_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel Numbe r | Force Axis |
| :---: | :---: | :---: | :---: | :---: |
| Front left | $\operatorname{VehF}(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front right | $\operatorname{VehF}(1,2)$ | 1 | 2 |  |
| Rear left | $\operatorname{VehF}(1,3)$ | 2 | 1 |  |
| Rear right | $\operatorname{VehF}(1,4)$ | 2 | 2 |  |
| Front left | $\operatorname{VehF}(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front right | $\operatorname{VehF}(2,2)$ | 1 | 2 |  |
| Rear left | $\operatorname{VehF}(2,3)$ | 2 | 1 |  |
| Rear right | $\operatorname{VehF}(2,4)$ | 2 | 2 |  |
| Front left | $\operatorname{VehF}(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front right | $\operatorname{VehF}(3,2)$ | 1 | 2 |  |
| Rear left | $\operatorname{VehF}(3,3)$ | 2 | 1 |  |
| Rear right | $\operatorname{VehF}(3,4)$ | 2 | 2 |  |

VehM - Suspension moment on vehicle
array
Longitudinal, lateral, and vertical suspension moment at axle a, wheel $t$, applied to the vehicle at the suspension connection point, in $\mathrm{N} \cdot \mathrm{m}$. Array dimensions are 3 by the number of wheels on the vehicle.

- VehM ( $1, \ldots$ ) - Suspension moment applied to the vehicle about the vehicle-fixed $x$-axis (longitudinal)
- VehM ( $2, \ldots$ ) - Suspension moment applied to the vehicle about the vehicle-fixed $y$-axis (lateral)
- VehM ( $3, \ldots$ ) - Suspension moment applied to the vehicle about the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the VehM:

- Signal dimensions are [3×4].
- Signal contains suspension moments applied to vehicle according to the axle and wheel locations.

$$
\text { VehM }=M_{v}=\left[\begin{array}{llll}
M_{v x_{1,1}} & M_{v x_{1,2}} & M_{v x_{2,1}} & M_{v x_{2,2}} \\
M_{v y 1,1} & M_{v y_{1,2}} & M_{v y 2,1} & M_{v y_{2,2}} \\
M_{v z_{1,1}} & M_{v z_{1,2}} & M_{v z_{2,1}} & M_{v z_{2,2}}
\end{array}\right]
$$

| Array Element | Axle | Wheel <br> Number | Moment Axis |
| :--- | :--- | :--- | :--- |
| VehM $(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| $\operatorname{VehM}(1,2)$ | 1 | 2 |  |
| $\operatorname{VehM}(1,3)$ | 2 | 1 |  |
| $\operatorname{VehM}(1,4)$ | 2 | 2 |  |
| $\operatorname{VehM}(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| $\operatorname{VehM}(2,2)$ | 1 | 2 |  |
| $\operatorname{VehM}(2,3)$ | 2 | 1 |  |
| $\operatorname{VehM}(2,4)$ | 2 | 2 |  |
| $\operatorname{VehM}(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| $\operatorname{VehM}(3,2)$ | 1 | 2 |  |
| $\operatorname{VehM}(3,3)$ | 2 | 1 |  |
| $\operatorname{VehM}(3,4)$ | 2 | 2 |  |

WhIF - Suspension force on wheel
array
Longitudinal, lateral, and vertical suspension forces at axle a, wheel $t$, applied to the wheel at the axle wheel carrier reference coordinate, in N. Array dimensions are 3 by the number of wheels on the vehicle.

- $\operatorname{WhlF}(1, \ldots)$ - Suspension force on wheel along the vehicle-fixed $x$-axis (longitudinal)
- $\operatorname{WhlF}(2, \ldots)$ - Suspension force on wheel along the vehicle-fixed $y$-axis (lateral)
- $\operatorname{WhlF}(3, \ldots)$ - Suspension force on wheel along the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the WhlF:

- Signal dimensions are [3×4].
- Signal contains wheel forces applied to the vehicle according to the axle and wheel locations.

$$
\text { WhlF }=F_{w}=\left[\begin{array}{lllll}
F_{w x_{1,1}} & F_{w x_{1,2}} & F_{w x_{2,1}} & F_{w x_{2,2}} \\
F_{w y 1,1} & F_{w y 1,2} & F_{w y 2,1} & F_{w y 2,2} \\
F_{w z_{1,1}} & F_{w z_{1,2}} & F_{w z_{2,1}} & F_{w z 2,2}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> $\mathbf{r}$ | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | WhlF $(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |


| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> right | WhlF (1,2) | 1 | 2 |  |
| Rear <br> left | WhlF (1,3) | 2 | 1 |  |
| Rear <br> right | WhlF (1,4) | 2 | 2 |  |
| Front <br> left | WhlF (2,1) | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front <br> right | WhlF (2,2) | 1 | 2 |  |
| Rear <br> left | WhlF $(2,3)$ | 2 | 1 |  |
| Rear <br> right | WhlF (2,4) | 2 | 2 |  |
| Front <br> left | WhlF (3,1) | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front <br> right | WhlF (3,2) | 1 | 2 |  |
| Rear <br> left | WhlF (3,3) | 2 | 1 |  |
| Rear <br> right | WhlF (3,4) | 2 | 2 |  |

## WhIV - Wheel velocity

array
Longitudinal, lateral, and vertical wheel velocity at axle a, wheel t , in $\mathrm{m} / \mathrm{s}$. Array dimensions are 3 by the number of wheels on the vehicle.

- WhlV (1, ...) - Wheel velocity along the vehicle-fixed $x$-axis (longitudinal)
- $\operatorname{WhlV}(2, \ldots)-$ Wheel velocity along the vehicle-fixed $y$-axis (lateral)
- $\operatorname{WhlV}(3, \ldots)-$ Wheel velocity along the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the WhlV:

- Signal dimensions are [3×4].
- Signal contains wheel forces applied to the vehicle according to the axle and wheel locations.

$$
\text { WhlV }=\left[\begin{array}{l}
\dot{x}_{w} \\
\dot{y}_{w} \\
\dot{z}_{w}
\end{array}\right]=\left[\begin{array}{llll}
\dot{x}_{w_{1,1}} & \dot{x}_{w_{1,2}} & \dot{x}_{w_{2,1}} & \dot{x}_{w_{2,2}} \\
\dot{y}_{w_{1,1}} & \dot{y}_{w_{1,2}} & \dot{y}_{w_{2,1}} & \dot{y}_{w_{2,2}} \\
\dot{z}_{w_{1,1}} & \dot{z}_{w_{1,2}} & \dot{z}_{w_{2,1}} & \dot{z}_{w_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel Numbe r | Force Axis |
| :---: | :---: | :---: | :---: | :---: |
| Front left | WhlV (1,1) | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front right | WhlV (1,2) | 1 | 2 |  |
| Rear <br> left | WhlV (1,3) | 2 | 1 |  |
| Rear right | WhlV $(1,4)$ | 2 | 2 |  |
| Front left | WhlV $(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front right | WhlV $(2,2)$ | 1 | 2 |  |
| Rear left | WhlV $(2,3)$ | 2 | 1 |  |
| Rear right | WhlV $(2,4)$ | 2 | 2 |  |
| Front left | WhlV $(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front right | WhlV (3,2) | 1 | 2 |  |
| $\begin{aligned} & \text { Rear } \\ & \text { left } \end{aligned}$ | Whlv (3, 3) | 2 | 1 |  |
| Rear right | WhlV $(3,4)$ | 2 | 2 |  |

WhIAng - Wheel camber, caster, toe angles
array
Camber, caster, and toe angles at axle a, wheel $t$, in rad. Array dimensions are 3 by the number of wheels on the vehicle.

- WhlAng(1,...) - Camber angle
- WhlAng $(2, \ldots)$ - Caster angle
- Whlang $(3, \ldots)$ - Toe angle

For example, for a two-axle vehicle with two wheels per axle, the WhlAng:

- Signal dimensions are [3×4].
- Signal contains angles according to the axle and wheel locations.

$$
\text { WhlAng }=\left[\begin{array}{l}
\xi \\
\eta \\
\zeta
\end{array}\right]=\left[\begin{array}{llll}
\xi_{1,1} & \xi_{1,2} & \xi_{2,1} & \xi_{2,2} \\
\eta_{1,1} & \eta_{1,2} & \eta_{2,1} & \eta_{2,2} \\
\zeta_{1,1} & \zeta_{1,2} & \zeta_{2,1} & \zeta_{2,2}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Angle |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | WhlAng (1,1) | 1 | 1 | Camber |
| Front <br> right | WhlAng (1,2) | 1 | 2 |  |
| Rear <br> left | WhlAng (1,3) | 2 | 1 |  |
| Rear <br> right | WhlAng (1,4) | 2 | 2 |  |
| Front <br> left | WhlAng (2,1) | 1 | 1 | Caster |
| Front <br> right | WhlAng (2,2) | 1 | 2 |  |
| Rear <br> left | WhlAng (2,3) | 2 | 1 |  |
| Rear <br> right | WhlAng (2,4) | 2 | 2 |  |
| Front <br> left | WhlAng (3,1) | 1 | 1 | Toe |
| Front <br> right | WhlF(3,2) | 1 | 2 |  |
| Rear <br> left | WhlF(3,3) | 2 | 1 |  |
| Rear <br> right | WhlF(3,4) | 2 | 2 |  |

## Parameters

Steered axle enable by axle, StrgEnByAxI - Boolean vector to enable axle steering
[1 0] (default)| vector
Boolean vector that enables axle steering, $E n_{\text {steer }}$, dimensionless. Vector is 1 by the number of vehicle axles, $N_{a}$. For example:

- [1 0] - For a two-axle vehicle, enables axle 1 steering and disables axle 2 steering
- [ll $\left.\begin{array}{ll}1 & 1\end{array}\right]$ - For a two-axle vehicle, enables axle 1 and axle 2 steering


## Dependencies

Setting any element of the Steered axle enable by axle, StrgEnByAxl vector to 1 creates Input port StrgAng.

Anti-sway axle enable by axle, AntiSwayEnByAxI - Boolean vector to enable axle anti-sway [0 0] (default)|vector

Boolean vector that enables axle anti-sway for axle $a$, dimensionless. For example, [ 1 0] enables axle 1 anti-sway and disables axle 2 anti-sway. Vector is 1 by the number of vehicle axles, $N_{a}$.

If you enable an anti-sway bar on the axle, the anti-sway bar stiffness is the difference between the anti-sway bar torque parameter, Suspension roll stiffness with anti-roll bar, RollStiffArb, and the roll stiffness parameter measured with no anti-sway bar present Suspension roll stiffness without anti-roll bar, RollStiffNoArb.

If you do not enable an anti-sway bar, the stiffness is 0 .

## Suspension Parameters

## Suspension type - Type of suspension

Independent front and rear|Independent front and twist beam rear

Select type of suspension.
Drivetrain type - Type of drivetrain
FWD (default) | RWD \| AWD
Select type of drivetrain.

- AWD - All-wheel drive
- FWD - Front-wheel drive
- RWD - Rear-wheel drive


## Directions

+ Steer angle - Positive steer angle
Right (default) | Left
Direction of positive steer angle during kinematics and compliance test.
+ Fx used in compliance tests - Positive longitudinal force
Front (default) | Rear
Direction of positive longitudinal force during kinematics and compliance test.
+ Fy used in compliance tests - Positive lateral force
Right (default) |Left
Direction of positive lateral force during kinematics and compliance test.
+ Suspension Jounce - Positive suspension jounce
Up (default) | Down
Direction of positive suspension jounce during kinematics and compliance test.
+ WhIMz used in compliance tests - Positive yaw moment
Counter-clockwise (default)|Clockwise
Direction of positive yaw moment during kinematics and compliance test.


## Shock force

Shock type - Type of shock force
Table-based (default)|Table-based individualConstant
Type of shock force.
If a table-based individual setting is chosen, table-based shock force is implemented together with constant motion ratios. If a table-based setting is chosen both shock force and motion ratios are calculated from lookup tables.

| Setting | Implementation |
| :--- | :--- |
| Table-based | Table-based shock force and motion ratios. |
| Table-based individual | Table-based shock force and constant motion <br> ratios. |
| Constant | Constant shock force and motion ratios. |

## Shock force vs shock compression rate, ShckFrceVsCompRate - Table

struct('FL',[-100. -5000;0 0;100. 5000],'FR',[-100. -5000;0 0;100.
5000],'RL',[-100. -5000;0 0;100. 5000],'RR',[-100. -5000;0 0;100. 5000]) (default)

Shock force versus shock compression rate, specified as a structure, in $\mathrm{N} / \mathrm{mm}$ per sec.

## Dependencies

To create this parameter, set Shock type to Table-based or Table-based individual.

## Data Types: struct

Motion ratios by axle, MotRatios - Table
struct('FL',[-0.1 -0.1;0 0;0.1 0.1],'FR',[-0.1 -0.1;0 0;0.1 0.1],'RL',[-0.1 -0.1;0 0;0.1 0.1],'RR',[-0.1 -0.1;0 0;0.1 0.1]) (default)

Motion ratios by axle, specified as a structure.
Data Types: struct

## Bounce test

Bump steer, BumpSteer - Table

```
struct('FL',[-0.1 1.1459;0 0;0.1 -1.1459],'FR',[-0.1 1.1459;0 0;0.1
```

-1.1459],'RL',[-0.1 0.;0 0;0.1 0.],'RR',[-0.1 0.;0 0;0.1 0.]) (default)

Bump steer, specified as a structure, in deg/m.
Data Types: struct
Bump camber, BumpCamber - Table
struct('FL',[-0.1 1.7189;0 0;0.1 -1.7189],'FR',[-0.1 1.7189;0 0;0.1
-1.7189],'RL',[-0.1 0.;0 0;0.1 0.],'RR',[-0.1 0.;0 0;0.1 0.]) (default)
Bump camber, specified as a structure, in deg/m.
Data Types: struct

## Bump caster, BumpCaster - Table

```
struct('FL',[-0.1 1.1459;0 0;0.1 -1.1459],'FR',[-0.1 1.1459;0 0;0.1
-1.1459],'RL',[-0.1 -11.4592;0 0;0.1 11.4592],'RR',[-0.1 -11.4592;0 0;0.1
11.4592]) (default)
```

Bump caster, specified as a structure, in deg/m.
Data Types: struct

## Lateral wheel center displacement, LatWhICtrDisp - Table

struct('FL',[-0.1 0.02;0 0;0.1 -0.02],'FR',[-0.1 0.02;0 0;0.1 -0.02],'RL', [-0.1 0.;0 0;0.1 0.],'RR',[-0.1 0.;0 0;0.1 0.]) (default)

Lateral wheel center displacement, specified as a structure, in $\mathrm{mm} / \mathrm{mm}$.
Data Types: struct

## Longitudinal wheel center displacement, LngWhICtrDisp - Table

struct('FL',[-0.1 -0.002;0 0;0.1 0.002],'FR',[-0.1 -0.002;0 0;0.1
0.002],'RL',[-0.1 0.;0 0;0.1 0.],'RR',[-0.1 0.02;0 0;0.1 0.01]) (default)

Longitudinal wheel center displacement, specified as a structure, in $\mathrm{mm} / \mathrm{mm}$.
Data Types: struct
Normal wheel rates, NrmIWhIRates - Table
struct('FL',[-100. -5000;0 0;100. 5000],'FR',[-100. -5000;0 0;100.
5000],'RL',[-100. -5000;0 0;100. 5000],'RR',[-100. -5000;0 0;100. 5000])
(default) | vector
Normal wheel rates, specified as a structure, in N/mm.
Data Types: struct
Normal wheel force offsets, NrmIWhIFrcOff - Force offset
[0 0 0 0] (default)
Normal wheel force offsets, specified as a vector, in N.

## Dependencies

To create this parameter, specify a Normal wheel rates, NrmlWhlRates vector.
Data Types: struct
Roll test
Suspension roll stiffness with anti-roll bar, RollStiffArb - Anti-sway bar enabled [800 700] (default) | 1-by-2 vector

Suspension roll stiffness with anti-roll bar, specified as a 1-by-2 vector, in Nm/deg. The first element is the front axle roll stiffness. The second element is the rear axle roll stiffness.

If you enable an anti-sway bar on the axle, the anti-sway bar stiffness is the difference between the anti-sway bar torque parameter, Suspension roll stiffness with anti-roll bar, RollStiffArb, and the roll stiffness parameter measured with no anti-sway bar present Suspension roll stiffness without anti-roll bar, RollStiffNoArb.

If you do not enable an anti-sway bar, the stiffness is 0 .

## Dependencies

To enable this parameter, set Suspension type to Independent front and rear.
Data Types: double
Suspension roll stiffness without anti-roll bar, RollStiffNoArb - Anti-sway bar not enabled
[0 0] (default) | 1-by-2 vector
Suspension roll stiffness without anti-roll bar, specified as a 1-by-2 vector, in Nm/deg. The first element is the front axle roll stiffness. The second element is the rear axle roll stiffness.

If you enable an anti-sway bar on the axle, the anti-sway bar stiffness is the difference between the anti-sway bar torque parameter, Suspension roll stiffness with anti-roll bar, RollStiffArb, and the roll stiffness parameter measured with no anti-sway bar present Suspension roll stiffness without anti-roll bar, RollStiffNoArb.

If you do not enable an anti-sway bar, the stiffness is 0 .

## Dependencies

To enable this parameter, set Suspension type to Independent front and rear.
Data Types: double

## Steer test

Camber vs steer angle, CambVsSteerAng - Table
struct('FL',[-10. -1.;0 0;10. 1.],'FR',[-10. 1.;0 0;10. -1.],'RL',[-10. -1.;0
0;10. 1.],'RR',[-10. 1.;0 0;10. -1.]) (default)
Camber vs steer angle, specified as a structure, in deg/deg.
Data Types: struct
Caster vs steer angle, CastVsSteerAng - Table
struct('FL',[-10. -1.;0 0;10. 1.],'FR',[-10. 1.;0 0;10. -1.],'RL',[-10. -1.;0 0;10. 1.],'RR',[-10. 1.;0 0;10. -1.]) (default)

Caster vs steer angle, specified as a structure, in deg/deg.

## Data Types: struct

## Longitudinal compliance test

Longitudinal steer compliance, LngSteerCompl - Table

```
struct('NegFx',struct('FL',[-2. -1.;0 0;2. 1.],'FR',[-2. 1.;0 0;2. -1.],'RL',
[-2. -1.;0 0;2. 1.],'RR',[-2. 1.;0 0;2. -1.]),'PosFx',struct('FL',[-2. -1.;0
0;2. 1.],'FR',[-2. 1.;0 0;2. -1.],'RL',[-2. -1.;0 0;2. 1.],'RR',[-2. 1.;0
0;2. -1.])) (default)
```

Longitudinal steer compliance, specified as a structure, in deg/kN.

## Data Types: struct

Longitudinal camber compliance, LngCambCompl - Table

```
struct('NegFx',struct('FL',[-2. -1.;0 0;2. 1.],'FR',[-2. 1.;0 0;2. -1.],'RL',
[-2. -1.;0 0;2. 1.],'RR',[-2. 1.;0 0;2. -1.]),'PosFX',struct('FL',[-2. -1.;0
```

```
0;2. 1.],'FR',[-2. 1.;0 0;2. -1.],'RL',[-2. -1.;0 0;2. 1.],'RR',[-2. 1.;0
0;2. -1.])) (default)
```

Longitudinal camber compliance, specified as a structure, in deg/kN.
Data Types: struct

## Longitudinal caster compliance, LngCastCompl - Table

```
struct('NegFx',struct('FL',[-2. -1.;0 0;2. 1.],'FR',[-2. 1.;0 0;2. -1.],'RL',
```

[-2. -1.;0 0;2. 1.],'RR',[-2. 1.;0 0;2. -1.]), 'PosFx',struct('FL', [-2. -1.;0
$0 ; 2.1.], ' F R^{\prime},[-2.1 . ; 00 ; 2 .-1],. R^{\prime},[-2 .-1 . ; 00 ; 2.1],. R^{\prime},[-2.1 . ; 0$
0;2. -1.])) (default)

Longitudinal caster compliance, specified as a structure, in deg/kN.

## Data Types: struct

## Longitudinal wheel center compliance, LngWhICtrCompl - Table

```
struct('NegFx',struct('FL',[-2. -10.;0 0;2. 10.],'FR',[-2. 10.;0 0;2.
```

-10.],'RL',[-2. -10.;0 0;2. 10.],'RR',[-2. 10.;0 0;2.
-10.]),'PosFx',struct('FL',[-2. -10.;0 0;2. 10.],'FR',[-2. 10.;0 0;2.
-10.],'RL',[-2. -10.;0 0;2. 10.],'RR',[-2. 10.;0 0;2. -10.])) (default)

Longitudinal wheel center compliance, specified as a structure, in $\mathrm{mm} / \mathrm{kN}$.

## Data Types: struct

## Lateral wheel center compliance from braking, LatWhICtrComplLngBrk - Table

struct('NegFx',struct('FL',[-2. -10.;0 0;2. 10.],'FR',[-2. 10.;0 0;2.
-10.],'RL',[-2. -10.;0 0;2. 10.],'RR',[-2. 10.;0 0;2.
-10.]), 'PosFx', struct('FL',[-2. -10.;0 0;2. 10.],'FR',[-2. 10.;0 0;2.
-10.],'RL', [-2. -10.;0 0;2. 10.],'RR',[-2. 10.;0 0;2. -10.])) (default)
Lateral wheel center compliance from braking, specified as a structure, in $\mathrm{mm} / \mathrm{kN}$.
Data Types: struct
Lateral compliance-opposed test
Lateral steer compliance, LatSteerCompl - Table
struct('FL', [-2. -1.;0 0;2. 1.],'FR',[-2. 1.;0 0;2. -1.],'RL',[-2. -1.;0 0;2.
1.],'RR',[-2. 1.;0 0;2. -1.]) (default)

Lateral steer compliance, specified as a structure, in deg/kN.
Data Types: struct
Lateral camber compliance, LatCambCompl - Table
struct('FL',[-2. -1.;0 0;2. 1.],'FR',[-2. 1.;0 0;2. -1.],'RL',[-2. -1.;0 0;2. 1.],'RR',[-2. 1.;0 0;2. -1.]) (default)

Lateral camber compliance, specified as a structure, in deg/kN.

## Data Types: struct

Lateral wheel center compliance from lateral sources, LatWhICtrComplLat - Table
struct('FL', [-2. -5.;0 0;2. 5.],'FR',[-2. 5.;0 0;2. -5.],'RL',[-2. -5.;0 0;2. 5.],'RR',[-2. 5.;0 0;2. -5.]) (default)

Lateral wheel center compliance from lateral sources, specified as a structure, in mm/kN.
Data Types: struct

## Aligning torque compliance-opposed test

Aligning torque steer compliance, AlgnTrqSteerCompl - Table

```
struct('FL',[-0.2 -1.;0 0;0.2 1.],'FR',[-0.2 1.;0 0;0.2 -1.],'RL',[-0.2 -1.;0
0;0.2 1.],'RR',[-0.2 1.;0 0;0.2 -1.]) (default)
```

Aligning torque steer compliance, specified as a structure, in deg/kNm.

## Data Types: struct

## Aligning torque camber compliance, AlgnTrqCambCompl - Table

```
struct('FL',[-0.2 -1.;0 0;0.2 1.],'FR',[-0.2 1.;0 0;0.2 -1.],'RL',[-0.2 -1.;0
```

0;0.2 1.],'RR',[-0.2 1.;0 0;0.2 -1.]) (default)

Aligning torque camber compliance, specified as a structure, in deg $/ \mathrm{kNm}$.

## Data Types: struct

## Static alignment settings

Toe, StatToe - Wheel toe angle
[0 0 0 0] (default) | 1-by-4 vector
Static toe angle for each wheel, specified as a 1-by-4 vector, in deg.

| Wheel | Array Element | Axle | Wheel Location |
| :--- | :--- | :--- | :--- |
| Front left | $(1,1)$ | 1 | 1 |
| Front right | $(1,2)$ | 1 | 2 |
| Rear left | $(1,3)$ | 2 | 1 |
| Rear left | $(1,4)$ | 2 | 2 |

## Data Types: double

Camber, StatCamber - Wheel camber angle
[0 0 0 0] (default) | 1-by-4 vector
Static camber angle for each wheel, specified as a 1-by-4 vector, in deg.

| Wheel | Array Element | Axle |
| :--- | :--- | :--- |
| Front left | $(1,1)$ | 1 |
| Front right | $(1,2)$ | 1 |
| Rear left | $(1,3)$ | 2 |
| Rear left | $(1,4)$ | 2 |

## Data Types: double

Caster, StatCaster - Wheel caster angle
[0 0 0 0] (default) | 1-by-4 vector
Static caster angle for each wheel, specified as a 1-by-4 vector, in deg.

| Wheel | Array Element | Axle |
| :--- | :--- | :--- |
| Front left | $(1,1)$ | 1 |
| Front right | $(1,2)$ | 1 |
| Rear left | $(1,3)$ | 2 |
| Rear left | $(1,4)$ | 2 |

Data Types: double

## Wheels

Static loaded radius of wheels, StatLdWhIR - Wheel radius
[0.3 0.3 0.3 0.3] (default)| 1-by-4 vector
Static loaded radius of wheels, specified as a 1-by-4 vector, in m.

| Wheel | Array Element | Axle |
| :--- | :--- | :--- |
| Front left | $(1,1)$ | 1 |
| Front right | $(1,2)$ | 1 |
| Rear left | $(1,3)$ | 2 |
| Rear left | $(1,4)$ | 2 |

Data Types: double

## Version History

## Introduced in R2022a

R2022b: Parameter name change from NumTracksByAxl to NumWhlsByAxl
Behavior changed in R2022b
The Number of tracks by axle, NumTracksByAxl parameter is renamed to Number of wheels by axle, NumWhlsByAxl.

The block uses the number of wheels per axle to index the input and output block signals.

## R2022b: New Suspension type and Drivetrain type Parameters

Behavior changed in R2022b
Starting from R2022b, the Independent Suspension - K and C block includes Suspension type and Drivetrain type parameters that allow you specify a suspension and drivetrain. Previously, the block was configured for front wheel drive with independent front and rear suspensions.

## References

[1] Gillespie, Thomas. Fundamentals of Vehicle Dynamics. Warrendale, PA: Society of Automotive Engineers, 1992.

## Extended Capabilities

C/C++ Code Generation
Generate C and C++ code using Simulink ${ }^{\circledR}$ Coder $^{\mathrm{TM}}$.

## See Also

Independent Suspension - Double Wishbone | Independent Suspension - Mapped | Independent Suspension - MacPherson

## Twist-Beam Suspension - K and C

Twist-beam kinematics and compliance test suspension


## Libraries:

Vehicle Dynamics Blockset / Suspension

## Description

In the Vehicle Dynamics Blockset library, there are two types of suspension blocks that implement the kinematics and compliance ( K and C ) test suspension characteristics measured from simulated or actual laboratory suspension tests.



## $K$ and C Effects on Suspension

To determine the overall suspension forces and geometric effects on the vehicle and wheels, the block adds the individual effects from kinematic (bounce, roll, steering) and compliance (longitudinal and lateral forces, aligning moments) inputs. Specifically, the block multiplies the suspension geometry states by either gradient or table values to determine the K and C effects on wheel orientation and suspension forces.

## Wheel orientation:

- Camber, caster, and steer angles
- Lateral wheel center displacement
- Longitudinal wheel center displacement

Vertical suspension forces:

- Anti-sway bar
- Shock force
- Wheel rate
- Contact patch swing arm (CPSA) force
- Longitudinal side view swing arm (SVSA) anti-effects


## Camber, Caster, and Steer Angles

The block uses these parameters to account for the K and C effects on the camber, caster, and steer angles.

- Bounce test- Independent suspension
- Roll test- Independent suspension
- Steer test
- Longitudinal compliance test
- Lateral compliance-opposed test
- Aligning torque compliance-opposed test

Use the Static alignment settings parameters to set the initial state of the suspension.

## Lateral Wheel Center Displacement

The block uses these parameters to account for the K and C effects the lateral wheel center displacement.

- Bounce test
- Longitudinal compliance test
- Lateral compliance-opposed test


## Longitudinal Wheel Center Displacement

The block uses these parameters to account for the K and C effects on the longitudinal wheel center displacement.

- Bounce test
- Longitudinal compliance test


## Shock Force

The block uses the Shock force parameters to calculate the shock force effect on the vertical suspension force. You can specify table-based or constant parameter values.

## Wheel Rate

The block uses the Bounce test parameters to calculate the wheel rate effect on the vertical suspension force.

## Contact Patch Swing Arm

The block uses these equations to calculate the effect of the contact patch swing arm (CPSA) forces on vertical suspension force.

$$
\begin{aligned}
& \tan \left(\theta_{C P S A}\right)=f\left(Z_{w}\right) \\
& F_{z C P S A}=F_{y} \tan \left(\theta_{C P S A}\right)
\end{aligned}
$$

The block also uses the Static loaded radius of wheels parameter in the CPSA force calculation.
The equations use these variables.
$\theta_{\text {CPSA }} \quad$ Contact patch swing arm angle
$F_{y} \quad$ Lateral suspension force
$F_{z C P S A} \quad$ CPSA effect on vertical suspension force
$z_{w} \quad$ Wheel displacement

## Longitudinal Side View Swing Arm Anti-Effects

The block uses these equations to calculate the effect of the side view swing arm (SVSA) forces on vertical suspension force during acceleration and braking.

$$
\begin{aligned}
& \tan \left(\theta_{S V S A}\right)=f\left(Z_{w}\right) \\
& F_{z S V S A}=F_{x} \tan \left(\theta_{S V S A}\right)
\end{aligned}
$$

Use the Drivetrain type parameter to ensure that the block applies the acceleration anti-effects to the correct wheels.

The equations use these variables.

| $\theta_{S V S A}$ | Contact patch swing arm angle |
| :--- | :--- |
| $F_{x}$ | Longitudinal wheel force |
| $F_{z S V S A}$ | SVSA effect on vertical suspension force |
| $z_{w}$ | Wheel displacement |

## Anti-Sway Bar

Optionally, use the Anti-sway axle enable by axle, AntiSwayEnByAxl parameter to implement antisway bar reaction forces by axle.

If you do not enable an anti-sway bar, the axle roll stiffness is 0 .

## Front Axle

If you enable an anti-sway bar on the axle, the anti-sway bar stiffness is the difference between the anti-sway bar torque parameter, Front suspension roll stiffness with anti-roll bar,
RollStiffArbFrnt, and the roll stiffness parameter measured with no anti-sway bar present Front suspension roll stiffness without anti-roll bar, RollStiffNoArbFrnt.

## Rear Axle

If you enable an anti-sway bar on the rear axle, the block uses this equation to calculate the twistbeam roll stiffness.

$$
T B_{r s}=S_{r s}-\frac{\Pi\left[\frac{1}{2} W R_{\nabla} T W^{2}\right]}{180}
$$

The equation uses these variables.

| $T B_{r s}$ | Twist beam roll stiffness |
| :--- | :--- |
| $S_{r s}$ | Suspension roll stiffness without twist beam, RollStiffNoTwstRear parameter |
| $W R_{\nabla}$ | Normal wheel rate gradient, calculated from NrmlWhlRates parameter and <br> suspension displacement |
| $T W$ | Track width |

## Ports

The block uses the wheel number, $t$, to index the input and output signals. This table summarizes the wheel, axle, and corresponding wheel number for a vehicle with:

- Two axles
- Two wheels per axle

| Wheel | Axle | Wheel Number |
| :--- | :--- | :--- |
| Front left | Front | 1 |
| Front right | Front | 2 |
| Rear left | Rear | 1 |
| Rear right | Rear | 2 |

## Input

WhIPz - Wheel z-axis displacement
array
Wheel displacement, $z_{w}$, along wheel-fixed $z$-axis, in $m$. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlPz:

- Signal array dimensions are [1×4].

$$
\mathrm{WhlPz}=z_{w}=\left[\begin{array}{llll}
z_{w_{1,1}} & z_{w_{1,2}} & z_{w_{2,1}} & z_{w_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlPz $(1,1)$ | 1 | 1 |
| Front right | WhlPz $(1,2)$ | 1 | 2 |
| Rear left | WhlPz $(1,3)$ | 2 | 1 |
| Rear right | WhlPz $(1,4)$ | 2 | 2 |

WhIRe - Wheel effective radius
array
Effective wheel radius, $R e_{w}$, in $m$. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlRe:

- Signal array dimensions are [1x4].

$$
\text { WhlRe }=R e_{w}=\left[\begin{array}{lll}
R e_{w_{1,1}} & R e_{w_{1,2}} & R e_{w_{2,1}}
\end{array} R e_{w_{2,2}}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlRe $(1,1)$ | 1 | 1 |
| Front right | WhlRe $(1,2)$ | 1 | 2 |
| Rear left | WhlRe $(1,3)$ | 2 | 1 |
| Rear right | WhlRe $(1,4)$ | 2 | 2 |

WhIVz - Wheel z-axis velocity array

Wheel velocity, $\dot{z}_{w}$, along wheel-fixed $z$-axis, in m. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlVz:

- Signal array dimensions are [1×4].

$$
\text { WhlVz }=\dot{z}_{w}=\left[\begin{array}{l}
\dot{z}_{w_{1,1}}
\end{array} \dot{z}_{w_{1,2}} \dot{z}_{w_{2,1}} \dot{z}_{w_{2,2}}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlVz $(1,1)$ | 1 | 1 |
| Front right | WhlVz $(1,2)$ | 1 | 2 |
| Rear left | WhlVz $(1,3)$ | 2 | 1 |
| Rear right | WhlVz $(1,4)$ | 2 | 2 |

WhIFx - Longitudinal wheel force on vehicle
array
Longitudinal wheel force applied to vehicle, $F_{w x}$, along the vehicle-fixed $x$-axis. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlFx:

- Signal array dimensions are [1×4].

WhlFx $=F_{w x}=\left[F_{w x_{1,1}} F_{w x_{1,2}} F_{w x_{2,1}} F_{w x_{2,2}}\right]$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlFx $(1,1)$ | 1 | 1 |
| Front right | WhlFx $(1,2)$ | 1 | 2 |
| Rear left | WhlFx $(1,3)$ | 2 | 1 |
| Rear right | WhlFx $(1,4)$ | 2 | 2 |

WhIFy - Lateral wheel force on vehicle array

Lateral wheel force applied to vehicle, $F_{w y}$, along the vehicle-fixed $y$-axis. Array dimensions are 1 by the total number of wheels on the vehicle.

For example, for a two-axle vehicle with two wheels per axle, the WhlFy:

- Signal array dimensions are [1×4].

$$
\text { WhlFy }=F_{w y}=\left[F_{w y_{1,1}} F_{w y_{1,2}} F_{w y_{2,1}} F_{w y_{2,2}}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | WhlFy $(1,1)$ | 1 | 1 |
| Front right | WhlFy $(1,2)$ | 1 | 2 |
| Rear left | WhlFy $(1.3)$ | 2 | 1 |


| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Rear right | WhlFy $(1,4)$ | 2 | 2 |

WhIM - Suspension moment on wheel
array
Longitudinal, lateral, and vertical suspension moments at axle $a$, wheel $t$, applied to the wheel at the axle wheel carrier reference coordinate, in $N \cdot m$. Input array dimensions are 3 by the number of wheels on the vehicle.

- WhlM (1, ...) - Suspension moment applied to the wheel about the vehicle-fixed $x$-axis (longitudinal)
- WhlM $(2, \ldots)$ - Suspension moment applied to the wheel about the vehicle-fixed $y$-axis (lateral)
- WhlM $(3, \ldots)$ - Suspension moment applied to the wheel about the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the WhlM:

- Signal dimensions are [3×4].
- Signal contains suspension moments applied to four wheels according to their axle and wheel locations.

$$
\text { WhlM }=M_{w}=\left[\begin{array}{lllll}
M_{w x_{1,1}} & M_{w x_{1,2}} & M_{w x_{2,1}} & M_{w x_{2,2}} \\
M_{w y_{1,1}} & M_{w y 1,2} & M_{w y_{2,1}} & M_{w y 2,2} \\
M_{w z_{1,1}} & M_{w z_{1,2}} & M_{w z_{2,1}} & M_{w z_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Moment Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | WhlM $(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front <br> right | WhlM $(1,2)$ | 1 | 2 |  |
| Rear <br> left | WhlM $(1,3)$ | 2 | 1 |  |
| Rear <br> right | WhlM $(1,4)$ | 2 | 2 |  |
| Front <br> left | WhlM $(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front <br> right | WhlM $(2,2)$ | 1 | 2 |  |
| Rear <br> left | WhlM $(2,3)$ | 2 | 1 |  |
| Rear <br> right | WhlM $(2,4)$ | 2 | 2 |  |
| Front <br> left | WhlM( 3,1$)$ | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |


| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Moment Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> right | WhlM $(3,2)$ | 1 | 2 |  |
| Rear <br> left | WhlM $(3,3)$ | 2 | 1 |  |
| Rear <br> right | WhlM(3,4) | 2 | 2 |  |

VehP - Vehicle displacement
array
Vehicle displacement from axle a, wheel $t$ along vehicle-fixed coordinate system, in m. Input array dimensions are 3 the number of wheels on the vehicle.

- $\operatorname{VehP}(1, \ldots)$ - Vehicle displacement from wheel, $\chi_{v}$, along the vehicle-fixed $x$-axis
- $\operatorname{VehP}(2, \ldots)$ - Vehicle displacement from wheel, $y_{v}$, along the vehicle-fixed $y$-axis
- $\operatorname{VehP}(3, \ldots)-$ Vehicle displacement from wheel, $z_{v}$, along the vehicle-fixed $z$-axis

For example, for a two-axle vehicle with two wheels per axle, the VehP:

- Signal dimensions are [3×4].
- Signal contains four displacements according to their axle and wheel locations.

VehP $=\left[\begin{array}{l}x_{v} \\ y_{v} \\ z_{v}\end{array}\right]=\left[\begin{array}{llll}x_{v_{1,1}} & x_{v_{1,2}} & x_{v_{2,1}} & x_{v_{2,2}} \\ y_{v_{1,1}} & y_{v_{1,2}} & v_{v_{2,1}} & y_{v_{2,2}} \\ z_{v_{1,1}} & z_{v_{1,2}} & z_{v_{2,1}} & z_{v_{2,2}}\end{array}\right]$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | $\operatorname{VehP}(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis |
| Front <br> right | $\operatorname{VehP}(1,2)$ | 1 | 2 |  |
| Rear <br> left | $\operatorname{VehP}(1,3)$ | 2 | 1 |  |
| Rear <br> right | $\operatorname{VehP}(1,4)$ | 2 | 2 |  |
| Front <br> left | $\operatorname{VehP}(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis |
| Front <br> right | $\operatorname{VehP}(2,2)$ | 1 | 2 |  |
| Rear <br> left | $\operatorname{VehP}(2,3)$ | 2 | 1 |  |


| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Axis |
| :--- | :--- | :--- | :--- | :--- |
| Rear <br> right | $\operatorname{VehP}(2,4)$ | 2 | 2 |  |
| Front <br> left | $\operatorname{VehP}(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis |
| Front <br> right | $\operatorname{VehP}(3,2)$ | 1 | 2 |  |
| Rear <br> left | $\operatorname{VehP}(3,3)$ | 2 | 1 |  |
| Rear <br> right | $\operatorname{VehP}(3,4)$ | 2 | 2 |  |

VehV - Vehicle velocity
array
Vehicle velocity at axle a, wheel $t$ along vehicle-fixed coordinate system, in m. Input array dimensions are 3 by the number of wheels on the vehicle.

- VehV $(1, \ldots)$ - Vehicle velocity at wheel, $x_{v}$, along the vehicle-fixed $x$-axis
- VehV $(2, \ldots)-$ Vehicle velocity at wheel, $y_{v}$, along the vehicle-fixed $y$-axis
- $\operatorname{VehV}(3, \ldots)-$ Vehicle velocity at wheel, $z_{v}$, along the vehicle-fixed $z$-axis

For example, for a two-axle vehicle with two wheels per axle, the VehV:

- Signal dimensions are [3×4].
- Signal contains 4 velocities according to their axle and wheel locations.

VehV $=\left[\begin{array}{c}\dot{x}_{v} \\ \dot{y}_{v} \\ \dot{z}_{v}\end{array}\right]=\left[\begin{array}{lllll}\dot{x}_{v_{1,1}} & \dot{x}_{v_{1,2}} & \dot{x}_{v_{2,1}} & \dot{x}_{v_{2,2}} \\ \dot{y}_{v_{1,1}} & \dot{y}_{v_{1,2}} & \dot{y}_{v_{2,1}} & \dot{y}_{v_{2,2}} \\ \dot{z}_{v_{1,1}} & \dot{z}_{v_{1,2}} & \dot{z}_{v_{2,1}} & \dot{z}_{v_{2,2}}\end{array}\right]$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | VehV (1,1) | 1 | 1 | Vehicle-fixed $x$-axis |
| Front <br> right | VehV (1,2) | 1 | 2 |  |
| Rear <br> left | VehV (1,3) | 2 | 1 |  |
| Rear <br> right | VehV (1,4) | 2 | 2 |  |
| Front <br> left | VehV(2,1) | 1 | 1 | Vehicle-fixed $y$-axis |


| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> right | VehV $(2,2)$ | 1 | 2 |  |
| Rear <br> left | VehV $(2,3)$ | 2 | 1 |  |
| Rear <br> right | VehV $(2,4)$ | 2 | 2 |  |
| Front <br> left | $\operatorname{VehV}(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis |
| Front <br> right | $\operatorname{VehV}(3,2)$ | 1 | 2 |  |
| Rear <br> left | $\operatorname{VehV}(3,3)$ | 2 | 1 |  |
| Rear <br> right | $\operatorname{VehV}(3,4)$ | 2 | 2 |  |

StrgAng - Steering angle, optional
array
Optional steering angle for each wheel, $\delta$. Input array dimensions are 1 by the number of steered wheels.

For example, for a two-axle vehicle with two wheels per axle, you can input steering angles for both wheels on the first axle.

- To create the StrgAng port, set Steered axle enable by axle, StrgEnByAxl to [1 0]. The input signal array dimensions are [1×2].
- The StrgAng signal contains two steering angles according to their axle and wheel locations.

$$
\text { StrgAng }=\delta_{\text {steer }}=\left[\delta_{\text {steer }_{1,1}} \delta_{\text {steer }_{1,2}}\right]
$$

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | StrgAng $(1,1)$ | 1 | 1 |
| Front right | StrgAng $(1,2)$ | 1 | 2 |

## Dependencies

To create input port StrgAng, set an element of the Steered axle enable by axle, StrgEnByAxl vector to 1 .

Phi - Vehicle pitch angle
scalar
Vehicle pitch angle about earth-fixed $Y$-axis, in rad.
TrckWdth - Track width

```
array
```

Distance between wheels on each axle. Input array dimensions are 1-by-2.

| Array Element | Description |
| :--- | :--- |
| TrckWdth $(1,1)$ | Distance between wheels on front axle |
| TrckWdth $(1,2)$ | Distance between wheels on rear axle |

## Output

Info - Bus signal
bus
Bus signal containing block values. The signals are arrays that depend on the wheel location.
For example, here are the indices for a two-axle, two-wheel vehicle. The total number of wheels is four.

- 1D array signal (1-by-4)

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | $(1,1)$ | 1 | 1 |
| Front right | $(1,2)$ | 1 | 2 |
| Rear left | $(1,3)$ | 2 | 1 |
| Rear right | $(1,4)$ | 2 | 2 |

- 3D array signal (3-by-4)

| Wheel | Array Element | Axle | Wheel Number |
| :--- | :--- | :--- | :--- |
| Front left | $(1,1)$ | 1 | 1 |
| Front right | $(1,2)$ | 1 | 2 |
| Rear left | $(1,3)$ | 2 | 1 |
| Rear right | $(1,4)$ | 2 | 2 |
| Front left | $(2,1)$ | 1 | 1 |
| Front right | $(2,2)$ | 1 | 2 |
| Rear left | $(2,3)$ | 2 | 1 |
| Rear right | $(2,4)$ | 2 | 2 |
| Front left | $(3,1)$ | 1 | 1 |
| Front right | $(3,2)$ | 1 | 2 |
| Rear left | $(3,3)$ | 2 | 1 |
| Rear right | $(3,4)$ | 2 | 2 |


| Signal | Description | Array Signal | Variable | Units |
| :---: | :---: | :---: | :---: | :---: |
| Camber | Wheel angles according to the axle and wheel location. | 1D | WhlAng[1, ...] = $=\left[\xi_{a, t}\right]$ | rad |
| Caster |  |  | WhlAng $[2, \ldots]=\eta=\left[\eta_{a, t}\right]$ |  |
| Toe |  |  | WhlAng $[3, \ldots]=\zeta=\left[\zeta_{a, t}\right]$ |  |


| Signal | Description | Array Signal | Variable U | Units |
| :---: | :---: | :---: | :---: | :---: |
| Height | Suspension height | 1D | H m | m |
| Power | Suspension power dissipation | 1D |  | W |
| Energy | Suspension absorbed energy | 1D | $E_{\text {susp }}$ | J |
| VehF | Suspension forces applied to the vehicle | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { VehF }=F_{v}= \\ & {\left[\begin{array}{llll} F_{v x_{1,1}} & F_{v x_{1}, 2} & F_{v x_{2,1}} & F_{v x_{2,2}} \\ F_{v v_{1,1}} & F_{v y 1,2} & F_{v y_{2,1}} & F_{v y_{2,2}} \\ F_{v z_{1,1}} & F_{v z_{1,2}} & F_{v z_{2,1}} & F_{v z_{2,2}} \end{array}\right.} \end{aligned}$ | N |
| VehM | Suspension moments applied to vehicle | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { VehM }=M_{v}= \\ & {\left[\begin{array}{llll} M_{v x_{1}, 1} & M_{v x_{1}, 2} & M_{v x_{2,1}} & M_{v \chi_{2},}, \\ M_{v y_{1,1}} & M_{v y_{1,2}} & M_{v y_{2,1}} & M_{v y_{2},} \\ M_{v \chi_{1,1}} & M_{v \chi_{1,2}} & M_{v z_{2,1}} & M_{v \chi_{2},} \end{array}\right.} \end{aligned}$ | $\overline{\mathrm{N} \cdot \mathrm{~m}}$ <br> 2, 2 <br> 2, 2 <br> 2, 2 |


| Signal | Description | Array Signal | Variable | Units |
| :---: | :---: | :---: | :---: | :---: |
| WhlF | Suspension force applied to wheel | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { WhlF }=F_{w}= \\ & {\left[\begin{array}{llll} F_{w x_{1,1}} & F_{w x_{1}, 2} & F_{w x_{2,1}} & F_{w x_{2},}, \\ F_{w y_{1,1}} & F_{w y 1,2} & F_{w y_{2,1}} & F_{w y_{2},} \\ F_{w z_{1,1}} & F_{w z_{1,2}} & F_{w z_{2,1}} & F_{w z_{2},} \end{array}\right.} \end{aligned}$ |  |
| WhlP | Wheel displacement | 3D | For a two-axle, two wheels per axle vehicle: $\begin{aligned} & \text { WhlP }=\left[\begin{array}{l} x_{w} \\ y_{w} \\ z_{w} \end{array}\right]= \\ & {\left[\begin{array}{llll} x_{w_{1,1}} & x_{w_{1,2}} & x_{w_{2,1}} & x_{w_{2},} \\ y_{w_{1,1}} & y_{w_{1,2}} & y_{w_{2,1}} & y_{w w_{2}} \\ z_{w t r_{1,1}} & z_{w t r_{1,2}} & z_{w t r_{2,1}} & z_{w t r_{2}} \end{array}\right.} \end{aligned}$ |  |
| Whlv | Wheel velocity | 3D | For a two-axle, two wheels per axle vehicle: $\left.\begin{array}{l} \text { WhlV }=\left[\begin{array}{l} \dot{x}_{w} \\ \dot{y}_{w} \\ \dot{z}_{w} \end{array}\right] \\ = \\ {\left[\begin{array}{lll} \dot{x}_{w_{1,1}} & \dot{x}_{w_{1,2}} & \dot{x}_{w_{2,1}} \\ \dot{x}_{w_{2,2}} \\ \dot{y}_{w_{1,1}} & \dot{y}_{w_{1,2}} & \dot{y}_{w_{2,1}} \end{array} \dot{y}_{w_{2,2}}\right.} \\ \dot{z}_{w_{1,1}} \\ \dot{z}_{w_{1,2}} \\ \dot{z}_{w_{2,1}} \\ \dot{z}_{w_{2,2}} \end{array}\right]\left[\begin{array}{l} \text { an } \end{array}\right]$ | $\mathrm{m} / \mathrm{s}$ |


| Signal | Description | Array Signal | Variable | Units |
| :---: | :---: | :---: | :---: | :---: |
| WhlAng | Wheel camber, caster toe angles | 3D | For a two-axle, two wheels per axle vehicle: $\left.\begin{array}{l} \text { WhlAng }=\left[\begin{array}{l} \xi \\ \eta \\ \zeta \end{array}\right] \\ =\left[\begin{array}{lll} \xi_{1,1} & \xi_{1,2} & \xi_{2,1} \\ \xi_{2,2} \\ \eta_{1,1} & \eta_{1,2} & \eta_{2,1} \\ \eta_{2,2} \\ \zeta_{1,1} & \zeta_{1,2} & \zeta_{2,1} \end{array} \zeta_{2,2}\right. \end{array}\right] . \begin{aligned} & \eta_{2} \end{aligned}$ | rad |

## VehF - Suspension force on vehicle

array
Longitudinal, lateral, and vertical suspension force at axle a, wheel $t$, applied to the vehicle at the suspension connection point, in N . Array dimensions are 3 by the number of wheels on the vehicle.

- $\operatorname{VehF}(1, \ldots)$ - Suspension force applied to vehicle along the vehicle-fixed $x$-axis (longitudinal)
- $\operatorname{VehF}(2, \ldots)$ - Suspension force applied to vehicle along the vehicle-fixed $y$-axis (lateral)
- $\operatorname{VehF}(3, \ldots)$ - Suspension force applied to vehicle along the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the VehF:

- Signal dimensions are [3×4].
- Signal contains suspension forces applied to the vehicle according to the axle and wheel locations.

$$
\text { VehF }=F_{v}=\left[\begin{array}{lllll}
F_{v x_{1,1}} & F_{v x_{1,2}} & F_{v x_{2,1}} & F_{v x_{2,2}} \\
F_{v y_{1,1}} & F_{v y_{1,2}} & F_{v y_{2,1}} & F_{v y_{2,2}} \\
F_{v z_{1,1}} & F_{v z_{1,2}} & F_{v z_{2,1}} & F_{v z_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | $\operatorname{VehF}(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front <br> right | $\operatorname{VehF}(1,2)$ | 1 | 2 |  |
| Rear <br> left | $\operatorname{VehF}(1,3)$ | 2 | 1 |  |
| Rear <br> right | $\operatorname{VehF}(1,4)$ | 2 | 2 |  |
| Front <br> left | $\operatorname{VehF}(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front <br> right | $\operatorname{VehF}(2,2)$ | 1 | 2 |  |


| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Rear <br> left | $\operatorname{VehF}(2,3)$ | 2 | 1 |  |
| Rear <br> right | $\operatorname{VehF}(2,4)$ | 2 | 2 |  |
| Front <br> left | $\operatorname{VehF}(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front <br> right | $\operatorname{VehF}(3,2)$ | 1 | 2 |  |
| Rear <br> left | $\operatorname{VehF}(3,3)$ | 2 | 1 |  |
| Rear <br> right | $\operatorname{VehF}(3,4)$ | 2 | 2 |  |

VehM - Suspension moment on vehicle
array
Longitudinal, lateral, and vertical suspension moment at axle a, wheel $t$, applied to the vehicle at the suspension connection point, in $\mathrm{N} \cdot \mathrm{m}$. Array dimensions are 3 by the number of wheels on the vehicle.

- VehM (1, ...) - Suspension moment applied to the vehicle about the vehicle-fixed $x$-axis (longitudinal)
- VehM ( $2, \ldots$ ) - Suspension moment applied to the vehicle about the vehicle-fixed $y$-axis (lateral)
- VehM $(3, \ldots)$ - Suspension moment applied to the vehicle about the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the VehM:

- Signal dimensions are [3×4].
- Signal contains suspension moments applied to vehicle according to the axle and wheel locations.
$\mathrm{VehM}=M_{v}=\left[\begin{array}{lllll}M_{v x_{1,1}} & M_{v x_{1,2}} & M_{v x_{2,1}} & M_{v x_{2,2}} \\ M_{v y_{1,1}} & M_{v y_{1,2}} & M_{v y_{2,1}} & M_{v y_{2,2}} \\ M_{v z_{1,1}} & M_{v z_{1,2}} & M_{v z_{2,1}} & M_{v z_{2,2}}\end{array}\right]$

| Array Element | Axle | Wheel <br> Number | Moment Axis |
| :--- | :--- | :--- | :--- |
| $\operatorname{VehM}(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| $\operatorname{VehM}(1,2)$ | 1 | 2 |  |
| $\operatorname{VehM}(1,3)$ | 2 | 1 |  |
| $\operatorname{VehM}(1,4)$ | 2 | 2 |  |
| $\operatorname{VehM}(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| $\operatorname{VehM}(2,2)$ | 1 | 2 |  |


| Array Element | Axle | Wheel <br> Number | Moment Axis |
| :--- | :--- | :--- | :--- |
| $\operatorname{VehM}(2,3)$ | 2 | 1 |  |
| $\operatorname{VehM}(2,4)$ | 2 | 2 |  |
| $\operatorname{VehM}(3,1)$ | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| $\operatorname{VehM}(3,2)$ | 1 | 2 |  |
| $\operatorname{VehM}(3,3)$ | 2 | 1 |  |
| $\operatorname{VehM}(3,4)$ | 2 | 2 |  |

WhIF - Suspension force on wheel
array
Longitudinal, lateral, and vertical suspension forces at axle a, wheel $t$, applied to the wheel at the axle wheel carrier reference coordinate, in N . Array dimensions are 3 by the number of wheels on the vehicle.

- $\operatorname{WhlF}(1, \ldots)$ - Suspension force on wheel along the vehicle-fixed $x$-axis (longitudinal)
- $\operatorname{WhlF}(2, \ldots)$ - Suspension force on wheel along the vehicle-fixed $y$-axis (lateral)
- WhlF $(3, \ldots)$ - Suspension force on wheel along the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the WhlF:

- Signal dimensions are [3×4].
- Signal contains wheel forces applied to the vehicle according to the axle and wheel locations.

WhlF $=F_{w}=\left[\begin{array}{lllll}F_{w x_{1,1}} & F_{w x_{1,2}} & F_{w x_{2,1}} & F_{w x_{2,2}} \\ F_{w y_{1,1}} & F_{w y_{1,2}} & F_{w y_{2,1}} & F_{w y_{2,2}} \\ F_{w z_{1,1}} & F_{w z_{1,2}} & F_{w z_{2,1}} & F_{w z_{2,2}}\end{array}\right]$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | WhlF $(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front <br> right | WhlF $(1,2)$ | 1 | 2 |  |
| Rear <br> left | WhlF $(1,3)$ | 2 | 1 |  |
| Rear <br> right | WhlF $(1,4)$ | 2 | 2 |  |
| Front <br> left | WhlF $(2,1)$ | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front <br> right | WhlF $(2,2)$ | 1 | 2 |  |


| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Rear <br> left | WhlF $(2,3)$ | 2 | 1 |  |
| Rear <br> right | WhlF $(2,4)$ | 2 | 2 |  |
| Front <br> left | WhlF (3,1) | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front <br> right | WhlF (3,2) | 1 | 2 |  |
| Rear <br> left | WhlF $(3,3)$ | 2 | 1 |  |
| Rear <br> right | WhlF (3,4) | 2 | 2 |  |

WhIV - Wheel velocity
array
Longitudinal, lateral, and vertical wheel velocity at axle a, wheel t , in $\mathrm{m} / \mathrm{s}$. Array dimensions are 3 by the number of wheels on the vehicle.

- WhlV $(1, \ldots)$ - Wheel velocity along the vehicle-fixed $x$-axis (longitudinal)
- WhlV $(2, \ldots)-$ Wheel velocity along the vehicle-fixed $y$-axis (lateral)
- WhlV $(3, \ldots)-$ Wheel velocity along the vehicle-fixed $z$-axis (vertical)

For example, for a two-axle vehicle with two wheels per axle, the Whlv:

- Signal dimensions are [3×4].
- Signal contains wheel forces applied to the vehicle according to the axle and wheel locations.

$$
\text { WhlV }=\left[\begin{array}{l}
\dot{x}_{w} \\
\dot{y}_{w} \\
\dot{z}_{w}
\end{array}\right]=\left[\begin{array}{llll}
\dot{x}_{w_{1,1}} & \dot{x}_{w_{1,2}} & \dot{x}_{w_{2,1}} & \dot{x}_{w_{2,2}} \\
\dot{y}_{w_{1,1}} & \dot{y}_{w_{1,2}} & \dot{y}_{w_{2,1}} & \dot{y}_{w_{2,2}} \\
\dot{z}_{w_{1,1}} & \dot{z}_{w_{1,2}} & \dot{z}_{w_{2,1}} & \dot{z}_{w_{2,2}}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Force Axis |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | WhlV $(1,1)$ | 1 | 1 | Vehicle-fixed $x$-axis (longitudinal) |
| Front <br> right | WhlV $(1,2)$ | 1 | 2 |  |
| Rear <br> left | WhlV $(1,3)$ | 2 | 1 |  |
| Rear <br> right | WhlV $(1,4)$ | 2 | 2 |  |


| Wheel | Array Element | Axle | Wheel Numbe r | Force Axis |
| :---: | :---: | :---: | :---: | :---: |
| Front left | WhlV (2,1) | 1 | 1 | Vehicle-fixed $y$-axis (lateral) |
| Front right | WhlV (2,2) | 1 | 2 |  |
| Rear left | WhlV (2,3) | 2 | 1 |  |
| Rear right | WhlV (2,4) | 2 | 2 |  |
| Front left | WhlV (3,1) | 1 | 1 | Vehicle-fixed $z$-axis (vertical) |
| Front right | WhlV (3,2) | 1 | 2 |  |
| Rear left | WhlV (3, 3) | 2 | 1 |  |
| Rear right | WhlV(3,4) | 2 | 2 |  |

WhIAng - Wheel camber, caster, toe angles
array
Camber, caster, and toe angles at axle $a$, wheel $t$, in rad. Array dimensions are 3 by the number of wheels on the vehicle.

- WhlAng (1,...) - Camber angle
- WhlAng ( $2, \ldots$ ) - Caster angle
- Whlang $(3, \ldots)$ - Toe angle

For example, for a two-axle vehicle with two wheels per axle, the WhlAng:

- Signal dimensions are [3×4].
- Signal contains angles according to the axle and wheel locations.

$$
\text { WhlAng }=\left[\begin{array}{l}
\xi \\
\eta \\
\zeta
\end{array}\right]=\left[\begin{array}{llll}
\xi_{1,1} & \xi_{1,2} & \xi_{2,1} & \xi_{2,2} \\
\eta_{1,1} & \eta_{1,2} & \eta_{2,1} & \eta_{2,2} \\
\zeta_{1,1} & \zeta_{1,2} & \zeta_{2,1} & \zeta_{2,2}
\end{array}\right]
$$

| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Angle |
| :--- | :--- | :--- | :--- | :--- |
| Front <br> left | WhlAng (1,1) | 1 | 1 | Camber |
| Front <br> right | WhlAng (1,2) | 1 | 2 |  |


| Wheel | Array Element | Axle | Wheel <br> Numbe <br> r | Angle |
| :--- | :--- | :--- | :--- | :--- |
| Rear <br> left | WhlAng (1,3) | 2 | 1 |  |
| Rear <br> right | WhlAng (1,4) | 2 | 2 |  |
| Front <br> left | WhlAng (2,1) | 1 | 1 | Caster |
| Front <br> right | WhlAng (2,2) | 1 | 2 |  |
| Rear <br> left | WhlAng (2,3) | 2 | 1 |  |
| Rear <br> right | WhlAng (2,4) | 2 | 2 |  |
| Front <br> left | WhlAng (3,1) | 1 | 1 | Toe |
| Front <br> right | WhlF (3,2) | 1 | 2 |  |
| Rear <br> left | WhlF(3,3) | 2 | 1 |  |
| Rear <br> right | WhlF(3,4) | 2 | 2 |  |

## Parameters

Steered axle enable by axle, StrgEnByAxI - Boolean vector to enable axle steering
[1 0] (default) |vector
Boolean vector that enables axle steering, $E n_{\text {steer }}$, dimensionless. Vector is 1 by the number of vehicle axles, $N_{a}$. For example:

- [1 0] - For a two-axle vehicle, enables axle 1 steering and disables axle 2 steering
- [1 1] - For a two-axle vehicle, enables axle 1 and axle 2 steering


## Dependencies

Setting any element of the Steered axle enable by axle, StrgEnByAxl vector to 1 creates Input port StrgAng.

Anti-sway axle enable by axle, AntiSwayEnByAxI - Boolean vector to enable axle anti-sway [0 0] (default)|vector

Boolean vector that enables axle anti-sway for axle $a$, dimensionless. For example, [10] enables a front axle anti-sway and disables a rear axle anti-sway. Vector is 1 by the number of vehicle axles, $N_{a}$.

If you enable an anti-sway bar on the front axle, the anti-sway bar stiffness is the difference between the anti-sway bar torque parameter, Suspension roll stiffness with anti-roll bar, RollStiffArb,
and the roll stiffness parameter measured with no anti-roll bar present Suspension roll stiffness without anti-roll bar, RollStiffNoArb.

If you enable an anti-sway bar on the rear axle, the block uses this equation to calculate the twistbeam roll stiffness.

$$
T B_{r s}=S_{r s}-\frac{\Pi\left[\frac{1}{2} W R_{\nabla} T W^{2}\right]}{180}
$$

The equation uses these variables.

| $T B_{r s}$ | Twist beam roll stiffness |
| :--- | :--- |
| $S_{r s}$ | Suspension roll stiffness without twist beam, RollStiffNoTwstRear parameter |
| $W R_{\nabla}$ | Normal wheel rate gradient, calculated from NrmIWhlRates parameter and <br> suspension displacement |
| $T W$ | Track width |

If you do not enable an anti-sway bar, the stiffness is 0 .

## Suspension Parameters

Suspension type - Type of suspension
Independent front and rear|Independent front and twist beam rear
Select type of suspension.
Drivetrain type - Type of drivetrain
FWD (default) \| RWD \| AWD
Select type of drivetrain.

- AWD - All-wheel drive
- FWD - Front-wheel drive
- RWD - Rear-wheel drive


## Directions

+ Steer angle - Positive steer angle
Right (default) | Left
Direction of positive steer angle during kinematics and compliance test.
+ Fx used in compliance tests - Positive longitudinal force
Front (default) | Rear
Direction of positive longitudinal force during kinematics and compliance test.
+ Fy used in compliance tests - Positive lateral force
Right (default) |Left
Direction of positive lateral force during kinematics and compliance test.
+ Suspension Jounce - Positive suspension jounce
Up (default) | Down

Direction of positive suspension jounce during kinematics and compliance test.

+ WhIMz used in compliance tests - Positive yaw moment
Counter-clockwise (default)|Clockwise
Direction of positive yaw moment during kinematics and compliance test.


## Shock force

Shock type - Type of shock force
Table-based (default)|Table-based individualConstant
Type of shock force.
If a table-based individual setting is chosen, table-based shock force is implemented together with constant motion ratios. If a table-based setting is chosen both shock force and motion ratios are calculated from lookup tables.

| Setting | Implementation |
| :--- | :--- |
| Table-based | Table-based shock force and motion ratios. |
| Table-based individual | Table-based shock force and constant motion <br> ratios. |
| Constant | Constant shock force and motion ratios. |

## Shock force vs shock compression rate, ShckFrceVsCompRate - Table

struct('FL',[-100. -5000;0 0;100. 5000],'FR',[-100. -5000;0 0;100.
5000],'RL',[-100. -5000;0 0;100. 5000],'RR',[-100. -5000;0 0;100. 5000])
(default)
Shock force versus shock compression rate, specified as a structure, in $\mathrm{N} / \mathrm{mm}$ per sec.

## Dependencies

To create this parameter, set Shock type to Table-based or Table-based individual.
Data Types: struct
Motion ratios by axle, MotRatios - Table
struct('FL',[-0.1-0.1;0 0;0.1 0.1],'FR',[-0.1 -0.1;0 0;0.1 0.1],'RL',[-0.1
-0.1;0 0;0.1 0.1],'RR',[-0.1 -0.1;0 0;0.1 0.1]) (default)
Motion ratios by axle, specified as a structure.
Data Types: struct

## Bounce test

Bump steer, BumpSteer - Table
struct('FL', [-0.1 1.1459;0 0;0.1 -1.1459], 'FR', [-0.1 1.1459;0 0;0.1 -1.1459],'RL',[-0.1 0.;0 0;0.1 0.],'RR',[-0.1 0.;0 0;0.1 0.]) (default)

Bump steer, specified as a structure, in deg/m.
Data Types: struct

Bump camber, BumpCamber - Table

```
struct('FL',[-0.1 1.7189;0 0;0.1 -1.7189],'FR',[-0.1 1.7189;0 0;0.1
-1.7189],'RL',[-0.1 0.;0 0;0.1 0.],'RR',[-0.1 0.;0 0;0.1 0.]) (default)
```

Bump camber, specified as a structure, in deg/m.
Data Types: struct
Bump caster, BumpCaster - Table
struct('FL',[-0.1 1.1459;0 0;0.1 -1.1459],'FR',[-0.1 1.1459;0 0;0.1
-1.1459],'RL',[-0.1 -11.4592;0 0;0.1 11.4592],'RR',[-0.1 -11.4592;0 0;0.1
11.4592]) (default)

Bump caster, specified as a structure, in deg/m.
Data Types: struct
Lateral wheel center displacement, LatWhICtrDisp - Table
struct('FL',[-0.1 0.02;0 0;0.1 -0.02],'FR',[-0.1 0.02;0 0;0.1 -0.02],'RL', [-0.1 0.;0 0;0.1 0.],'RR',[-0.1 0.;0 0;0.1 0.]) (default)

Lateral wheel center displacement, specified as a structure, in $\mathrm{mm} / \mathrm{mm}$.
Data Types: struct
Longitudinal wheel center displacement, LngWhICtrDisp - Table
struct('FL',[-0.1 -0.002;0 0;0.1 0.002],'FR',[-0.1 -0.002;0 0;0.1
0.002],'RL',[-0.1 0.;0 0;0.1 0.],'RR',[-0.1 0.02;0 0;0.1 0.01]) (default)

Longitudinal wheel center displacement, specified as a structure, in $\mathrm{mm} / \mathrm{mm}$.
Data Types: struct
Normal wheel rates, NrmIWhIRates - Table
struct('FL',[-100. -5000;0 0;100. 5000],'FR',[-100. -5000;0 0;100.
5000],'RL',[-100. -5000;0 0;100. 5000],'RR',[-100. -5000;0 0;100. 5000]) (default) | vector

Normal wheel rates, specified as a structure, in N/mm.
Data Types: struct
Normal wheel force offsets, NrmIWhIFrcOff - Force offset
[0 0 0 0] (default)
Normal wheel force offsets, specified as a vector, in N .

## Dependencies

To create this parameter, specify a Normal wheel rates, NrmlWhlRates vector.
Data Types: struct

## Roll test

Roll steer, RollSteer - Table
struct('RL',[-10. -1.;0 0;10. 1.],'RR',[-10. 1.;0 0;10. -1.]) (default)
Rear axle roll steer, specified as a structure, in deg/deg.

## Dependencies

To enable this parameter, set Suspension type to Independent front and twist-beam rear.
Data Types: struct
Roll camber, RollCamber - Table
struct('RL',[-10. -1.;0 0;10. 1.],'RR',[-10. 1.;0 0;10. -1.]) (default)
Rear axle roll camber, specified as a structure, in deg/deg.

## Dependencies

To enable this parameter, set Suspension type to Independent front and twist-beam rear.
Data Types: struct
Roll caster, RollCaster - Table
struct('RL',[-10. -1.;0 0;10. 1.],'RR',[-10. 1.;0 0;10. -1.]) (default)
Rear axle roll caster, specified as a structure, in deg/deg.

## Dependencies

To enable this parameter, set Suspension type to Independent front and twist-beam rear.
Data Types: struct
Front suspension roll stiffness with anti-roll bar, RollStiffArbFrnt - Anti-sway bar enabled 800 (default) | scalar

Front axle suspension roll stiffness with anti-roll bar, specified as a scalar.
If you enable an anti-sway bar on the axle, the anti-sway bar stiffness is the difference between the anti-sway bar torque parameter, Front suspension roll stiffness with anti-roll bar,
RollStiffArbFrnt, and the roll stiffness parameter measured with no anti-sway bar present, Front suspension roll stiffness without anti-roll bar, RollStiffNoArbFrnt.

If you do not enable an anti-sway bar, the front axle roll stiffness is 0 .

## Dependencies

To enable this parameter, set Suspension type to Independent front and twist-beam rear.
Data Types: double
Front suspension roll stiffness without anti-roll bar, RollStiffNoArbFrnt - Anti-sway bar not enabled
0 (default) | scalar
Front suspension roll stiffness without an anti-roll bar, specified as a scalar, in Nm/deg.
If you enable an anti-sway bar on the axle, the anti-sway bar stiffness is the difference between the anti-sway bar torque parameter, Front suspension roll stiffness with anti-roll bar,
RollStiffArbFrnt, and the roll stiffness parameter measured with no anti-sway bar present, Front suspension roll stiffness without anti-roll bar, RollStiffNoArbFrnt.

If you do not enable an anti-sway bar, the axle roll stiffness is 0 .

## Dependencies

To enable this parameter, set Suspension type to Independent front and twist-beam rear.

## Data Types: double

Rear suspension roll stiffness without twist-beam, RollStiffNoTwstRear - Anti-sway bar not enabled
0 (default) | scalar
Rear suspension roll stiffness without an twist beam, specified as a scalar, in Nm/deg. T
If you do not enable an anti-sway bar, the rear axle roll stiffness is 0 .
If you enable an anti-sway bar on the rear axle, the block uses this equation to calculate the twistbeam roll stiffness.

$$
T B_{r s}=S_{r s}-\frac{\Pi\left[\frac{1}{2} W R_{\nabla} T W^{2}\right]}{180}
$$

The equation uses these variables.

| $T B_{r s}$ | Twist beam roll stiffness |
| :--- | :--- |
| $S_{r s}$ | Suspension roll stiffness without twist beam, RollStiffNoTwstRear parameter |
| $W R_{\nabla}$ | Normal wheel rate gradient, calculated from NrmlWhlRates parameter and <br> suspension displacement |
| $T W$ | Track width |
| Dependencies |  |

To enable this parameter, set Suspension type to Independent front and twist-beam rear.
Data Types: double

## Steer test

Camber vs steer angle, CambVsSteerAng - Table
struct('FL',[-10. -1.;0 0;10. 1.],'FR',[-10. 1.;0 0;10. -1.],'RL',[-10. -1.;0 0;10. 1.],'RR',[-10. 1.;0 0;10. -1.]) (default)

Camber vs steer angle, specified as a structure, in deg/deg.
Data Types: struct
Caster vs steer angle, CastVsSteerAng - Table
struct('FL',[-10. -1.;0 0;10. 1.],'FR',[-10. 1.;0 0;10. -1.],'RL',[-10. -1.;0 0;10. 1.],'RR',[-10. 1.;0 0;10. -1.]) (default)

Caster vs steer angle, specified as a structure, in deg/deg.
Data Types: struct

## Longitudinal compliance test

Longitudinal steer compliance, LngSteerCompl - Table
struct('NegFx', struct('FL',[-2. -1.;0 0;2. 1.],'FR',[-2. 1.;0 0;2. -1.],'RL',
$\left.[-2 .-1 . ; 0 \quad 0 ; 2.1],. ' R R^{\prime},[-2.1 . ; 0 \quad 0 ; 2 .-1].\right), ' P o s F X^{\prime}$, struct('FL',[-2. -1.;0

```
0;2. 1.],'FR',[-2. 1.;0 0;2. -1.],'RL',[-2. -1.;0 0;2. 1.],'RR',[-2. 1.;0
0;2. -1.])) (default)
```

Longitudinal steer compliance, specified as a structure, in deg/kN.

## Data Types: struct

Longitudinal camber compliance, LngCambCompl - Table struct('NegFx',struct('FL',[-2. -1.;0 0;2. 1.],'FR',[-2. 1.;0 0;2. -1.],'RL', [-2. -1.;0 0;2. 1.],'RR',[-2. 1.;0 0;2. -1.]),'PosFx',struct('FL',[-2. -1.;0 0;2. 1.],'FR',[-2. 1.;0 0;2. -1.],'RL',[-2. -1.;0 0;2. 1.],'RR',[-2. 1.;0 0;2. -1.]) ) (default)

Longitudinal camber compliance, specified as a structure, in deg/kN.

## Data Types: struct

Longitudinal caster compliance, LngCastCompI - Table

```
struct('NegFx',struct('FL',[-2. -1.;0 0;2. 1.],'FR',[-2. 1.;0 0;2. -1.],'RL',
[-2. -1.;0 0;2. 1.],'RR',[-2. 1.;0 0;2. -1.]),'PosFx',struct('FL',[-2. -1.;0
0;2. 1.],'FR',[-2. 1.;0 0;2. -1.],'RL',[-2. -1.;0 0;2. 1.],'RR',[-2. 1.;0
0;2. -1.])) (default)
```

Longitudinal caster compliance, specified as a structure, in deg/kN.

## Data Types: struct

Longitudinal wheel center compliance, LngWhICtrCompl - Table
struct('NegFx',struct('FL',[-2. -10.;0 0;2. 10.],'FR',[-2. 10.;0 0;2.
-10.],'RL',[-2. -10.;0 0;2. 10.],'RR',[-2. 10.;0 0;2.
-10.]),'PosFx',struct('FL',[-2. -10.;0 0;2. 10.],'FR',[-2. 10.;0 0;2.
-10.],'RL',[-2. -10.;0 0;2. 10.],'RR',[-2. 10.;0 0;2. -10.])) (default)
Longitudinal wheel center compliance, specified as a structure, in mm/kN.
Data Types: struct
Lateral wheel center compliance from braking, LatWhICtrComplLngBrk - Table
struct('NegFx', struct('FL',[-2. -10.;0 0;2. 10.],'FR',[-2. 10.;0 0;2. -10.],'RL',[-2. -10.;0 0;2. 10.],'RR',[-2. 10.;0 0;2.
-10.]),'PosFx',struct('FL',[-2. -10.;0 0;2. 10.],'FR',[-2. 10.;0 0;2.
-10.],'RL',[-2. -10.;0 0;2. 10.],'RR',[-2. 10.;0 0;2. -10.])) (default)
Lateral wheel center compliance from braking, specified as a structure, in mm/kN.
Data Types: struct

## Lateral compliance-opposed test

## Lateral steer compliance, LatSteerCompl - Table

struct('FL', [-2. -1.;0 0;2. 1.],'FR',[-2. 1.;0 0;2. -1.],'RL',[-2. -1.;0 0;2. 1.],'RR',[-2. 1.;0 0;2. -1.]) (default)

Lateral steer compliance, specified as a structure, in deg/kN.
Data Types: struct

## Lateral camber compliance, LatCambCompl - Table

struct('FL',[-2. -1.;0 0;2. 1.],'FR',[-2. 1.;0 0;2. -1.],'RL',[-2. -1.;0 0;2. 1.],'RR',[-2. 1.;0 0;2. -1.]) (default)

Lateral camber compliance, specified as a structure, in deg/kN.
Data Types: struct

## Lateral wheel center compliance from lateral sources, LatWhICtrComplLat - Table

```
struct('FL',[-2. -5.;0 0;2. 5.],'FR',[-2. 5.;0 0;2. -5.],'RL',[-2. -5.;0 0;2.
```

5.],'RR',[-2. 5.;0 0;2. -5.]) (default)

Lateral wheel center compliance from lateral sources, specified as a structure, in $\mathrm{mm} / \mathrm{kN}$.
Data Types: struct

## Aligning torque compliance-opposed test

Aligning torque steer compliance, AlgnTrqSteerCompl - Table
struct('FL',[-0.2-1.;0 0;0.2 1.],'FR',[-0.2 1.;0 0;0.2 -1.],'RL',[-0.2 -1.;0 0;0.2 1.],'RR',[-0.2 1.;0 0;0.2 -1.]) (default)

Aligning torque steer compliance, specified as a structure, in deg/kNm.
Data Types: struct
Aligning torque camber compliance, AlgnTrqCambCompl - Table

```
struct('FL',[-0.2 -1.;0 0;0.2 1.],'FR',[-0.2 1.;0 0;0.2 -1.],'RL',[-0.2 -1.;0
0;0.2 1.],'RR',[-0.2 1.;0 0;0.2 -1.])(default)
```

Aligning torque camber compliance, specified as a structure, in deg/kNm.
Data Types: struct

## Parallel lateral force compliance test

Vertical load transfer, VrtLdTrnsfr - Table
struct('FL',[-2. -1.;0 0;2. 1.],'FR',[-2. 1.;0 0;2. -1.],'RL',[-2. -1.;0 0;2.
1.],'RR',[-2. 1.;0 0;2. -1.]) (default)

Vertical load transfer, specified as a structure, in $\mathrm{N} / \mathrm{kN}$.

## Dependencies

To create this parameter, set Suspension type to Independent front and twist-beam rear.
Data Types: struct

## Static alignment settings

Toe, StatToe - Wheel toe angle
[0 0 0 0] (default) | 1-by-4 vector
Static toe angle for each wheel, specified as a 1-by-4 vector, in deg.

| Wheel | Array Element | Axle | Wheel Location |
| :--- | :--- | :--- | :--- |
| Front left | $(1,1)$ | 1 | 1 |


| Wheel | Array Element | Axle | Wheel Location |
| :--- | :--- | :--- | :--- |
| Front right | $(1,2)$ | 1 | 2 |
| Rear left | $(1,3)$ | 2 | 1 |
| Rear left | $(1,4)$ | 2 | 2 |

## Data Types: double

Camber, StatCamber - Wheel camber angle

```
[0 0 0 0] (default)| 1-by-4 vector
```

Static camber angle for each wheel, specified as a 1-by-4 vector, in deg.

| Wheel | Array Element | Axle |
| :--- | :--- | :--- |
| Front left | $(1,1)$ | 1 |
| Front right | $(1,2)$ | 1 |
| Rear left | $(1,3)$ | 2 |
| Rear left | $(1,4)$ | 2 |

## Data Types: double

Caster, StatCaster - Wheel caster angle
[0 0 0 0] (default) | 1-by-4 vector
Static caster angle for each wheel, specified as a 1-by-4 vector, in deg.

| Wheel | Array Element | Axle |
| :--- | :--- | :--- |
| Front left | $(1,1)$ | 1 |
| Front right | $(1,2)$ | 1 |
| Rear left | $(1,3)$ | 2 |
| Rear left | $(1,4)$ | 2 |

Data Types: double

## Wheels

Static loaded radius of wheels, StatLdWhIR - Wheel radius
[0.3 0.3 0.3 0.3] (default)| 1-by-4 vector
Static loaded radius of wheels, specified as a 1-by-4 vector, in m.

| Wheel | Array Element | Axle |
| :--- | :--- | :--- |
| Front left | $(1,1)$ | 1 |
| Front right | $(1,2)$ | 1 |
| Rear left | $(1,3)$ | 2 |
| Rear left | $(1,4)$ | 2 |

Data Types: double

## Version History

Introduced in R2022b

## References

[1] Gillespie, Thomas. Fundamentals of Vehicle Dynamics. Warrendale, PA: Society of Automotive Engineers, 1992.

## Extended Capabilities

C/C++ Code Generation
Generate C and C++ code using Simulink ${ }^{\circledR}$ Coder $^{\mathrm{TM}}$.

## See Also

Independent Suspension - Double Wishbone | Independent Suspension - Mapped | Independent Suspension-MacPherson

## Drivetrain Blocks

## Rotational Inertia

Ideal mechanical rotational inertia


## Libraries:

Powertrain Blockset / Drivetrain / Couplings
Vehicle Dynamics Blockset / Powertrain / Drivetrain / Couplings

## Description

The Rotational Inertia block implements an ideal mechanical rotational inertia.

## Power Accounting

For the power accounting, the block implements these equations.

| Bus Signal | Description | Variable | Equations |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| PwrInfo | PwrTrnsfrd - Power <br> transferred between <br> blocks | PwrR | Mechanical power <br> from base shaft | $P_{T R}$ | $P_{T R}=T_{R} \omega$ |
| Positive signals <br> indicate flow into <br> block <br> -Negative signals <br> indicate flow out of <br> block | PwrC | Mechanical power <br> from follower <br> shaft | $P_{T C}$ | $P_{T C}=T_{C} \omega$ |  |
| PwrNotTrnsfrd - <br> Power crossing the <br> block boundary, but <br> not transferred | PwrDampLoss | Power loss due to <br> damping <br> Positive signals <br> indicate an input <br> -Negative signals <br> indicate a loss | $P_{d}$ | $P_{d}=-b\|\omega\|^{2}$ |  |
| PwrStored - Stored <br> energy rate of change <br> - Positive signals <br> indicate an increase | PwrStoredShft | Rate change of <br> stored internal <br> torsional energy | $P_{s}$ | $P_{S}=\omega \dot{\omega} J$ |  |
| Negative signals <br> indicate a decrease |  |  |  |  |  |

The equations use these variables.

[^0]| $T_{C}$ | Output torque |
| :--- | :--- |
| $\omega$ | Driveshaft angular velocity |
| $J$ | Rotational inertia |
| $b$ | Rotational viscous damping |
| $P_{d}$ | Power loss due to damping |
| $P_{s}$ | Rate change of stored internal torsional energy |

## Ports

Input
RTrq - Input torque
scalar
Applied input driveshaft torque, $T_{R}$, in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

To enable this port, for Port Configuration, select Simulink.
CTrq - Output torque
scalar
Load driveshaft torque, $T_{C}$, in $\mathrm{N} \cdot \mathrm{m}$.
Dependencies
To enable this port, for Port Configuration, select Simulink.
$\mathbf{R}$ - Angular velocity and torque
two-way connector port
Angular velocity in rad/s. Torque is in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

To enable this port, for Port Configuration, select Two-way connection.
Inertia - Input
scalar
Rotational inertia, in $\mathrm{kg} \cdot \mathrm{m} \wedge 2$.
Dependencies
To create the Inertia port, select External inertia input.
Output
Info - Bus signal
bus
Bus signal containing these block calculations.

| Signal |  |  | Description | Variable | Units |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Trq | R |  | Applied input driveshaft torque | $T_{R}$ | $\mathrm{N} \cdot \mathrm{m}$ |
|  | C |  | Output driveshaft torque | $T_{C}$ | $\mathrm{N} \cdot \mathrm{m}$ |
|  | Damp |  | Damping torque | $T_{d}=b \omega$ | $\mathrm{N} \cdot \mathrm{m}$ |
| Spd |  |  | Angular driveshaft speed | $\omega$ | rad/s |
| PwrInfo | PwrTrnsfrd | PwrR | Mechanical power from base shaft | $P_{T R}$ | W |
|  |  | PwrC | Mechanical power from follower shaft | $P_{T C}$ | W |
|  | PwrNotTrnsf rd | PwrDampLos S | Power loss due to damping | $P_{d}$ | W |
|  | PwrStored | PwrStoredS hft | Rate change of stored internal torsional energy | $P_{s}$ | W |

## Dependencies

To enable this port, select Output Info bus.
Spd - Driveshaft speed
scalar
Angular driveshaft speed, $\omega$, in rad/s.

## Dependencies

To enable this port, for Port Configuration, select Simulink.
C - Angular velocity and torque
two-way connector port
Angular velocity in rad/s. Torque is in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

To enable this port, for Port Configuration, select Two-way connection.

## Parameters

## Block Options

Port Configuration - Specify configuration
Simulink (default) |Two-way connection
Specify the port configuration.

## Dependencies

Specifying Simulink creates these ports:

- RTrq
- CTrq
- Spd

Specifying Two-way connection creates these ports:

- R
- C

Output Info bus - Selection
off (default) | on
Select to create the Info output port.
External inertia input - Input rotational inertia
off (default) | on

## Dependencies

To create the Inertia port, select External inertia input.

## Parameters

Rotational inertia, J - Inertia

```
.01 (default) | scalar
```

Rotational inertia, in $\mathrm{kg} \cdot \mathrm{m} \wedge 2$.

## Dependencies

To enable this parameter, clear Input rotational inertia.
Torsional damping, b - Damping
. 001 (default) | scalar
Torsional damping, in $\mathrm{N} \cdot \mathrm{m} \cdot \mathrm{s} / \mathrm{rad}$.
Initial velocity, omega_o - Angular
0 (default) | scalar
Initial angular velocity, in rad/s.

## Version History

Introduced in R2017a

## Extended Capabilities

C/C++ Code Generation
Generate C and C++ code using Simulink ${ }^{\circledR}$ Coder ${ }^{\mathrm{TM}}$.

## See Also

Split Torsional Compliance | Torsional Compliance

## Split Torsional Compliance

Split torsional coupler


Libraries:
Powertrain Blockset / Drivetrain / Couplings
Vehicle Dynamics Blockset / Powertrain / Drivetrain / Couplings

## Description

The Split Torsional Compliance block implements parallel spring-damper coupling between shafts. You can specify the type of coupling by selecting one of the Coupling Configuration parameters:

- Shaft split - Single input shaft coupled to two output shafts
- Shaft merge - Two input shafts coupled to a single output shaft

In fuel economy and emissions studies, you can use the Split Torsional Compliance block to model mechanical rotational compliance between common driveline elements such as motors, planetary gears, and clutches. For example, use the Shaft split configuration to couple a motor and two planetary gear sets. Use the Shaft merge configuration to couple a dual clutch transmission to an output shaft.

## Shaft Split

For the Shaft split configuration, the block implements this schematic and equations.


$$
\begin{aligned}
& T_{\text {in }}=-\left(\omega_{\text {in }}-\omega_{1 \text { out }}\right) b_{1}-\left(\omega_{\text {in }}-\omega_{2 \text { out }}\right) b_{2}-\theta_{1} k_{1}-\theta_{2} k_{2} \\
& T_{1 \text { out }}=\left(\omega_{\text {in }}-\omega_{1 \text { out }}\right) b_{1}+\theta_{1} k_{1} \\
& T_{2 \text { out }}=\left(\omega_{\text {in }}-\omega_{2 \text { out }}\right) b_{2}+\theta_{2} k_{2} \\
& \dot{\theta}_{1}=\left(\omega_{\text {in }}-\omega_{1 \text { out }}\right) \\
& \dot{\theta}_{2}=\left(\omega_{\text {in }}-\omega_{2 \text { out }}\right)
\end{aligned}
$$

To account for frequency-dependent damping, both damping terms incorporate a low-pass filter. The equations use these variables.

| $T_{\text {in }}$ | Resulting applied input reaction torque |
| :--- | :--- |
| $\omega_{\text {in }}$ | Input shaft rotational velocity |
| $T_{\text {lout }}$ | Resulting applied torque to first output shaft |
| $\omega_{\text {lout }}$ | First output shaft rotational velocity |
| $T_{2 \text { out }}$ | Resulting applied torque to second output shaft |
| $\omega_{2 \text { out }}$ | Second output shaft rotational velocity |
| $\theta_{1}, \theta_{2}$ | First, second shaft rotation, respectively |
| $b_{1}, b_{2}$ | First, second shaft viscous damping, respectively |
| $k_{1}, k_{2}$ | First, second shaft torsional stiffness, respectively |

## Shaft Merge

For the Shaft merge configuration, the block implements this schematic and equations.


$$
\begin{aligned}
& T_{\text {out }}=\left(-\omega_{\text {out }}+\omega_{1 \text { in }}\right) b_{1}+\left(-\omega_{\text {out }}+\omega_{2 \text { in }}\right) b_{2}+\theta_{1} k_{1}+\theta_{2} k_{2} \\
& T_{1 \text { out }}=\left(\omega_{\text {out }}-\omega_{1 \text { in }}\right) b_{1}-\theta_{1} k_{1} \\
& T_{2 \text { out }}=\left(\omega_{\text {out }}-\omega_{2 \text { in }}\right) b_{2}-\theta_{2} k_{2} \\
& \dot{\theta}_{1}=\left(\omega_{1 \text { in }}-\omega_{\text {out }}\right) \\
& \dot{\theta}_{2}=\left(\omega_{2 \text { in }}-\omega_{\text {out }}\right)
\end{aligned}
$$

To account for frequency-dependent damping, both damping terms incorporate a low-pass filter.

The equations use these variables.

| $T_{\text {out }}$ | Resulting applied output torque |
| :--- | :--- |
| $\omega_{\text {out }}$ | Output shaft rotational velocity |
| $T_{1 \text { in }}$ | Resulting reaction torque to first input shaft |
| $\omega_{1 \text { in }}$ | First input shaft rotational velocity |
| $T_{2 \text { in }}$ | Resulting reaction torque to second input shaft |
| $\omega_{2 \text { in }}$ | Second input shaft rotational velocity |
| $\theta_{1}, \theta_{2}$ | First, second shaft rotation, respectively |
| $b_{1}, b_{2}$ | First, second shaft viscous damping, respectively |
| $k_{1}, k_{2}$ | First, second shaft torsional stiffness, respectively |

## Power Accounting

For the power accounting, the block implements these equations.

| Bus Signal |  |  | Description | Variable | Equations |
| :---: | :---: | :---: | :---: | :---: | :---: |
| PwrInfo | PwrTrnsfrd - Power transferred between blocks <br> - Positive signals indicate flow into block <br> - Negative signals indicate flow out of block | PwrR | For the Shaft split configuration, mechanical power from input shaft | $P_{\text {TR }}$ | $P_{T R}=-T_{R} \omega_{R}$ |
|  |  | PwrC1 | For the Shaft split configuration, mechanical power from first output shaft | $P_{\text {TC1 }}$ | $\begin{aligned} & P_{T C 1}= \\ & -T_{C 1} \omega_{C 1} \end{aligned}$ |
|  |  | PwrC2 | For the Shaft split configuration, mechanical power from second output shaft | $P_{\text {TC2 }}$ | $\begin{aligned} & P_{T C 2}= \\ & -T_{C 2} \omega_{C 2} \end{aligned}$ |
|  |  | PwrC | For the Shaft merge configuration, mechanical power from output shaft | $P_{\text {TC }}$ | $P_{T C}=T_{C} \omega_{C}$ |


| Bus Signal |  |  | Description | Variable | Equations |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | PwrR1 | For the Shaft merge configuration, mechanical power from first input shaft | $P_{\text {TR1 }}$ | $\begin{gathered} P_{T R 1}= \\ T_{R 1} \omega_{R 1} \end{gathered}$ |
|  |  | PwrR2 | For the Shaft merge configuration, mechanical power from second input shaft | $P_{\text {TR2 }}$ | $\begin{gathered} P_{T R 2}= \\ T_{R 2} \omega_{R 2} \end{gathered}$ |
|  | PwrNotTrnsfrd Power crossing the block boundary, but not transferred <br> - Positive signals indicate an input <br> - Negative signals indicate a loss | PwrDampLoss | Mechanical damping loss | $P_{d}$ | $\begin{aligned} & P_{d}=-\left(b_{1}\left\|\dot{\theta}_{1}\right\|^{2}\right. \\ & \left.+b_{2}\left\|\dot{\theta}_{2}\right\|^{2}\right) \end{aligned}$ |
|  | PwrStored - Stored energy rate of change <br> - Positive signals indicate an increase <br> - Negative signals indicate a decrease | PwrStoredShft | Rate change in spring energy | $P_{s}$ | $\begin{aligned} & P_{s}=\left(k_{1} \theta_{1} \dot{\theta}_{1}\right. \\ & \left.+k_{2} \theta_{2} \dot{\theta}_{2}\right) \end{aligned}$ |

The equations use these variables.

| $T_{R}$ | Shaft R torque |
| :--- | :--- |
| $T_{C}$ | Shaft C torque |
| $\omega_{R}$ | Shaft R angular velocity |
| $\omega_{C}$ | Shaft C angular velocity |
| $\theta$ | Coupled shaft rotation |
| $k$ | Shaft torsional stiffness |
| $b$ | Rotational viscous damping |
| $P_{t}$ | Total mechanical power |
| $P_{d}$ | Power loss due to damping |
| $P_{s}$ | Rate change of stored spring energy |

## Ports

Input
RSpd - Input shaft speed
scalar
Input shaft rotational velocity, $\omega_{i n}$, in rad/s.

## Dependencies

To enable this port, set both of these parameters:

- Port Configuration to Simulink
- Coupling Configuration to Shaft split

C1Spd - First output shaft speed
scalar
First output shaft rotational velocity, $\omega_{1 \text { out }}$, in rad/s.

## Dependencies

To enable this port, set both of these parameters:

- Port Configuration to Simulink
- Coupling Configuration to Shaft split

C2Spd - Second output shaft speed
scalar
Second output shaft rotational velocity, $\omega_{\text {2out }}$ in rad/s.

## Dependencies

To enable this port, set both of these parameters:

- Port Configuration to Simulink
- Coupling Configuration to Shaft split

CSpd - Input speed
scalar
Output shaft rotational velocity, $\omega_{\text {out }}$, in rad/s.

## Dependencies

To enable this port, set both of these parameters:

- Port Configuration to Simulink
- Coupling Configuration to Shaft merge

R1Spd - First input shaft speed
scalar
First input shaft rotational velocity, $\omega_{1 \text { in }}$, in rad/s.

## Dependencies

To enable this port, set both of these parameters:

- Port Configuration to Simulink
- Coupling Configuration to Shaft merge

R2Spd - Second input shaft speed

## scalar

Second input shaft rotational velocity, $\omega_{2 i n}$, in rad/s.

## Dependencies

To enable this port, set both of these parameters:

- Port Configuration to Simulink
- Coupling Configuration to Shaft merge
$\mathbf{R}$ - Input shaft angular velocity and torque
two-way connector port
Input shaft angular velocity, $\omega_{i n}$, in rad/s and torque, $T_{i n}$, in $\mathrm{N} \cdot \mathrm{m}$.
Dependencies
To enable this port, select:
- Port Configuration>Two-way connection
- Coupling Configuration>Shaft split

R1 - First input shaft angular velocity and torque
two-way connector port
First input shaft angular velocity, $\omega_{1 i n}$, in rad/s and torque, $T_{1 i n}$, in $N \cdot \mathrm{~m}$.

## Dependencies

To enable this port, select:

- Port Configuration>Two-way connection
- Coupling Configuration>Shaft merge

R2 - Second input shaft angular velocity and torque
two-way connector port
Second input shaft angular velocity, $\omega_{2 i n}$, in rad/s and torque, $T_{2 i n}$, in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

To enable this port, select:

- Port Configuration>Two-way connection
- Coupling Configuration>Shaft merge


## Output

Info - Bus signal
bus
If you set Coupling Configuration to Shaft split, the Info bus contains these signals.

| Signal |  |  | Description | Variable | Units |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Trq | R |  | Input shaft torque | $T_{\text {in }}$ | $\mathrm{N} \cdot \mathrm{m}$ |
|  | C1 |  | First output shaft torque | $T_{1 \text { out }}$ | $\mathrm{N} \cdot \mathrm{m}$ |
|  | C2 |  | Second output shaft torque | $T_{\text {out }}$ | $\mathrm{N} \cdot \mathrm{m}$ |
|  | Damp | C1 | First output shaft damping torque | $b_{1} \omega_{1 \text { out }}$ | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | C2 | Second output shaft damping torque | $b_{2} \omega_{2 \text { out }}$ | $\mathrm{N} \cdot \mathrm{m}$ |
|  | Spring | C1 | First output shaft spring torque | $k_{1} \theta_{1}$ | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | C2 | Second output shaft spring torque | $k_{2} \theta_{2}$ | $\mathrm{N} \cdot \mathrm{m}$ |
| Spd | R |  | Input shaft angular velocity | $\omega_{\text {in }}$ | rad/s |
|  | C1 |  | First output shaft angular velocity | $\omega_{1 \text { out }}$ | rad/s |
|  | C2 |  | Second output shaft angular velocity | $\omega_{\text {2out }}$ | $\mathrm{rad} / \mathrm{s}$ |
|  | deltadot1 |  | Difference in input and first output shaft angular velocity | $\dot{\theta}_{1}$ | rad/s |
|  | deltadot2 |  | Difference in input and second output shaft angular velocity | $\dot{\theta}_{2}$ | rad/s |
| PwrInfo | PwrTrnsfrd | PwrR | Mechanical power from input shaft | $P_{T R}$ | W |
|  |  | PwrC1 | Mechanical power from first output shaft | $P_{\text {TC1 }}$ | W |
|  |  | PwrC2 | Mechanical power from second output shaft | $P_{\text {TC2 }}$ | W |
|  | PwrNotTrnsf rd | PwrDampLo SS | Mechanical damping loss | $P_{d}$ | W |
|  | PwrStored | PwrStored Shft | Rate change of stored internal torsional energy | $P_{s}$ | W |

If you set Coupling Configuration to Shaft merge, the Info bus contains these signals.

| Signal |  | Description | Variable | Units |
| :--- | :--- | :--- | :--- | :--- |
| Trq | C | Output shaft torque | $T_{\text {out }}$ | $\mathrm{N} \cdot \mathrm{m}$ |
|  | R1 | First input shaft torque | $T_{1 \text { in }}$ | $\mathrm{N} \cdot \mathrm{m}$ |
|  | R2 | Second input shaft torque | $T_{2 i n}$ | $\mathrm{~N} \cdot \mathrm{~m}$ |


| Signal |  |  | Description | Variable | Units |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Damp | R1 | First input shaft damping torque | $b_{1} \omega_{1 \text { in }}$ | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | R2 | Second in shaft damping torque | $b_{2} \omega_{2 i n}$ | $\mathrm{N} \cdot \mathrm{m}$ |
|  | Spring | R1 | First input shaft spring torque | $k_{1} \theta_{1}$ | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | R2 | Second in shaft spring torque | $k_{2} \theta_{2}$ | $\mathrm{N} \cdot \mathrm{m}$ |
| Spd | C |  | Output shaft angular velocity | $\omega_{\text {out }}$ | rad/s |
|  | R1 |  | First input shaft angular velocity | $\omega_{1 i n}$ | rad/s |
|  | R2 |  | Second input shaft angular velocity | $\omega_{2 i n}$ | rad/s |
|  | deltadot1 |  | Difference in first input and output shaft angular velocity | $\dot{\theta}_{1}$ | rad/s |
|  | deltadot2 |  | Difference in second input and output shaft angular velocity | $\dot{\theta}_{2}$ | rad/s |
| PwrInfo | PwrTrnsfrd | PwrC | Mechanical power from output shaft | $P_{T C}$ | W |
|  |  | PwrR1 | Mechanical power from first input shaft | $P_{\text {TR1 }}$ | W |
|  |  | PwrR2 | Mechanical power from second input shaft | $P_{\text {TR2 }}$ | W |
|  | PwrNotTrnsf rd | PwrDampLo ss | Mechanical damping loss | $P_{d}$ | W |
|  | PwrStored | PwrStored Shft | Rate change of stored internal torsional energy | $P_{s}$ | W |

## Dependencies

To enable this port, select Output Info bus.
RTrq - Input shaft torque
scalar
Input shaft torque, $T_{\text {in }}$, in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

To enable this port, set both of these parameters:

- Port Configuration to Simulink
- Coupling Configuration to Shaft split

C1Trq - First output shaft torque
scalar
First output shaft torque, $T_{1 o u t}$, in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

To enable this port, set both of these parameters:

- Port Configuration to Simulink
- Coupling Configuration to Shaft split

C2Trq - Second output shaft torque scalar

Second output shaft torque, $T_{2 o u t}$, in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

To enable this port, set both of these parameters:

- Port Configuration to Simulink
- Coupling Configuration to Shaft split

CTrq - Output shaft torque
scalar
Output shaft torque, $T_{\text {out }}$, in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

To enable this port, set both of these parameters:

- Port Configuration to Simulink
- Coupling Configuration to Shaft merge
$\mathbf{R 1} \mathbf{T r q}$ - First input shaft torque
scalar
First input shaft torque, $T_{1 i n}$, in $\mathrm{N} \cdot \mathrm{m}$.


## Dependencies

To enable this port, set both of these parameters:

- Port Configuration to Simulink
- Coupling Configuration to Shaft merge

R2Trq - Second input shaft torque scalar

Second input shaft torque, $T_{2 i n}$, in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

To enable this port, set both of these parameters:

- Port Configuration to Simulink
- Coupling Configuration to Shaft merge

C1 - First output shaft angular velocity and torque two-way connector port

First output shaft angular velocity, $\omega_{1 \text { out }}$, in rad/s and torque, $T_{1 \text { out }}$, in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

To enable this port, select:

- Port Configuration>Two-way connection
- Coupling Configuration>Shaft split

C2 - Second output shaft angular velocity and torque
two-way connector port
Second output shaft angular velocity, $\omega_{2 o u t}$, in rad/s and torque, $T_{2 \text { out }}$, in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

To enable this port, select:

- Port Configuration>Two-way connection
- Coupling Configuration>Shaft split

C - Output shaft angular velocity and torque
two-way connector port
Output shaft angular velocity, $\omega_{\text {out }}$, in rad/s and torque, $T_{\text {out }}$ in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

To enable this port, select:

- Port Configuration>Two-way connection
- Coupling Configuration>Shaft merge


## Parameters

## Block Options

Port Configuration - Specify configuration
Simulink (default)|Two-way connection
Specify the port configuration.
Coupling Configuration - Specify configuration
Shaft split (default)|Shaft merge
Specify the coupling type.
Output Info bus - Selection
off (default) | on
Select to create the Info output port.

## Coupling 1

Torsional stiffness, k1 - Stiffness
5e4 (default) | scalar
Rotational inertia, $k_{1}$, in $\mathrm{N} \cdot \mathrm{m} / \mathrm{rad}$.

Torsional damping, b1 - Damping
le2 (default) | scalar
Torsional damping, $b_{1}$, in $\mathrm{N} \cdot \mathrm{m} \cdot \mathrm{s} / \mathrm{rad}$.
Damping cutoff frequency, omega1_c - Frequency 3000 (default)| scalar

Damping cutoff frequency, in rad/s.

## Coupling 2

Torsional stiffness, k2 - Stiffness
5e4 (default) | scalar
Rotational inertia, $k_{2}$, in $\mathrm{N} \cdot \mathrm{m} / \mathrm{rad}$.
Torsional damping, b2 - Damping
le2 (default) | scalar
Torsional damping, $b_{2}$, in $\mathrm{N} \cdot \mathrm{m} \cdot \mathrm{s} / \mathrm{rad}$
Damping cutoff frequency, omega2_c - Frequency 3000 (default) | scalar

Damping cutoff frequency, in rad/s.

## Version History

Introduced in R2017b

## Extended Capabilities

C/C++ Code Generation
Generate C and C++ code using Simulink $\circledR^{\circledR}$ Coder ${ }^{\mathrm{TM}}$.

## See Also

Rotational Inertia | Torsional Compliance

## Torsional Compliance

Parallel spring-damper


Libraries:
Powertrain Blockset / Drivetrain / Couplings
Vehicle Dynamics Blockset / Powertrain / Drivetrain / Couplings

## Description

The Torsional Compliance block implements a parallel spring-damper to couple two rotating driveshafts. The block uses the driveshaft angular velocities, torsional stiffness, and torsional damping to determine the torques.
$T_{R}=-\left(\omega_{R}-\omega_{C}\right) b-\theta k$
$T_{C}=\left(\omega_{R}-\omega_{C}\right) b+\theta k$
$\dot{\theta}=\left(\omega_{R}-\omega_{C}\right)$

## Power Accounting

For the power accounting, the block implements these equations.

| Bus Signal |  |  | Description | Variable | Equations |
| :---: | :---: | :---: | :---: | :---: | :---: |
| PwrInfo | PwrTrnsfrd - Power transferred between blocks <br> - Positive signals indicate flow into block <br> - Negative signals indicate flow out of block | PwrR | Mechanical power from driveshaft R | $P_{\text {TR }}$ | $\begin{gathered} P_{T R}= \\ T_{R} \omega_{R} \end{gathered}$ |
|  |  | PwrC | Mechanical power from driveshaft C | $P_{\text {TC }}$ | $\begin{array}{r} P_{T C}= \\ T_{C} \omega_{C} \end{array}$ |
|  | PwrNotTrnsfrd - Power crossing the block boundary, but not transferred <br> - Positive signals indicate an input <br> - Negative signals indicate a loss | PwrDampLoss | Mechanical damping loss | $P_{d}$ | $\begin{aligned} & P_{d}= \\ & -b\|\dot{\theta}\|^{2} \end{aligned}$ |
|  | PwrStored - Stored energy rate of change <br> - Positive signals indicate an increase <br> - Negative signals indicate a decrease | PwrStoredShft | Rate change in spring energy | $P_{S}$ | $P_{S}=-\theta k \dot{\theta}$ |

The equations use these variables.

| $T_{R}$ | Driveshaft R torque |
| :--- | :--- |
| $T_{C}$ | Driveshaft C torque |
| $\omega_{R}$ | Driveshaft R angular velocity |
| $\omega_{C}$ | Driveshaft C angular velocity |
| $\theta$ | Coupled driveshaft rotation |
| $k$ | Driveshaft torsional stiffness |
| $b$ | Rotational viscous damping |
| $P_{d}$ | Power loss due to damping |
| $P_{s}$ | Rate change of stored spring energy |

## Ports

Input
RSpd - Driveshaft R angular velocity
scalar
Input driveshaft angular velocity, in rad/s.

## Dependencies

To enable this port, for Port Configuration, select Simulink.
CSpd - Driveshaft C angular velocity
scalar
Output driveshaft angular velocity, in rad/s.

## Dependencies

To enable this port, for Port Configuration, select Simulink.
$\mathbf{R}$ - Angular velocity and torque
two-way connector port
Angular velocity in rad/s. Torque is in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

To enable this port, for Port Configuration, select Two-way connection.

## Output

Info - Bus signal
bus
Bus signal containing these block calculations.

| Signal | Description | Variable | Units |  |
| :--- | :--- | :--- | :--- | :--- |
| $\operatorname{Trq}$ | R | Input driveshaft torque | $T_{R}$ | $\mathrm{~N} \cdot \mathrm{~m}$ |
|  | C | Output driveshaft torque | $T_{C}$ | $\mathrm{~N} \cdot \mathrm{~m}$ |


| Signal |  |  | Description | Variable | Units |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Damp |  | Damping torque | $T_{s}=b \dot{\theta}$ | N.m |
|  | Spring |  | Spring torque | $T_{d}=k \theta$ | $\mathrm{N} \cdot \mathrm{m}$ |
| Spd | R |  | Input driveshaft angular velocity | $\omega_{R}$ | rad/s |
|  | C |  | Output driveshaft angular velocity | $\omega_{C}$ | rad/s |
|  | deltadot |  | Difference in input and output driveshaft angular velocity | $\dot{\theta}$ | rad/s |
| PwrInfo | PwrTrnsfrd | PwrR | Mechanical power from driveshaft R | $P_{T R}$ | W |
|  |  | PwrC | Mechanical power from driveshaft C | $P_{\text {TC }}$ | W |
|  | PwrNotTrnsf rd | PwrDampLos <br> S | Power loss due to damping | $P_{d}$ | W |
|  | PwrStored | PwrStoredS hft | Rate change of stored internal kinetic energy | $P_{s}$ | W |

## Dependencies

To enable this port, select Output Info bus.
RTrq - Driveshaft R torque
scalar
Input drive shaft torque, in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

To enable this port, for Port Configuration, select Simulink.
CTrq - Driveshaft C torque
scalar
Applied output driveshaft torque, in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

To enable this port, for Port Configuration, select Simulink.
C - Angular velocity and torque
two-way connector port
Angular velocity in rad/s. Torque is in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

To enable this port, for Port Configuration, select Two-way connection.

## Parameters

## Block Options

Port Configuration - Specify configuration
Simulink (default)|Two-way connection
Specify the port configuration.
Dependencies
Specifying Simulink creates these ports:

- RSpd
- CSpd
- RTrq
- CTrq

Specifying Two-way connection creates these ports:

- R
- C

Output Info bus - Selection
off (default) | on
Select to create the Info output port.
Torsional stiffness, $\mathbf{k}$ - Inertia
le4 (default) | scalar
Torsional stiffness, in $\mathrm{N} \cdot \mathrm{m} / \mathrm{rad}$.
Torsional damping, $\mathbf{b}$ - Damping
1e2 (default) | scalar
Torsional damping, in $\mathrm{N} \cdot \mathrm{m} \cdot \mathrm{s} / \mathrm{rad}$.
Initial deflection, theta_o - Angular
0 (default) | scalar
Initial deflection, in rad.
Initial velocity difference, domega_o - Angular
0 (default) | scalar
Initial velocity difference, in rad/s.
Damping cut-off frequency, omega_c - Frequency 3000 (default) | scalar

Damping cut-off frequency, in rad/s.

## Version History

Introduced in R2017a

## Extended Capabilities

C/C++ Code Generation
Generate C and C++ code using Simulink $\circledR^{\circledR}$ Coder ${ }^{\mathrm{TM}}$.
See Also
Rotational Inertia | Split Torsional Compliance

## Active Differential

Spur or planetary active differential gear


## Libraries:

Vehicle Dynamics Blockset / Powertrain / Drivetrain / Final Drive Unit

## Description

The Active Differential block implements an active differential to account for the power transfer from the transmission to the axles. The block models the active differential as an open differential coupled to either a spur or planetary differential gear set. The block uses external pressure signals to regulate the clutch pressure to either speed up or slow down each axle rotation.

Use the block in hardware-in-the-loop (HIL) and optimization workflows to dynamically couple the driveshaft to the wheel axles when you want to direct the transmission torque to a specific axle. For detailed front wheel driving studies, use the block to couple the driveshaft to universal joints. The block is suitable to use in system-level closed-loop control studies, for example, yaw stability and torque vectoring. All the parameters are tunable.

To specify the active differential, open the Active Differential parameters and specify Active differential type.

| Setting | Block Implementation |
| :--- | :--- |
| Spur gears, superposition <br> clutches | Clutches are in superposition through a three-gang gear system <br> and a differential case |
| Double planetary gears, <br> stationary clutches | Clutches are fixed to the carrier and axles through double <br> planetary gear sets |

Use the Open Differential parameter Crown wheel (ring gear) located to specify the open differential location, either to the left or right of the center-line.

Depending on the available data, to specify the method to couple the different torques applied to the axles, use the Slip Coupling parameter Coupling type.

| Setting | Block Implementation |
| :--- | :--- |
| Pre-loaded ideal clutch | Torque modeled as a dry clutch with constant friction coefficients |
| Slip speed dependent <br> torque data | Torque determined from a lookup table that is a function of slip- <br> speed and clutch pressure |

The Active Differential block does not include a controller or external clutch actuator dynamics. Use this information to control the input clutch pressure. The info bus contains the slip speeds at clutch 1, $\Delta \omega_{\text {cl1 }}$, and clutch 2, $\Delta \omega_{c l 2}$.

| Input Axle Torque | $\Delta \boldsymbol{\omega}_{\text {cl1 }}$ | $\Delta \omega_{c \mid 2}$ | Input Clutch Pressure |
| :--- | :--- | :--- | :--- |
| Positive axle 1 torque | $>0$ | N/A | Increase clutch 1 <br> pressure |
| Positive axle 1 torque | $<0$ | N/A | Disengage clutch 1 and <br> 2 |
| Positive axle 2 torque | N/A | $>0$ | Increase clutch 1 <br> pressure |
| Positive axle 2 torque | N/A | $<0$ | Disengage clutch 1 and <br> 2 |

## Differentials

The Active Differential block implements these equations to represent the mechanical dynamic response for the superposition and stationary clutch configurations. To determine the gear ratios, the block uses the clutch speed and the number of teeth for each gear pair. The allowable wheel speed difference (AWSD) limits the wheel speed difference for positive torque.

| $\begin{array}{c}\text { Mechanical } \\ \text { Dynamic } \\ \text { Response }\end{array}$ | Equations |  |
| :--- | :--- | :--- |
|  | $\begin{array}{c}\text { Superposition Clutches and Spur } \\ \text { Gearing }\end{array}$ | Stationary Clutches and Planetary |
| Gearing |  |  |$]$

## Superposition Clutches and Spur Gearing

These superposition clutch illustrations show the clutch configuration and schematic for torque transfer to the left wheel.


## Stationary Clutches and Planetary Gearing

The illustrations show the stationary clutch configuration and schematic.


## Slip Coupling

For both the ideal clutch and slip-speed configurations, the slip coupling is a function of the slipspeed and clutch pressure. The slip-speed depends on the slip velocity at each of the clutch interfaces.

$$
\varpi=\left[\Delta \omega_{c 1}, \Delta \omega_{c 2}\right]
$$

## Ideal Clutch

The ideal clutch coupling model uses the axle slip speed, clutch pressure, and friction to calculate the clutch torque. The friction coefficient is a function of the slip speed.

$$
T_{C}=F_{T} N_{d} \mu(|\bar{\omega}|) R_{e f f} \tanh (4 \bar{\omega})
$$

To calculate the total clutch force, the block uses the effective radius, clutch pressure, and clutch preload force.

$$
F_{T}=F_{C}+P_{1,2} \mathrm{~A}_{e f f}, \quad F_{T} \geq 0
$$

The disc radii determine the effective clutch radius over which the clutch force acts.

$$
R_{e f f}=\frac{2\left(R_{0}{ }^{3}-R_{i} 3\right)}{\left.3\left(R_{0}{ }^{2}-R_{i}\right)^{2}\right)}
$$

## Slip-Speed

To calculate the clutch torque, the slip speed coupling model uses torque data that is a function of slip speed and clutch pressure. The angular velocities of the axles determine the slip speed.

$$
T_{C}=T_{C}\left(\varpi, \quad P_{1,2}\right)
$$

The equations use these variables.

| $A_{e f f}$ | Effective clutch pressure area |
| :--- | :--- |
| $b_{d}$ | Crown gear linear viscous damping |
| $b_{1}, b_{2}$ | Axle 1 and 2 linear viscous damping, respectively |
| $F_{c}, F_{T}$ | Clutch preload force and total force, respectively |
| $J_{d}$ | Carrier rotational inertia |
| $J_{g c}$ | Three-gang gear rotational inertia |
| $J_{c 1}, J_{c 2}$ | Planetary carrier 1 and 2 rotational inertia, respectively |
| $J_{r 1}, J_{r 2}$ | Planetary ring gear 1 and 2 rotational inertia, respectively |
| $J_{s 1}, J_{s 2}$ | Planetary sun gear 1 and 2 rotational inertia, respectively |
| $J_{1}, J_{2}$ | Axle 1 and 2 rotational inertia, respectively |
| $N$ | Carrier-to-drive shaft gear ratio |
| $N_{d}$ | Number of disks |
| $N_{s 1}, N_{s 2}$ | Clutch 1 and 2 carrier-to-spur gear ratio, respectively |
| $N_{p 1}, N_{p 2}$ | Planetary 1 and 2 carrier-to-axle gear ratio, respectively |
| $P_{1}, P_{2}$ | Clutch 1 and 2 pressure, respectively |


| $R_{e f f}$ | Effective clutch radius |
| :--- | :--- |
| $R_{i}, R_{o}$ | Annular disk inner and outer radius, respectively |
| $T_{c}$ | Clutch torque |
| $T_{c l 1}, T_{c l 2}$ | Clutch 1 and 2 coupling torque, respectively |
| $T_{d}$ | Driveshaft torque |
| $T_{1}, T_{2}$ | Axle 1 and 2 torque, respectively |
| $T_{i}$ | Axle internal resistance torque |
| $T_{i 1}, T_{i 2}$ | Axle 1 and 2 internal resistance torque |
| $\omega_{d}$ | Driveshaft angular velocity |
| $\omega$ | Slip speed |
| $\omega_{1}, \omega_{2}$ | Axle 1 and 2 angular velocity, respectively |
| $\Delta \omega_{c l 1}, \Delta \omega_{c l 2}$ | Clutch 1 and 2 slip speed at interface, respectively |
| $\omega_{c l 1}, \omega_{c l 2}$ | Clutch 1 and 2 angular velocity, respectively |
| $\mu$ | Clutch coefficient of friction |
| $z_{i}$ | Number of teeth on gear $i$ |

## Ports

Inputs
Prs1 - Clutch 1 pressure
scalar
Clutch 1 pressure, $P_{1}$, in Pa.
Prs2 - Clutch 2 pressure
scalar
Clutch 2 pressure, $P_{2}$, in Pa.
DriveshftTrq - Driveshaft torque
scalar
Applied input torque, $T_{d}$, typically from the engine driveshaft, in $\mathrm{N} \cdot \mathrm{m}$.
AxI1Trq - Torque
scalar
Axle 1 torque, $T_{1}$, in $\mathrm{N} \cdot \mathrm{m}$.
AxI2Trq - Torque
scalar
Axle 2 torque, $T_{2}$, in $N \cdot m$.
Output
Info - Bus signal
bus

Bus signal containing these block calculations.

| Signal |  | Description | Units |
| :--- | :--- | :--- | :--- |
| Driveshft | DriveshftTrq | Drive shaft torque | $\mathrm{N} \cdot \mathrm{m}$ |
|  | DriveshftSpd | Drive shaft angular velocity | $\mathrm{rad} / \mathrm{s}$ |
|  | Axl1Trq | Axle 1 torque | $\mathrm{N} \cdot \mathrm{m}$ |
|  | Axl1Spd | Axle 1 angular velocity | $\mathrm{rad} / \mathrm{s}$ |
| Cplng | Axl2Trq | Axle 2 torque | $\mathrm{N} \cdot \mathrm{m}$ |
|  | Axl2Spd | Axle 2 angular velocity | $\mathrm{rad} / \mathrm{s}$ |
|  | CplngTrq1 | Clutch 1 coupling torque | $\mathrm{N} \cdot \mathrm{m}$ |
|  | CplngTrq2 | Clutch 2 coupling torque | $\mathrm{N} \cdot \mathrm{m}$ |
|  | CplngSlipSpd1 | Clutch 1 slip speed | $\mathrm{rad} / \mathrm{s}$ |
|  | CplngSlipSpd2 | Clutch 2 slip speed | $\mathrm{rad} / \mathrm{s}$ |
|  | CplngPrs1 | Clutch 1 input pressure | Pa |
|  | CplngPrs2 | Clutch 2 input pressure | Pa |

DriveshftSpd - Angular velocity
scalar
Driveshaft angular velocity, $\omega_{d}$, in rad/s.
AxIISpd - Angular velocity
scalar
Axle 1 angular velocity, $\omega_{1}$, in rad/s.
AxI2Spd - Angular velocity
scalar
Axle 2 angular velocity, $\omega_{2}$, in rad/s.

## Parameters

## Active Differential

## Active differential type - Differential

Spur gears, superposition clutches (default)|Double planetary gears, stationary clutches

Specify the type of active differential.

| Setting | Block Implementation |
| :--- | :--- |
| Spur gears, superposition <br> clutches | Clutches are in superposition through a three-gang gear system <br> and a differential case |
| Double planetary gears, <br> stationary clutches | Clutches are fixed to the carrier and axles through double <br> planetary gear sets |

Clutch 1 to differential case gear ratio, Ns1 - Clutch 1-spur gear ratio

## . 875 (default) | scalar

Clutch 1-to-carrier spur gear ratio, $N_{s 1}$, dimensionless.

## Dependencies

To enable the spur gear parameters, select Spur gears, superposition clutches for the Active differential type parameter.

Clutch 2 to differential case gear ratio, Ns2 - Clutch 2-spur gear ratio 1.125 (default) | scalar

Clutch 2-to-carrier spur gear ratio, $N_{s 2}$, dimensionless.

## Dependencies

To enable the spur gear parameters, select Spur gears, superposition clutches for the Active differential type parameter.

Three-gang gear inertia, Jgc - Rotational inertia

## . 003 (default) | scalar

Three-gang gear rotational inertia, $J_{g c}$, in $\mathrm{kg} \cdot \mathrm{m} \wedge 2$.

## Dependencies

To enable the spur gear parameters, select Spur gears, superposition clutches for the Active differential type parameter.

Axle 1 planetary carrier to axle gear ratio, Np1 - Planetary 1 carrier gear ratio
1.125 (default) | scalar

Planetary 1 carrier-to-axle gear ratio, $N_{p 1}$, dimensionless.

## Dependencies

To enable the planetary gear parameters, select Double planetary gears, stationary clutches for the Active differential type parameter.

Axle 1 sun gear inertia, Js1 - Planetary 1 sun gear inertia
. 001 (default) | scalar
Planetary 1 sun gear inertia, $J_{s 1}$, in $\mathrm{kg} \cdot \mathrm{m}^{\wedge} 2$.

## Dependencies

To enable the planetary gear parameters, select Double planetary gears, stationary clutches for the Active differential type parameter.

Axle 1 carrier inertia, Jc1 - Planetary 1 carrier inertia
. 001 (default) | scalar
Planetary 1 carrier inertia, $J_{c 1}$, in $\mathrm{kg} \cdot \mathrm{m}^{\wedge} 2$.

## Dependencies

To enable the planetary gear parameters, select Double planetary gears, stationary clutches for the Active differential type parameter.

Axle 1 ring inertia, Jr1 - Planetary 1 ring gear inertia

## . 002 (default) | scalar

Planetary 1 ring gear inertia, $J_{r 1}, \mathrm{~kg} \cdot \mathrm{~m}^{\wedge} 2$.

## Dependencies

To enable the planetary gear parameters, select Double planetary gears, stationary clutches for the Active differential type parameter.

Axle 2 planetary carrier to axle gear ratio, Np2 - Planetary 2 carrier gear ratio
1.125 (default) | scalar

Planetary 2 carrier-to-axle gear ratio, $N_{p 2}$, dimensionless.

## Dependencies

To enable the planetary gear parameters, select Double planetary gears, stationary clutches for the Active differential type parameter.

Axle 2 sun gear inertia, Js2 - Planetary 2 sun gear inertia
. 001 (default) | scalar
Planetary 2 sun gear inertia, $J_{s 2}$, in $\mathrm{kg} \cdot \mathrm{m}^{\wedge} 2$.

## Dependencies

To enable the planetary gear parameters, select Double planetary gears, stationary clutches for the Active differential type parameter.

Axle 2 carrier inertia, Jc2 - Planetary 2 carrier inertia
. 001 (default) | scalar
Planetary 2 carrier inertia, $J_{c 2}$, in $\mathrm{kg} \cdot \mathrm{m}^{\wedge} 2$.

## Dependencies

To enable the planetary gear parameters, select Double planetary gears, stationary clutches for the Active differential type parameter.

Axle 2 ring inertia, Jr2 - Planetary 2 ring gear inertia
. 002 (default) | scalar
Planetary 2 ring gear inertia, $J_{r 2}$, in $\mathrm{kg} \cdot \mathrm{m}^{\wedge} 2$.
Dependencies
To enable the planetary gear parameters, select Double planetary gears, stationary clutches for the Active differential type parameter.

## Open Differential

Crown wheel (ring gear) located - Specify crown wheel connection
To the left of center-line (default)|To the right of center-line
Specify the crown wheel connection to the drive shaft.

Carrier to drive shaft ratio, NC/ND - Ratio
4 (default) | scalar
Carrier-to-drive shaft gear ratio, $N$.
Carrier inertia, Jd - Inertia
. 1 (default) | scalar
Rotational inertia of the crown gear assembly, $J_{d}$, in $\mathrm{kg} \cdot \mathrm{m} \wedge 2$. You can include the drive shaft inertia.
Carrier damping, bd - Damping
le-3 (default) | scalar
Crown gear linear viscous damping, $b_{d}$, in $N \cdot m \cdot s / r a d$.
Axle 1 inertia, Jw1 - Inertia
. 1 (default) | scalar
Axle 1 rotational inertia, $J_{1}$, in $\mathrm{kg} \cdot \mathrm{m}^{\wedge} 2$.
Axle 1 damping, bw1 - Damping
1e-3 (default) | scalar
Axle 1 linear viscous damping, $b_{1}$, in $\mathrm{N} \cdot \mathrm{m} \cdot \mathrm{s} / \mathrm{rad}$.
Axle 2 inertia, Jw2 - Inertia
. 1 (default) | scalar
Axle 2 rotational inertia, $J_{2}$, in $\mathrm{kg} \cdot \mathrm{m}^{\wedge} 2$.
Axle 2 damping, bw2 - Damping
1e-3 (default) | scalar
Axle 2 linear viscous damping, $b_{2}$, in $\mathrm{N} \cdot \mathrm{m} \cdot \mathrm{s} / \mathrm{rad}$.
Axle 1 initial velocity, omegaw1o - Angular velocity
0 (default) | scalar
Axle 1 initial velocity, $\omega_{01}$, in rad/s.
Axle 2 initial velocity, omegaw2o - Angular velocity
0 (default) | scalar
Axle 2 initial velocity, $\omega_{02}$, in rad/s.

## Slip Coupling

## Coupling type - Torque coupling

Ideal pre-loaded clutch (default)|Slip speed dependent torque data|Input torque dependent torque data

Specify the type of torque coupling.

| Setting | Block Implementation |
| :--- | :--- |
| Pre-loaded ideal clutch | Torque modeled as a wet clutch with a constant velocity |


| Setting | Block Implementation |
| :--- | :--- |
| Slip speed dependent <br> torque data | Torque determined from a lookup table that is a function of slip- <br> speed and clutch pressure |

## Effective applied pressure area - Pressure area

0.01 (default) | scalar

Effective applied pressure area, in $\mathrm{N} / \mathrm{m}^{\wedge} 2$.

## Dependencies

To enable the clutch parameters, select Ideal pre-loaded clutch for the Coupling type parameter.

Number of disks, Ndisks - Torque coupling
4 (default) | scalar
Number of disks.

## Dependencies

To enable the clutch parameters, select Ideal pre-loaded clutch for the Coupling type parameter.

Effective radius, Reff - Radius
. 20 (default) | scalar
The effective radius, $R_{e f f}$, used with the applied clutch friction force to determine the friction force. The effective radius is defined as:

$$
R_{e f f}=\frac{2\left(R_{O}^{3}-R_{i} 3\right)}{3\left(R_{0}^{2}-R_{i}^{2}\right)}
$$

The equation uses these variables.

| $R_{o}$ | Annular disk outer radius |
| :--- | :--- |
| $R_{i}$ | Annular disk inner radius |

## Dependencies

To enable the clutch parameters, select Ideal pre-loaded clutch for the Coupling type parameter.

Nominal preload force, Fc - Force
500 (default) | scalar
Nominal preload force, in N.

## Dependencies

To enable the clutch parameters, select Ideal pre-loaded clutch for the Coupling type parameter.

Friction coefficient vector, mu - Friction

```
[.16 0.13 0.115 0.11 0.105 0.1025 0.10125 .10125] (default)|vector
```

Friction coefficient vector.

## Dependencies

To enable the clutch parameters, select Ideal pre-loaded clutch for the Coupling type parameter.

Slip speed vector, dw - Angular velocity
[0 10 20406080100 500] (default)| vector
Slip speed vector, in rad/s.
To enable the clutch parameters, select Ideal pre-loaded clutch for the Coupling type parameter.

Torque - slip speed matrix, TdPdw - Clutch torque
[-1000, -500, -90, -50, -5, $0,5,50,90,500,1000] . * o n e s(11)$ (default)|matrix
Torque matrix, $T_{c}$, in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

To enable the slip speed parameters, select Slip speed dependent torque data for the Coupling type parameter.

Clutch pressure vector, $\mathbf{p T}$ - Clutch pressure breakpoints
[0 1e3 5e3 7e3 1e4 2e4 5e4 1e5 5e5 le6 5e6] (default)|vector
Clutch pressure breakpoints vector, $P_{1,2}$, in Pa.

## Dependencies

To enable the slip speed parameters, select Slip speed dependent torque data for the Coupling type parameter.

Slip speed vector, dwT - Slip speed breakpoints
[-500-200, -175, -100, - 50, 0, 50, 100, 175, 200, 500] (default)| vector
Slip speed breakpoints vector, $\omega$, in rad/s.

## Dependencies

To enable the slip speed parameters, select Slip speed dependent torque data for the Coupling type parameter.

Coupling time constant, tauC - Constant

```
.01 (default)| scalar
```

Coupling time constant, in s.

## Version History

Introduced in R2018b

## References

[1] Deur, J., Ivanović, V., Hancock, M., and Assadian, F. "Modeling of Active Differential Dynamics." In ASME proceedings. Transportation Systems. Vol. 17, pp: 427-436.

## Extended Capabilities

C/C++ Code Generation
Generate C and $\mathrm{C}++$ code using Simulink $®$ Coder $^{\mathrm{TM}}$.

## See Also

Open Differential | Limited Slip Differential

## Limited Slip Differential

Limited differential as a planetary bevel gear


## Libraries:

Powertrain Blockset / Drivetrain / Final Drive Unit
Vehicle Dynamics Blockset / Powertrain / Drivetrain / Final Drive Unit

## Description

The Limited Slip Differential block implements a differential as a planetary bevel gear train. The block matches the driveshaft bevel gear to the crown (ring) bevel gear. You can specify:

- Carrier-to-driveshaft ratio
- Crown wheel location
- Viscous and damping coefficients for the axles and carrier
- Type of slip coupling

Use the block in system-level driveline analysis to account for the power transfer from the transmission to the wheels. The block is suitable for use in hardware-in-the-loop (HIL) and optimization workflows. All the parameters are tunable.

In a limited slip differential, to prevent one of the wheels from slipping, the differential splits the torque applied to the left and right axles. With different torque applied to the axles, the wheels can move at different angular velocities, preventing slip. The block implements three methods for coupling the different torques applied to the axes:

- Pre-loaded ideal clutch
- Slip speed-dependent torque data
- Input torque dependent torque data

The block uses a coordinate system that produces positive tire and vehicle motion for standard engine, transmission, and differential configurations. The arrows indicate positive motion.


## Efficiency

To account for the block efficiency, use the Efficiency factors parameter. This table summarizes the block implementation for each setting.

| Setting | Implementation |
| :--- | :--- |
| Constant | Constant efficiency that you can set with the Constant efficiency factor, <br> eta parameter. |
| Driveshaft torque, <br> temperature and <br> speed | Efficiency as a function of base gear input torque, air temperature, and <br> driveshaft speed. Use these parameters to specify the lookup table and <br> breakpoints: <br> - $\quad$ Efficiency lookup table, eta_tbl <br> - $\quad$ Efficiency torque breakpoints, Trq_bpts <br> - $\quad$ Efficiency speed breakpoints, omega_bpts <br> - $\quad$ Efficiency temperature breakpoints, Temp_bpts <br> For the air temperature, you can either: |
|  | - Select Input temperature to create an input port. <br> - Set a Ambient temperature, Tamb parameter value. <br> To select the interpolation method, use the Interpolation method <br> parameter. For more information, see "Interpolation Methods". |

## Power Accounting

For the power accounting, the block implements these equations.

| Bus Signal |  |  | Description | Equations |
| :---: | :---: | :---: | :---: | :---: |
| PwrInfo | PwrTrnsfrd - Power transferred between blocks <br> - Positive signals indicate flow into block <br> - Negative signals indicate flow out of block | PwrDriveshft | Mechanical power from driveshaft | $\eta T_{d} \omega_{d}$ |
|  |  | PwrAxl1 | Mechanical power from axle 1 | $\eta T_{1} \omega_{1}$ |
|  |  | PwrAxl2 | Mechanical power from axle 2 | $\eta T_{2} \omega_{2}$ |
|  | PwrNotTrnsfrd - Power crossing the block boundary, but not transferred <br> - Positive signals indicate an input <br> - Negative signals indicate a loss | PwrMechLoss | Total power loss | $\begin{aligned} & \dot{W}_{\text {loss }}=-\left(P_{t}+P_{d}+1\right. \\ & P_{t}=\eta\left(T_{d} \omega_{d}+T_{1} \omega_{1}+T\right. \end{aligned}$ |
|  |  | PwrDampLoss | Power loss due to damping | $\begin{aligned} & P_{d}=-\left(b_{1}\left\|\omega_{1}\right\|\right. \\ & \left.+b_{2}\left\|\omega_{2}\right\|+b_{d}\left\|\omega_{d}\right\|\right) \end{aligned}$ |
|  |  | PwrCplngLoss | Power loss due to clutch | $P_{C}=T_{C}\|\bar{\omega}\|$ |
|  | PwrStored - Stored energy rate of change <br> - Positive signals indicate an increase <br> - Negative signals indicate a decrease | PwrStoredShft | Rate change of stored internal energy | $\begin{aligned} & P_{s}=-\left(\omega_{1} \dot{\omega}_{1} J_{1}\right. \\ & \left.+\omega_{2} \dot{\omega}_{2} J_{2}+\omega_{d} \dot{\omega}_{d} J_{d}\right) \end{aligned}$ |

## Dynamics

The Limited Slip Differential block implements these differential equations to represent the mechanical dynamic response for the crown gear, left axle, and right axle.

| Mechanical <br> Dynamic <br> Response | Differential Equation |
| :--- | :--- |
| Crown Gear | $\dot{\omega}_{d} J_{d}=\eta T_{d}-\omega_{d} b_{d}-T_{i}$ |
| Left Axle | $\dot{\omega}_{1} J_{1}=\eta T_{1}-\omega_{1} b_{1}-T_{i 1}$ |
| Right Axle | $\dot{\omega}_{2} J_{2}=\eta T_{2}-\omega_{2} b_{2}-T_{i 2}$ |

The block assumes rigid coupling between the crown gear and axles. These constraint equations apply.

$$
\begin{aligned}
& \eta T_{1}=\frac{N}{2} T_{i}-\frac{1}{2} T_{c} \\
& \eta T_{2}=\frac{N}{2} T_{i}+\frac{1}{2} T_{c}
\end{aligned}
$$

$$
\omega_{d}=\frac{N}{2}\left(\omega_{1}+\omega_{2}\right)
$$

The equations use these variables.

| $N$ | Carrier-to-driveshaft gear ratio |
| :--- | :--- |
| $J_{d}$ | Rotational inertia of the crown gear assembly |
| $b_{d}$ | Crown gear linear viscous damping |
| $\omega_{d}$ | Driveshaft angular speed |
| $\omega$ | Slip speed |
| $J_{1}$ | Axle 1 rotational inertia |
| $b_{1}$ | Axle 1 linear viscous damping |
| $\omega_{1}$ | Axle 1 speed |
| $J_{2}$ | Axle 2 rotational inertia |
| $b_{2}$ | Axle 2 linear viscous damping |
| $\omega_{2}$ | Axle 2 angular speed |
| $\eta$ | Efficiency |
| $T_{d}$ | Driveshaft torque |
| $T_{1}$ | Axle 1 torque |
| $T_{2}$ | Axle 2 torque |
| $T_{i}$ | Axle internal resistance torque |
| $T_{i 1}$ | Axle 1 internal resistance torque |
| $T_{i 2}$ | Axle 2 internal resistance torque |
| $\mu$ | Coefficient of friction |
| $R_{e f f}$ | Effective clutch radius |
| $R_{0}$ | Annular disk outer radius |
| $R_{i}$ | Annular disk inner radius |
| $F_{c}$ | Clutch force |
| $T_{c}$ | Clutch torque |
| $\mu$ | Coefficient of friction |

Table blocks in the Limited Slip Differential have these parameter settings:

- Interpolation method - Linear
- Extrapolation method - Clip

Ideal Clutch Coupling
The ideal clutch coupling model uses the axle slip speed and friction to calculate the clutch torque. The friction coefficient is a function of the slip speed.

$$
T_{c}=F_{C} N \mu(|\sigma|) R_{e f f} \tanh (4|\sigma|)
$$

The disc radii determine the effective clutch radius over which the clutch force acts.

$$
R_{e f f}=\frac{2\left(R_{0}{ }^{3}-R_{i} 3\right)}{3\left(R_{0}{ }^{2}-R_{i} 2\right)}
$$

The angular velocities of the axles determine the slip speed.

$$
\varpi=\omega_{1}-\omega_{2}
$$

## Slip Speed Coupling

To calculate the clutch torque, the slip speed coupling model uses torque data that is a function of slip speed. The angular velocities of the axles determine the slip speed.

$$
\varpi=\omega_{1}-\omega_{2}
$$

## Input Torque Coupling

To calculate the clutch torque, the input torque coupling model uses torque data that is a function of input torque.

The Open Differential block assumes rigid coupling between the crown gear and axles. These constraint equations apply.

$$
\begin{aligned}
& \eta T_{i 1}=\eta T_{i 2}=\frac{N}{2} T_{i} \\
& \omega_{d}=\frac{N}{2}\left(\omega_{1}+\omega_{2}\right)
\end{aligned}
$$

## Ports

Inputs
DriveshftTrq - Torque
scalar
Applied input torque, typically from the engine crankshaft, in $\mathrm{N} \cdot \mathrm{m}$.
AxIITrq - Torque
scalar
Axle 1 torque, $T_{1}$, in $\mathrm{N} \cdot \mathrm{m}$.
AxI2Trq - Torque
scalar
Axle 2 torque, $T_{2}$, in $\mathrm{N} \cdot \mathrm{m}$.
Temp - Temperature
scalar
Temperature, in K.

## Dependencies

To enable this port:

- Set Efficiency factors to Driveshaft torque, speed and temperature.
- Select Input temperature.


## Output

Info - Bus signal
bus
Bus signal containing these block calculations.

| Signal |  |  | Description | Units |
| :---: | :---: | :---: | :---: | :---: |
| Driveshft | DriveshftTrq |  | Driveshaft torque | $\mathrm{N} \cdot \mathrm{m}$ |
|  | DriveshftSpd |  | Driveshaft speed | rad/s |
| Axl1 | Axl1Trq |  | Axle 1 torque | $\mathrm{N} \cdot \mathrm{m}$ |
|  | Axl1Spd |  | Axle 1 speed | rad/s |
| Axl2 | Axl2Trq |  | Axle 2 torque | $\mathrm{N} \cdot \mathrm{m}$ |
|  | Axl2Spd |  | Axle 2 speed | rad/s |
| Cplng | CplngTrq |  | Torque coupling | $\mathrm{N} \cdot \mathrm{m}$ |
|  | CplngSlipSpd |  | Slip speed | rad/s |
| PwrInfo | PwrTrnsfrd | PwrDrivesh ft | Mechanical power from driveshaft | W |
|  |  | PwrAxl1 | Mechanical power from axle 1 | W |
|  |  | PwrAxl2 | Mechanical power from axle 2 | W |
|  | PwrNotTrns frd | PwrMechLos S | Total power loss | W |
|  |  | PwrDampLos s | Power loss due to damping | W |
|  |  | PwrCplngLo ss | Power loss due to clutch | W |
|  | PwrStoredS hft | PwrStoredS hft | Rate change of stored internal energy | W |

## DriveshftSpd - Angular speed

## scalar

Driveshaft angular speed, $\omega_{d}$, in rad/s.
AxI1Spd - Angular speed
scalar
Axle 1 angular speed, $\omega_{1}$, in rad/s.
AxI2Spd - Angular speed
scalar
Axle 2 angular speed, $\omega_{2}$, in rad/s.

## Parameters

## Block Options

Efficiency factors - Specify configuration
Constant (default)|Driveshaft torque, speed and temperature
To account for the block efficiency, use the Efficiency factors parameter. This table summarizes the block implementation for each setting.

| Setting | Implementation |
| :--- | :--- |
| Constant | Constant efficiency that you can set with the Constant efficiency factor, <br> eta parameter. |
| Driveshaft torque, <br> temperature and <br> speed | Efficiency as a function of base gear input torque, air temperature, and <br> driveshaft speed. Use these parameters to specify the lookup table and <br> breakpoints: <br> - $\quad$ Efficiency lookup table, eta_tbl <br> - $\quad$ Efficiency torque breakpoints, Trq_bpts <br> - $\quad$ Efficiency speed breakpoints, omega_bpts <br> - $\quad$ Efficiency temperature breakpoints, Temp_bpts <br> For the air temperature, you can either: |
|  | - Select Input temperature to create an input port. <br> - Set a Ambient temperature, Tamb parameter value. <br> To select the interpolation method, use the Interpolation method <br> parameter. For more information, see "Interpolation Methods". |

## Interpolation method - Method

Flat|Nearest|Linear point-slope|Linear Lagrange|Cubic spline
For more information, see "Interpolation Methods".

## Dependencies

To enable this parameter, set Efficiency factors to Driveshaft torque, speed and temperature.

Input temperature - Create input port
off (default) | on
Select to create input port Temp for the temperature.

## Dependencies

To enable this parameter, set Efficiency factors to Driveshaft torque, speed and temperature.

## Open Differential

Crown wheel (ring gear) located - Specify crown wheel connection
To the left of center-line (default)|To the right of center-line

Specify the crown wheel connection to the driveshaft.

## Carrier to drive shaft ratio, NC/ND - Ratio

4 (default) | scalar
Carrier-to-driveshaft gear ratio, $N$.
Carrier inertia, Jd - Inertia
. 1 (default) | scalar
Rotational inertia of the crown gear assembly, $J_{d}$, in $\mathrm{kg} \cdot \mathrm{m}^{\wedge} 2$. You can include the driveshaft inertia.
Carrier damping, bd - Damping
le-3 (default) | scalar
Crown gear linear viscous damping, $b_{d}$, in $N \cdot \mathrm{~m} \cdot \mathrm{~s} / \mathrm{rad}$.
Axle 1 inertia, Jw1 - Inertia
. 1 (default) | scalar
Axle 1 rotational inertia, $J_{1}$, in $\mathrm{kg} \cdot \mathrm{m}^{\wedge} 2$.
Axle 1 damping, bw 1 - Damping
1e-3 (default) | scalar
Axle 1 linear viscous damping, $b_{1}$, in $\mathrm{N} \cdot \mathrm{m} \cdot \mathrm{s} / \mathrm{rad}$.
Axle 2 inertia, Jw2 - Inertia
. 1 (default) | scalar
Axle 2 rotational inertia, $J_{2}$, in $\mathrm{kg} \cdot \mathrm{m}^{\wedge} 2$.
Axle 2 damping, bw2 - Damping
1e-3 (default) | scalar
Axle 2 linear viscous damping, $b_{2}$, in $\mathrm{N} \cdot \mathrm{m} \cdot \mathrm{s} / \mathrm{rad}$.
Axle 1 initial velocity, omegaw10 - Angular velocity
0 (default) | scalar
Axle 1 initial velocity, $\omega_{o 1}$, in rad/s.
Axle 2 initial velocity, omegaw2o - Angular velocity
0 (default) | scalar
Axle 2 initial velocity, $\omega_{o 2}$, in rad/s.
Constant efficiency factor, eta - Efficiency
1 (default) | scalar
Constant efficiency, $\eta$.

## Dependencies

To enable this parameter, set Efficiency factors to Constant.

Efficiency lookup table, eta_tbl - Lookup table
M-by-N-by-L array
Dimensionless array of values for efficiency as a function of:

- M input torques
- $N$ input speed
- L air temperatures

Each value specifies the efficiency for a specific combination of torque, speed, and temperature. The array size must match the dimensions defined by the torque, speed, and temperature breakpoint vectors.

## Dependencies

To enable this parameter, set Efficiency factors to Driveshaft torque, speed and temperature.

Efficiency torque breakpoints, Trq_bpts - Torque breakpoints
[25, 50, 75, 100, 150, 200, 250] (default) | 1-by-M vector
Vector of input torque, breakpoints for efficiency, in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

To enable this parameter, set Efficiency factors to Driveshaft torque, speed and temperature.

Efficiency speed breakpoints, omega_bpts - Speed breakpoints
[52.4 78.5 105131157183209262314419 524] (default)| 1-by-N vector
Vector of speed, breakpoints for efficiency, in rad/s.

## Dependencies

To enable this parameter, set Efficiency factors to Driveshaft torque, speed and temperature.

Efficiency temperature breakpoints, Temp_bpts - Temperature breakpoints
[290 358] (default) | 1-by-L vector
Vector of ambient temperature breakpoints for efficiency, in K.
Dependencies
To enable this parameter, set Efficiency factors to Driveshaft torque, speed and temperature.

Ambient temperature, Tamb - Ambient temperature
297.15 (default) | scalar

Ambient air temperature, $T_{\text {air }}$, in K.
Dependencies
To enable this parameter:

- Set Efficiency factors to Driveshaft torque, speed and temperature.
- Clear Input temperature.


## Slip Coupling

Coupling type - Torque coupling
Pre-loaded ideal clutch (default)|Slip speed dependent torque data|Input torque dependent torque data

Specify the type of torque coupling.
Number of disks, Ndisks - Torque coupling
4 (default) | scalar
Number of disks.

## Dependencies

To enable the ideal clutch parameters, select Pre-loaded ideal clutch for the Coupling type parameter.

Effective radius, Reff - Radius
. 20 (default) | scalar
The effective radius, $R_{e f f}$, used with the applied clutch friction force to determine the friction force. The effective radius is defined as:

$$
R_{e f f}=\frac{2\left(R_{O}{ }^{3}-R_{i} 3\right)}{\left.3\left(R_{O}^{2}-R_{i}\right)^{2}\right)}
$$

The equation uses these variables.
$R_{0} \quad$ Annular disk outer radius
$R_{i} \quad$ Annular disk inner radius

## Dependencies

To enable the clutch parameters, select Pre-loaded ideal clutch for the Coupling type parameter.

Nominal preload force, Fc - Force
500 (default) | scalar
Nominal preload force, in N .

## Dependencies

To enable the clutch parameters, select Pre-loaded ideal clutch for the Coupling type parameter.

Friction coefficient vector, muc - Friction
[. 160.130 .1150 .110 .1050 .10250 .10125$]$ (default)|vector
Friction coefficient vector.

## Dependencies

To enable the clutch parameters, select Pre-loaded ideal clutch for the Coupling type parameter.

Slip speed vector, dw - Angular velocity
[0 1020406080 100] (default) |vector
Slip speed vector, in rad/s.

## Dependencies

To enable the clutch parameters, select Pre-loaded ideal clutch for the Coupling type parameter.

Torque - slip speed vector, Tdw - Torque
[-100, -90, -50, -5, 0, 5, 50, 90, 100] (default)|vector
Torque vector, in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

To enable the slip speed parameters, select Slip speed dependent torque data for the Coupling type parameter.

Slip speed vector, dwT - Angular velocity
[-200, -175, -100, - 50, 0, 50, 100, 175, 200] (default)|vector
Slip speed vector, in rad/s.

## Dependencies

To enable the slip speed parameters, select Slip speed dependent torque data for the Coupling type parameter.

Torque - input torque vector, TTin - Torque
[-200-175-100-50 050100175 200] (default)|vector
Torque vector, in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

To enable the input torque parameters, select Input torque dependent torque data for the Coupling type parameter.

Input torque vector, Tin - Torque
[-200-175-100-50 050100175 200] (default)|vector
Torque vector, in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

To enable the input torque parameters, select Input torque dependent torque data for the Coupling type parameter.

## Coupling time constant, tauC - Constant

```
. }01\mathrm{ (default)| scalar
```

Coupling time constant, in s.

## Version History

Introduced in R2017a

## References

[1] Deur, J., Ivanović, V., Hancock, M., and Assadian, F. "Modeling of Active Differential Dynamics." In ASME proceedings. Transportation Systems. Vol. 17, pp: 427-436.

## Extended Capabilities

C/C++ Code Generation
Generate C and C++ code using Simulink® Coder ${ }^{\mathrm{TM}}$.

## See Also

Open Differential

## Open Differential

Differential as a planetary bevel gear


## Libraries:

Powertrain Blockset / Drivetrain / Final Drive Unit
Vehicle Dynamics Blockset / Powertrain / Drivetrain / Final Drive Unit

## Description

The Open Differential block implements a differential as a planetary bevel gear train. The block matches the driveshaft bevel gear to the crown (ring) bevel gear. You can specify:

- Carrier-to-driveshaft ratio
- Crown wheel location
- Viscous and damping coefficients for the axles and carrier

Use the Open Differential block to:

- Dynamically couple the post-transmission driveshaft to the wheel axles or universal joints
- Model simplified or older drivetrains when optimal traction control does not require passive or active torque vectoring
- Model mechanical power splitting in generic gearbox and drive line scenarios

The block is suitable for use in hardware-in-the-loop (HIL) and optimization workflows. All the parameters are tunable.

The block uses a coordinate system that produces positive tire and vehicle motion for standard engine, transmission, and differential configurations. The arrows indicate positive motion.


## Efficiency

To account for the block efficiency, use the Efficiency factors parameter. This table summarizes the block implementation for each setting.

| Setting | Implementation |
| :--- | :--- |
| Constant | Constant efficiency that you can set with the Constant efficiency factor, <br> eta parameter. |
| Driveshaft torque, <br> temperature and <br> speed | Efficiency as a function of base gear input torque, air temperature, and <br> driveshaft speed. Use these parameters to specify the lookup table and <br> breakpoints: <br> - $\quad$ Efficiency lookup table, eta_tbl <br> - $\quad$ Efficiency torque breakpoints, Trq_bpts <br> - $\quad$ Efficiency speed breakpoints, omega_bpts <br> - $\quad$ Efficiency temperature breakpoints, Temp_bpts <br> For the air temperature, you can either: |
|  | - Select Input temperature to create an input port. <br> - Set a Ambient temperature, Tamb parameter value. <br> To select the interpolation method, use the Interpolation method <br> parameter. For more information, see "Interpolation Methods". |

## Power Accounting

For the power accounting, the block implements these equations.

| Bus Signal |  |  | Description | Equations |
| :---: | :---: | :---: | :---: | :---: |
| PwrInfo | PwrTrnsfrd - Power transferred between blocks <br> - Positive signals indicate flow into block <br> - Negative signals indicate flow out of block | PwrDriveshft | Mechanical power from driveshaft | $\eta T_{d} \omega_{d}$ |
|  |  | PwrAxl1 | Mechanical power from axle 1 | $\eta T_{1} \omega_{1}$ |
|  |  | PwrAxl2 | Mechanical power from axle 2 | $\eta T_{2} \omega_{2}$ |
|  | PwrNotTrnsfrd - Power crossing the block boundary, but not transferred <br> - Positive signals indicate an input <br> - Negative signals indicate a loss | PwrMechLoss | Total power loss | $\begin{aligned} & \dot{W}_{\text {loss }}=-\left(P_{t}+P_{d}\right)+ \\ & P_{t}=\eta T_{d} \omega_{d}+\eta T_{1} \omega_{1}+\eta ? \end{aligned}$ |
|  |  | PwrDampLoss | Power loss due to damping | $\begin{aligned} & P_{d}=-\left(b_{1}\left\|\omega_{1}\right\|\right. \\ & \left.+b_{2}\left\|\omega_{2}\right\|+b_{d}\left\|\omega_{d}\right\|\right) \end{aligned}$ |
|  | PwrStored - Stored energy rate of change <br> - Positive signals indicate an increase <br> - Negative signals indicate a decrease | PwrStoredShft | Rate change of stored internal energy | $\begin{aligned} & P_{s}=-\left(\omega_{1} \dot{\omega}_{1} J_{1}\right. \\ & \left.+\omega_{2} \dot{\omega}_{2} J_{2}+\omega_{d} \dot{\omega}_{d} J_{d}\right) \end{aligned}$ |

## Dynamics

The Open Differential block implements these differential equations to represent the mechanical dynamic response for the crown gear, left axle, and right axle.

| Mechanical <br> Dynamic <br> Response | Differential Equation |
| :--- | :--- |
| Crown Gear | $\dot{\omega}_{d} J_{d}=\eta T_{d}-\omega_{d} b_{d}-T_{i}$ |
| Left Axle | $\dot{\omega}_{1} J_{1}=\eta T_{1}-\omega_{1} b_{1}-T_{i 1}$ |
| Right Axle | $\dot{\omega}_{2} J_{2}=\eta T_{2}-\omega_{2} b_{2}-T_{i 2}$ |

The Open Differential block assumes rigid coupling between the crown gear and axles. These constraint equations apply.

$$
\begin{aligned}
& \eta T_{i 1}=\eta T_{i 2}=\frac{N}{2} T_{i} \\
& \omega_{d}=\frac{N}{2}\left(\omega_{1}+\omega_{2}\right)
\end{aligned}
$$

The equations use these variables.

| $N$ | Carrier-to-driveshaft gear ratio |
| :--- | :--- |
| $J_{d}$ | Rotational inertia of the crown gear assembly |
| $b_{d}$ | Crown gear linear viscous damping |
| $\omega_{d}$ | Driveshaft angular speed |
| $\eta$ | Differential efficiency |
| $J_{1}$ | Axle 1 rotational inertia |
| $b_{1}$ | Axle 1 linear viscous damping |
| $\omega_{1}$ | Axle 1 speed |
| $J_{2}$ | Axle 2 rotational inertia |
| $b_{2}$ | Axle 2 linear viscous damping |
| $\omega_{2}$ | Axle 2 angular speed |
| $T_{d}$ | Driveshaft torque |
| $T_{1}$ | Axle 1 torque |
| $T_{2}$ | Axle 2 torque |
| $T_{i}$ | Driveshaft internal resistance torque |
| $T_{i 1}$ | Axle 1 internal resistance torque |
| $T_{i 2}$ | Axle 2 internal resistance torque |

## Ports

Inputs
DriveshftTrq - Torque
scalar
Applied input torque, typically from the engine crankshaft, in $\mathrm{N} \cdot \mathrm{m}$.
AxI1Trq - Torque
scalar
Axle 1 torque, $T_{1}$, in $\mathrm{N} \cdot \mathrm{m}$.
AxI2Trq - Torque
scalar
Axle 2 torque, $T_{2}$, in $\mathrm{N} \cdot \mathrm{m}$.
Temp - Temperature
scalar
Temperature, in K.

## Dependencies

To enable this port:

- Set Efficiency factors to Driveshaft torque, speed and temperature.
- Select Input temperature.


## Output

Info - Bus signal
bus
Bus signal containing these block calculations.

| Signal |  |  | Description | Units |
| :---: | :---: | :---: | :---: | :---: |
| Driveshft | DriveshftTrq |  | Driveshaft torque | $\mathrm{N} \cdot \mathrm{m}$ |
|  | DriveshftSpd |  | Driveshaft speed | rad/s |
| Axl1 | Axl1Trq |  | Axle 1 torque | $\mathrm{N} \cdot \mathrm{m}$ |
|  | Axl1Spd |  | Axle 1 speed | rad/s |
| Axl2 | Axl2Trq |  | Axle 2 torque | $\mathrm{N} \cdot \mathrm{m}$ |
|  | Axl2Spd |  | Axle 2 speed | rad/s |
| PwrInfo | PwrTrnsfrd | PwrDriveshft | Mechanical power from driveshaft | W |
|  |  | PwrAxl1 | Mechanical power from axle 1 | W |
|  |  | PwrAxl2 | Mechanical power from axle 2 | W |
|  | PwrTrnsfrd | PwrMechLoss | Total power loss | W |
|  |  | PwrDampLoss | Power loss due to damping | W |
|  | PwrStored | PwrStoredShft | Rate change of stored internal energy | W |

DriveshftSpd - Angular speed
scalar
Driveshaft angular speed, $\omega_{d}$, in rad/s.
AxI1Spd - Angular speed
scalar
Axle 1 angular speed, $\omega_{1}$, in rad/s.
AxI2Spd - Angular speed
scalar
Axle 2 angular speed, $\omega_{2}$, in rad/s.

## Parameters

## Block Options

Efficiency factors - Specify configuration
Constant (default)|Driveshaft torque, speed and temperature
To account for the block efficiency, use the Efficiency factors parameter. This table summarizes the block implementation for each setting.

| Setting | Implementation |
| :--- | :--- |
| Constant | Constant efficiency that you can set with the Constant efficiency factor, <br> eta parameter. |
| Driveshaft torque, <br> temperature and <br> speed | Efficiency as a function of base gear input torque, air temperature, and <br> driveshaft speed. Use these parameters to specify the lookup table and <br> breakpoints: <br> - $\quad$ Efficiency lookup table, eta_tbl <br> - $\quad$ Efficiency torque breakpoints, Trq_bpts <br> - $\quad$ Efficiency speed breakpoints, omega_bpts <br> - $\quad$ Efficiency temperature breakpoints, Temp_bpts <br> For the air temperature, you can either: |
|  | - Select Input temperature to create an input port. <br> - Set a Ambient temperature, Tamb parameter value. <br> To select the interpolation method, use the Interpolation method <br> parameter. For more information, see "Interpolation Methods". |

Interpolation method - Method
Flat|Nearest|Linear point-slope|Linear Lagrange|Cubic spline
For more information, see "Interpolation Methods".

## Dependencies

To enable this parameter, set Efficiency factors to Driveshaft torque, speed and temperature.

Input temperature - Create input port
off (default) | on
Select to create input port Temp for the temperature.

## Dependencies

To enable this parameter, set Efficiency factors to Driveshaft torque, speed and temperature.

Crown wheel (ring gear) located - Specify crown wheel connection
To the left of center-line (default)|To the right of center-line
Specify the crown wheel connection to the driveshaft.

Carrier to drive shaft ratio, Ndiff - Ratio
4 (default) | scalar
Carrier-to-driveshaft gear ratio, $N$, dimensionless.
Carrier inertia, Jd - Inertia
. 1 (default) | scalar
Rotational inertia of the crown gear assembly, $J_{d}$, in $\mathrm{kg} \cdot \mathrm{m}^{\wedge} 2$. You can include the driveshaft inertia.
Carrier damping, bd - Damping
1e-3 (default) | scalar
Crown gear linear viscous damping, $b_{d}$, in $\mathrm{N} \cdot \mathrm{m} \cdot \mathrm{s} / \mathrm{rad}$.
Axle 1 inertia, Jw1 - Inertia
. 1 (default) | scalar
Axle 1 rotational inertia, $J_{1}$, in $\mathrm{kg} \cdot \mathrm{m}^{\wedge} 2$.
Axle 1 damping, bw1 - Damping
1e-3 (default) | scalar
Axle 1 linear viscous damping, $b_{1}$, in $\mathrm{N} \cdot \mathrm{m} \cdot \mathrm{s} / \mathrm{rad}$.
Axle 2 inertia, Jw2 - Inertia
. 1 (default) | scalar
Axle 2 rotational inertia, $J_{2}$, in $\mathrm{kg} \cdot \mathrm{m}^{\wedge} 2$.
Axle 2 damping, bw2 - Damping
1e-3 (default) | scalar
Axle 2 linear viscous damping, $b_{2}$, in $\mathrm{N} \cdot \mathrm{m} \cdot \mathrm{s} / \mathrm{rad}$.
Axle 1 initial velocity, omegaw 10 - Angular velocity
0 (default) | scalar
Axle 1 initial velocity, $\omega_{01}$, in rad/s.
Axle 2 initial velocity, omegaw 20 - Angular velocity
0 (default) | scalar
Axle 2 initial velocity, $\omega_{02}$, in rad/s.
Efficiency
Constant efficiency factor, eta - Efficiency
1 (default) | scalar
Constant efficiency, $\eta$.

## Dependencies

To enable this parameter, set Efficiency factors to Constant.

## Efficiency lookup table, eta_tbl - Lookup table

M-by-N-by-L array
Dimensionless array of values for efficiency as a function of:

- M input torques
- $N$ input speed
- L air temperatures

Each value specifies the efficiency for a specific combination of torque, speed, and temperature. The array size must match the dimensions defined by the torque, speed, and temperature breakpoint vectors.

## Dependencies

To enable this parameter, set Efficiency factors to Driveshaft torque, speed and temperature.

Efficiency torque breakpoints, Trq_bpts - Torque breakpoints
[25, 50, 75, 100, 150, 200, 250] (default) | 1-by-M vector
Vector of input torque, breakpoints for efficiency, in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

To enable this parameter, set Efficiency factors to Driveshaft torque, speed and temperature.

Efficiency speed breakpoints, omega_bpts - Speed breakpoints
[52.4 78.5 105131157183209262314419 524] (default)| 1-by-N vector
Vector of speed, breakpoints for efficiency, in rad/s.

## Dependencies

To enable this parameter, set Efficiency factors to Driveshaft torque, speed and temperature.

Efficiency temperature breakpoints, Temp_bpts - Temperature breakpoints
[290 358] (default) | 1-by-L vector
Vector of ambient temperature breakpoints for efficiency, in K.
Dependencies
To enable this parameter, set Efficiency factors to Driveshaft torque, speed and temperature.

Ambient temperature, Tamb - Ambient temperature
297.15 (default) | scalar

Ambient air temperature, $T_{\text {air }}$, in K.
Dependencies
To enable this parameter:

- Set Efficiency factors to Driveshaft torque, speed and temperature.
- Clear Input temperature.


## Version History

Introduced in R2017a

## Extended Capabilities

C/C++ Code Generation
Generate C and C++ code using Simulink ${ }^{\circledR}$ Coder ${ }^{\mathrm{TM}}$.

## See Also

Limited Slip Differential

## Ideal Fixed Gear Transmission

Ideal fixed gear transmission without clutch or synchronization


## Libraries:

Powertrain Blockset / Transmission / Transmission Systems
Vehicle Dynamics Blockset / Powertrain / Transmission

## Description

The Ideal Fixed Gear Transmission implements an idealized fixed-gear transmission without a clutch or synchronization. Use the block to model the overall gear ratio and power loss when you do not need a detailed transmission model, for example, in component-sizing, fuel economy, and emission studies. The block implements a transmission model with minimal parameterization or computational cost.

To specify the block efficiency calculation, for Efficiency factors, select either of these options.

| Setting | Block Implementation |
| :--- | :--- |
| Gear only | Efficiency determined from a 1D lookup table that is a function of <br> the gear. |
| Gear, input torque, input <br> speed, and temperature | Efficiency determined from a 4D lookup table that is a function of:  <br>  - <br>  Gear <br>  Input torque <br>  - <br>  Input speed <br>  Oil temperature |

The block uses this equation to determine the transmission dynamics:

$$
\begin{aligned}
& \dot{\omega_{i}} \frac{J_{N}}{N^{2}}=\eta_{N}\left(\frac{T_{O}}{N}+T_{i}\right)-\frac{\omega_{i}}{N^{2}} b_{N} \\
& \omega_{i}=N \omega_{o}
\end{aligned}
$$

The block filters the gear command signal:

$$
\frac{G}{G_{c m d}}(s)=\frac{1}{\tau_{s} s+1}
$$

## Neutral Gear

When Initial gear number, G_o is equal to 0, the initial gear is neutral. The block uses these parameters to decouple the input flywheel from the downstream gearing.

## - Initial input velocity, omega_o

- Initial neutral input velocity, omegainN_o

The block uses these equations for the neutral gear speed and flywheel.

$$
\begin{aligned}
& \dot{\omega}_{\text {neutral }} \frac{J_{N}}{N^{2}}=\eta_{N} \frac{T_{o}}{N}-\frac{\omega_{\text {neutral }}}{N^{2}} b_{N} \\
& \omega_{\text {neutral }}=N \omega_{o} \\
& \dot{\omega}_{1} J_{F}=\eta_{@ N=0} T_{i}-b_{@ N=0} \omega_{i} \\
& J_{F}=J_{@ N}=1-J_{@ N}=0
\end{aligned}
$$

## Power Accounting

For the power accounting, the block implements these equations.

| Bus Signal |  |  | Description | Varia | Equations |
| :---: | :---: | :---: | :---: | :---: | :---: |
| PwrIn fo | PwrTrnsfrd - Power transferred between blocks <br> - Positive signals indicate flow into block <br> - Negative signals indicate flow out of block | PwrEng | Engine power | $P_{\text {eng }}$ | $\omega_{i} T_{i}$ |
|  |  | PwrDif frntl | Differential power | $P_{\text {diff }}$ | $\omega_{o} T_{o}$ |
|  | PwrNotTrnsfrd - Power crossing the block boundary, but not transferred <br> - Positive signals indicate an input <br> - Negative signals indicate a loss | PwrEff Loss | Mechanical power loss | $P_{\text {effloss }}$ | $\omega_{o} T_{o}\left(\eta_{N}-1\right)$ |
|  |  | PwrDam ploss | Mechanical damping loss | $P_{\text {dampl }}$ oss | For $G=0: \quad-\frac{b_{N} \omega_{i}^{2}}{\left\|N^{2}\right\|}$ <br> For $\mathrm{G} \neq 0:-b_{N} \omega_{i}^{2}-\frac{b_{N} \omega_{\text {neutral }}^{2}}{\left\|N^{2}\right\|}$ |
|  | PwrStored - Stored energy rate of change <br> - Positive signals indicate an increase <br> - Negative signals indicate a decrease | PwrSto redTra ns | Rate change in rotational kinetic energy | $P_{\text {str }}$ | For $\mathrm{G}=0: \quad \frac{J_{N}}{N^{2}} \dot{\omega}_{i} \omega_{i}$ <br> For $\mathrm{G} \neq 0: \quad J_{F} \dot{\omega}_{i} \omega_{i}+\frac{J_{N}}{N^{2}} \dot{\omega}_{\text {neutral }} \omega_{\text {neutr }}$ |

The equations use these variables.

| $b_{N}$ | Engaged gear viscous damping |
| :--- | :--- |
| $J_{N}$ | Engaged gear rotational inertia |
| $J_{F}$ | Flywheel rotational inertia |
| $\eta_{N}$ | Engaged gear efficiency |
| $G$ | Engaged gear number |
| $G_{c m d}$ | Gear number to engage |
| $N$ | Engaged gear ratio |

$T_{i} \quad$ Applied input torque, typically from the engine crankshaft or dual mass flywheel
$T_{o} \quad$ Applied load torque, typically from the differential or drive shaft
$\omega_{o} \quad$ Initial input drive shaft rotational velocity
$\omega_{i}, \omega_{i} \quad$ Applied drive shaft angular speed and acceleration
$\omega_{N o} \quad$ Initial neutral gear input rotational velocity
$\omega_{\text {neutral }} \quad$ Neutral gear drive shaft rotational velocity
$\tau_{s} \quad$ Shift time constant

## Ports

## Inputs

Gear - Gear number to engage
scalar
Integer value of gear number to engage, $G_{c m d}$.
EngTrq - Applied input torque
scalar
Applied input torque, $T_{i}$, typically from the engine crankshaft or dual mass flywheel damper, in $\mathrm{N} \cdot \mathrm{m}$.
DiffTrq - Applied load torque
scalar
Applied load torque, $T_{o}$, typically from the differential, in $\mathrm{N} \cdot \mathrm{m}$.
Temp - Oil temperature
scalar
Oil temperature, in K. To determine the efficiency, the block uses a 4D lookup table that is a function of:

- Gear
- Input torque
- Input speed
- Oil temperature


## Dependencies

To enable this port, set Efficiency factors to Gear, input torque, input speed, and temperature.

## Output

Info - Bus signal
bus
Bus signal containing these block calculations.

| Signal |  |  | Description | Variabl | Units |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Eng | EngTrq |  | Applied input torque, typically from the engine crankshaft or dual mass flywheel damper | $T_{i}$ | $\mathrm{N} \cdot \mathrm{m}$ |
|  | EngSpd |  | Applied drive shaft angular speed input | $\omega_{i}$ | rad/s |
| Diff | DiffTrq |  | Applied load torque, typically from the differential | $T_{o}$ | $\mathrm{N} \cdot \mathrm{m}$ |
|  | DiffSpd |  | Drive shaft angular speed output | $\omega_{0}$ | rad/s |
| Trans | TransSpdRatio |  | Input to output speed ratio at time t | $\Phi(t)$ | N/A |
|  | TransEta |  | Ratio of output power to input power | $\eta_{N}$ | N/A |
|  | TransGearCmd |  | Commanded gear | $N_{\text {cmd }}$ | N/A |
|  | TransGear |  | Engaged gear | $N$ | N/A |
| PwrInfo | PwrTrnsfrd | PwrEng | Engine power | $P_{\text {eng }}$ | W |
|  |  | PwrDiffrntl | Differential power | $P_{\text {diff }}$ | W |
|  | PwrNotTrnsfrd | PwrEffLoss | Mechanical power loss | $P_{\text {effloss }}$ | W |
|  |  | PwrDampLoss | Mechanical damping loss | $P_{\text {damploss }}$ | W |
|  | PwrStored | PwrStoredTrans | Rate change in rotational kinetic energy | $P_{\text {str }}$ | W |

EngSpd - Angular speed
scalar
Applied drive shaft angular speed input, $\omega_{i}$, in rad/s.

## DiffSpd - Angular speed

scalar
Drive shaft angular speed output, $\omega_{o}$, in rad/s.

## Parameters

Efficiency factors - Specify efficiency calculation
Gear only (default)|Gear, input torque, input speed, and temperature
To specify the block efficiency calculation, for Efficiency factors, select either of these options.

| Setting | Block Implementation |
| :--- | :--- |
| Gear only | Efficiency determined from a 1D lookup table that is a function of <br> the gear. |
| Gear, input torque, input <br> speed, and temperature | Efficiency determined from a 4D lookup table that is a function of: <br>  <br> - <br>  <br>  <br>  <br>  <br>  <br>  <br> - <br> - <br> - Input torque |

## Dependencies

| Setting Parameter To | Enables |
| :--- | :--- |
| Gear only | Efficiency vector, eta |
| Gear, input torque, input <br> speed, and temperature | Efficiency torque breakpoints, Trq_bpts |
|  | Efficiency speed breakpoints, omega_bpts |
|  | Efficiency temperature breakpoints, Temp_bpts |
|  | Efficiency lookup table, eta_tbl |

Gear property interpolation method - Interpolation
Nearest (default)|Linear|Flat|Cubic spline
Method that the block uses to switch the gear ratio during gear shifting.

## Transmission

Gear number vector, G - Specify number of transmission speeds

```
[-1,0,1,2,3,4,5] (default)| vector
```

Vector of integer gear commands used to specify the number of transmission speeds. Neutral gear is 0 . For example, you can set these parameter values.

| To Specify | Set Gear number, G To |
| :--- | :--- |
| Four transmission speeds, including <br> neutral | $[0,1,2,3,4]$ |
| Three transmission speeds, including <br> neutral and reverse | $[-1,0,1,2,3]$ |
| Five transmission speeds, including <br> neutral and reverse | $[-1,0,1,2,3,4,5]$ |

Vector dimensions for the Gear number vector, Gear ratio vector, Inertia vector, Damping vector, and Efficiency vector parameters must be equal.

## Efficiency torque breakpoints, Trq_bpts - Breakpoints

[25,50, 75, 100, 150, 200, 250] (default) | vector
Torque breakpoints for efficiency table.

## Dependencies

To enable this parameter, set Efficiency factors to Gear, input torque, input speed, and temperature.

Efficiency speed breakpoints, omega_bpts - Breakpoints
[52.4 78.5 105131157183209262314419 524] (default)|vector
Speed breakpoints for efficiency table.

## Dependencies

To enable this parameter, set Efficiency factors to Gear, input torque, input speed, and temperature.

Efficiency temperature breakpoints, Temp_bpts - Breakpoints
[313 358] (default)|vector
Temperature breakpoints for efficiency table.

## Dependencies

To enable this parameter, set Efficiency factors to Gear, input torque, input speed, and temperature.

Gear ratio vector, $\mathbf{N}$ - Ratio of input speed to output speed
[-4.47,4.47,4.47,2.47,1.47,1, 0.8] (default) | vector
Vector of gear ratios (that is, input speed to output speed) with indices corresponding to the ratios specified in Gear number, G. For neutral, set the gear ratio to 1. For example, you can set these parameter values.

| To Specify Gear Ratios For | Set Gear number, G To | Set Gear ratio, N To |
| :--- | :--- | :--- |
| Four transmission speeds, <br> including neutral | $[0,1,2,3,4]$ | $[1,4.47,2.47,1.47,1]$ |
| Five transmission speeds, <br> including neutral and reverse | $[-1,0,1,2,3,4,5]$ | $[-4.47,1,4.47,2.47,1.47,1,0.8]$ |

Vector dimensions for the Gear number vector, Gear ratio vector, Inertia vector, Damping vector, and Efficiency vector parameters must be equal.

Inertia vector, Jout - Gear rotational inertia
[0.128 0.01 0.128 0.1 0.062 0.028 0.01] (default)|vector
Vector of gear rotational inertias, $J_{N}$, with indices corresponding to the inertias specified in Gear number, $\mathbf{G}$, in $\mathrm{kg}^{*} \mathrm{~m}^{\wedge} 2$. For example, you can set these parameter values.

| To Specify Inertia For | Set Gear number, G To | Set Inertia, J To |
| :--- | :--- | :--- |
| Four gears, including neutral | $[0,1,2,3,4]$ | $[0.01,2.28,2.04,0.32,0.028]$ |
| Inertia for five gears, including | $[-1,0,1,2,3,4,5]$ | $[2.28,0.01,2.28$, |
| reverse and neutral |  | $2.04,0.32,0.028,0.01]$ |

Vector dimensions for the Gear number vector, Gear ratio vector, Inertia vector, Damping vector, and Efficiency vector parameters must be equal.

Damping vector, bout - Gear viscous damping coefficient
[.003 . 001 . 003 . 0025 . 002 . 001 .001] (default) |vector
Vector of gear viscous damping coefficients, $b_{N}$, with indices corresponding to the coefficients specified in Gear number, G, in $\mathrm{N} \cdot \mathrm{m} \cdot \mathrm{s} / \mathrm{rad}$. For example, you can set these parameter values.

| To Specify Damping For | Set Gear number, G To | Set Damping, b To |
| :--- | :--- | :--- |
| Four gears, including neutral | $[0,1,2,3,4]$ | $[0.001,0.003$, <br> $0.0025,0.002,0.001]$ |
| Five gears, including reverse <br> and neutral | $[-1,0,1,2,3,4,5]$ | $[0.003,0.001,0.003,0.0025$, |
|  |  | $0.002,0.001,0.001]$ |

Vector dimensions for the Gear number vector, Gear ratio vector, Inertia vector, Damping vector, and Efficiency vector parameters must be equal.

Efficiency vector, eta - Gear efficiency
[0.9,0.9,0.9, 0.9,0.9,0.95,0.95] (default) | vector
Vector of gear mechanical efficiency, $\eta_{N}$, with indices corresponding to the efficiencies specified in Gear number, G. For example, you can set these parameter values.

| To Specify Efficiency For | Set Gear number, G To | Set Efficiency, eta To |
| :--- | :--- | :--- |
| Four gears, including neutral | $[0,1,2,3,4]$ | $[0.9,0.9,0.9,0.9,0.95]$ |
| Five gears, including reverse | $[-1,0,1,2,3,4,5]$ | $[0.9,0.9,0.9$, |
| and neutral |  | $0.9,0.9,0.95,0.95]$ |

Vector dimensions for the Gear number vector, Gear ratio vector, Inertia vector, Damping vector, and Efficiency vector parameters must be equal.

## Dependencies

To enable this parameter, set Efficiency factors to Gear only.
Efficiency lookup table, eta_tbl - Gear efficiency
array
Table of gear mechanical efficiency, $\eta_{N}$ as a function of gear, input torque, input speed, and temperature.

## Dependencies

To enable this parameter, set Efficiency factors to Gear, input torque, input speed, and temperature.

Initial gear number, G_o - Gear
0 (default) | scalar
Initial gear number, $G_{o}$, dimensionless.
Initial output velocity, omega_o - Output speed
0 (default) | scalar
Transmission initial output rotational velocity, $\omega_{0}$, in rad/s.
Initial neutral input velocity, omegainN_o - Neutral gear input speed 0 (default) | scalar

Initial neutral gear input rotational velocity, $\omega_{N o}$, in rad/s.
Shift time constant, tau_s - Time
. 01 (default) | scalar
Shift time constant, $\tau_{s}$, in $s$.

## Version History

Introduced in R2017a

## Extended Capabilities

$\mathbf{C} / \mathbf{C}++$ Code Generation
Generate C and $\mathrm{C}++$ code using Simulink ${ }^{\circledR}$ Coder $^{\mathrm{TM}}$.

## See Also

Limited Slip Differential | Open Differential

## Transfer Case

Differential as a planetary bevel gear


## Libraries:

Powertrain Blockset / Drivetrain / Final Drive Unit
Vehicle Dynamics Blockset / Powertrain / Drivetrain / Final Drive Unit

## Description

The Transfer Case block implements a differential as a planetary bevel gear train. The block matches the driveshaft bevel gear to the crown (ring) bevel gear. You can specify:

- Carrier-to-driveshaft ratio
- Crown wheel location
- Viscous and damping coefficients for the axles and carrier

Use the Transfer Case block to:

- Dynamically couple the post-transmission driveshaft to the wheel axles or universal joints
- Model simplified or older drivetrains when optimal traction control does not require passive or active torque vectoring
- Model mechanical power splitting in generic gearbox and drive line scenarios

The block is suitable for use in hardware-in-the-loop (HIL) and optimization workflows. All the parameters are tunable.

## Efficiency

To account for the block efficiency, use the Efficiency factors parameter. This table summarizes the block implementation for each setting.

| Setting | Implementation |
| :--- | :--- |
| Constant | Constant efficiency that you can set with the Constant efficiency factor, <br> eta parameter. |


| Setting | Implementation |
| :---: | :---: |
| Driveshaft torque, temperature and speed | Efficiency as a function of base gear input torque, air temperature, and driveshaft speed. Use these parameters to specify the lookup table and breakpoints: <br> - Efficiency lookup table, eta_tbl <br> - Efficiency torque breakpoints, Trq_bpts <br> - Efficiency speed breakpoints, omega_bpts <br> - Efficiency temperature breakpoints, Temp_bpts <br> For the air temperature, you can either: <br> - Select Input temperature to create an input port. <br> - Set a Ambient temperature, Tamb parameter value. <br> To select the interpolation method, use the Interpolation method parameter. For more information, see "Interpolation Methods". |

## Power Accounting

For the power accounting, the block implements these equations.

| Bus Signal |  |  | Description | Equations |
| :---: | :---: | :---: | :---: | :---: |
| PwrInfo | PwrTrnsfrd - Power transferred between blocks <br> - Positive signals indicate flow into block <br> - Negative signals indicate flow out of block | PwrDriveshft | Mechanical power from driveshaft | $\eta T_{d} \omega_{d}$ |
|  |  | PwrAxl1 | Mechanical power from axle 1 | $\eta T_{1} \omega_{1}$ |
|  |  | PwrAxl2 | Mechanical power from axle 2 | $\eta T_{2} \omega_{2}$ |
|  | PwrNotTrnsfrd - Power crossing the block boundary, but not transferred <br> - Positive signals indicate an input <br> - Negative signals indicate a loss | PwrMechLoss | Total power loss | $\begin{aligned} & \dot{W}_{\text {loss }}=-\left(P_{t}+P_{d}\right)+ \\ & P_{t}=\eta T_{d} \omega_{d}+\eta T_{1} \omega_{1}+\eta T \end{aligned}$ |
|  |  | PwrDampLoss | Power loss due to damping | $\begin{aligned} & P_{d}=-\left(b_{1}\left\|\omega_{1}\right\|\right. \\ & \left.+b_{2}\left\|\omega_{2}\right\|+b_{d}\left\|\omega_{d}\right\|\right) \end{aligned}$ |
|  | PwrStored - Stored energy rate of change <br> - Positive signals indicate an increase <br> - Negative signals indicate a decrease | PwrStoredShft | Rate change of stored internal energy | $\begin{aligned} & P_{s}=-\left(\omega_{1} \dot{\omega}_{1} J_{1}\right. \\ & \left.+\omega_{2} \dot{\omega}_{2} J_{2}+\omega_{d} \dot{\omega}_{d} J_{d}\right) \end{aligned}$ |

## Dynamics

The Transfer Case block implements these differential equations to represent the mechanical dynamic response for the crown gear, front axle, and rear axle.

| Mechanical <br> Dynamic <br> Response | Differential Equation |
| :--- | :--- |
| Crown Gear | $\dot{\omega}_{d} J_{d}=\eta T_{d}-\omega_{d} b_{d}-T_{i}$ |
| Front Axle | $\dot{\omega}_{1} J_{1}=\eta T_{1}-\omega_{1} b_{1}-T_{i 1}$ |
| Rear Axle | $\dot{\omega}_{2} J_{2}=\eta T_{2}-\omega_{2} b_{2}-T_{i 2}$ |

The equations use these variables.

| $N$ | Carrier-to-driveshaft gear ratio |
| :--- | :--- |
| $J_{d}$ | Rotational inertia of the crown gear assembly |
| $b_{d}$ | Crown gear linear viscous damping |
| $\omega_{d}$ | Driveshaft angular speed |
| $\eta$ | Differential efficiency |
| $J_{1}$ | Axle 1 rotational inertia |
| $b_{1}$ | Axle 1 linear viscous damping |
| $\omega_{1}$ | Axle 1 speed |
| $J_{2}$ | Axle 2 rotational inertia |
| $b_{2}$ | Axle 2 linear viscous damping |
| $\omega_{2}$ | Axle 2 angular speed |
| $T_{d}$ | Driveshaft torque |
| $T_{1}$ | Axle 1 torque |
| $T_{2}$ | Axle 2 torque |
| $T_{i}$ | Driveshaft internal resistance torque |
| $T_{i 1}$ | Axle 1 internal resistance torque |
| $T_{i 2}$ | Axle 2 internal resistance torque |

## Ports

Inputs
DriveshftTrq - Torque
scalar
Applied input torque, typically from the engine crankshaft, in $N \cdot m$.
AxI1Trq - Torque
scalar
Axle 1 torque, $T_{1}$, in $\mathrm{N} \cdot \mathrm{m}$.

## AxI2Trq - Torque

scalar
Axle 2 torque, $T_{2}$, in $N \cdot \mathrm{~m}$.
Temp - Temperature
scalar

Temperature, in K.

## Dependencies

To enable this port:

- Set Efficiency factors to Driveshaft torque, speed and temperature.
- Select Input temperature.

TrqSplitRatioConstant - Front axle torque split ratio
scalar

Front axle torque split ratio.

## Dependencies

To enable this port, select Input front axle torque split ratio, TrqSplitRatio.
SpdLockConstant - Axle speed lock
scalar
Axle speed lock.

## Dependencies

To enable this port, select Input axle speed lock, SpdLock.
Output
Info - Bus signal
bus
Bus signal containing these block calculations.

| Signal |  | Description | Units |
| :--- | :--- | :--- | :--- |
| Driveshft | DriveshftTrq | Driveshaft torque | $\mathrm{N} \cdot \mathrm{m}$ |
|  | DriveshftSpd | Driveshaft speed | $\mathrm{rad} / \mathrm{s}$ |
| Axl1 | Axl1Trq | Axle 1 torque | $\mathrm{N} \cdot \mathrm{m}$ |
|  | Axl1Spd | Axle 1 speed | $\mathrm{rad} / \mathrm{s}$ |
| Axl2 | Axl2Trq | Axle 2 torque | $\mathrm{N} \cdot \mathrm{m}$ |
|  | Axl2Spd | Axle 2 speed | rad/s |
| PwrInfo | PwrTrnsfrd | PwrDriveshft | Mechanical power from <br> driveshaft |


| Signal |  | PwrAxl1 | Description | Units |
| :--- | :--- | :--- | :--- | :--- |
|  |  | PwrAxl2 | Mechanical power from <br> axle 1 | W |
|  |  | PwrTrnsfrd | Mechanical power from <br> axle 2 | W |
|  |  | PwrMechLoss | Total power loss | W |
|  | PwrDampLoss | Power loss due to <br> damping | W |  |
|  | PwrStored | PwrStoredShft | Rate change of stored <br> internal energy | W |

DriveshftSpd - Angular speed

## scalar

Driveshaft angular speed, $\omega_{d}$, in rad/s.
AxI1Spd - Angular speed
scalar
Axle 1 angular speed, $\omega_{1}$, in rad/s.
AxI2Spd - Angular speed
scalar
Axle 2 angular speed, $\omega_{2}$, in rad/s.

## Parameters

## Block Options

Efficiency factors - Specify configuration
Constant (default)|Driveshaft torque, speed and temperature
To account for the block efficiency, use the Efficiency factors parameter. This table summarizes the block implementation for each setting.

| Setting | Implementation |
| :--- | :--- |
| Constant | Constant efficiency that you can set with the Constant efficiency factor, <br> eta parameter. |


| Setting | Implementation |
| :---: | :---: |
| Driveshaft torque, temperature and speed | Efficiency as a function of base gear input torque, air temperature, and driveshaft speed. Use these parameters to specify the lookup table and breakpoints: <br> - Efficiency lookup table, eta_tbl <br> - Efficiency torque breakpoints, Trq_bpts <br> - Efficiency speed breakpoints, omega_bpts <br> - Efficiency temperature breakpoints, Temp_bpts <br> For the air temperature, you can either: <br> - Select Input temperature to create an input port. <br> - Set a Ambient temperature, Tamb parameter value. <br> To select the interpolation method, use the Interpolation method parameter. For more information, see "Interpolation Methods". |

Interpolation method - Method
Flat | Nearest | Linear point-slope | Linear Lagrange | Cubic spline
For more information, see "Interpolation Methods".

## Dependencies

To enable this parameter, set Efficiency factors to Driveshaft torque, speed and temperature.

Input temperature - Create input port
off (default) | on
Select to create input port Temp for the temperature.

## Dependencies

To enable this parameter, set Efficiency factors to Driveshaft torque, speed and temperature.

Input front axle torque split ratio, TrqSplitRatio - Create input port
off (default) | on
Select to create input port TrqSplitRatioConstant for the front axle torque split ratio.
Input axle speed lock, SpdLock - Create input port
off (default) | on
Select to create input port SpdLockConstant for the axle speed lock.
Crown wheel (ring gear) located - Specify crown wheel connection
To the left of center-line (default)|To the right of center-line
Specify the crown wheel connection to the driveshaft.

## Carrier to drive shaft ratio, Ndiff - Ratio

4 (default) | scalar

Carrier-to-driveshaft gear ratio, $N$, dimensionless.

## Carrier inertia, Jd - Inertia

. 1 (default) | scalar
Rotational inertia of the crown gear assembly, $J_{d}$, in $\mathrm{kg} \cdot \mathrm{m}^{\wedge} 2$. You can include the driveshaft inertia.
Carrier damping, bd - Damping
le-3 (default) | scalar
Crown gear linear viscous damping, $b_{d}$, in $\mathrm{N} \cdot \mathrm{m} \cdot \mathrm{s} / \mathrm{rad}$.
Axle 1 inertia, Jw1 - Inertia
. 1 (default) | scalar
Axle 1 rotational inertia, $J_{1}$, in $\mathrm{kg} \cdot \mathrm{m}^{\wedge} 2$.
Axle 1 damping, bw1 - Damping
1e-3 (default) | scalar
Axle 1 linear viscous damping, $b_{1}$, in $\mathrm{N} \cdot \mathrm{m} \cdot \mathrm{s} / \mathrm{rad}$.
Axle 2 inertia, Jw2 - Inertia
. 1 (default) | scalar
Axle 2 rotational inertia, $J_{2}$, in $\mathrm{kg} \cdot \mathrm{m}^{\wedge} 2$.
Axle 2 damping, bw2 - Damping
le-3 (default) |scalar
Axle 2 linear viscous damping, $b_{2}$, in $\mathrm{N} \cdot \mathrm{m} \cdot \mathrm{s} / \mathrm{rad}$.
Axle 1 initial velocity, omegaw 10 - Angular velocity
0 (default) | scalar
Axle 1 initial velocity, $\omega_{01}$, in rad/s.
Axle 2 initial velocity, omegaw 20 - Angular velocity
0 (default) | scalar
Axle 2 initial velocity, $\omega_{02}$, in rad/s.
Efficiency
Constant efficiency factor, eta - Efficiency
1 (default) | scalar
Constant efficiency, $\eta$.

## Dependencies

To enable this parameter, set Efficiency factors to Constant.
Efficiency lookup table, eta_tbl - Lookup table
M-by-N-by-L array
Dimensionless array of values for efficiency as a function of:

- M input torques
- N input speed
- L air temperatures

Each value specifies the efficiency for a specific combination of torque, speed, and temperature. The array size must match the dimensions defined by the torque, speed, and temperature breakpoint vectors.

## Dependencies

To enable this parameter, set Efficiency factors to Driveshaft torque, speed and temperature.

Efficiency torque breakpoints, Trq_bpts - Torque breakpoints
[25, 50, 75, 100, 150, 200, 250] (default)| 1-by-M vector
Vector of input torque, breakpoints for efficiency, in $N \cdot m$.

## Dependencies

To enable this parameter, set Efficiency factors to Driveshaft torque, speed and temperature.

Efficiency speed breakpoints, omega_bpts - Speed breakpoints
$[52.478 .5105131157183209262314419$ 524] (default)| 1-by-N vector
Vector of speed, breakpoints for efficiency, in rad/s.

## Dependencies

To enable this parameter, set Efficiency factors to Driveshaft torque, speed and temperature.

Efficiency temperature breakpoints, Temp_bpts - Temperature breakpoints
[290 358] (default) | 1-by-L vector
Vector of ambient temperature breakpoints for efficiency, in K.

## Dependencies

To enable this parameter, set Efficiency factors to Driveshaft torque, speed and temperature.

Ambient temperature, Tamb - Ambient temperature
297.15 (default) | scalar

Ambient air temperature, $T_{\text {air }}$, in K.

## Dependencies

To enable this parameter:

- Set Efficiency factors to Driveshaft torque, speed and temperature.
- Clear Input temperature.

Front axle torque split ratio, TrqSplitRatio - Front axle torque split ratio
0.5 (default) | scalar

Front axle torque split ratio.

## Dependencies

To enable this parameter, clear Input front axle torque split ratio, TrqSplitRatio.
Axle speed lock, SpdLock - Axle speed lock
0 (default) | scalar
Axle speed lock. Set this value to 0 to make the front and rear axle rotational speed not fixed. Set this value to 1 to make the front and rear axle rotational speed fixed.

Dependencies
To enable this parameter, clear Input axle speed lock, SpdLock.

## Version History

Introduced in R2021b

## Extended Capabilities

C/C++ Code Generation
Generate C and C++ code using Simulink ${ }^{\circledR}$ Coder ${ }^{\mathrm{TM}}$.

## See Also

Limited Slip Differential

## Wheel and Tire Blocks

## Longitudinal Wheel

Longitudinal wheel with disc, drum, or mapped brake


## Libraries:

Powertrain Blockset / Drivetrain / Wheels
Vehicle Dynamics Blockset / Wheels and Tires

## Description

The Longitudinal Wheel block implements the longitudinal behavior of an ideal wheel. You can specify the longitudinal force and rolling resistance calculation method, and brake type. Use the block in driveline and longitudinal vehicle simulations where low frequency tire-road and braking forces are required to determine vehicle acceleration, braking, and wheel-rolling resistance. For example, you can use the block to determine the torque and power requirements for a specified drive cycle or braking event. The block is not suitable for applications that require combined lateral slip.

There are four types of Longitudinal Wheel blocks. Each block implements a different brake type.

| Block Name | Brake Type Setting | Brake Implementation |
| :--- | :--- | :--- |
| Longitudinal Wheel - No <br> Brake | None | None |
| Longitudinal Wheel - Disc <br> Brake | Disc | Brake that converts the brake cylinder <br> pressure into a braking force. |
| Longitudinal Wheel - Drum <br> Brake | Drum | Simplex drum brake that converts the <br> applied force and brake geometry into a <br> net braking torque. |
| Longitudinal Wheel - Mapped <br> Brake | Mapped | Lookup table that is a function of the <br> wheel speed and applied brake pressure. |

The block models longitudinal force as a function of wheel slip relative to the road surface. To calculate the longitudinal force, specify one of these Longitudinal Force parameters.

| Setting | Block Implementation |
| :--- | :--- |
| Magic Formula constant value | Magic Formula with constant coefficient for stiffness, shape, <br> peak, and curvature. |
| Magic Formula pure <br> longitudinal slip | Magic Formula with load-dependent coefficients that <br> implement equations 4.E9 through 4.E18 in Tire and Vehicle <br> Dynamics. |
| Mapped force | Lookup table that is a function of the normal force and wheel <br> slip ratio. |

To calculate the rolling resistance torque, specify one of these Rolling Resistance parameters.

| Setting | Block Implementation |
| :--- | :--- |
| None | None |
| Pressure and velocity | Method in Stepwise Coastdown Methodology for Measuring <br> Tire Rolling Resistance. The rolling resistance is a function of <br> tire pressure, normal force, and velocity. |
| ISO 28580 | Method specified in ISO 28580:2018, Passenger car, truck <br> and bus tyre rolling resistance measurement method - <br> Single point test and correlation of measurement results. |
| Magic Formula | Magic formula equations from 4.E70 in Tire and Vehicle <br> Dynamics. The magic formula is an empirical equation based <br> on fitting coefficients. |
| Mapped torque | Lookup table that is a function of the normal force and spin <br> axis longitudinal velocity. |

To calculate vertical motion, specify one of these Vertical Motion parameters.

| Setting | Block Implementation |
| :--- | :--- |
| None | Block passes the applied chassis forces directly through to <br> the rolling resistance and longitudinal force calculations. |
| Mapped stiffness and damping | Vertical motion depends on wheel stiffness and damping. <br> Stiffness is a function of tire sidewall displacement and <br> pressure. Damping is a function of tire sidewall velocity and <br> pressure. |

## Rotational Wheel Dynamics

The block calculates the inertial response of the wheel subject to:

- Axle losses
- Brake and drive torque
- Tire rolling resistance
- Ground contact through the tire-road interface

The input torque is the summation of the applied axle torque, braking torque, and moment arising from the combined tire torque.

$$
T_{i}=T_{a}-T_{b}+T_{d}
$$

For the moment arising from the combined tire torque, the block implements tractive wheel forces and rolling resistance with first order dynamics. The rolling resistance has a time constant parameterized in terms of a relaxation length.

$$
T_{d}(s)=\frac{1}{\frac{L_{e}}{|\omega| R_{e}} s+1}+\left(F_{\chi} R_{e}+M_{y}\right)
$$

To calculate the rolling resistance torque, you can specify one of these Rolling Resistance parameters.

| Setting | Block Implementation |
| :--- | :--- |
| None | Block sets rolling resistance, $M_{y}$, to zero. |
| Pressure and <br> velocity | Block uses the method in SAE Stepwise Coastdown Methodology for Measuring <br> Tire Rolling Resistance. The rolling resistance is a function of tire pressure, <br> normal force, and velocity, specifically, <br>  <br> $M_{y}=R_{e}\left\{a+b\left\|V_{x}\right\|+c V_{x}{ }^{2}\right\}\left\{F_{z} \beta p_{i} \alpha\right\} \tanh \left(4 V_{x}\right)$ |
| IS0 28580 | Block uses the method specified in ISO 28580:2018, Passenger car, truck and <br> bus tyre rolling resistance measurement method - Single point test and <br> correlation of measurement results. The method accounts for normal load, <br> parasitic loss, and thermal corrections from test conditions, specifically, |
| $\quad M_{y}=R_{e}\left(\frac{F_{z} C_{r}}{1+K_{t}\left(T_{a m b}-T_{\text {meas }}\right)}-F_{p l}\right)$ tanh( $\omega$ ) |  |

If the brakes are enabled, the block determines the braking locked or unlocked condition based on an idealized dry clutch friction model. Based on the lock-up condition, the block implements these friction and dynamic models.

| If | Lock-Up <br> Condition | Friction Model | Dynamic Model |
| :--- | :--- | :--- | :--- |
| $\omega \neq 0$ | Unlocked | $T_{f}=T_{k}$, |  |
| or |  |  |  |
| $T_{S}<\left\|T_{i}+T_{f}-\omega b\right\|$ |  | $T_{k}=F_{c} R_{e f f} \mu_{k} \tanh \left[4\left(-\omega_{d}\right)\right]$ <br> $T_{S}=F_{c} R_{e f f} \mu_{S}$ <br>  <br> $R_{e f f}=\frac{2\left(R_{0} 3-R_{i} 3\right)}{3\left(R_{o} 2-R_{i} 2\right)}$ |  |
| $\omega=0$ <br> and <br> $T_{S} \geq\left\|T_{i}+T_{f}-\omega b\right\|$ | Locked | $T_{f}=T_{S}$ |  |

The equations use these variables.

| $\omega$ | Wheel angular velocity |
| :--- | :--- |
| $a$ | Velocity-independent force component |
| $b$ | Linear velocity force component |
| $c$ | Quadratic velocity force component |


| $L_{e}$ | Tire relaxation length |
| :--- | :--- |
| $J$ | Moment of inertia |
| $M_{y}$ | Rolling resistance torque |
| $T_{a}$ | Applied axle torque |
| $T_{b}$ | Braking torque |
| $T_{d}$ | Combined tire torque |
| $T_{f}$ | Frictional torque |
| $T_{i}$ | Net input torque |
| $T_{k}$ | Kinetic frictional torque |
| $T_{o}$ | Net output torque |
| $T_{s}$ | Static frictional torque |
| $F_{c}$ | Applied clutch force |
| $F_{x}$ | Longitudinal force developed by the tire road interface due to slip |
| $R_{e f f}$ | Effective clutch radius |
| $R_{o}$ | Annular disk outer radius |
| $R_{i}$ | Annular disk inner radius |
| $R_{e}$ | Effective tire radius while under load and for a given pressure |
| $V_{x}$ | Longitudinal axle velocity |
| $F_{z}$ | Vehicle normal force |
| $C_{r}$ | Rolling resistance constant |
| $T_{a m b}$ | Ambient temperature |
| $T_{m e a s}$ | Measured temperature for rolling resistance constant |
| $F_{p l}$ | Parasitic force loss |
| $K_{t}$ | Thermal correction factor |
| $\alpha$ | Tire pressure exponent |
| $\beta$ | Normal force exponent |
| $p_{i}$ | Tire pressure |
| $\mu_{s}$ | Coefficient of static friction |
| $\mu_{k}$ | Coefficient of kinetic friction |
| Brakes |  |
| Disc |  |
|  |  |

If you specify the Brake Type parameter as Disc, the block implements a disc brake. This figure shows the side and front views of a disc brake.


A disc brake converts brake cylinder pressure from the brake cylinder into force. The disc brake applies the force at the brake pad mean radius.

The block uses these equations to calculate brake torque for the disc brake.

$$
\begin{aligned}
& T= \begin{cases}\frac{\mu P_{\pi B} B_{a} 2 R_{m} N_{\text {pads }}}{4} & \text { when } N \neq 0 \\
\frac{\mu_{\text {static } P \pi B_{a} 2 R_{m} N_{\text {pads }}}^{4}}{2} & \text { when } N=0\end{cases} \\
& R m=\frac{R o+R i}{2}
\end{aligned}
$$

The equations use these variables.

| Variable | Value |
| :--- | :--- |
| $T$ | Brake torque |
| $P$ | Applied brake pressure |
| $N$ | Wheel speed |
| $N_{\text {pads }}$ | Number of brake pads in disc brake assembly |
| $\mu_{\text {static }}$ | Disc pad-rotor coefficient of static friction |
| $\mu$ | Disc pad-rotor coefficient of kinetic friction |
| $B_{a}$ | Brake actuator bore diameter |
| $R_{m}$ | Mean radius of brake pad force application on brake rotor |

Variable Value
$R_{o} \quad$ Outer radius of brake pad
$R_{i} \quad$ Inner radius of brake pad

## Drum

If you specify the Brake Type parameter as Drum, the block implements a static (steady-state) simplex drum brake. A simplex drum brake consists of a single two-sided hydraulic actuator and two brake shoes. The brake shoes do not share a common hinge pin.

The simplex drum brake model uses the applied force and brake geometry to calculate a net torque for each brake shoe. The drum model assumes that the actuators and shoe geometry are symmetrical for both sides, allowing a single set of geometry and friction parameters to be used for both shoes.

The block implements equations that are derived from these equations in Fundamentals of Machine Elements.

$$
\begin{aligned}
& T_{\text {rshoe }}=\left(\frac{\pi \mu c r\left(\cos \theta_{2}-\cos \theta_{1}\right) B_{a} 2}{2 \mu\left(2 r\left(\cos \theta_{2}-\cos \theta_{1}\right)+a\left(\cos ^{2} \theta_{2}-\cos ^{2} \theta_{1}\right)\right)+\operatorname{ar}\left(2 \theta_{1}-2 \theta_{2}+\sin 2 \theta_{2}-\sin 2 \theta_{1}\right)}\right) P \\
& T_{\text {lshoe }}=\left(\frac{\pi \mu c r\left(\cos \theta_{2}-\cos \theta_{1}\right) B_{a} 2}{-2 \mu\left(2 r\left(\cos \theta_{2}-\cos \theta_{1}\right)+a\left(\cos ^{2} \theta_{2}-\cos ^{2} \theta_{1}\right)\right)+\operatorname{ar}\left(2 \theta_{1}-2 \theta_{2}+\sin 2 \theta_{2}-\sin 2 \theta_{1}\right)}\right) P \\
& T= \begin{cases}T_{\text {rshoe }}+T_{\text {lshoe }} & \text { when } N \neq 0 \\
\left(T_{\text {rshoe }}+T_{\text {lshoe }}\right) \frac{\mu_{\text {static }}}{\mu} & \text { when } N=0\end{cases}
\end{aligned}
$$



The equations use these variables.

| Variable | Value |
| :--- | :--- |
| $T$ | Brake torque |
| $P$ | Applied brake pressure |
| $N$ | Wheel speed |
| $\mu_{\text {static }}$ | Disc pad-rotor coefficient of static friction |
| $\mu$ | Disc pad-rotor coefficient of kinetic friction |
| $T_{\text {rshoe }}$ | Right shoe brake torque |
| $T_{\text {lshoe }}$ | Left shoe brake torque |
| $a$ | Distance from drum center to shoe hinge pin center |
| $c$ | Distance from shoe hinge pin center to brake actuator connection on brake shoe |
| $r$ | Drum internal radius |
| $B_{a}$ | Brake actuator bore diameter |
| $\Theta_{1}$ | Angle from shoe hinge pin center to start of brake pad material on shoe |
| $\Theta_{2}$ | Angle from shoe hinge pin center to end of brake pad material on shoe |
| Mapped |  |

If you specify the Brake Type parameter as Mapped, the block uses a lookup table to determine the brake torque.

$$
T=\left\{\begin{array}{lr}
f_{\text {brake }}(P, N) & \text { when } N \neq 0 \\
\left(\frac{\mu_{\text {static }}}{\mu}\right) f_{\text {brake }}(P, N) & \text { when } N=0
\end{array}\right.
$$

The equations use these variables.

| Variable | Value |
| :--- | :--- |
| $T$ | Brake torque |
| $f_{\text {brake }}(P, N)$ | Brake torque lookup table |
| $P$ | Applied brake pressure |
| $N$ | Wheel speed |
| $\mu_{\text {static }}$ | Friction coefficient of drum pad-face interface under static conditions |
| $\mu$ | Friction coefficient of disc pad-rotor interface |

The lookup table for the brake torque, $f_{\text {brake }}(P, N)$, is a function of applied brake pressure and wheel speed, where:

- $T$ is brake torque, in $\mathrm{N} \cdot \mathrm{m}$.
- $P$ is applied brake pressure, in bar.
- $N$ is wheel speed, in rpm.



## Longitudinal Force

To model the Longitudinal Wheel block longitudinal forces, you can use the Magic Formula. The model provides a steady-state tire characteristic function $F_{\mathrm{x}}=f\left(\kappa, F_{z}\right)$, the longitudinal force $F_{\mathrm{x}}$ on the tire, based on:

- Vertical load $F_{z}$
- Wheel slip $\kappa$


The Magic Formula model uses these variables.

| $\Omega$ | Wheel angular velocity |
| :--- | :--- |
| $r_{\mathrm{w}}$ | Wheel radius |
| $V_{\mathrm{x}}$ | Wheel hub longitudinal velocity |
| $r_{\mathrm{w}} \Omega$ | Tire tread longitudinal velocity |
| $V_{\mathrm{sx}}=r_{\mathrm{w}} \Omega-V_{\mathrm{x}}$ | Wheel slip velocity |
| $K=V_{\mathrm{sx}} /\left\|V_{\mathrm{x}}\right\|$ | Wheel slip |
| $F_{z}, F_{\mathrm{z} 0}$ | Vertical load and nominal vertical load on tire |

$F_{\mathrm{x}}=f\left(\kappa, F_{\mathrm{z}}\right) \quad \begin{aligned} & \text { Longitudinal force exerted on the tire at the contact point. Also a } \\ & \text { characteristic function } f \text { of the tire. }\end{aligned}$

## Magic Formula Constant Value

If you set Longitudinal Force to Magic Formula constant value, the block implements the Magic Formula as a specific form of the tire characteristic function, characterized by four dimensionless coefficients $(B, C, D, E)$, or stiffness, shape, peak, and curvature:

$$
F_{\mathrm{x}}=f\left(\kappa, F_{\mathrm{z}}\right)=F_{\mathrm{z}} D \sin \left(C \tan ^{-1}\left[\left\{B K-E\left[B K-\tan ^{-1}\left(B_{K}\right)\right]\right\}\right]\right)
$$

The slope of $f$ at $k=0$ is $B C D \cdot F_{z}$.
The coefficients are based on empirical tire data. These values are typical sets of constant Magic Formula coefficients for common road conditions.

| Surface | B | C | D | E |
| :--- | :--- | :--- | :--- | :--- |
| Dry tarmac | 10 | 1.9 | 1 | 0.97 |
| Wet tarmac | 12 | 2.3 | 0.82 | 1 |
| Snow | 5 | 2 | 0.3 | 1 |
| Ice | 4 | 2 | 0.1 | 1 |

## Magic Formula Pure Longitudinal Slip

If you set Longitudinal Force to Magic Formula pure longitudinal slip, the block implements a more general Magic Formula using dimensionless coefficients that are functions of the tire load. The block implements the longitudinal force equations in Chapter 4 of Tire and Vehicle Dynamics, including 4.E9 through 4.E18:

$$
F_{\mathrm{x} 0}=D_{\mathrm{x}} \sin \left(C_{\mathrm{x}} \tan ^{-1}\left[\left\{B_{\mathrm{x}} K_{\mathrm{X}}-E_{\mathrm{X}}\left[B_{\mathrm{x}} K_{\mathrm{x}}-\tan ^{-1}\left(B_{\mathrm{x}} K_{\mathrm{x}}\right)\right]\right\}\right]\right)+S_{\mathrm{Vx}}
$$

where:

$$
\begin{aligned}
& K_{\mathrm{X}}=K+S_{H x} \\
& C_{\mathrm{x}}=p_{C x 1} \lambda_{C x} \\
& D_{\mathrm{x}}=\mu_{\mathrm{x}} F_{\mathrm{z}} S_{1} \\
& \mu_{\mathrm{x}}=\left(p_{D \times 1}+p_{D \times 2} d f_{\mathrm{z}}\right)\left(1+p_{p \times 3} d p_{i}+p_{p \times 4} d p_{i}{ }^{2}\right)\left(1-p_{D \times 3} \gamma^{2}\right) \lambda^{*}{ }_{\mu x} \\
& E_{\mathrm{x}}=\left(p_{E x 1}+p_{E x 2} d f_{\mathrm{z}}+p_{E x 3} d f_{\mathrm{z}}{ }^{2}\right)\left[1-p_{E x 4} \operatorname{sgn}\left(K_{\mathrm{x}}\right)\right] \lambda_{E x} \\
& K_{\mathrm{xK}}=F_{\mathrm{z}}\left(p_{K \times 1}+p_{K \times 2} d f_{\mathrm{z}}\right) \exp \left(\mathrm{p}_{\mathrm{Kx} 3} d f_{\mathrm{z}}\right)\left(1+p_{p \times 1} d p_{i}+p_{p \times 2} d p_{i} 2\right) \\
& B_{\mathrm{x}}=K_{\mathrm{xK}} /\left(C_{\mathrm{x}} D_{\mathrm{x}}+\varepsilon_{\mathrm{x}}\right) \\
& S_{H x}=p_{H \times 1}+p_{H \times 2} d f_{\mathrm{z}} \\
& S_{V x}=F_{z} \cdot\left(p_{V x 1}+p_{V x 2} d f_{z}\right) \lambda_{V x} \lambda^{\prime}{ }_{\mu x} S_{1}
\end{aligned}
$$

$S_{H x}$ and $S_{V x}$ represent offsets to the slip and longitudinal force in the force-slip function, or horizontal and vertical offsets if the function is plotted as a curve. $\mu_{x}$ is the longitudinal load-dependent friction coefficient. $\varepsilon_{\chi}$ is a small number inserted to prevent division by zero as $F_{z}$ approaches zero.

## Vertical Dynamics

If you select no vertical degrees-of-freedom by setting Vertical Motion to None, the block passes the applied chassis forces directly through to the rolling resistance and longitudinal force calculations.

If you set Vertical Motion to Mapped stiffness and damping, the vertical motion depends on wheel stiffness and damping. Stiffness is a function of tire sidewall displacement and pressure. Damping is a function of tire sidewall velocity and pressure.

$$
F z \operatorname{tire}\left(z, \dot{z}, P_{\text {tire }}\right)=F_{z k}\left(z, P_{\text {tire }}\right)+F_{z b}\left(\dot{z}, P_{\text {tire }}\right)
$$

The block determines the vertical response using this differential equation.

$$
\ddot{z} m=\text { Fztire }-F_{z}-m g
$$

When you disable the vertical degree-of-freedom, the input normal force from the vehicle passes directly to the longitudinal and rolling force calculations.

$$
\begin{aligned}
& \ddot{z}=\dot{z}=m=0 \\
& \text { Fztire }=m g
\end{aligned}
$$

The block uses the wheel-fixed frame to resolve the vertical forces.


The equations use these variables.
Fztire $\quad$ Tire normal force along the wheel-fixed $z$-axis
m
Axle mass
$F_{z k} \quad$ Tire normal force due to wheel stiffness along the wheel-fixed $z$-axis

| $F_{z b}$ | Tire normal force due to wheel damping along the wheel-fixed $z$-axis |
| :--- | :--- |
| $F_{z}$ | Suspension or vehicle normal force along the wheel-fixed $z$-axis |
| $P_{\text {Tire }}$ | Tire pressure |
| $z, \dot{z}, \ddot{z}$ | Tire displacement, velocity, and acceleration, respectively, along the wheel-fixed $z$ - |
|  | axis |

## Power Accounting

For the power accounting, the block implements these equations.

| Bus Signal |  |  | Description | Equations |
| :---: | :---: | :---: | :---: | :---: |
| PwrInf <br> 0 | PwrTrnsfrd - <br> Power transferred between blocks <br> - Positive signals indicate flow into block <br> - Negative signals indicate flow out of block | PwrRoad | Tractive power applied from the axle | $P_{\text {road }}=F_{x} V_{\chi}$ |
|  |  | PwrAxlTrq | External torque applied by the axle to the wheel | $P_{T}=T \omega$ |
|  |  | PwrFz | Vertical force applied to the wheel by the vehicle or suspension | $P_{F z}=F_{z} \dot{z}$ |
|  | PwrNotTrnsfrd - Power crossing the block boundary, but not transferred <br> - Positive signals indicate an input <br> - Negative signals indicate a loss | PwrSlip | Tractive power loss | $\begin{aligned} & P_{K}=F_{x} V_{x}+( \\ & \left.-F_{c p} R_{e}+M_{y}\right) \omega \end{aligned}$ |
|  |  | PwrMyRoll | Rolling resistance power | $P_{M y}=M_{y} \omega$ |
|  |  | PwrMyBrk | Braking power | $P_{b r k}=M_{b r k}$ |
|  |  | PwrMyb | Rolling viscous damping loss | $P_{b}=-b \omega^{2}$ |
|  |  | PwrFzDamp | Vertical damping power | $P_{F z b}=F_{z b} \dot{\chi}$ |
|  | PwrStored - <br> Stored energy rate of change <br> - Positive signals indicate an increase <br> - Negative signals indicate a decrease | PwrStoredzdot | Rate of change of vertical kinetic energy | $P_{\dot{z}}=m \ddot{z} \dot{z}$ |
|  |  | PwrStoredq | Rate of change of rotational kinetic energy | $P_{\omega}=I_{y y} \dot{\omega} \omega$ |
|  |  | PwrStoredFsFzSp rng | Rate of change of stored sidewall potential energy | $P_{F z k}=F_{z k} \dot{z}_{\chi}$ |
|  |  | PwrStoredGrvty | Rate of change of gravitational potential energy | $P_{g}=-m g \dot{Z}$ |

The equations use these variables.
$\omega \quad$ Wheel angular velocity
$b \quad$ Linear velocity force component

| $F_{x}$ | Longitudinal force developed by the tire road interface due to slip |
| :--- | :--- |
| $F_{c p}$ | Tire slip force at contact patch |
| $F_{z}$ | Vehicle normal force |
| $F_{z b}$ | Tire normal force due to wheel damping |
| $F_{z k}$ | Tire normal force due to wheel stiffness |
| $I_{y y}$ | Wheel rotational inertia |
| $M_{b r k}$ | Braking moment |
| $M_{y}$ | Rolling resistance torque |
| $R_{e}$ | Effective tire radius while under load and for a given pressure |
| $T$ | Axle torque applied on wheel |
| $V_{x}$ | Longitudinal axle velocity |
| $z, \dot{z}, \ddot{z}$ | Tire displacement, velocity, and acceleration, respectively |
| $\omega$ | Wheel angular velocity |
| $\dot{Z}$ | Vehicle vertical velocity along the vehicle-fixed $z$-axis |

## Ports

Input
BrkPrs - Brake pressure
scalar
Brake pressure, in Pa.

## Dependencies

To enable this port, for the Brake Type parameter, specify one of these types:

- Disc
- Drum
- Mapped

AxITrq - Axle torque
scalar
Axle torque, $T_{a}$, about wheel spin axis, in $\mathrm{N} \cdot \mathrm{m}$.
Vx - Velocity
scalar
Axle longitudinal velocity along vehicle(body)-fixed $x$-axis, in $\mathrm{m} / \mathrm{s}$.
Fz - Normal force
scalar
Absolute value of suspension or vehicle normal force along body-fixed $z$-axis, in N .
Gnd - Ground displacement
scalar

Ground displacement, Grndz, along negative wheel-fixed $z$-axis, in m .


## Dependencies

To create Gnd:

- Set Vertical Motion to Mapped stiffness and damping.
- On the Vertical pane, select Input ground displacement.

Iam_mux - Friction scaling factor
scal̃ar
Longitudinal friction scaling factor, dimensionless.

## Dependencies

To enable this port, select Input friction scale factor.
TirePrs - Tire pressure
scalar
Tire pressure, in Pa.
Dependencies
To enable this port:

- Set one of these parameters:
- Longitudinal Force to Magic Formula pure longitudinal slip.
- Rolling Resistance to Pressure and velocity or Magic Formula.
- Vertical Motion to Mapped stiffness and damping.
- On the Wheel Dynamics pane, select Input tire pressure.

Tamb - Ambient temperature
scalar
Ambient temperature, $T_{\text {amb }}$, in K .
The ambient temperature, $T_{\text {amb }}$, is the temperature near tire in application environment, in K. For example, the measured ambient temperature is the ambient temperature near the tire when the vehicle is on the road.

Select to create input port Tamb to input the measured ambient temperature.

## Dependencies

To enable this port:
1 Set Rolling Resistance to ISO 28580.
2 On the Rolling Resistance pane, select to Input ambient temperature.

## Output

Info - Bus signal
bus
Bus signal containing these block calculations.

| Signal | Description | Units |
| :--- | :--- | :--- |
| AxlTrq | Axle torque about body-fixed <br> $y$-axis | $\mathrm{N} \cdot \mathrm{m}$ |
| Omega | Wheel angular velocity about <br> body-fixed $y$-axis | $\mathrm{rad} / \mathrm{s}$ |
| Omegadot | Wheel angular acceleration <br> about body-fixed $y$-axis | $\mathrm{rad} / \mathrm{s}^{\wedge} 2$ |
| Fx | Longitudinal vehicle force <br> along body-fixed $x$-axis | N |
| Fz | Vertical vehicle force along <br> body-fixed $z$-axis | N |
| Fzb | Tire normal force due to <br> wheel damping along the <br> wheel-fixed $z$-axis | N |
| Fzk | Tire normal force due to <br> wheel stiffness along the <br> wheel-fixed $z$-axis | N |
| My | Rolling resistance torque <br> about body-fixed $y$-axis | $\mathrm{N} \cdot \mathrm{m}$ |


| Signal |  | Description |
| :--- | :--- | :--- |
| Myb | Rolling resistance torque due <br> to damping about body-fixed <br> y-axis | $\mathrm{N} \cdot \mathrm{m}$ |
| Kappa | Slip ratio | NA |
| Vx | Vehicle longitudinal velocity <br> along body-fixed $x$-axis | $\mathrm{m} / \mathrm{s}$ |
| Re | Wheel effective radius along <br> wheel-fixed $z$-axis | m |
| BrkTrq | Brake torque about body-fixed <br> y-axis | N -m |
| BrkPrs | Brake pressure | Pa |
| z | Wheel vertical deflection <br> along wheel-fixed $z$-axis | m |
| zdot | Wheel vertical velocity along <br> wheel-fixed $z$-axis | $\mathrm{m} / \mathrm{s}$ |
| zddot | Wheel vertical acceleration <br> along wheel-fixed $z$-axis | $\mathrm{m} / \mathrm{s} \wedge 2$ |
| Gndz |  | Ground displacement along <br> negative of wheel-fixed $z$-axis <br> (positive input produces wheel <br> lift) |


| Signal |  | Description | Units |  |
| :--- | :--- | :--- | :--- | :--- |
|  |  | PwrStoredq | Rate of change of stored <br> sidewall potential energy | W |
|  |  | PwrStoredFsFzSprng | Rate of change of <br> gravitational potential energy | W |
|  |  | PwrStoredGrvty | Tractive power applied from <br> the axle | W |

Fx - Longitudinal axle force scalar

Longitudinal force acting on axle, along body-fixed $x$-axis, in N. Positive force acts to move the vehicle forward.

Omega - Wheel angular velocity
scalar
Wheel angular velocity, about body-fixed $y$-axis, in rad/s.
z - Wheel vertical deflection
scalar
Wheel vertical deflection along wheel-fixed $z$-axis, in m.

## Dependencies

To enable this port, set Vertical Motion to Mapped stiffness and damping.
zdot - Wheel vertical velocity
scalar
Wheel vertical velocity along wheel-fixed $z$-axis, in $\mathrm{m} / \mathrm{s}$.

## Dependencies

To enable this port, set Vertical Motion to Mapped stiffness and damping.

## Parameters

## Block Options

Longitudinal Force - Select type
Magic Formula constant value (default)|Magic Formula pure longitudinal slip| Mapped force

The block models longitudinal force as a function of wheel slip relative to the road surface. To calculate the longitudinal force, specify one of these Longitudinal Force parameters.

| Setting | Block Implementation |
| :--- | :--- |
| Magic Formula constant value | Magic Formula with constant coefficient for stiffness, shape, <br> peak, and curvature. |


| Setting | Block Implementation |
| :--- | :--- |
| Magic Formula pure <br> longitudinal slip | Magic Formula with load-dependent coefficients that <br> implement equations 4.E9 through 4.E18 in Tire and Vehicle <br> Dynamics. |
| Mapped force | Lookup table that is a function of the normal force and wheel <br> slip ratio. |

## Dependencies

| Selecting |
| :--- |
| Magic Formula constant value |
|  |
|  |
|  |

Enables These Parameters
Pure longitudinal peak factor, $\mathbf{D x}$
Pure longitudinal shape factor, $\mathbf{C x}$
Pure longitudinal stiffness factor, Bx
Pure longitudinal curvature factor, Ex

| Selecting | Enables These Parameters |
| :---: | :---: |
| Magic Formula pure longitudinal slip | Cfx shape factor, PCX1 |
|  | Longitudinal friction at nominal normal load, PDX1 |
|  | Longitudinal friction at nominal normal load, PDX1 |
|  | Frictional variation with load, PDX2 |
|  | Frictional variation with camber, PDX3 |
|  | Longitudinal curvature at nominal normal load, PEX1 |
|  | Variation of curvature factor with load, PEX2 |
|  | Variation of curvature factor with square of load, PEX3 |
|  | Longitudinal curvature factor with slip, PEX4 |
|  | Longitudinal slip stiffness at nominal normal load, PKX1 |
|  | Variation of slip stiffness with load, PKX2 |
|  | Slip stiffness exponent factor, PKX3 |
|  | Horizontal shift in slip ratio at nominal normal load, PHX1 |
|  | Variation of horizontal slip ratio with load, PHX2 |
|  | Vertical shift in load at nominal normal load, PVX1 |
|  | Variation of vertical shift with load, PVX2 |
|  | Linear variation of longitudinal slip stiffness with tire pressure, PPX1 |
|  | Quadratic variation of longitudinal slip stiffness with tire pressure, PPX2 |
|  | Linear variation of peak longitudinal friction with tire pressure, PPX3 |
|  | Quadratic variation of peak longitudinal friction with tire pressure, PPX4 |
|  | Linear variation of longitudinal slip stiffness with tire pressure, PPX1 |
|  | Slip speed decay function scaling factor, lam_muV |
|  | Brake slip stiffness scaling factor, lam_Kxkappa |
|  | Longitudinal shape scaling factor, lam_Cx |
|  | Longitudinal curvature scaling factor, lam_Ex |


| Selecting | Enables These Parameters |
| :--- | :--- |
|  | Longitudinal horizontal shift scaling factor, lam_Hx |
|  | Longitudinal vertical shift scaling factor, lam_Vx |
| Mapped force | Slip ratio breakpoints, kappaFx |
|  | Normal force breakpoints, FzFx |
|  | Longitudinal force map, FxMap |

Rolling Resistance - Rolling resistance torque
None (default)|Pressure and velocity |ISO 28580|Magic Formula|Mapped torque
To calculate the rolling resistance torque, specify one of these Rolling Resistance parameters.

| Setting | Block Implementation |
| :--- | :--- |
| None | None |
| Pressure and velocity | Method in Stepwise Coastdown Methodology for Measuring <br> Tire Rolling Resistance. The rolling resistance is a function of <br> tire pressure, normal force, and velocity. |
| ISO 28580 | Method specified in ISO 28580:2018, Passenger car, truck <br> and bus tyre rolling resistance measurement method - <br> Single point test and correlation of measurement results. |
| Magic Formula | Magic formula equations from 4.E70 in Tire and Vehicle <br> Dynamics. The magic formula is an empirical equation based <br> on fitting coefficients. |
| Mapped torque | Lookup table that is a function of the normal force and spin <br> axis longitudinal velocity. |

## Dependencies

Each Rolling Resistance setting enables additional parameters.

| Setting | Parameters Enabled |
| :--- | :--- |
| Pressure and velocity | - Velocity independent force coefficient, aMy |
|  | - Linear velocity force component, bMy |
|  | - Quadratic velocity force component, cMy |
|  | - Tire pressure exponent, alphaMy |
|  | - Normal force exponent, betaMy |
| ISO 28580 | - Parasitic losses force, Fpl |
|  | - Rolling resistance constant, Cr |
|  | - Thermal correction factor, Kt |
|  | - Measured temperature, Tmeas |
|  | - Parasitic losses force, Fpl |
|  | - Ambient temperature, Tamb |


| Setting | Parameters Enabled |
| :--- | :--- |
| Magic Formula | Rolling resistance torque coefficient, QSY |
|  | Longitudinal force rolling resistance coefficient, QSY2 |
|  | Linear rotational speed rolling resistance coefficient, <br> QSY3 <br>  <br>  <br>  <br>  <br>  <br>  <br>  <br>  <br> Quartic rotational speed rolling resistance coefficient, <br> Camber squared rolling resistance torque, QSY5 <br> Load based camber squared rolling resistance torque, <br> QSY6 <br> Normal load rolling resistance coefficient, QSY7 |
| Pressure load rolling resistance coefficient, QSY8 |  |
|  | Rolling resistance scaling factor, lam_My |
|  | Spin axis velocity breakpoints, VxMy |
| Normal force breakpoints, FzMy |  |
|  | Rolling resistance torque map, MyMap |

Brake Type - Select type
None | Disc | Drum | Mapped
There are four types of Longitudinal Wheel blocks. Each block implements a different brake type.

| Block Name | Brake Type Setting | Brake Implementation |
| :--- | :--- | :--- |
| Longitudinal Wheel - No <br> Brake | None | None |
| Longitudinal Wheel - Disc <br> Brake | Disc | Brake that converts the brake cylinder <br> pressure into a braking force. |
| Longitudinal Wheel - Drum <br> Brake | Drum | Simplex drum brake that converts the <br> applied force and brake geometry into a <br> net braking torque. |
| Longitudinal Wheel - Mapped <br> Brake | Mapped | Lookup table that is a function of the <br> wheel speed and applied brake pressure. |

## Vertical Motion - Select type

None (default)| Mapped stiffness and damping
To calculate vertical motion, specify one of these Vertical Motion parameters.

| Setting | Block Implementation |
| :--- | :--- |
| None | Block passes the applied chassis forces directly through to <br> the rolling resistance and longitudinal force calculations. |


| Setting | Block Implementation |
| :--- | :--- |
| Mapped stiffness and damping | Vertical motion depends on wheel stiffness and damping. <br> Stiffness is a function of tire sidewall displacement and <br> pressure. Damping is a function of tire sidewall velocity and <br> pressure. |


| Selecting | Enables These Parameters | Creates These Output Ports |
| :--- | :--- | :--- |
| Mapped stiffness <br> and damping | Wheel and unsprung mass, m <br> Initial deflection, zo <br> Initial velocity, zdoto <br> Gravitational acceleration, g <br> Vertical deflection breakpoints, zFz <br> Pressure breakpoints, pFz | zdot |
|  | Force due to deflection, Fzz <br> Vertical velocity breakpoints, zdotFz <br> Force due to velocity, Fzzdot <br> Ground displacement, Gndz <br> Input ground displacement |  |
|  |  |  |

Longitudinal scaling factor, lam_x - Friction scaling factor
1 (default)
Longitudinal friction scaling factor, dimensionless.

## Dependencies

To enable this parameter, clear Input friction scale factor.
Input friction scale factor - Selection
Off (default)
Create input port for longitudinal friction scaling factor.

## Dependencies

Selecting this parameter:

- Creates input port lam_mux.
- Disables parameter Longitudinal scaling factor, lam_x.


## Wheel Dynamics

Axle viscous damping coefficient, br - Damping
0.001 (default)| scalar

Axle viscous damping coefficient, $b r$, in $\mathrm{N} \cdot \mathrm{m} \cdot \mathrm{s} / \mathrm{rad}$.
Wheel inertia, lyy - Inertia
0.8 (default) | scalar

Wheel inertia, in $\mathrm{kg} \cdot \mathrm{m}^{\wedge} 2$.
Wheel initial angular velocity, omegao - Wheel speed
0 (default) | scalar
Initial angular velocity of wheel, along body-fixed $y$-axis, in rad/s.
Relaxation length, Lrel - Relaxation length
0.5 (default) | scalar

Wheel relaxation length, in m.
Loaded radius, $\mathbf{R e}$ - Loaded radius
0.3 (default) | scalar

Loaded wheel radius, Re , in m .


Unloaded radius, UNLOADED_RADIUS - Unloaded radius
0.4 (default) | scalar

Unloaded wheel radius, in m.

## Dependencies

To create this parameter, set Rolling Resistance to Pressure and velocity or Magic Formula.

Nominal longitudinal speed, LONGVL - Speed
16 (default) | scalar
Nominal longitudinal speed along body-fixed $x$-axis, in $\mathrm{m} / \mathrm{s}$.
Dependencies
To enable this parameter, set Longitudinal Force to Magic Formula pure longitudinal slip.
Nominal camber angle, gamma - Camber
0 (default) | scalar
Nominal camber angle, in rad.

## Dependencies

To enable this parameter, set either:

- Longitudinal Force to Magic Formula pure longitudinal slip.
- Rolling Resistance to Magic Formula.

Nominal pressure, NOMPRES - Pressure
220000 (default) | scalar
Nominal pressure, in Pa.

## Dependencies

To enable this parameter, set either:

- Longitudinal Force to Magic Formula pure longitudinal slip.
- Rolling Resistance to Magic Formula.

Pressure, press - Pressure
220000 (default) | scalar
Pressure, in Pa.

## Dependencies

To enable this parameter:

- Set one of these:
- Longitudinal Force to Magic Formula pure longitudinal slip.
- Rolling Resistance to Pressure and velocity or Magic Formula.
- Vertical Motion to Mapped stiffness and damping.
- On the Wheel Dynamics pane, clear Input tire pressure.


## Longitudinal

Magic Formula Constant Value
Pure longitudinal peak factor, Dx - Factor
1 (default) | scalar
Pure longitudinal peak factor, dimensionless.

The coefficients are based on empirical tire data. These values are typical sets of constant Magic Formula coefficients for common road conditions.

| Surface | B | C | D | E |
| :--- | :--- | :--- | :--- | :--- |
| Dry tarmac | 10 | 1.9 | 1 | 0.97 |
| Wet tarmac | 12 | 2.3 | 0.82 | 1 |
| Snow | 5 | 2 | 0.3 | 1 |
| Ice | 4 | 2 | 0.1 | 1 |

## Dependencies

To create this parameter, select the Longitudinal Force parameter Magic Formula constant value.

## Pure longitudinal shape factor, $\mathbf{C x}$ - Factor

1.65 (default) | scalar

Pure longitudinal shape factor, dimensionless.
The coefficients are based on empirical tire data. These values are typical sets of constant Magic Formula coefficients for common road conditions.

| Surface | B | C | D | E |
| :--- | :--- | :--- | :--- | :--- |
| Dry tarmac | 10 | 1.9 | 1 | 0.97 |
| Wet tarmac | 12 | 2.3 | 0.82 | 1 |
| Snow | 5 | 2 | 0.3 | 1 |
| Ice | 4 | 2 | 0.1 | 1 |

## Dependencies

To create this parameter, select the Longitudinal Force parameter Magic Formula constant value.

Pure longitudinal stiffness factor, Bx - Factor
10 (default) | scalar
Pure longitudinal stiffness factor, dimensionless.
The coefficients are based on empirical tire data. These values are typical sets of constant Magic Formula coefficients for common road conditions.

| Surface | B | C | D | E |
| :--- | :--- | :--- | :--- | :--- |
| Dry tarmac | 10 | 1.9 | 1 | 0.97 |
| Wet tarmac | 12 | 2.3 | 0.82 | 1 |
| Snow | 5 | 2 | 0.3 | 1 |
| Ice | 4 | 2 | 0.1 | 1 |

## Dependencies

To create this parameter, select the Longitudinal Force parameter Magic Formula constant value.

Pure longitudinal curvature factor, Ex - Factor
0.01 (default) | scalar

Pure longitudinal curvature factor, dimensionless.
The coefficients are based on empirical tire data. These values are typical sets of constant Magic Formula coefficients for common road conditions.

| Surface | B | C | D | E |
| :--- | :--- | :--- | :--- | :--- |
| Dry tarmac | 10 | 1.9 | 1 | 0.97 |
| Wet tarmac | 12 | 2.3 | 0.82 | 1 |
| Snow | 5 | 2 | 0.3 | 1 |
| Ice | 4 | 2 | 0.1 | 1 |

## Dependencies

To create this parameter, select the Longitudinal Force parameter Magic Formula constant value.

Magic Formula Pure Longitudinal Slip
Cfx shape factor, PCX1 - Factor
1.6 (default)| scalar

Cfx shape factor, PCX1, dimensionless.

## Dependencies

To create this parameter, select the Longitudinal Force parameter Magic Formula pure longitudinal slip.

Longitudinal friction at nominal normal load, PDX1 - Factor
1 (default) | scalar
Longitudinal friction at nominal normal load, PDX1, dimensionless.

## Dependencies

To create this parameter, select the Longitudinal Force parameter Magic Formula pure longitudinal slip.

Frictional variation with load, PDX2 - Factor
-0.08 (default) | scalar
Frictional variation with load, PDX2, dimensionless.

## Dependencies

To create this parameter, select the Longitudinal Force parameter Magic Formula pure longitudinal slip.

Frictional variation with camber, PDX3 - Factor
0 (default) | scalar
Frictional variation with camber, PDX3, 1/rad^2.

## Dependencies

To create this parameter, select the Longitudinal Force parameter Magic Formula pure longitudinal slip.

## Longitudinal curvature at nominal normal load, PEX1 - Factor

0.112 (default) | scalar

Longitudinal curvature at nominal normal load, PEX1, dimensionless.

## Dependencies

To create this parameter, select the Longitudinal Force parameter Magic Formula pure longitudinal slip.

Variation of curvature factor with load, PEX2 - Factor
0.313 (default) | scalar

Variation of curvature factor with load, PEX2, dimensionless.

## Dependencies

To create this parameter, select the Longitudinal Force parameter Magic Formula pure longitudinal slip.

Variation of curvature factor with square of load, PEX3 - Factor
0 (default) | scalar
Variation of curvature factor with square of load, PEX3, dimensionless.

## Dependencies

To create this parameter, select the Longitudinal Force parameter Magic Formula pure longitudinal slip.

## Longitudinal curvature factor with slip, PEX4 - Factor

0.0016 (default) | scalar

Longitudinal curvature factor with slip, PEX4, dimensionless.

## Dependencies

To create this parameter, select the Longitudinal Force parameter Magic Formula pure longitudinal slip.

## Longitudinal slip stiffness at nominal normal load, PKX1 - Factor

21.7 (default) | scalar

Longitudinal slip stiffness at nominal normal load, PKX1, dimensionless.

## Dependencies

To create this parameter, select the Longitudinal Force parameter Magic Formula pure longitudinal slip.

## Variation of slip stiffness with load, PKX2 - Factor

13.77 (default) | scalar

Variation of slip stiffness with load, PKX2, dimensionless.
Dependencies
To create this parameter, select the Longitudinal Force parameter Magic Formula pure longitudinal slip.

Slip stiffness exponent factor, PKX3 - Factor

- 0.412 (default) | scalar

Slip stiffness exponent factor, PKX3, dimensionless.

## Dependencies

To create this parameter, select the Longitudinal Force parameter Magic Formula pure longitudinal slip.

Horizontal shift in slip ratio at nominal normal load, PHX1 - Factor
2.1585E-4 (default) | scalar

Horizontal shift in slip ratio at nominal normal load, PHX1, dimensionless.

## Dependencies

To create this parameter, select the Longitudinal Force parameter Magic Formula pure longitudinal slip.

Variation of horizontal slip ratio with load, PHX2 - Factor
0.00115 (default) | scalar

Variation of horizontal slip ratio with load, PHX2, dimensionless.

## Dependencies

To create this parameter, select the Longitudinal Force parameter Magic Formula pure longitudinal slip.

Vertical shift in load at nominal normal load, PVX1 - Factor
1.5973E-5 (default) | scalar

Vertical shift in load at nominal normal load, PVX1, dimensionless.

## Dependencies

To create this parameter, select the Longitudinal Force parameter Magic Formula pure longitudinal slip.

Variation of vertical shift with load, PVX2 - Factor
1.043E-4 (default) | scalar

Variation of vertical shift with load, PVX2, dimensionless.

## Dependencies

To create this parameter, select the Longitudinal Force parameter Magic Formula pure longitudinal slip.

Linear variation of longitudinal slip stiffness with tire pressure, PPX1 - Factor - 0.3489 (default) | scalar

Linear variation of longitudinal slip stiffness with tire pressure, PPX1, dimensionless.

## Dependencies

To create this parameter, select the Longitudinal Force parameter Magic Formula pure longitudinal slip.

Quadratic variation of longitudinal slip stiffness with tire pressure, PPX2 - Factor 0.382 (default) | scalar

Quadratic variation of longitudinal slip stiffness with tire pressure, PPX2, dimensionless.

## Dependencies

To create this parameter, select the Longitudinal Force parameter Magic Formula pure longitudinal slip.

## Linear variation of peak longitudinal friction with tire pressure, PPX3 - Factor -0.09634 (default) | scalar

Linear variation of peak longitudinal friction with tire pressure, PPX3, dimensionless.

## Dependencies

To create this parameter, select the Longitudinal Force parameter Magic Formula pure longitudinal slip.

Quadratic variation of peak longitudinal friction with tire pressure, PPX4 - Factor 0.06447 (default) | scalar

Quadratic variation of peak longitudinal friction with tire pressure, PPX4, dimensionless.

## Dependencies

To create this parameter, select the Longitudinal Force parameter Magic Formula pure longitudinal slip.

Slip speed decay function scaling factor, lam_muV - Factor 1 (default) | scalar

Slip speed decay function scaling factor, lam_muV, dimensionless.

## Dependencies

To create this parameter, select the Longitudinal Force parameter Magic Formula pure longitudinal slip.

Brake slip stiffness scaling factor, lam_Kxkappa - Factor
1 (default) | scalar
Brake slip stiffness scaling factor, lam_Kxkappa, dimensionless.

## Dependencies

To create this parameter, select the Longitudinal Force parameter Magic Formula pure longitudinal slip.

## Longitudinal shape scaling factor, lam_Cx - Factor

1 (default) | scalar
Longitudinal shape scaling factor, lam Cx, dimensionless.

## Dependencies

To create this parameter, select the Longitudinal Force parameter Magic Formula pure longitudinal slip.

## Longitudinal curvature scaling factor, lam_Ex - Factor

0 (default) | scalar
Longitudinal curvature scaling factor, lam_Ex, dimensionless.

## Dependencies

To create this parameter, select the Longitudinal Force parameter Magic Formula pure longitudinal slip.

## Longitudinal horizontal shift scaling factor, lam_Hx - Factor

1 (default) | scalar
Longitudinal horizontal shift scaling factor, lam_Hx, dimensionless.

## Dependencies

To create this parameter, select the Longitudinal Force parameter Magic Formula pure longitudinal slip.

## Longitudinal vertical shift scaling factor, lam_Vx - Factor

1 (default) | scalar
Longitudinal vertical shift scaling factor, lam_Vx, dimensionless.

## Dependencies

To create this parameter, select the Longitudinal Force parameter Magic Formula pure longitudinal slip.

## Mapped Force

Slip ratio breakpoints, kappaFx - Breakpoints
vector
Slip ratio breakpoints, dimensionless.

## Dependencies

To create this parameter, select the Longitudinal Force parameter Mapped force.
Normal force breakpoints, FzFx - Breakpoints
vector
Normal force breakpoints, N.

## Dependencies

To create this parameter, select the Longitudinal Force parameter Mapped force.

Longitudinal force map, FxMap - Lookup table
array
Longitudinal force versus slip ratio and normal force, N .

## Dependencies

To create this parameter, select the Longitudinal Force parameter Mapped force.

## Rolling Resistance

Pressure and Velocity
Velocity independent force coefficient, $\mathbf{a M y}$ - Velocity-independent force coefficient
8e-4 (default) | scalar
Velocity-independent force coefficient, $a$, in $\mathrm{s} / \mathrm{m}$.

## Dependencies

To enable this parameter, set Rolling Resistance to Pressure and velocity.
Linear velocity force component, bMy - Linear velocity force component
0.001 (default) | scalar

Linear velocity force component, $b$, in $\mathrm{s} / \mathrm{m}$.
Dependencies
To enable this parameter, set Rolling Resistance to Pressure and velocity.
Quadratic velocity force component, cMy - Quadratic velocity force component
1.6e-4 (default) | scalar

Quadratic velocity force component, $c$, in $\mathrm{s}^{\wedge} 2 / \mathrm{m}^{\wedge} 2$.

## Dependencies

To enable this parameter, set Rolling Resistance to Pressure and velocity.
Tire pressure exponent, alphaMy - Tire pressure exponent
-0.003 (default) | scalar
Tire pressure exponent, $\alpha$, dimensionless.
Dependencies
To enable this parameter, set Rolling Resistance to Pressure and velocity.
Normal force exponent, betaMy - Normal force exponent
0.97 (default) | scalar

Normal force exponent, $\beta$, dimensionless.

## Dependencies

To enable this parameter, set Rolling Resistance to Pressure and velocity.

ISO 28580
Parasitic losses force, FpI - Parasitic force loss
10 (default) | scalar
Parasitic force loss, $F_{p l}$ in $N$.

## Dependencies

To enable this parameter, set Rolling Resistance to ISO 28580.
Rolling resistance constant, $\mathbf{C r}$ - Rolling resistance constant
1e-3 (default) | scalar
Rolling resistance constant, $C_{r}$, in $\mathrm{N} / \mathrm{kN}$. ISO 28580 specifies the rolling resistance unit as one newton of tractive resistance for every kilonewtons of normal load.

## Dependencies

To enable this parameter, set Rolling Resistance to ISO 28580.
Thermal correction factor, $\mathbf{K t}$ - Thermal correction factor
0.008 (default) | scalar

Thermal correction factor, $K_{t}$, in $1 /$ degC.
Dependencies
To enable this parameter, set Rolling Resistance to ISO 28580.
Measured temperature, Tmeas - Temperature during testing
298.15 (default) | scalar

Measured ambient temperature, $T_{\text {meas }}$, near tire during tire testing, in K .

## Dependencies

To enable this parameter, set Rolling Resistance to ISO 28580.
Ambient temperature, Tamb - Temperature in application environment 298.15 (default) | scalar

Measured ambient temperature, $T_{\text {amb }}$, near tire in application environment, in K. For example, the measured ambient temperature is the ambient temperature near the tire when the vehicle is on the road.

## Dependencies

To enable this parameter, set Rolling Resistance to ISO 28580.
Input ambient temperature - Option to input ambient temperature
off (default) | on
Select to create input port Tamb to input the measured ambient temperature.
The measured ambient temperature, $T_{\text {amb }}$, is the temperature near tire in application environment, in K . For example, the measured ambient temperature is the ambient temperature near the tire when the vehicle is on the road.

## Dependencies

To enable this parameter, set Rolling Resistance to ISO 28580.

## Magic Formula

Rolling resistance torque coefficient, QSY1 - Torque coefficient 0.007 (default) | scalar

Rolling resistance torque coefficient, dimensionless.

## Dependencies

To enable this parameter, set Rolling Resistance to Magic Formula.
Longitudinal force rolling resistance coefficient, QSY2 - Force resistance coefficient 0 (default) | scalar

Longitudinal force rolling resistance coefficient, dimensionless.

## Dependencies

To enable this parameter, set Rolling Resistance to Magic Formula.
Linear rotational speed rolling resistance coefficient, QSY3 - Linear speed coefficient 0.0015 (default) | scalar

Linear rotational speed rolling resistance coefficient, dimensionless.

## Dependencies

To enable this parameter, set Rolling Resistance to Magic Formula.
Quartic rotational speed rolling resistance coefficient, QSY4 - Quartic speed coefficient 8.5e-05 (default) | scalar

Quartic rotational speed rolling resistance coefficient, dimensionless.

## Dependencies

To enable this parameter, set Rolling Resistance to Magic Formula.
Camber squared rolling resistance torque, QSY5 - Camber resistance torque
0 (default) | scalar
Camber squared rolling resistance torque, in $1 / \mathrm{rad}^{\wedge} 2$.

## Dependencies

To enable this parameter, set Rolling Resistance to Magic Formula.
Load based camber squared rolling resistance torque, QSY6 - Load resistance torque 0 (default) | scalar

Load based camber squared rolling resistance torque, in $1 / \mathrm{rad}^{\wedge} 2$.

## Dependencies

To enable this parameter, set Rolling Resistance to Magic Formula.

Normal load rolling resistance coefficient, QSY7 - Normal resistance coefficient 0.9 (default) | scalar

Normal load rolling resistance coefficient, dimensionless.

## Dependencies

To enable this parameter, set Rolling Resistance to Magic Formula.
Pressure load rolling resistance coefficient, QSY8 - Pressure resistance coefficient -0.4 (default) | scalar

Pressure load rolling resistance coefficient, dimensionless.
Dependencies
To enable this parameter, set Rolling Resistance to Magic Formula.
Rolling resistance scaling factor, lam_My - Scaling factor
1 (default) | scalar
Rolling resistance scaling factor, dimensionless.

## Dependencies

To enable this parameter, set Rolling Resistance to Magic Formula.

## Mapped

Spin axis velocity breakpoints, VxMy - Spin axis velocity breakpoints
-20:1:20 (default) | vector
Spin axis velocity breakpoints, in $\mathrm{m} / \mathrm{s}$.

## Dependencies

To enable this parameter, set Rolling Resistance to Mapped torque.
Normal force breakpoints, FzMy - Normal force breakpoints
0:200:1e4 (default)| vector
Normal force breakpoints, in N.

## Dependencies

To enable this parameter, set Rolling Resistance to Mapped torque.
Rolling resistance torque map, MyMap - Rolling resistance torque map array

Rolling resistance torque versus axle speed and normal force, in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

To enable this parameter, set Rolling Resistance to Mapped torque.

## Brake

## Static friction coefficient, mu_static - Static friction

## . 3 (default) | scalar

Static friction coefficient, specified as a scalar, dimensionless.

## Dependencies

To enable this parameter, for the Brake Type parameter, specify one of these types:

- Disc
- Drum
- Mapped


## Kinetic friction coefficient, mu_kinetic - Kinetic friction

. 2 (default) | scalar
Kinematic friction coefficient, specified as a scalar, dimensionless.

## Dependencies

To enable this parameter, for the Brake Type parameter, specify one of these types:

- Disc
- Drum
- Mapped

Disc
Disc brake actuator bore, disc_abore - Bore distance
. 05 (default) | scalar
Disc brake actuator bore, specified as a scalar, in $m$.

## Dependencies

To enable the disc brake parameters, select Disc for the Brake Type parameter.
Brake pad mean radius, Rm - Radius
. 177 (default) | scalar
Brake pad mean radius, specified as a scalar, in $m$.

## Dependencies

To enable the disc brake parameters, select Disc for the Brake Type parameter.
Number of brake pads, num_pads - Count
2 (default) | scalar
Number of brake pads, specified as a scalar, dimensionless.

## Dependencies

To enable the disc brake parameters, select Disc for the Brake Type parameter.

## Drum

## Drum brake actuator bore, disc_abore - Bore distance

0.0508 (default) | scalar

Drum brake actuator bore, specified as a scalar, in m.

## Dependencies

To enable the drum brake parameters, select Drum for the Brake Type parameter.
Shoe pin to drum center distance, drum_a - Distance
0.123 (default) | scalar

Shoe pin to drum center distance, in $m$.
Dependencies
To enable the drum brake parameters, select Drum for the Brake Type parameter.
Shoe pin center to force application point distance, drum_c - Distance
0.212 (default) | scalar

Shoe pin center to force application point distance, in m.
Dependencies
To enable the drum brake parameters, select Drum for the Brake Type parameter.
Drum internal radius, drum_r - Radius
0.15 (default) | scalar

Drum internal radius, in m.

## Dependencies

To enable the drum brake parameters, select Drum for the Brake Type parameter.
Shoe pin to pad start angle, drum_thetal - Angle
0 (default) | scalar
Shoe pin to pad start angle, in deg.
Dependencies
To enable the drum brake parameters, select Drum for the Brake Type parameter.
Shoe pin to pad end angle, drum_theta 2 - Angle
126 (default) | scalar
Shoe pin to pad end angle, in deg.

## Dependencies

To enable the drum brake parameters, select Drum for the Brake Type parameter.

## Mapped

Brake actuator pressure breakpoints, brake_p_bpt - Breakpoints

## vector

Brake actuator pressure breakpoints, in bar.

## Dependencies

To enable the mapped brake parameters, select Mapped for the Brake Type parameter.
Wheel speed breakpoints, brake_n_bpt - Breakpoints
vector
Wheel speed breakpoints, in rpm.

## Dependencies

To enable the mapped brake parameters, select Mapped for the Brake Type parameter.
Brake torque map, f_brake_t - Lookup table
array
The lookup table for the brake torque, $f_{\text {brake }}(P, N)$, is a function of applied brake pressure and wheel speed, where:

- $\quad T$ is brake torque, in $\mathrm{N} \cdot \mathrm{m}$.
- $P$ is applied brake pressure, in bar.
- $N$ is wheel speed, in rpm.



## Dependencies

To enable the mapped brake parameters, select Mapped for the Brake Type parameter.

## Vertical

Nominal normal force, FNOMIN - Force
2000 (default) | scalar
Nominal rated wheel load along wheel-fixed $z$-axis, in N .

## Dependencies

To enable this parameter, set either:

- Longitudinal Force to Magic Formula pure longitudinal slip.
- Rolling Resistance to Magic Formula.

Nominal rated load scaling factor, lam_Fzo - Factor
1 (default) | scalar
Nominal rated load scaling factor, dimensionless. Used to scale the normal for specific applications and load conditions.

## Dependencies

To enable this parameter, set Longitudinal Force to Magic Formula pure longitudinal slip.
Wheel and unsprung mass, $\mathbf{m}$ - Mass
10 (default) | scalar
Wheel and unsprung mass, in kg. Used in the vertical motion calculations.

## Dependencies

To enable this parameter, set Vertical Motion to Mapped stiffness and damping.
Initial deflection, zo - Deflection
0 (default) | scalar
Initial axle displacement along wheel-fixed $z$-axis, in m .

## Dependencies

To enable this parameter, set Vertical Motion to Mapped stiffness and damping.
Initial velocity, zdoto - Velocity
0 (default) | scalar
Initial axle velocity along wheel-fixed $z$-axis, in m .

## Dependencies

To enable this parameter, set Vertical Motion to Mapped stiffness and damping.
Gravitational acceleration, $\mathbf{g}$ - Gravity
9.81 (default) | scalar

Gravitational acceleration, in $\mathrm{m} / \mathrm{s}^{\wedge} 2$.

## Dependencies

To enable this parameter, set Vertical Motion to Mapped stiffness and damping.
Ground displacement, Gndz - Displacement
0 (default) | scalar
Ground displacement, Grndz , along negative wheel-fixed $z$-axis, in m .


## Dependencies

To enable this parameter, set Vertical Motion to Mapped stiffness and damping.

## Mapped Stiffness and Damping

Vertical deflection breakpoints, zFz - Breakpoints
[0.01 .1] (default)|vector
Vector of sidewall deflection breakpoints corresponding to the force table, in m .

## Dependencies

To enable this parameter, set Vertical Motion to Mapped stiffness and damping.
Pressure breakpoints, pFz - Breakpoints
[10000 1000000] (default) | vector
Vector of pressure data points corresponding to the force table, in Pa.

## Dependencies

To enable this parameter, set Vertical Motion to Mapped stiffness and damping.
Force due to deflection, Fzz - Force
[0 le3 le4; 0 le4 le5] (default)|vector
Force due to sidewall deflection and pressure along wheel-fixed $z$-axis, in N .

## Dependencies

To enable this parameter, set Vertical Motion to Mapped stiffness and damping.

## Vertical velocity breakpoints, zdotFz - Breakpoints

[-20 0 20] (default) |scalar
Vector of sidewall velocity breakpoints corresponding to the force due to velocity table, in $m$.

## Dependencies

To enable this parameter, set Vertical Motion to Mapped stiffness and damping.

## Force due to velocity, Fzzdot - Force

[500 0 -500;250 0 -250] (default) |array
Force due to sidewall velocity and pressure along wheel-fixed $z$-axis, in N .

## Dependencies

To enable this parameter, set Vertical Motion to Mapped stiffness and damping.

## Simulation Setup

Minimum normal force, FZMIN - Minimum normal force
0 (default) | scalar
Minimum normal force, in N. Used with all vertical force calculations.
Maximum normal force, FZMAX - Maximum normal force 10000 (default) | scalar

Maximum normal force, in N. Used with all vertical force calculations.
Max allowable slip ratio (absolute), kappamax - Ratio
1.5 (default) | scalar

Maximum allowable absolute slip ratio, dimensionless.
Velocity tolerance used to handle low velocity situations, VXLOW - Tolerance
1 (default) | scalar
Velocity tolerance used to handle low-velocity situations, in m/s.
Minimum ambient temperature, TMIN - Minimum ambient temperature
0 (default) | scalar
Minimum ambient temperature, $T_{\text {MIN }}$, in K .

## Dependencies

To enable this parameter, set Rolling Resistance to ISO 28580.
Maximum ambient temperature, TMAX - Maximum ambient temperature
400 (default) | scalar
Maximum ambient temperature, $T_{M A X}$, in K .

## Dependencies

To enable this parameter, set Rolling Resistance to ISO 28580.

## Version History

Introduced in R2017a

## References

[1] Highway Tire Committee. Stepwise Coastdown Methodology for Measuring Tire Rolling Resistance. Standard J2452_199906. Warrendale, PA: SAE International, June 1999.
[2] Pacejka, H. B. Tire and Vehicle Dynamics. 3rd ed. Oxford, United Kingdom: SAE and ButterworthHeinemann, 2012.
[3] Schmid, Steven R., Bernard J. Hamrock, and Bo O. Jacobson. "Chapter 18: Brakes and Clutches." Fundamentals of Machine Elements, SI Version. 3rd ed. Boca Raton, FL: CRC Press, 2014.
[4] Shigley, Joseph E., and Larry Mitchel. Mechanical Engineering Design. 4th ed. New York, NY: McGraw Hill, 1983.
[5] ISO 28580:2018. Passenger car, truck and bus tyre rolling resistance measurement method -Single point test and correlation of measurement results. ISO (International Organization for Standardization), 2018.

## Extended Capabilities

## C/C++ Code Generation

Generate C and C++ code using Simulink ${ }^{\circledR}$ Coder ${ }^{\mathrm{TM}}$.

## See Also

Drive Cycle Source | Longitudinal Driver | Combined Slip Wheel 2DOF

## Combined Slip Wheel 2DOF

Combined slip 2DOF wheel with disc, drum, or mapped brake


## Libraries:

Vehicle Dynamics Blockset / Wheels and Tires

## Description

Combined Slip Wheel 2DOF incorporates two degrees of freedom (DOF's) of wheel motion, and 6 DOF's of tire forcing, in combined longitudinal and lateral slip conditions.

- Wheel motion: Rotation about spin axis, and vertical displacement.
- Tire forces and moments: Fx, Fy, and Fz; Mx, My, and Mz.

It models the tire using the Magic Formula. ${ }^{[1]}$ and ${ }^{[2]}$ Set the Magic Formula coefficients by either importing your own file (in MF 6.X format), or selecting one of the resident datasets from the Global Center for Automotive Performance Simulation (GCAPS).

Use this block in simulations like the following.

- Vehicle braking and acceleration, including rolling resistance.
- Vehicle ride motions, including effects of suspension modes.
- Maneuvers with combined lateral and longitudinal slip, such as lateral vehicle motion and yaw stability.

Use the Tire type parameter to either import a tire coefficient file or select a resident one. These are known generically as ".tir" files. Manufacturers and testing agencies commonly use these to communicate tire data.

| Goal | Action |
| :---: | :---: |
| Import your own external file containing Magic Formula coefficients, and use them to drive the empirical equations modeling the tire ${ }^{1 \text { and } 2}$. The file you import can be a .mat, .tir, or .txt type, and must contain parameter names corresponding to those in the tire block. | Update the block parameters with fitting coefficients from a file: <br> Set Tire type to External file. <br> On the Wheel and Tire Parameters > External tire source pane, select Select file. <br> 3 Select the tire coefficient file. <br> 4 Select Update mask values from file. In the dialog box that prompts you for confirmation, click OK. The block updates the parameters. <br> 5 Select Apply. |
| Select one of the Magic Formula coefficient sets resident in the block to drive the empirical equations modeling the tire ${ }^{1}$ and 2 . These fitted tire data sets are provided by the Global Center for Automotive Performance Simulation (GCAPS). | Update the applicable block parameters with GCAPS fitted tire data: <br> 1 Set Tire type to the tire that you want to implement. Options include: <br> - Light passenger car 205/60R15 <br> - Mid-size passenger car 235/45R18 <br> - Performance car 225/40R19 <br> - SUV 265/50R20 <br> - Light truck 275/65R18 <br> - Commercial truck 295/75R22.5 <br> 2 Select Update applicable Tire Parameters with tire type values. On the Tire Parameters tab, the block updates the applicable parameters, including Wheel width, Rim radius, and Wheel mass. <br> 3 Select Apply. |

Use the Brake Type parameter to select the brake.

| Action | Brake Type Setting |
| :--- | :--- |
| No braking | None |
| Implement brake that converts the <br> brake cylinder pressure into a <br> braking force | Disc |
| Implement simplex drum brake that <br> converts the applied force and brake <br> geometry into a net braking torque | Drum |
| Implement lookup table that is a <br> function of the wheel speed and <br> applied brake pressure | Mapped |

## Rotational Wheel Dynamics

The block calculates the inertial response of the wheel subject to:

- Axle losses
- Brake and drive torque
- Tire rolling resistance
- Ground contact through the tire-road interface

To implement the Magic Formula, the block uses these equations from the cited references:

| Calculation | Equations |
| :--- | :--- |
| Longitudinal force | Tire and Vehicle Dynamics ${ }^{2}$ equations 4.E9 through 4.E57 |
| Lateral force - pure <br> sideslip | Tire and Vehicle Dynamics ${ }^{2}$ equations 4.E19 through 4.E30 |
| Lateral force - combined <br> slip | Tire and Vehicle Dynamics ${ }^{2}$ equations 4.E58 through 4.E67 |
| Vertical dynamics | Tire and Vehicle Dynamics ${ }^{2}$ equations 4.E68, 4.E1, 4.E2a, and 4.E2b |
| Overturning couple | Tire and Vehicle Dynamics ${ }^{2}$ equation 4.E69 <br> Rolling resistance <br> - An improved Magic Formula/Swift tyre model that can handle inflation <br> - Tire and Vehicle Dynamics ${ }^{2}$ equation 4.E70 <br> Aligning moment <br> Aligning torque - <br> combined slipTire and Vehicle Dynamics ${ }^{2}$ equation 4.E31 through 4.E49 <br> If you clear Include turn slip, the block sets some of these equations to 1. |

The input torque is the summation of the applied axle torque, braking torque, and moment arising from the combined tire torque.

$$
T_{i}=T_{a}-T_{b}+T_{d}
$$

For the moment arising from the combined tire torque, the block implements tractive wheel forces and rolling resistance with first-order dynamics. The rolling resistance has a time constant parameterized in terms of a relaxation length.

$$
T_{d}(s)=\frac{1}{\frac{L_{e}}{|\omega| R_{e}} s+1}+\left(F_{\chi} R_{e}+M_{y}\right)
$$

Braking torque is based on an idealized dry clutch friction model (if brakes are selected). Depending on the lockup condition, the block implements these friction and dynamic models:

| If | Lockup <br> Conditio <br> n | Friction Model | Dynamic Model |
| :--- | :--- | :--- | :--- |
| $\omega \neq 0$ <br> or <br> $T_{S}<\left\|T_{i}+T_{f}-\omega b\right\|$ | Unlocke <br> d | $T_{f}=T_{k}$, <br> where <br> $T_{k}=F_{c} R_{e f f} \mu_{k} \tanh \left[4\left(-\omega_{d}\right)\right]$ <br> $T_{S}=F_{c} R_{e f f} \mu_{s}$ <br> $R_{e f f}=\frac{2\left(R_{o} 3-R_{i} 3\right)}{3\left(R_{o}^{2}-R_{i} 2\right)}$ | $\dot{\omega} J=-\omega b+T_{i}+T_{o}$ |
| $\omega=0$ <br> and <br> $T_{S} \geq\left\|T_{i}+T_{f}-\omega b\right\|$ | Locked | $T_{f}=T_{s}$ | $\omega=0$ |

The equations use these variables.

| $\omega$ | Wheel angular velocity |
| :--- | :--- |
| $a$ | Velocity independent force component |
| $b$ | Linear velocity force component |
| $c$ | Quadratic velocity force component |
| $L_{e}$ | Tire relaxation length |
| $J$ | Moment of inertia |
| $M_{y}$ | Rolling resistance torque |
| $T_{a}$ | Applied axle torque about wheel spin axis |
| $T_{b}$ | Braking torque |
| $T_{d}$ | Combined tire torque |
| $T_{f}$ | Frictional torque |
| $T_{i}$ | Net input torque |
| $T_{k}$ | Kinetic frictional torque |
| $T_{o}$ | Net output torque |
| $T_{s}$ | Static frictional torque |
| $F_{c}$ | Applied clutch force |
| $F_{x}$ | Longitudinal force developed by the tire road interface due to slip |
| $R_{e f f}$ | Effective clutch radius |
| $R_{o}$ | Annular disk outer radius |
| $R_{i}$ | Annular disk inner radius |
| $R_{e}$ | Effective tire radius while under load and for a given pressure |
| $V_{x}$ | Longitudinal axle velocity |
| $F_{z}$ | Vehicle normal force |
| $\alpha$ | Tire pressure exponent |
| $\beta$ | Normal force exponent |


| $p_{i}$ | Tire pressure |
| :--- | :--- |
| $\mu_{s}$ | Coefficient of static friction |
| $\mu_{k}$ | Coefficient of kinetic friction |

## Tire and Wheel Coordinate Systems

To resolve the forces and moments, the block uses the Z-Up orientation of the tire and wheel coordinate systems.

- Tire coordinate system axes $\left(X_{T}, Y_{T}, Z_{T}\right)$ are fixed in a reference frame attached to the tire. The origin is at the tire contact with the ground.
- Wheel coordinate system axes ( $X_{W}, Y_{W}, Z_{W}$ ) are fixed in a reference frame attached to the wheel. The origin is at the wheel center.


## Z-Up Orientation ${ }^{1}$



## Brakes

## Disc

If you specify the Brake Type parameter as Disc, the block implements a disc brake. This figure shows the side and front views of a disc brake.

[^1]

A disc brake converts brake cylinder pressure from the brake cylinder into force. The disc brake applies the force at the brake pad mean radius.

The block uses these equations to calculate brake torque for the disc brake.

$$
\begin{aligned}
& T= \begin{cases}\frac{\mu P_{\pi B} B_{a} 2 R_{m} N_{\text {pads }}}{4} & \text { when } N \neq 0 \\
\frac{\mu_{\text {static } P \pi B_{a} 2 R_{m} N_{\text {pads }}}^{4}}{2} & \text { when } N=0\end{cases} \\
& R m=\frac{R o+R i}{2}
\end{aligned}
$$

The equations use these variables.

| Variable | Value |
| :--- | :--- |
| $T$ | Brake torque |
| $P$ | Applied brake pressure |
| $N$ | Wheel speed |
| $N_{\text {pads }}$ | Number of brake pads in disc brake assembly |
| $\mu_{\text {static }}$ | Disc pad-rotor coefficient of static friction |
| $\mu$ | Disc pad-rotor coefficient of kinetic friction |
| $B_{a}$ | Brake actuator bore diameter |
| $R_{m}$ | Mean radius of brake pad force application on brake rotor |


| Variable | Value |
| :--- | :--- |
| $R_{o}$ | Outer radius of brake pad |
| $R_{i}$ | Inner radius of brake pad |

## Drum

If you specify the Brake Type parameter as Drum, the block implements a static (steady-state) simplex drum brake. A simplex drum brake consists of a single two-sided hydraulic actuator and two brake shoes. The brake shoes do not share a common hinge pin.

The simplex drum brake model uses the applied force and brake geometry to calculate a net torque for each brake shoe. The drum model assumes that the actuators and shoe geometry are symmetrical for both sides, allowing a single set of geometry and friction parameters to be used for both shoes.

The block implements equations that are derived from these equations in Fundamentals of Machine Elements.

$$
\begin{aligned}
& T_{\text {rshoe }}=\left(\frac{\pi \mu c r\left(\cos \theta_{2}-\cos \theta_{1}\right) B_{a}{ }^{2}}{2 \mu\left(2 r\left(\cos \theta_{2}-\cos \theta_{1}\right)+a\left(\cos ^{2} \theta_{2}-\cos ^{2} \theta_{1}\right)\right)+\operatorname{ar}\left(2 \theta_{1}-2 \theta_{2}+\sin 2 \theta_{2}-\sin 2 \theta_{1}\right)}\right) P \\
& T_{\text {lshoe }}=\left(\frac{\pi \mu c r\left(\cos \theta_{2}-\cos \theta_{1}\right) B_{a} 2}{-2 \mu\left(2 r\left(\cos \theta_{2}-\cos \theta_{1}\right)+a\left(\cos ^{2} \theta_{2}-\cos ^{2} \theta_{1}\right)\right)+\operatorname{ar}\left(2 \theta_{1}-2 \theta_{2}+\sin 2 \theta_{2}-\sin 2 \theta_{1}\right)}\right) P \\
& T= \begin{cases}T_{\text {rshoe }}+T_{\text {lshoe }} & \text { when } N \neq 0 \\
\left(T_{\text {rshoe }}+T_{\text {lshoe }}\right) \frac{\mu_{\text {static }}}{\mu} & \text { when } N=0\end{cases}
\end{aligned}
$$



The equations use these variables.

| Variable | Value |
| :--- | :--- |
| $T$ | Brake torque |
| $P$ | Applied brake pressure |
| $N$ | Wheel speed |
| $\mu_{\text {static }}$ | Disc pad-rotor coefficient of static friction |
| $\mu$ | Disc pad-rotor coefficient of kinetic friction |
| $T_{\text {rshoe }}$ | Right shoe brake torque |
| $T_{\text {lshoe }}$ | Left shoe brake torque |
| $a$ | Distance from drum center to shoe hinge pin center |
| $c$ | Distance from shoe hinge pin center to brake actuator connection on brake shoe |
| $r$ | Drum internal radius |
| $B_{a}$ | Brake actuator bore diameter |
| $\Theta_{1}$ | Angle from shoe hinge pin center to start of brake pad material on shoe |
| $\Theta_{2}$ | Angle from shoe hinge pin center to end of brake pad material on shoe |
| Mapped |  |

If you specify the Brake Type parameter as Mapped, the block uses a lookup table to determine the brake torque.

$$
T=\left\{\begin{array}{lr}
f_{\text {brake }}(P, N) & \text { when } N \neq 0 \\
\left(\frac{\mu_{\text {static }}}{\mu}\right) f_{\text {brake }}(P, N) & \text { when } N=0
\end{array}\right.
$$

The equations use these variables.

| Variable | Value |
| :--- | :--- |
| $T$ | Brake torque |
| $f_{\text {brake }}(P, N)$ | Brake torque lookup table |
| $P$ | Applied brake pressure |
| $N$ | Wheel speed |
| $\mu_{\text {static }}$ | Friction coefficient of drum pad-face interface under static conditions |
| $\mu$ | Friction coefficient of disc pad-rotor interface |

The lookup table for the brake torque, $f_{\text {brake }}(P, N)$, is a function of applied brake pressure and wheel speed, where:

- $T$ is brake torque, in $\mathrm{N} \cdot \mathrm{m}$.
- $P$ is applied brake pressure, in bar.
- $N$ is wheel speed, in rpm.



## Ports

## Input

BrkPrs - Brake pressure
scalar | N-by-1 vector
Brake pressure, in Pa.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

## Dependencies

To enable this port, set the Brake Type parameter, to one of these types:

- Disc
- Drum
- Mapped

AxITrq - Axle torque
scalar | $N$-by-1 vector
Axle torque, $T_{a}$, about wheel spin axis, in $\mathrm{N} \cdot \mathrm{m}$.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

Vx - Longitudinal velocity
scalar | $N$-by-1 vector
Axle longitudinal velocity, $V_{x}$, along tire-fixed $x$-axis, in $\mathrm{m} / \mathrm{s}$.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.
$\mathbf{V y}$ - Lateral velocity
scalar | $N$-by-1 vector
Axle lateral velocity, $V_{y}$, along tire-fixed $y$-axis, in $\mathrm{m} / \mathrm{s}$.

Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

Camber - Inclination angle
scalar | $N$-by-1 vector
Camber angle, $\gamma$, or inclination angle, $\varepsilon$, in rad.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

YawRate - Tire angular velocity
scalar | $N$-by- 1 vector
Tire angular velocity, $r$, about the tire-fixed $z$-axis (yaw rate), in rad/s.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

Prs - Tire inflation pressure
scalar | $N$-by- 1 vector
Tire inflation pressure, $p_{i}$, in Pa.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

Gnd - Ground displacement
scalar | $N$-by-1 vector
Ground displacement along tire-fixed $z$-axis, in m . Positive input produces wheel lift.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

Fext - Axle force applied to tire
scalar | N-by-1 vector
Axle force applied to tire, $F_{\text {ext }}$, along vehicle-fixed $z$-axis (positive input compresses the tire), in N .
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

ScaleFctrs - Scale factors
27-by-N array
Magic Formula scale factor array. Array dimensions are 27 by the number of wheels, $N$.
The Magic Formula equations use scale factors to account for static or simulation run-time variations. Nominally, most are set to 1.

| Array Element | Variable | Scale Factor |
| :--- | :--- | :--- |
| ScaleFctrs(1,1) | lam_Fzo | Nominal load |
| ScaleFctrs(2,1) | lam_mux | Longitudinal peak friction coefficient |


| Array Element | Variable | Scale Factor |
| :---: | :---: | :---: |
| ScaleFctrs(3,1) | lam_muy | Lateral peak friction coefficient |
| ScaleFctrs (4,1) | lam_muV | Slip speed, Vs, decaying friction |
| ScaleFctrs $(5,1)$ | lam_Kxkappa | Brake slip stiffness |
| ScaleFctrs (6,1) | lam_Kyalpha | Cornering stiffness |
| ScaleFctrs(7,1) | lam_Cx | Longitudinal shape factor |
| ScaleFctrs $(8,1)$ | lam_Cy | Lateral shape factor |
| ScaleFctrs (9,1) | lam_Ex | Longitudinal curvature factor |
| ScaleFctrs(10,1) | lam_Ey | Lateral curvature factor |
| ScaleFctrs(11,1) | lam_Hx | Longitudinal horizontal shift |
| ScaleFctrs(12,1) | lam_Hy | Lateral horizontal shift |
| ScaleFctrs(13,1) | lam_Vx | Longitudinal vertical shift |
| ScaleFctrs(14,1) | lam_Vy | Lateral vertical shift |
| ScaleFctrs(15,1) | lam_Kygamma | Camber force stiffness |
| ScaleFctrs(16,1) | lam_Kzgamma | Camber torque stiffness |
| ScaleFctrs(17,1) | lam_t | Pneumatic trail (effecting aligning torque stiffness) |
| ScaleFctrs(18,1) | lam_Mr | Residual torque |
| ScaleFctrs $(19,1)$ | lam_xalpha | Alpha influence on Fx (kappa) |
| ScaleFctrs(20,1) | lam_ykappa | Kappa influence on Fy (alpha) |
| ScaleFctrs $(21,1)$ | lam_Vykappa | Induced ply steer Fy |
| ScaleFctrs(22,1) | lam_s | Moment arm of FX |
| ScaleFctrs $(23,1)$ | lam_Cz | Radial tire stiffness |
| ScaleFctrs $(24,1)$ | lam_Mx | Overturning couple stiffness |
| ScaleFctrs $(25,1)$ | lam_VMx | Overturning couple vertical shift |
| ScaleFctrs $(26,1)$ | lam_My | Rolling resistance moment |
| ScaleFctrs $(27,1)$ | lam_Mphi | Parking torque Mz |

## Output

## Info - Block data

bus
Block data, returned as a bus signal containing these block values.

| Signal | Description | Units |
| :--- | :--- | :--- |
| AxlTrq | Axle torque about wheel-fixed $y$-axis | $\mathrm{N} \cdot \mathrm{m}$ |
| Omega | Wheel angular velocity about wheel-fixed $y$-axis | $\mathrm{rad} / \mathrm{s}$ |
| Fx | Longitudinal vehicle force along tire-fixed $x$-axis | N |
| Fy | Lateral vehicle force along tire-fixed $y$-axis | N |


| Signal | Description | Units |
| :--- | :--- | :--- |
| Fz | Vertical vehicle force along tire-fixed $z$-axis | N |
| Mx | Overturning moment about tire-fixed $x$-axis | $\mathrm{N} \cdot \mathrm{m}$ |
| My | Rolling resistance torque about tire-fixed $y$-axis | $\mathrm{N} \cdot \mathrm{m}$ |
| Mz | Aligning moment about tire-fixed $z$-axis | $\mathrm{N} \cdot \mathrm{m}$ |
| Vx | Vehicle longitudinal velocity along tire-fixed $x$-axis | $\mathrm{m} / \mathrm{s}$ |
| Vy | Vehicle lateral velocity along tire-fixed $y$-axis | $\mathrm{m} / \mathrm{s}$ |
| Re | Loaded effective radius | m |
| Kappa | Longitudinal slip ratio | NA |
| Alpha | Side slip angle | rad |
| a | Contact patch half length | m |
| b | Contact patch half width | m |
| Gamma | Camber angle | rad |
| psidot |  |  |
| rate $)$ |  |  |

Omega - Wheel angular velocity
scalar | N-by-1 vector
Wheel angular velocity, $\omega$, about wheel-fixed $y$-axis, in rad/s.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

Fx - Longitudinal axle force
scalar | $N$-by-1 vector
Longitudinal force acting on axle, $F_{x}$, along tire-fixed $x$-axis, in N. Positive force acts to move the vehicle forward.

Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

## Fy - Lateral axle force

scalar | $N$-by-1 vector
Lateral force acting on axle, $F_{y}$, along tire-fixed $y$-axis, in N .

Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

Fz - Vertical axle force
scalar | $N$-by-1 vector
Vertical force acting on axle, $F_{z}$, along tire-fixed $z$-axis, in N .
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

Mx - Overturning moment
scalar | $N$-by-1 vector
Longitudinal moment acting on axle, $M_{x}$, about tire-fixed $x$-axis, in $\mathrm{N} \cdot \mathrm{m}$.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

My - Rolling resistive moment
scalar | N-by-1 vector
Lateral moment acting on axle, $M_{y}$, about tire-fixed $y$-axis, in $\mathrm{N} \cdot \mathrm{m}$.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.
$\mathbf{M z}$ - Aligning moment
scalar | $N$-by-1 vector
Vertical moment acting on axle, $M_{z}$, about tire-fixed $z$-axis, in $\mathrm{N} \cdot \mathrm{m}$.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

## Parameters

## Block Options

Tire Type - Select type

```
External file (default)| Light passenger car 205/60R15|Mid-size passenger car
235/45R18|Performance car 225/40R19|SUV 265/50R20|Light truck 275/65R18|
Commercial truck 295/75R22.5
```

Use the Tire type parameter to either import a tire coefficient file or select a resident one. These are known generically as ".tir" files. Manufacturers and testing agencies commonly use these to communicate tire data.

| Goal | Action |
| :---: | :---: |
| Import your own external file containing Magic Formula coefficients, and use them to drive the empirical equations modeling the tire ${ }^{1 \text { and } 2}$. The file you import can be a .mat, .tir, or .txt type, and must contain parameter names corresponding to those in the tire block. | Update the block parameters with fitting coefficients from a file: <br> 1 Set Tire type to External file. <br> 2 On the Wheel and Tire Parameters > External tire source pane, select Select file. <br> 3 Select the tire coefficient file. <br> 4 Select Update mask values from file. In the dialog box that prompts you for confirmation, click OK. The block updates the parameters. <br> 5 Select Apply. |
| Select one of the Magic Formula coefficient sets resident in the block to drive the empirical equations modeling the tire ${ }^{1 \text { and } 2}$. These fitted tire data sets are provided by the Global Center for Automotive Performance Simulation (GCAPS). | Update the applicable block parameters with GCAPS fitted tire data: <br> 1 Set Tire type to the tire that you want to implement. Options include: <br> - Light passenger car 205/60R15 <br> - Mid-size passenger car 235/45R18 <br> - Performance car 225/40R19 <br> - SUV 265/50R20 <br> - Light truck 275/65R18 <br> - Commercial truck 295/75R22.5 <br> 2 Select Update applicable Tire Parameters with tire type values. On the Tire Parameters tab, the block updates the applicable parameters, including Wheel width, Rim radius, and Wheel mass. <br> 3 Select Apply. |

Brake type - Brake type
None | Disc| Drum | Mapped
Use the Brake Type parameter to select the brake.

| Action | Brake Type Setting |
| :--- | :--- |
| No braking | None |
| Implement brake that converts the <br> brake cylinder pressure into a <br> braking force | Disc |
| Implement simplex drum brake that <br> converts the applied force and brake <br> geometry into a net braking torque | Drum |
| Implement lookup table that is a <br> function of the wheel speed and <br> applied brake pressure | Mapped |

## Vertical Motion - Vertical motion model <br> Magic Formula (default) | None

Type of vertical motion. By default, the block uses the Magic Formula to calculate the vertical motion of the tire.

Ply steer - Include ply steer
on (default) | off
Select to include ply steer in the Magic Formula equations.
By default, the blocks include ply steer and turn slip in the Magic Formula equations. The equations are fit to flat-belt test data and predict a number of tire effects, including ply steer and turn slip. Consider removing the effects if your:

- Test data does not include ply steer or turn slip data.
- Analysis does not require ply steer or turn slip effects.

If you clear Ply steer, the block internally sets these parameters to 0 :

- Vertical shift of overturning moment, QSX1
- Combined slip Fx shift factor reduction, RHX1
- Efy curvature constant camber dependency, PEY3
- SHY horizontal shift at FZNOM, PHY1
- SHY variation with load, PHY2
- Svy/Fz vertical shift at FZNOM, PVY1
- Svy/Fz variation with load, PVY2
- Fy shift reduction with slip angle, RBY3
- Slip ratio side force Svyk/Muy*Fz at FZNOM, RVY1
- Side force Svyk/Muy*Fz variation with load, RVY2
- Bpt slope variation with camber, QBZ4
- Dpt peak trail variation with camber, QDZ3
- Dmr peak residual torque, QDZ6
- Dmr peak residual torque variation with load, QDZ7
- Ept variation with sign of alpha-t, QEZ4
- Sht horizontal trail shift at FZNOM, QHZ1
- Sht variation with load, QHZ2
- Nominal value of s/R0: effect of Fx on Mz, SSZ1

Turn slip - Include turn slip
on (default) | off
Select to include ply steer in Magic Formula equations.
By default, the blocks include ply steer and turn slip in the Magic Formula equations. The equations are fit to flat-belt test data and predict a number of tire effects, including ply steer and turn slip. Consider removing the effects if your:

- Test data does not include ply steer or turn slip data.
- Analysis does not require ply steer or turn slip effects.

If you clear Turn slip, the block internally:

- Sets the Magic Formula turn slip equations to 1. Specifically, equations 4.E77, 4.E79, 4.E81, 4.E83, 4.E84, 4.E92, 4.E102, 4.E101, and 4.E105.².
- Uses Magic Formula terms that effect horizontal shift.
- Uses Magic Formula small turn slip values in 4.E27².


## Brake

Static friction coefficient, mu_static - Static friction coefficient
0.3 (default) | scalar | $N$-by-1 vector

Static friction coefficient, specified as a scalar or $N$-by- 1 vector, dimensionless. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other brake parameters.
$N$ is the number of wheels and must match the input signal dimensions.

## Dependencies

To enable this parameter, set Brake Type to Disc, Drum, or Mapped

## Kinetic friction coefficient, mu_kinetic - Kinetic friction

## 0.2 (default) | scalar | $N$-by-1 vector

Kinematic friction coefficient, specified as a scalar or $N$-by-1 vector, dimensionless. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other brake parameters.
$N$ is the number of wheels and must match the input signal dimensions.

## Dependencies

To enable this parameter, set Brake Type to Disc, Drum, or Mapped

## Disc

## Disc brake actuator bore, disc_abore - Bore distance

0.05 (default) | scalar | $N$-by-1 vector

Disc brake actuator bore, specified as a scalar or $N$-by- 1 vector, in $m$. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other brake parameters.
$N$ is the number of wheels and must match the input signal dimensions.

## Dependencies

To enable this parameter, set Brake Type to Disc.
Brake pad mean radius, Rm - Radius
0.177 (default) | scalar | $N$-by-1 vector

Brake pad mean radius, specified as a scalar or $N$-by-1 vector, in $m$. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other brake parameters.
$N$ is the number of wheels and must match the input signal dimensions.

## Dependencies

To enable this parameter, set Brake Type to Disc.
Number of brake pads, num_pads - Number of brake pads
2 (default) | scalar $\mid N$-by-1 vector
Number of brake pads, specified as a scalar or $N$-by-1 vector, dimensionless. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other brake parameters.
$N$ is the number of wheels and must match the input signal dimensions.

## Dependencies

To enable this parameter, set Brake Type to Disc.

## Drum

## Drum brake actuator bore, disc_abore - Bore distance

0.0508 (default) | scalar | $N$-by-1 vector

Drum brake actuator bore, specified as a scalar or $N$-by- 1 vector, in m. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other brake parameters.
$N$ is the number of wheels and must match the input signal dimensions.

## Dependencies

To enable this parameter, set Brake Type to Drum.
Shoe pin to drum center distance, drum_a - Shoe pin to drum center distance
0.123 (default) | scalar

Shoe pin to drum center distance, in m.

## Dependencies

To enable this parameter, set Brake Type to Drum.
Shoe pin center to force application point distance, drum_c - Shoe pin center to force application point distance
0.212 (default) | scalar

Shoe pin center to force application point distance, in m.

## Dependencies

To enable this parameter, set Brake Type to Drum.

Drum internal radius, drum_r - Drum internal radius
0.15 (default) | scalar

Drum internal radius, in $m$.

## Dependencies

To enable this parameter, set Brake Type to Drum.
Shoe pin to pad start angle, drum_thetal - Shoe pin to pad start angle
0 (default) | scalar
Shoe pin to pad start angle, in deg.

## Dependencies

To enable this parameter, set Brake Type to Drum.
Shoe pin to pad end angle, drum_theta 2 - Shoe pin to pad end angle 126 (default) | scalar

Shoe pin to pad end angle, in deg.

## Dependencies

To enable this parameter, set Brake Type to Drum.
Mapped
Brake actuator pressure breakpoints, brake_p_bpt - Brake actuator pressure breakpoints vector

Brake actuator pressure breakpoints, in bar.

## Dependencies

To enable this parameter, set Brake Type to Mapped.
Wheel speed breakpoints, brake_n_bpt - Wheel speed breakpoints
vector
Wheel speed breakpoints, in rpm.

## Dependencies

To enable this parameter, set Brake Type to Mapped.
Brake torque map, f_brake_t - Lookup table for brake torque array

The lookup table for the brake torque, $f_{\text {brake }}(P, N)$, is a function of applied brake pressure and wheel speed, where:

- $\quad T$ is brake torque, in $\mathrm{N} \cdot \mathrm{m}$.
- $P$ is applied brake pressure, in bar.
- $N$ is wheel speed, in rpm.



## Dependencies

To enable this parameter, set Brake Type to Mapped.

## Tire

Tire file or object, tireParamSet - Tire file
vdynPassCar.mat (default)|.tir|.txt
Tire file .tir or object containing empirical data to model tire longitudinal and lateral behavior with the Magic Formula. If you provide an .txt file, make sure the file contains names that correspond to the block parameters.

Update the block parameters with fitting coefficients from a file:
1 Set Tire type to External file.
2 On the Wheel and Tire Parameters > External tire source pane, select Select file.
3 Select the tire coefficient file.
4 Select Update mask values from file. In the dialog box that prompts you for confirmation, click OK. The block updates the parameters.
5 Select Apply.

## Simulation

Maximum pressure, PRESMAX - Maximum pressure
1003118 (default) | scalar
Maximum pressure, PRESMAX, in Pa.
Minimum pressure, PRESMIN - Minimum pressure
9982 (default) | scalar
Minimum pressure, PRESMIN, in Pa.

## Maximum normal force, FZMAX - Force

10000 (default) | scalar
Maximum normal force, FZMAX, in N.
Minimum normal force, FZMIN - Force
100 (default) | scalar

Minimum normal force, FZMIN, in N.

## Velocity tolerance used to handle low velocity situations, VXLOW - Tolerance

0.1 (default) | scalar

Velocity tolerance used to handle low velocity situations, VXLOW, in m/s.
Max allowable slip ratio (absolute), KPUMAX - Max allowable slip ratio 0.999 (default) | scalar

Max allowable slip ratio (absolute), KPUMAX, dimensionless.
Minimum allowable slip ratio (absolute), KPUMIN - Minimum allowable slip ratio -0. 999 (default) | scalar

Minimum allowable slip ratio (absolute), KPUMIN, dimensionless.
Max allowable slip angle (absolute), ALPMAX - Max allowable slip angle
1.5708 (default) | scalar

Max allowable slip angle (absolute), ALPMAX, in rad.
Minimum allowable slip angle (absolute), ALPMIN - Minimum allowable slip angle

- 1.5708 (default) | scalar

Minimum allowable slip angle (absolute), ALPMIN, in rad.
Maximum allowable camber angle, CAMMAX - Maximum allowable camber angle 0.173 | scalar

Maximum allowable camber angle CAMMAX, in rad.
Minimum allowable camber angle, CAMMIN - Minimum allowable camber angle -0.173 | scalar

Minimum allowable camber angle, CAMMIN, in rad.
Nominal longitudinal speed, LONGVL - Speed
16.7 (default) | scalar

Nominal longitudinal speed, $L O N G V L$, in $\mathrm{m} / \mathrm{s}$.

## Wheel

Initial rotational velocity, omegao - Initial rotational velocity
scalar | $N$-by-1 vector
Initial rotational velocity, specified as a scalar or $N$-by- 1 vector, in rad/s. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other rotational parameters.
$N$ is the number of wheels and must match the input signal dimensions.
Rotational damping, br - Rotational damping
scalar | N-by-1 vector

Rotational damping, specified as a scalar or $N$-by-1 vector, in $N \cdot m \cdot s / r a d$. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other rotational parameters.
$N$ is the number of wheels and must match the input signal dimensions.
Unloaded radius, UNLOADED_RADIUS - Radius
0.309 (default) | scalar

Unloaded radius, UNLOADED_RADIUS, in m.
Nominal pressure, NOMPRES - Pressure
224006 (default) | scalar
Nominal pressure, NOMPRES, in Pa.
Nominal normal force, FNOMIN - Force
4025 (default) | scalar
Nominal normal force, FNOMIN, in N.
Wheel width, WIDTH - Wheel width
scalar
Wheel width, WIDTH, in m.
Rim radius, RIM_RADIUS - Radius
. 19 (default) | scalar
Rim radius, RIM_RADIUS, in m.

## Inertial

Wheel mass, MASS - Mass
scalar | N-by-1 vector
Wheel mass, specified as a scalar or $N$-by-1 vector, in kg. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other inertial parameters.
$N$ is the number of wheels and must match the input signal dimensions.
Rotational inertia (rolling axis), IYY - Rotational inertia
scalar | N-by-1 vector
Rotational inertia (rolling axis), specified as a scalar or $N$-by- 1 vector, in $\mathrm{kg} \cdot \mathrm{m}^{2}$. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other rotational parameters.
$N$ is the number of wheels and must match the input signal dimensions.
Gravity, GRAVITY - Gravity
scalar
Gravity, GRAVITY, in $\mathrm{m} / \mathrm{s}^{\wedge} 2$.

## Vertical

Initial tire displacement, zo - Displacement
0 (default) | scalar | $N$-by-1 vector
Initial tire displacement, specified as a scalar or $N$-by-1 vector, in m. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other vertical parameters.
$N$ is the number of wheels and must match the input signal dimensions.
Initial wheel vertical velocity (wheel fixed frame), zdoto - Velocity
0 (default) | scalar | $N$-by- 1 vector
Initial wheel vertical velocity, specified as a scalar or $N$-by-1 vector, in $\mathrm{m} / \mathrm{s}$. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other vertical parameters.
$N$ is the number of wheels and must match the input signal dimensions.
Effective rolling radius at low load stiffness, BREFF - Stiffness
8.25094594147963 (default) | scalar

Effective rolling radius at low load stiffness, BREFF, dimensionless.
Effective rolling radius peak value, DREFF - Radius
0.260468730454265 (default) | scalar

Effective rolling radius peak value, $D R E F F$, dimensionless.
Effective rolling radius at high load stiffness, FREFF - Radius
0.0735298544471851 (default) | scalar

Effective rolling radius at high load stiffness, FREFF, dimensionless.
Unloaded to nominal rolling radius ratio, Q_REO - Ratio 1.00866439868088 (default) | scalar

Unloaded to nominal rolling radius ratio, $Q_{-} R E 0$, dimensionless.
Radius rotational speed dependence, Q_V1 - Speed 0.000760413786224011 (default) | scalar

Radius rotational speed dependence, $Q_{-}$V1, dimensionless.
Stiffness rotational speed dependence, Q_V2 - Speed
0.0463384792019201 (default) | scalar

Stiffness rotational speed dependence, $Q_{-} V 2$, dimensionless.
Linear load change with deflection, Q_FZ1 - Load change
0 (default) | scalar
Linear load change with deflection, $Q$ FZ1, dimensionless.

Quadratic load change with deflection, Q_FZ2 - Load change 15.6870832810226 (default) | scalar

Quadratic load change with deflection, Q_FZ2, dimensionless.
Linear load change with deflection and quadratic camber, Q_FZ3 - Load change
0 (default) | scalar
Linear load change with deflection and quadratic camber, $Q_{-} F Z 3$, dimensionless.
Load response to longitudinal force, Q_FCX - Force
0.138643970247602 (default) | scalar

Load response to longitudinal force, $Q_{-} F C X$, dimensionless.
Load response to lateral force, Q_FCY - Force
0.10843499565426 (default) | scalar

Load response to lateral force, $Q_{-} F C Y$, dimensionless.
Vertical stiffness change due to lateral load dependency on lateral stiffness, Q_FCY2 Stiffness
-0. 465763352339538 (default) | scalar
Vertical stiffness change due to lateral load dependency on lateral stiffness, Q_FCY2, dimensionless.

## Stiffness response to pressure, PFZ1 - Stiffness

0.69958166705601 (default) | scalar

Stiffness response to pressure, PFZ1, dimensionless.
Vertical tire stiffness, VERTICAL_STIFFNESS - Stiffness
207885. 061134007 (default) | scalar

Vertical tire stiffness, VERTICAL_STIFFNESS, in N/m.
Vertical tire damping, VERTICAL_DAMPING - Damping
494.649255786991 (default) | scalar

Vertical tire damping, VERTICAL_DAMPING, in N•s/m.
Rim bottoming out offset, BOTTOM_OFFST - Offset
. 01 (default) | scalar
Rim bottoming out offset, BOTTOM_OFFST, in m.
Bottoming out stiffness, BOTTOM_STIFF - Stiffness
2e6 (default) | scalar
Bottoming out stiffness, BOTTOM_STIFF, in N/m.

## Structural

Longitudinal stiffness, LONGITUDINAL_STIFFNESS - Stiffness
scalar

Longitudinal stiffness, LONGITUDINAL_STIFFNESS, in N/m.
Lateral stiffness, LATERAL_STIFFNESS - Stiffness
scalar
Longitudinal stiffness, LATERAL_STIFFNESS, in N/m.
Linear vertical deflection influence on longitudinal stiffness, PCFX1 - Deflection influence scalar

Linear vertical deflection influence on longitudinal stiffness, PCFX1, dimensionless.
Quadratic vertical deflection influence on longitudinal stiffness, PCFX2 - Deflection influence scalar

Quadratic vertical deflection influence on longitudinal stiffness, PCFX2, dimensionless.
Pressure dependency on longitudinal stiffness, PCFX3 - Pressure dependency scalar

Pressure dependency on longitudinal stiffness, $P C F X 3$, dimensionless.
Linear vertical deflection influence on lateral stiffness, PCFY1 - Deflection influence scalar

Linear vertical deflection influence on lateral stiffness, PCFY1, dimensionless.
Quadratic vertical deflection influence on lateral stiffness, PCFY2 - Deflection influence scalar

Quadratic vertical deflection influence on lateral stiffness, PCFY2, dimensionless.
Pressure dependency on longitudinal stiffness, PCFY3 - Pressure dependency scalar

Pressure dependency on longitudinal stiffness, PCFY3, dimensionless.

## Contact Patch

Contact length square root term, Q_RA1 - Length term
scalar
Contact length square root term, $Q_{-} R A 1$, dimensionless.
Contact length linear term, Q_RA2 - Length term

## scalar

Contact length linear term, Q_RA2, dimensionless.
Contact width root term, Q_RB1 - Width term
scalar
Contact width root term, $Q_{-} R B 1$, dimensionless.
Contact width linear term, Q_RB2 - Width term scalar

Contact width linear term, $Q_{-} R B 2$, dimensionless.
Longitudinal
Cfx shape factor, PCX1 - Shape factor
scalar
Shape factor, $C_{f x}, P C X 1$, dimensionless.
Longitudinal friction at nominal normal load, PDX1 - Friction scalar

Longitudinal friction at nominal normal load, PDX1, dimensionless.
Frictional variation with load, PDX2 - Friction variation scalar

Frictional variation with load, $P D X 2$, dimensionless.
Frictional variation with camber, PDX3 - Friction variation scalar

Frictional variation with camber, $P D X 3$, in $1 / \mathrm{rad}^{\wedge} 2$.
Longitudinal curvature at nominal normal load, PEX1 - Curvature scalar

Longitudinal curvature at nominal normal load, PEX1, dimensionless.
Variation of curvature factor with load, PEX2 - Curvature variation scalar

Variation of curvature factor with load, PEX2, dimensionless.
Variation of curvature factor with square of load, PEX3 - Curvature variation scalar

Variation of curvature factor with square of load, PEX3, dimensionless.
Longitudinal curvature factor with slip, PEX4 - Curvature scalar

Longitudinal curvature factor with slip, PEX4, dimensionless.
Longitudinal slip stiffness at nominal normal load, PKX1 - Stiffness
scalar
Longitudinal slip stiffness at nominal normal load, PKX1, dimensionless.
Variation of slip stiffness with load, PKX2 - Stiffness variation scalar

Variation of slip stiffness with load, $P K X 2$, dimensionless.
Slip stiffness exponent factor, PKX3 - Slip stiffness
scalar

Slip stiffness exponent factor, PKX3, dimensionless.
Horizontal shift in slip ratio at nominal normal load, PHX1 - Slip ratio shift scalar

Horizontal shift in slip ratio at nominal normal load, PHX1, dimensionless.
Variation of horizontal slip ratio with load, PHX2 - Slip variation scalar

Variation of horizontal slip ratio with load, PHX2, dimensionless.
Vertical shift in load at nominal normal load, PVX1 - Load shift scalar

Vertical shift in load at nominal normal load, PVX1, dimensionless.
Variation of vertical shift with load, PVX2 - Load variation
scalar
Variation of vertical shift with load, PVX2, dimensionless.
Linear variation of longitudinal slip stiffness with tire pressure, PPX1 - Stiffness variation scalar

Linear variation of longitudinal slip stiffness with tire pressure, PPX1, dimensionless.
Quadratic variation of longitudinal slip stiffness with tire pressure, PPX2 - Stiffness variation scalar

Quadratic variation of longitudinal slip stiffness with tire pressure, PPX2, dimensionless.
Linear variation of peak longitudinal friction with tire pressure, PPX3 - Friction variation scalar

Linear variation of peak longitudinal friction with tire pressure, $P P X 3$, dimensionless.
Quadratic variation of peak longitudinal friction with tire pressure, PPX4 - Friction variation scalar

Quadratic variation of peak longitudinal friction with tire pressure, PPX4, dimensionless.
Combined slip Fx slope factor reduction, RBX1 - Combined slip longitudinal force slope factor reduction
scalar
Combined slip longitudinal force, $F_{x}$, slope factor reduction, $R B X 1$, dimensionless.
Slip ratio Fx slope reduction variation, RBX2 - Slip ratio longitudinal force slope reduction variation
scalar
Slip ratio longitudinal force, $F_{x}$, slope reduction variation, $R B X 2$, dimensionless.

Camber influence on combined slip Fx stiffness, RBX3 - Camber influence on combined slip longitudinal force stiffness
scalar
Camber influence on combined slip longitudinal force, $F_{x}$, stiffness, $R B X 3$, dimensionless.
Shape factor for combined slip Fx reduction, RCX1 - Shape factor for combined slip longitudinal force reduction
scalar
Shape factor for combined slip longitudinal force, $F_{x}$, reduction, $R C X 1$, dimensionless.
Combined Fx curvature factor, REX1 - Combined longitudinal force curvature factor scalar

Combined longitudinal force, $F_{x}$, curvature factor, REX1, dimensionless.
Combined Fx curvature factor with load, REX2 - Combined longitudinal force curvature factor scalar

Combined longitudinal force, $F_{x}$, curvature factor with load, REX2, dimensionless.
Combined slip Fx shift factor reduction, RHX1 - Combined slip longitudinal force slip factor scalar

Combined slip longitudinal force, $F_{x}$, shift factor reduction, RHX1, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.

## Overturning

Vertical shift of overturning moment, QSX1 - Overturning moment
scalar
Vertical shift of overturning moment, QSX1, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Overturning moment due to camber, QSX2 - Overturning moment due to camber scalar

Overturning moment due to camber, QSX2, dimensionless.
Overturning moment due to Fy, QSX3 - Overturning moment due to lateral force scalar

Overturning moment due to lateral force, QSX3, dimensionless.
Mx combined lateral force load and camber, QSX4 - Overturning moment scalar

Overturning moment, $M_{x}$, combined lateral force load and camber, QSX4, dimensionless.

Mx load effect due to lateral force and camber, QSX5 - Overturning moment scalar

Overturning moment, $M_{x}$, load effect due to lateral force and camber, QSX5, dimensionless.
Mx load effect due to B-factor, QSX6 - Overturning moment scalar

Overturning moment, $M_{x}$, load effect due to B-factor, QSX6, dimensionless.
Mx due to camber and load, QSX7 - Overturning moment scalar

Overturning moment, $M_{x}$, due to camber and load, QSX7, dimensionless.
Mx due to lateral force and load, QSX8 - Overturning moment scalar

Overturning moment, $M_{x}$, due to lateral force and load, QSX8, dimensionless.
Mx due to B-factor of lateral force and load, QSX9 - Overturning moment scalar

Overturning moment, $M_{x}$, due to B-factor of lateral force and load, QSX9, dimensionless.
Mx due to vertical force and camber, QSX10 - Overturning moment scalar

Overturning moment, $M_{x}$, due to vertical force and camber, QSX10, dimensionless.
Mx due to B-factor of vertical force and camber, QSX11 - Overturning moment scalar

Overturning moment, $M_{x}$, due to B-factor of vertical force and camber, QSX11, dimensionless.
Mx due to squared camber, QSX12 - Overturning moment
scalar
Overturning moment, $M_{x}$, due to squared camber, QSX12, dimensionless.
Mx due to lateral force, QSX13 - Overturning moment
scalar
Overturning moment, $M_{x}$, due to lateral force, QSX13, dimensionless.
Mx due to lateral force with camber, QSX14 - Overturning moment scalar

Overturning moment, $M_{x}$, due to lateral force with camber, QSX14, dimensionless.
Mx due to inflation pressure, PPMX1 - Overturning moment due to pressure scalar

Overturning moment, $M_{x}$, due to inflation pressure, PPMX1, dimensionless.

## Lateral

Cfy shape factor for lateral force, PCY1 - Lateral force shape factor scalar

Shape factor for lateral force, $C_{f y}$, PCY1, dimensionless.
Lateral friction muy, PDY1 - Lateral friction
scalar
Lateral friction, $\mu_{y}$, PDY1, dimensionless.
Lateral friction variation of muy with load, PDY2 - Lateral friction variation scalar

Variation of lateral friction, $\mu_{y}$, with load, PDY2, dimensionless.
Lateral friction variation of muy with squared camber, PDY3 - Lateral friction variation scalar

Variation of lateral friction, $\mu_{y}$, with squared camber, PDY3, dimensionless.
Efy lateral curvature at nominal force FZNOM, PEY1 - Lateral curvature at nominal force scalar

Lateral curvature, $E f_{y}$, at nominal force, $F_{Z N O M}$, PEY1, dimensionless.
Efy curvature variation with load, PEY2 - Lateral curvature variation scalar

Lateral curvature, $E f_{y}$, variation with load, $P E Y 2$, dimensionless.
Efy curvature constant camber dependency, PEY3 - Lateral curvature constant scalar

Lateral curvature, $E f_{y}$, constant camber dependency, PEY3, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Efy curvature variation with camber, PEY4 - Lateral curvature variation scalar

Lateral curvature, $E f_{y}$, variation with camber, PEY4, dimensionless.
Efy curvature variation with camber squared, PEY5 - Lateral curvature variation scalar

Lateral curvature, $E f_{y}$, variation with camber squared, PEY5, dimensionless.
Maximum KFy/FZNOM stiffness, PKY1 - Maximum stiffness scalar

Maximum lateral force stiffness, $K F_{y}$, to nominal force, $F_{Z N O M}$, ratio, $P K Y 1$, dimensionless.

## Load at maximum KFy/FZNOM stiffness, PKY2 - Load scalar

Load at maximum lateral force stiffness, $K F_{y}$, to nominal force, $F_{Z N O M}$, ratio, $P K Y 2$, dimensionless.
KFy/FZNOM stiffness variation with camber, PKY3 - Stiffness variation scalar

Lateral force stiffness, $K F_{y}$, to nominal force, $F_{Z N O M}$, stiffness variation with camber, $P K Y 3$, dimensionless.

KFy curvature, PKY4 - Lateral force stiffness curvature scalar

Lateral force stiffness, $K F_{y}$ curvature, $P K Y 4$, dimensionless.
Variation of peak stiffness with squared camber, PKY5 - Stiffness variation scalar

Variation of peak stiffness with squared camber, PKY5, dimensionless.
Fy camber stiffness factor, PKY6 - Lateral force camber stiffness factor scalar

Lateral force, $F_{y}$, camber stiffness factor, PKY6, dimensionless.
Camber stiffness vertical load dependency, PKY7 - Stiffness scalar

Camber stiffness vertical load dependency, PKY7, dimensionless.
SHY horizontal shift at FZNOM, PHY1 - Horizontal shift at nominal force scalar

Horizontal shift, $S_{H Y}$, at nominal force, $F_{Z N O M}$, PHY1, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
SHY variation with load, PHY2 - Horizontal shift variation
scalar
Horizontal shift, $S_{H Y}$, variation with load, $P H Y 2$, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Svy/Fz vertical shift at FZNOM, PVY1 - Vertical shift at nominal force scalar

Vertical shift, $S_{v y}$, at nominal force, $F_{Z N O M}, P V Y 1$, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.

Svy/Fz variation with load, PVY2 - Vertical shift variation with load scalar

Vertical shift, $S_{v y}$, variation with load, $P V Y 2$, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Svy/Fz variation with camber, PVY3 - Vertical shift variation with camber scalar

Vertical shift, $S_{v y}$, variation with camber, $P V Y 3$, dimensionless.
Svy/Fz variation with load and camber, PVY4 - Vertical shift variation with load and camber scalar

Vertical shift, $S_{v y}$, variation with load and camber, $P V Y 4$, dimensionless.
Cornering stiffness variation with inflation pressure, PPY1 - Stiffness variation with pressure scalar

Cornering stiffness variation with inflation pressure, PPY1, dimensionless.
Cornering stiffness variation with inflation pressure induced nominal load dependency, PPY2 - Stiffness variation with pressure
scalar
Cornering stiffness variation with inflation pressure induced nominal load dependency, PPY2, dimensionless.

Linear inflation pressure on peak lateral friction, PPY3 - Pressure
scalar
Linear inflation pressure on peak lateral friction, $P P Y 3$, dimensionless.
Quadratic inflation pressure on peak lateral friction, PPY4 - Pressure
scalar
Quadratic inflation pressure on peak lateral friction, PPY4, dimensionless.
Inflation pressure effect on camber stiffness, PPY5 - Pressure scalar

Inflation pressure effect on camber stiffness, PPY5, dimensionless.
Combined Fy reduction slope factor, RBY1 - Combined lateral force reduction slope factor scalar

Combined lateral force, $F_{y}$, reduction slope factor, RBY1, dimensionless.
Fy slope reduction with slip angle, RBY2 - Lateral force slope reduction with slip angle scalar

Lateral force, $F_{y}$, slope reduction with slip angle, RBY2, dimensionless.

Fy shift reduction with slip angle, RBY3 - Lateral force shift reduction with slip angle scalar

Lateral force, $F_{y}$, shift reduction with slip angle, RBY3, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Fy combined stiffness variation from camber, RBY4 - Lateral force combined stiffness variation from camber
scalar
Lateral force, $F_{y}$, combined stiffness variation from camber, $R B Y 4$, dimensionless.
Fy combined reduction shape factor, RCY1 - Lateral force combined reduction shape factor scalar

Lateral force, $F_{y}$, combined reduction shape factor, RCY1, dimensionless.
Fy combined curvature factor, REY1 - Lateral force combined curvature factor scalar

Lateral force, $F_{y}$ combined curvature factor, REY1, dimensionless.
Fy combined curvature factor with load, REY2 - Lateral force combined curvature factor with load
scalar
Lateral force, $F_{y}$, combined curvature factor with load, REY2, dimensionless.
Fy combined reduction shift factor, RHY1 - Lateral force combined reduction shift factor scalar

Lateral force, $F_{y}$, combined reduction shift factor, RHY1, dimensionless.
Fy combined reduction shift factor with load, RHY2 - Lateral force combined reduction shift factor with load scalar

Lateral force, $F_{y}$, combined reduction shift factor with load, RHY2, dimensionless.
Slip ratio side force Svyk/Muy*Fz at FZNOM, RVY1 - Slip ratio slide force at nominal force scalar

Slip ratio side force at nominal force, $F_{Z N O M}, R V Y 1$, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Side force Svyk/Muy*Fz variation with load, RVY2 - Side force variation with load scalar

Side force variation with load, RVY2, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Side force Svyk/Muy*Fz variation with camber, RVY3 - Side force variation with camber scalar

Side force variation with camber, $R V Y 3$, dimensionless.
Side force Svyk/Muy*Fz variation with slip angle, RVY4 - Side force variation with slip angle scalar

Side force variation with slip angle, $R V Y 4$, dimensionless.
Side force Svyk/Muy*Fz variation with slip ratio, RVY5 - Side force variation with slip ratio scalar

Side force variation with slip ratio, RVY5, dimensionless.
Side force Svyk/Muy*Fz variation with slip ratio arctangent, RVY6 - Side force variation with slip ratio arctangent
scalar
Side force variation with slip ratio arctangent, RVY6, dimensionless.

## Rolling

Torque resistance coefficient, QSY1 - Torque resistance
scalar
Torque resistance coefficient, QSY1, dimensionless.
Torque resistance due to Fx, QSY2 - Torque resistance due to longitudinal force scalar

Torque resistance due to longitudinal force, $F_{x}$, QSY2, dimensionless.
Torque resistance due to speed, QSY3 - Torque resistance due to speed scalar

Torque resistance due to speed, QSY3, dimensionless.
Torque resistance due to speed^4, QSY4 - Torque resistance due to speed scalar

Torque resistance due to speed^4, QSY4, dimensionless.
Torque resistance due to square of camber, QSY5 - Torque resistance due to camber scalar

Torque resistance due to square of camber, QSY5, dimensionless.
Torque resistance due to square of camber and load, QSY6 - Torque resistance due to camber and load
scalar

Torque resistance due to square of camber and load, QSY6, dimensionless.
Torque resistance due to load, QSY7 - Torque resistance due to load scalar

Torque resistance due to load, QSY7, dimensionless.
Torque resistance due to pressure, QSY8 - Torque resistance due to pressure scalar

Torque resistance due to pressure, QSY8, dimensionless.

## Aligning

Trail slope factor for trail Bpt at FZNOM, QBZ1 - Trail slope factor at nominal force scalar

Trail slope factor for trail $B p t$ at nominal force, $F_{\text {ZNOM }}, Q B Z 1$, dimensionless.
Bpt slope variation with load, QBZ2 - Slope variation with load scalar

Slope variation with load, QBZ2, dimensionless.
Bpt slope variation with square of load, QBZ3 - Slope variation with load scalar

Slope variation with square of load, $Q B Z 3$, dimensionless.
Bpt slope variation with camber, QBZ4 - Slope variation with camber scalar

Slope variation with camber, QBZ4, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Bpt slope variation with absolute value of camber, QBZ5 - Slope variation with camber scalar

Slope variation with absolute value of camber, QBZ5, dimensionless.
Bpt slope variation with square of camber, QBZ6 - Slope variation with camber scalar

Slope variation with square of camber, QBZ6, dimensionless.
Br of Mzr slope scaling factor, QBZ9 - Slope scaling factor scalar

Slope scaling factor, QBZ9, dimensionless.
Br of Mzr cornering stiffness factor, QBZ10 - Cornering stiffness factor
0 (default) | scalar
$B r$ of $M z r$ cornering stiffness factor, $Q B Z 10$, dimensionless.

Cpt pneumatic trail shape factor, QCZ1 - Pneumatic trail shape factor scalar

Pneumatic trail shape factor, $C_{p t}, Q C Z 1$, dimensionless.
Dpt peak trail, QDZ1 - Peak trail
scalar
Peak trail, $D_{p t}$, QDZ1, dimensionless.
Dpt peak trail variation with load, QDZ2 - Peak trail variation with load scalar

Peak trail, $D_{p t}$, variation with load, $Q D Z 2$, dimensionless.
Dpt peak trail variation with camber, QDZ3 - Peak trail variation with camber scalar

Peak trail, $D_{p t}$, variation with camber, $Q D Z 3$, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Dpt peak trail variation with square of camber, QDZ4 - Peak trail variation with camber scalar

Peak trail, $D_{p t}$, variation with square of camber, $Q D Z 4$, dimensionless.
Dmr peak residual torque, QDZ6 - Peak residual torque
scalar
Peak residual torque, $D_{m r}$, QDZ6, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Dmr peak residual torque variation with load, QDZ7 - Peak residual torque variation with load scalar

Peak residual torque, $D_{m r}$, variation with load, $Q D Z 7$, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Dmr peak residual torque variation with camber, QDZ8 - Peak residual torque variation with camber
scalar
Peak residual torque, $D_{m r}$, variation with camber, QDZ8, dimensionless.
Dmr peak residual torque variation with camber and load, QDZ9 - Peak residual torque variation with camber and load scalar

Peak residual torque, $D_{m r}$, variation with camber and load, QDZ9, dimensionless.
Dmr peak residual torque variation with square of camber, QDZ10 - Peak residual torque variation with camber
scalar
Peak residual torque, $D_{m r}$, variation with square of camber, $Q D Z 10$, dimensionless.
Dmr peak residual torque variation with square of load, QDZ11 - Peak residual torque variation with load
scalar
Peak residual torque, $D_{m r}$, variation with square of load, $Q D Z 11$, dimensionless.
Ept trail curvature at FZNOM, QEZ1 - Trail curvature at nominal force scalar

Trail curvature, $E_{p t}$, at nominal force, $F_{Z N O M}, Q E Z 1$, dimensionless.
Ept variation with load, QEZ2 - Trail curvature variation with load scalar

Trail curvature, $E_{p t}$ variation with load, QEZ2, dimensionless.
Ept variation with square of load, QEZ3 - Trail curvature variation with load scalar

Trail curvature, $E_{p t}$ variation with square of load, $Q E Z 3$, dimensionless.
Ept variation with sign of alpha-t, QEZ4 - Trail curvature variation scalar

Trail curvature, $E_{p t}$ variation with sign of alpha-t, QEZ4, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.

## Ept variation with sign of alpha-t and camber, QEZ5 - Variation

scalar
Trail curvature, $E_{p t}$ variation with sign of alpha-t and camber, $Q E Z 5$, dimensionless.
Sht horizontal trail shift at FZNOM, QHZ1 - Horizontal trail shift at nominal load scalar

Horizontal trail shift, $S h_{t}$, at nominal load, $F_{Z N O M}, Q H Z 1$, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Sht variation with load, QHZ2 - Horizontal trail shift variation with load scalar

Horizontal trail shift, $S h_{t}$, variation with load, $Q H Z 2$, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Sht variation with camber, QHZ3 - Horizontal trail shift variation with camber scalar

Horizontal trail shift, $S h_{t}$, variation with camber, $Q H Z 3$, dimensionless.
Sht variation with load and camber, QHZ4 - Horizontal trail shift variation with load and camber scalar

Horizontal trail shift, $S h_{t}$, variation with load and camber, $Q H Z 4$, dimensionless.
Inflation pressure influence on trail length, PPZ1 - Pressure influence on trail length scalar

Inflation pressure influence on trail length, PPZ1, dimensionless.
Inflation pressure influence on residual aligning torque, PPZ2 - Pressure influence on aligning torque
scalar
Inflation pressure influence on residual aligning torque, PPZ2, dimensionless.
Nominal value of s/R0: effect of Fx on Mz, SSZ1 - Effect of longitudinal force on aligning torque scalar

Nominal value of s/R0: effect of longitudinal force, $F_{x}$, on aligning torque, $M_{z}$, SSZ1, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
s/R0 variation with lateral to nominal force ratio, SSZ2 - Variation with lateral to nominal force ratio
scalar
Variation with lateral to nominal force ratio, SSZ2, dimensionless.
s/R0 variation with camber, SSZ3 - Variation with camber
scalar
Variation with camber, SSZ3, dimensionless.
s/R0 variation with camber and load, SSZ4 - Variation with camber and load scalar

Variation with camber and load, SSZ4, dimensionless.

## Turnslip

Fx peak reduction due to spin, PDXP1 - Longitudinal force peak reduction due to spin scalar

Longitudinal force, $F_{x}$, peak reduction due to spin, $P D X P 1$, dimensionless.

Fx peak reduction due to spin with varying load, PDXP2 - Longitudinal force peak reduction due to spin
scalar
Longitudinal force, $F_{x}$, peak reduction due to spin with varying load, $P D X P 2$, dimensionless.
Fx peak reduction due to spin with slip ratio, PDXP3 - Longitudinal force peak reduction due to spin
scalar
Longitudinal force, $F_{x}$, peak reduction due to spin with slip ratio, $P D X P 3$, dimensionless.
Cornering stiffness reduction due to spin, PKYP1 - Stiffness reduction due to spin scalar

Cornering stiffness reduction due to spin, PKYP1, dimensionless.
Fy peak reduction due to spin, PDYP1 - Lateral force peak reduction due to spin scalar

Lateral force, $F_{y}$, peak reduction due to spin, PDYP1, dimensionless.
Fy peak reduction due to spin with varying load, PDYP2 - Lateral force peak reduction due to spin
scalar
Lateral force, $F_{y}$, peak reduction due to spin with varying load, $P D Y P 2$, dimensionless.
Fy peak reduction due to spin with slip angle, PDYP3 - Lateral force peak reduction due to spin scalar

Lateral force, $F_{y}$, peak reduction due to spin with slip angle, PDYP3, dimensionless.
Fy peak reduction due to square root of spin, PDYP4 - Lateral force peak reduction due to spin scalar

Lateral force, $F_{y}$, peak reduction due to square root of spin, PDYP4, dimensionless.
Fy vs. slip angle response lateral shift limit, PHYP1 - Lateral force versus slip angle response scalar

Lateral force, $F_{y}$, versus slip angle response lateral shift limit, PHYP1, dimensionless.
Fy vs. slip angle response max lateral shift limit, PHYP2 - Lateral force versus slip angle response scalar

Lateral force, $F_{y}$, versus slip angle response max lateral shift limit, PHYP2, dimensionless.
Fy vs. slip angle response max lateral shift limit with load, PHYP3 - Lateral force versus slip angle response scalar

Lateral force, $F_{y}$, versus slip angle response max lateral shift limit with load, PHYP3, dimensionless.

Fy vs. slip angle response lateral shift curvature factor, PHYP4 - Lateral force versus slip angle response
scalar
Lateral force, $F_{y}$, versus slip angle response lateral shift curvature factor, PHYP4, dimensionless.
Camber stiffness reduction due to spin, PECP1 - Camber stiffness reduction scalar

Camber stiffness reduction due to spin, PECP1, dimensionless.
Camber stiffness reduction due to spin with load, PECP2 - Camber stiffness reduction scalar

Camber stiffness reduction due to spin with load, PECP2, dimensionless.
Turn slip pneumatic trail reduction factor, QDTP1 - Turn slip pneumatic trail reduction factor scalar

Turn slip pneumatic trail reduction factor, QDTP1, dimensionless.
Turn moment for constant turning and zero longitudinal speed, QCRP1 - Turn moment for constant turning
scalar
Turn moment for constant turning and zero longitudinal speed, QCRP1, dimensionless.
Turn slip moment increase with spin at 90deg slip angle, QCRP2 - Turn slip moment scalar

Turn slip moment increase with spin at 90-degree slip angle, QCRP2, dimensionless.
Residual spin torque reduction from side slip, QBRP1 - Residual spin torque reduction scalar

Residual spin torque reduction from side slip, QBRP1, dimensionless.
Turn slip moment peak magnitude, QDRP1 - Turn slip moment peak magnitude scalar

Turn slip moment peak magnitude, $Q D R P 1$, dimensionless.
Turn slip moment curvature, QDRP2 - Turn slip moment curvature scalar

Turn slip moment curvature, QDRP2, dimensionless.

## Version History

Introduced in R2018a
R2022b: Specify Brake and Tire Parameters for Each Wheel
Behavior changed in R2022b

Starting from R2022b, you can to use the Combined Slip Wheel 2DOF block to specify brake and tire characteristics for each wheel on your vehicle. Specifically, the block allows $N$-by- 1 vectors for these parameters:

- Static friction coefficient, mu_static
- Kinetic friction coefficient, mu_kinetic
- Disc brake actuator bore, disc_abore
- Brake pad mean radius, Rm
- Number of brake pads, num_pads
- Drum brake actuator bore, disc_abore
- Initial rotational velocity, omegao
- Rotational damping, br
- Wheel mass, MASS
- Rotational inertia (rolling axis), IYY
- Initial tire displacement, zo
- Initial wheel vertical velocity (wheel fixed frame), zdoto
$N$ is the number of wheels and must match the input signal dimensions.


## R2022b: New Ply steer and Turn slip Parameters

Behavior changed in R2022b
Starting from R2022b, the Combined Slip Wheel 2DOF block includes Ply steer and Turn slip parameters. To remove ply steer and turn slip from the Magic Formula implementation of these blocks, clear the Ply steer and Turn slip parameters.

## R2023a: New Vertical Motion Parameter

Behavior changed in R2023a
Starting from R2023a, the Combined Slip Wheel 2DOF block includes the Vertical Motion parameter. By default, the Combined Slip Wheel 2DOF block uses the Magic Formula to calculate the vertical motion of the tire.

## References

[1] Besselink, Igo, Antoine J. M. Schmeitz, and Hans B. Pacejka, "An improved Magic Formula/Swift tyre model that can handle inflation pressure changes," Vehicle System Dynamics International Journal of Vehicle Mechanics and Mobility 48, sup. 1 (2010): 337-52, https:// doi.org/10.1080/00423111003748088.
[2] Pacejka, H. B. Tire and Vehicle Dynamics. 3rd ed. Oxford, United Kingdom: SAE and ButterworthHeinemann, 2012.
[3] Schmid, Steven R., Bernard J. Hamrock, and Bo O. Jacobson. Fundamentals of Machine Elements, SI Version. 3rd ed. Boca Raton: CRC Press, 2014.

## Extended Capabilities

C/C++ Code Generation
Generate C and C++ code using Simulink $\circledR_{\circledR}$ Coder ${ }^{\mathrm{TM}}$.

## See Also

Combined Slip Wheel 2DOF CPI | Combined Slip Wheel 2DOF STI | Fiala Wheel 2DOF | Longitudinal Wheel | Dugoff Wheel 2DOF

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"

## Fiala Wheel 2DOF

Fiala wheel 2DOF wheel with disc, drum, or mapped brake


## Libraries:

Vehicle Dynamics Blockset / Wheels and Tires

## Description

The Fiala Wheel 2DOF block implements a simplified tire with lateral and longitudinal slip capability based on the E. Fiala model ${ }^{[1]}$. The block uses a translational friction model to calculate the forces and moments during combined longitudinal and lateral slip, requiring fewer parameters than the Combined Slip Wheel 2DOF block. If you do not have the tire coefficients needed by the Magic Formula, consider using this block for studies that do not involve extensive nonlinear combined lateral slip or lateral dynamics. If your study does require nonlinear combined slip or lateral dynamics, consider using the Combined Slip Wheel 2DOF block.

The block determines the wheel rotation rate, vertical motion, and forces and moments in all six degrees-of-freedom (DOFs) based on the driveline torque, brake pressure, road height, wheel camber angle, and inflation pressure. You can use this block for these types of analyses:

- Driveline and vehicle simulations that require low frequency tire-road and braking forces for vehicle acceleration, braking, and wheel rolling resistance calculations with minimal tire parameters.
- Wheel interaction with an idealized road surface.
- Ride and handling maneuvers for vehicles undergoing mild combined slip. For this analysis, you can connect the block to driveline and chassis components such as differentials, suspension, and vehicle body systems.
- Yaw stability. For this analyses, you can connect this block to more detailed braking system models.
- Tire stiffness and unsprung mass interactions with ground variations, load transfer, or chassis motion using the block vertical DOF.

The block integrates rotational wheel, vertical mass, and braking dynamics models. For the slipdependent tire forces and moments, the block implements the Fiala tire model.

Use the Brake Type parameter to select the brake.

| Action | Brake Type Setting |
| :--- | :--- |
| No braking | None |


| Action | Brake Type Setting |
| :--- | :--- |
| Implement brake that converts the <br> brake cylinder pressure into a <br> braking force | Disc |
| Implement simplex drum brake that <br> converts the applied force and brake <br> geometry into a net braking torque | Drum |
| Implement lookup table that is a <br> function of the wheel speed and <br> applied brake pressure | Mapped |

To calculate the rolling resistance torque, specify one of these Rolling Resistance parameters.

| Setting | Block Implementation |
| :--- | :--- |
| None | None |
| Pressure and velocity | Method in Stepwise Coastdown Methodology for Measuring <br> Tire Rolling Resistance. The rolling resistance is a function of <br> tire pressure, normal force, and velocity. |
| ISO 28580 | Method specified in ISO 28580:2018, Passenger car, truck <br> and bus tyre rolling resistance measurement method <br> Single point test and correlation of measurement results. |
| Magic Formula | Magic formula equations from 4.E70 in Tire and Vehicle <br> Dynamics. The magic formula is an empirical equation based <br> on fitting coefficients. |
| Mapped torque | Lookup table that is a function of the normal force and spin <br> axis longitudinal velocity. |

To calculate vertical motion, specify one of these Vertical Motion parameters.

| Setting | Block Implementation |
| :--- | :--- |
| None | Block passes the applied chassis forces directly through to <br> the rolling resistance and longitudinal force calculations. |
| Mapped stiffness and damping | Vertical motion depends on wheel stiffness and damping. <br> Stiffness is a function of tire sidewall displacement and <br> pressure. Damping is a function of tire sidewall velocity and <br> pressure. |

## Rotational Wheel Dynamics

The block calculates the inertial response of the wheel subject to:

- Axle losses
- Brake and drive torque
- Tire rolling resistance
- Ground contact through the tire-road interface

The input torque is the summation of the applied axle torque, braking torque, and moment arising from the combined tire torque.

$$
T_{i}=T_{a}-T_{b}+T_{d}
$$

For the moment arising from the combined tire torque, the block implements tractive wheel forces and rolling resistance with first-order dynamics. The rolling resistance has a time constant parameterized in terms of a relaxation length.

$$
T_{d}(s)=\frac{1}{\frac{L_{e}}{|\omega| R_{e}} s+1}+\left(F_{\chi} R_{e}+M_{y}\right)
$$

To calculate the rolling resistance torque, you can specify one of these Rolling Resistance parameters.

| Setting | Block Implementation |
| :--- | :--- |
| None | Block sets rolling resistance, $M_{y}$, to zero. |
| Pressure and <br> velocity | Block uses the method in SAE Stepwise Coastdown Methodology for Measuring <br> Tire Rolling Resistance. The rolling resistance is a function of tire pressure, <br> normal force, and velocity, specifically, <br>  <br> $M_{y}=R_{e}\left\{a+b\left\|V_{x}\right\|+c V_{\chi}{ }^{2}\right\}\left\{F_{z} \beta p_{i} \alpha\right\} \tanh \left(4 V_{\chi}\right)$ |
| IS0 28580 | Block uses the method specified in ISO 28580:2018, Passenger car, truck and <br> bus tyre rolling resistance measurement method - Single point test and <br> correlation of measurement results. The method accounts for normal load, <br> parasitic loss, and thermal corrections from test conditions, specifically, |
| $\quad M_{y}=R_{e}\left(\frac{F_{z} C_{r}}{1+K_{t}\left(T_{a m b}-T_{\text {meas }}\right)}-F_{p l}\right)$ tanh( $\omega$ ) |  |

If the brakes are enabled, the block determines the braking locked or unlocked condition based on an idealized dry clutch friction model. Based on the lock-up condition, the block implements these friction and dynamic models.

| If | Lock-Up <br> Condition | Friction Model | Dynamic Model |
| :--- | :--- | :--- | :--- |
| $\omega \neq 0$ | Unlocked | $T_{f}=T_{k}$, | $\dot{\omega} J=-\omega b+T_{i}+T_{o}$ |
| or | where |  |  |
| $T_{S}<\left\|T_{i}+T_{f}-\omega b\right\|$ |  | $T_{k}=F_{c} R_{e f f} \mu_{k} \tanh \left[4\left(-\omega_{d}\right)\right]$ |  |
|  |  | $T_{S}=F_{c} R_{e f f} \mu_{S}$ |  |
|  | $R_{e f f}=\frac{2\left(R_{0} 3-R_{i} 3\right)}{3\left(R_{o}{ }^{2}-R_{i} 2\right)}$ |  |  |


| If | Lock-Up <br> Condition | Friction Model | Dynamic Model |
| :--- | :--- | :--- | :--- |
| $\omega=0$ <br> and <br> $T_{S} \geq\left\|T_{i}+T_{f}-\omega b\right\|$ | Locked | $T_{f}=T_{S}$ | $\omega=0$ |

The equations use these variables.

| Variable | Value |
| :--- | :--- |
| $\omega$ | Wheel angular velocity |
| $a$ | Velocity-independent force component |
| $b$ | Linear velocity force component |
| $c$ | Quadratic velocity force component |
| $L_{e}$ | Tire relaxation length |
| $J$ | Moment of inertia |
| $M_{y}$ | Rolling resistance torque |
| $T_{a}$ | Applied axle torque |
| $T_{b}$ | Braking torque |
| $T_{d}$ | Combined tire torque |
| $T_{f}$ | Frictional torque |
| $T_{i}$ | Net input torque |
| $T_{k}$ | Kinetic frictional torque |
| $T_{o}$ | Net output torque |
| $T_{s}$ | Static frictional torque |
| $F_{c}$ | Applied clutch force |
| $F_{x}$ | Longitudinal force developed by the tire road interface due to slip |
| $R_{e f f}$ | Effective clutch radius |
| $R_{o}$ | Annular disk outer radius |
| $R_{i}$ | Annular disk inner radius |
| $R_{e}$ | Effective tire radius while under load and for a given pressure |
| $V_{x}$ | Longitudinal axle velocity |
| $F_{z}$ | Vehicle normal force |
| $C_{r}$ | Rolling resistance constant |
| $T_{a m b}$ | Ambient temperature |
| $T_{m e a s}$ | Measured temperature for rolling resistance constant |
| $F_{p l}$ | Parasitic force loss |
| $K_{t}$ | Thermal correction factor |
| $\alpha$ | Tire pressure exponent |
| $\beta$ | Normal force exponent |
| $p_{i}$ | Tire pressure |
|  |  |


| Variable | Value |
| :--- | :--- |
| $\mu_{s}$ | Coefficient of static friction |
| $\mu_{k}$ | Coefficient of kinetic friction |

## Longitudinal Force

The block implements the longitudinal force as a function of wheel slip relative to the road surface using these equations.

| Calculation | Equation |  |
| :---: | :---: | :---: |
| Critical slip | $K^{\prime}$ Critical $=\left\|\frac{\mu F_{z}}{2 C_{K}}\right\|$ |  |
| Longitudinal force | $F_{x}=\left\{\begin{array}{l} C_{k} K^{\prime} \\ \tanh \left(4 K^{\prime}\right)\left(\mu\left\|F_{z}\right\|-\left\|\frac{\left(\mu F_{z}\right)^{2}}{4 K^{\prime} C_{K}}\right\|\right) \end{array}\right.$ | when $\left\|K^{\prime}\right\| \leq K_{C r i t i c a l ~}^{\prime}$ when $\left\|\kappa^{\prime}\right\|>\kappa^{\prime}$ Critical |
| Friction coefficient | $\mu=\left(\mu_{s}-\left(\mu_{S}-\mu_{k}\right) K_{k \alpha}\right) \lambda_{\mu}$ |  |
| Slip coefficient | $K_{k \alpha}=\sqrt{K^{\prime 2}+\tan ^{2}\left(\alpha^{\prime}\right)}$ |  |

The equations use these variables.

| Variable | Value |
| :--- | :--- |
| $K^{\prime}$ | Slip state |
| $F_{\chi}$ | Longitudinal force acting on axle along tire-fixed $x$-axis |
| $C_{K}$ | Longitudinal stiffness |
| $F_{z}$ | Vertical contact patch normal force along tire-fixed $z$-axis |
| $\mu$ | Friction coefficient |
| $\mu_{s}$ | Coefficient of static friction |
| $\mu_{k}$ | Coefficient of kinetic friction |
| $K_{k a}$ | Comprehensive slip coefficient |
| $\alpha^{\prime}$ | Slip angle state |
| $\lambda_{\mu}$ | Friction scaling |

## Lateral Force

The block implements the lateral force as a function of wheel slip angle state using these equations.

| Calculation | Equation |
| :--- | :--- |
| Critical slip angle | $\alpha^{\prime}$ Critical $=\operatorname{atan}\left(\frac{3 \mu\left\|F_{z}\right\|}{C_{a}}\right)$ |


| Calculation | Equation |
| :--- | :--- |
| Lateral force | $F_{y}=\left\{\begin{array}{lc\|}-\tanh \left(4 \alpha^{\prime}\right) \mu\left\|F_{z}\right\| & \text { when }\left\|\alpha^{\prime}\right\|>\alpha^{\prime} \text { Critical } \\ -\tanh \left(4 \alpha^{\prime}\right) \mu\left\|F_{z}\right\|\left(1-\xi^{3}\right)+\gamma C_{\gamma} & \text { when }\left\|\alpha^{\prime}\right\| \leq \alpha^{\prime} \text { Critical }\end{array}\right.$ |
|  | $\xi=1-\frac{C_{a}\left\|\tan \left(\alpha^{\prime}\right)\right\|}{3 \mu\left\|F_{z}\right\|}$ |

The equations use these variables.

| Variable | Value |
| :--- | :--- |
| $\alpha^{\prime}$ | Slip angle state |
| $F_{y}$ | Lateral force acting on axle along tire-fixed $y$-axis |
| $F_{z}$ | Vertical contact patch normal force along tire-fixed $z$-axis |
| $C_{\gamma}$ | Camber stiffness |
| $C_{\alpha}$ | Lateral stiffness per slip angle |
| $\mu$ | Friction coefficient |
| Vertical Dynamics |  |

The block implements these equations for the vertical dynamics.

| Calculation | Equation |
| :--- | :--- |
| Vertical response | $\ddot{z} m=F_{z t i r e}+m g-F z$ |
| Tire normal force | $F_{z t i r e}=\rho_{z} k-b \dot{z}$ |
| Vertical sidewall deflection | $\rho_{z}=z_{g n d}-z, z \geq 0$ |

The equations use these variables.

| Variable | Value |
| :--- | :--- |
| $z$ | Tire deflection along tire-fixed $z$-axis |
| $z_{\text {gnd }}$ | Ground displacement along tire-fixed $z$-axis |
| $F_{\text {ztire }}$ | Tire normal force along tire-fixed $z$-axis |
| $F_{z}$ | Vertical force acting on axle along tire-fixed $z$-axis |
| $\rho_{z}$ | Vertical sidewall deflection along tire-fixed $z$-axis |
| $k$ | Vertical sidewall stiffness |
| $b$ | Vertical sidewall damping |

## Overturning, Aligning, and Scaling

This table summarizes the overturning, aligning, and scaling implementation.

| Calculation | Implementation |
| :--- | :--- |
| Overturning moment | The Fiala model does not define an overturning moment. The block <br> implements this equation, requiring minimal parameters. <br> $M_{x}=F_{y} R_{e} \cos (\gamma)$ |
| Aligning moment | The block implements the aligning moment as a combination of yaw <br> rate damping and slip angle state. |
|  | $M_{z}= \begin{cases}\dot{\psi} b_{M_{z}} & \text { when }\left\|\alpha^{\prime}\right\|>\alpha^{\prime} \text { Critical } \\ \tanh \left(4 \alpha^{\prime}\right) w \mu\left\|F_{z}\right\|(1-\xi) \xi^{3}+\dot{\psi} b_{M_{z}} & \text { when }\left\|\alpha^{\prime}\right\| \leq \alpha_{C \text { Critical }}\end{cases}$ |
|  | $\xi=1-\frac{C_{a}\left\|\tan \left(\alpha^{\prime}\right)\right\|}{3 \mu\left\|F_{z}\right\|}$ |

The equations use these variables.

| Variable | Value |
| :--- | :--- |
| $M_{x}$ | Overturning moment acting on axle about tire-fixed $x$-axis |
| $M_{z}$ | Aligning moment acting on axle about tire-fixed $z$-axis |
| $R_{e}$ | Effective contact patch to wheel carrier radial distance |
| $\gamma$ | Camber angle |
| $k$ | Vertical sidewall stiffness |
| $b$ | Vertical sidewall damping |
| $\dot{\psi}$ | Tire angular velocity about the tire-fixed $z$-axis (yaw rate) |
| $w$ | Tire width |
| $\alpha^{\prime}$ | Slip angle state |
| $b_{M z}$ | Linear yaw rate resistance |
| $F_{y}$ | Lateral force acting on axle along tire-fixed $y$-axis |
| $C_{\gamma}$ | Camber stiffness |
| $C_{\alpha}$ | Lateral stiffness per slip angle |
| $\mu$ | Friction coefficient |
| $F_{z}$ | Vertical contact patch normal force along tire-fixed $z$-axis |

## Tire and Wheel Coordinate Systems

To resolve the forces and moments, the block uses the Z-Up orientation of the tire and wheel coordinate systems.

- Tire coordinate system axes $\left(X_{T}, Y_{T}, Z_{T}\right)$ are fixed in a reference frame attached to the tire. The origin is at the tire contact with the ground.
- Wheel coordinate system axes ( $X_{W}, Y_{W}, Z_{W}$ ) are fixed in a reference frame attached to the wheel. The origin is at the wheel center.


## Z-Up Orientation ${ }^{2}$



## Brakes

## Disc

If you specify the Brake Type parameter as Disc, the block implements a disc brake. This figure shows the side and front views of a disc brake.


[^2]A disc brake converts brake cylinder pressure from the brake cylinder into force. The disc brake applies the force at the brake pad mean radius.

The block uses these equations to calculate brake torque for the disc brake.

$$
\begin{aligned}
& T= \begin{cases}\frac{\mu P_{\pi B}{ }^{2} 2 R_{m} N_{\text {pads }}}{4} & \text { when } N \neq 0 \\
\frac{\mu_{\text {static }} P \pi B_{a} 2 R_{m} N_{\text {pads }}}{4} & \text { when } N=0\end{cases} \\
& R m=\frac{R o+R i}{2}
\end{aligned}
$$

The equations use these variables.

| Variable | Value |
| :--- | :--- |
| $T$ | Brake torque |
| $P$ | Applied brake pressure |
| $N$ | Wheel speed |
| $N_{\text {pads }}$ | Number of brake pads in disc brake assembly |
| $\mu_{\text {static }}$ | Disc pad-rotor coefficient of static friction |
| $\mu$ | Disc pad-rotor coefficient of kinetic friction |
| $B_{a}$ | Brake actuator bore diameter |
| $R_{m}$ | Mean radius of brake pad force application on brake rotor |
| $R_{o}$ | Outer radius of brake pad |
| $R_{i}$ | Inner radius of brake pad |

## Drum

If you specify the Brake Type parameter as Drum, the block implements a static (steady-state) simplex drum brake. A simplex drum brake consists of a single two-sided hydraulic actuator and two brake shoes. The brake shoes do not share a common hinge pin.

The simplex drum brake model uses the applied force and brake geometry to calculate a net torque for each brake shoe. The drum model assumes that the actuators and shoe geometry are symmetrical for both sides, allowing a single set of geometry and friction parameters to be used for both shoes.

The block implements equations that are derived from these equations in Fundamentals of Machine Elements.

$$
\begin{aligned}
& T_{\text {rshoe }}=\left(\frac{\pi \mu c r\left(\cos \theta_{2}-\cos \theta_{1}\right) B_{a} 2}{2 \mu\left(2 r\left(\cos \theta_{2}-\cos \theta_{1}\right)+a\left(\cos ^{2} \theta_{2}-\cos ^{2} \theta_{1}\right)\right)+a r\left(2 \theta_{1}-2 \theta_{2}+\sin 2 \theta_{2}-\sin 2 \theta_{1}\right)}\right) P \\
& T_{\text {lshoe }}=\left(\frac{\pi \mu c r\left(\cos \theta_{2}-\cos \theta_{1}\right) B_{a}^{2}}{-2 \mu\left(2 r\left(\cos \theta_{2}-\cos \theta_{1}\right)+a\left(\cos ^{2} \theta_{2}-\cos ^{2} \theta_{1}\right)\right)+\operatorname{ar}\left(2 \theta_{1}-2 \theta_{2}+\sin 2 \theta_{2}-\sin 2 \theta_{1}\right)}\right) P \\
& T=\left\{\begin{array}{l}
T_{\text {rshoe }}+T_{\text {lshoe }} \\
\left(T_{\text {rshoe }}+T_{\text {lshoe }}\right) \frac{\mu_{\text {static }}}{\mu} \\
\text { when } N \neq 0
\end{array}\right. \\
& \text { when } N=0
\end{aligned}
$$



The equations use these variables.

| Variable | Value |
| :--- | :--- |
| $T$ | Brake torque |
| $P$ | Applied brake pressure |
| $N$ | Wheel speed |
| $\mu_{\text {static }}$ | Disc pad-rotor coefficient of static friction |
| $\mu$ | Disc pad-rotor coefficient of kinetic friction |
| $T_{\text {rshoe }}$ | Right shoe brake torque |
| $T_{\text {lshoe }}$ | Left shoe brake torque |
| $a$ | Distance from drum center to shoe hinge pin center |
| $c$ | Distance from shoe hinge pin center to brake actuator connection on brake shoe |
| $r$ | Drum internal radius |
| $B_{a}$ | Brake actuator bore diameter |
| $\Theta_{1}$ | Angle from shoe hinge pin center to start of brake pad material on shoe |
| $\Theta_{2}$ | Angle from shoe hinge pin center to end of brake pad material on shoe |

## Mapped

If you specify the Brake Type parameter as Mapped, the block uses a lookup table to determine the brake torque.

$$
T=\left\{\begin{array}{lr}
f_{\text {brake }}(P, N) & \text { when } N \neq 0 \\
\left(\frac{\mu_{\text {static }}}{\mu}\right) f_{\text {brake }}(P, N) & \text { when } N=0
\end{array}\right.
$$

The equations use these variables.

| Variable | Value |
| :--- | :--- |
| $T$ | Brake torque |
| $f_{\text {brake }}(P, N)$ | Brake torque lookup table |
| $P$ | Applied brake pressure |
| $N$ | Wheel speed |
| $\mu_{\text {static }}$ | Friction coefficient of drum pad-face interface under static conditions |
| $\mu$ | Friction coefficient of disc pad-rotor interface |

The lookup table for the brake torque, $f_{\text {brake }}(P, N)$, is a function of applied brake pressure and wheel speed, where:

- $T$ is brake torque, in $\mathrm{N} \cdot \mathrm{m}$.
- $P$ is applied brake pressure, in bar.
- $N$ is wheel speed, in rpm.



## Ports

## Input

BrkPrs - Brake pressure
scalar | N-by-1 vector
Brake pressure, in Pa.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

## Dependencies

To enable this port, set the Brake Type parameter, to one of these types:

- Disc
- Drum
- Mapped

AxITrq - Axle torque
scalar | N-by-1 vector

Axle torque, $T_{a}$, about wheel spin axis, in $\mathrm{N} \cdot \mathrm{m}$.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

Vx - Longitudinal velocity
scalar | $N$-by-1 vector
Axle longitudinal velocity, $V_{x}$, along tire-fixed $x$-axis, in $\mathrm{m} / \mathrm{s}$.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.
$\mathbf{V y}$ - Lateral velocity
scalar | $N$-by- 1 vector
Axle lateral velocity, $V_{y}$, along tire-fixed $y$-axis, in $\mathrm{m} / \mathrm{s}$.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

Camber - Inclination angle
scalar | N-by-1 vector
Camber angle, $\gamma$, or inclination angle, $\varepsilon$, in rad.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

YawRate - Tire angular velocity
scalar | $N$-by-1 vector
Tire angular velocity, $r$, about the tire-fixed $z$-axis (yaw rate), in rad/s.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

Prs - Tire inflation pressure
scalar | $N$-by- 1 vector
Tire inflation pressure, $p_{i}$, in Pa.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

Gnd - Ground displacement
scalar | $N$-by-1 vector
Ground displacement along tire-fixed $z$-axis, in m . Positive input produces wheel lift.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

Fext - Axle force applied to tire
scalar | $N$-by- 1 vector

Axle force applied to tire, $F_{\text {ext }}$, along vehicle-fixed $z$-axis (positive input compresses the tire), in N .
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

ScaleFctrs - Scale factor
scalar | $N$-by- 1 vector
Scale factor to account for variations in the coefficient of friction.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

## Output

Info - Block data
bus
Block data, returned as a bus signal containing these block values.

| Signal | Description | Units |
| :--- | :--- | :--- |
| AxlTrq | Axle torque about wheel-fixed $y$-axis | $\mathrm{N} \cdot \mathrm{m}$ |
| Omega | Wheel angular velocity about wheel-fixed $y$-axis | $\mathrm{rad} / \mathrm{s}$ |
| Fx | Longitudinal vehicle force along tire-fixed $x$-axis | N |
| Fy | Lateral vehicle force along tire-fixed $y$-axis | N |
| Fz | Vertical vehicle force along tire-fixed $z$-axis | N |
| Mx | Overturning moment about tire-fixed $x$-axis | $\mathrm{N} \cdot \mathrm{m}$ |
| My | Rolling resistance torque about tire-fixed $y$-axis | $\mathrm{N} \cdot \mathrm{m}$ |
| Mz | Aligning moment about tire-fixed $z$-axis | $\mathrm{N} \cdot \mathrm{m}$ |
| Vx | Vehicle longitudinal velocity along tire-fixed $x$-axis | $\mathrm{m} / \mathrm{s}$ |
| Vy | Vehicle lateral velocity along tire-fixed $y$-axis | $\mathrm{m} / \mathrm{s}$ |
| Re | Loaded effective radius | m |
| Kappa | Longitudinal slip ratio | NA |
| Alpha | Side slip angle | rad |
| a | Contact patch half length | m |
| b | Contact patch half width | m |
| Gamma | Camber angle | rad |
| psidot | Tire angular velocity about the tire-fixed $z$-axis $($ yaw <br> rate) | $\mathrm{rad} / \mathrm{s}$ |
| BrkTrq | Brake torque about the vehicle-fixed $y$-axis | $\mathrm{N} \cdot \mathrm{m}$ |
| BrkPrs | Brake pressure | Pa |
| z | Axle vertical displacement along tire-fixed $z$-axis | m |
| zdot | Axle vertical velocity along tire-fixed $z$-axis | $\mathrm{m} / \mathrm{s}$ |


| Signal | Description | Units |
| :--- | :--- | :--- |
| Gnd | Ground displacement along tire-fixed $z$-axis (positive <br> input produces wheel lift) | m |
| GndFz | Vertical sidewall force on ground along tire-fixed $z$-axis | N |
| Prs | Tire inflation pressure | Pa |

Omega - Wheel angular velocity
scalar | $N$-by-1 vector
Wheel angular velocity, $\omega$, about wheel-fixed $y$-axis, in rad/s.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

Fx - Longitudinal axle force
scalar | $N$-by- 1 vector
Longitudinal force acting on axle, $F_{x}$, along tire-fixed $x$-axis, in $N$. Positive force acts to move the vehicle forward.

Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

## Fy - Lateral axle force

scalar | $N$-by-1 vector
Lateral force acting on axle, $F_{y}$, along tire-fixed $y$-axis, in N .
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

Fz - Vertical axle force
scalar | $N$-by-1 vector
Vertical force acting on axle, $F_{z}$, along tire-fixed $z$-axis, in N .
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

Mx - Overturning moment
scalar | $N$-by- 1 vector
Longitudinal moment acting on axle, $M_{x}$, about tire-fixed $x$-axis, in $\mathrm{N} \cdot \mathrm{m}$.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

My - Rolling resistive moment
scalar | $N$-by-1 vector
Lateral moment acting on axle, $M_{y}$, about tire-fixed $y$-axis, in $\mathrm{N} \cdot \mathrm{m}$.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

Mz - Aligning moment
scalar | $N$-by-1 vector
Vertical moment acting on axle, $M_{z}$, about tire-fixed $z$-axis, in $\mathrm{N} \cdot \mathrm{m}$.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

## Parameters

## Block Options

Brake type - Brake type
None | Disc | Drum | Mapped
Use the Brake Type parameter to select the brake.

| Action | Brake Type Setting |
| :--- | :--- |
| No braking | None |
| Implement brake that converts the <br> brake cylinder pressure into a <br> braking force | Disc |
| Implement simplex drum brake that <br> converts the applied force and brake <br> geometry into a net braking torque | Drum |
| Implement lookup table that is a <br> function of the wheel speed and <br> applied brake pressure | Mapped |

Rolling Resistance - Rolling resistance torque
None (default) | Pressure and velocity | ISO 28580|Magic Formula|Mapped torque
To calculate the rolling resistance torque, specify one of these Rolling Resistance parameters.

| Setting | Block Implementation |
| :--- | :--- |
| None | None |
| Pressure and velocity | Method in Stepwise Coastdown Methodology for Measuring <br> Tire Rolling Resistance. The rolling resistance is a function of <br> tire pressure, normal force, and velocity. |
| ISO 28580 | Method specified in ISO 28580:2018, Passenger car, truck <br> and bus tyre rolling resistance measurement method - <br> Single point test and correlation of measurement results. |
| Magic Formula | Magic formula equations from 4.E70 in Tire and Vehicle <br> Dynamics. The magic formula is an empirical equation based <br> on fitting coefficients. |
| Mapped torque | Lookup table that is a function of the normal force and spin <br> axis longitudinal velocity. |

## Dependencies

Each Rolling Resistance setting enables additional parameters.

| Setting | Parameters Enabled |
| :---: | :---: |
| Pressure and velocity | - Velocity independent force coefficient, aMy <br> - Linear velocity force component, bMy <br> - Quadratic velocity force component, cMy <br> - Tire pressure exponent, alphaMy <br> - Normal force exponent, betaMy |
| ISO 28580 | - Parasitic losses force, Fpl <br> - Rolling resistance constant, $\mathbf{C r}$ <br> - Thermal correction factor, Kt <br> - Measured temperature, Tmeas <br> - Parasitic losses force, Fpl <br> - Ambient temperature, Tamb |
| Magic Formula | Rolling resistance torque coefficient, QSY <br> Longitudinal force rolling resistance coefficient, QSY2 <br> Linear rotational speed rolling resistance coefficient, QSY3 <br> Quartic rotational speed rolling resistance coefficient, QSY4 <br> Camber squared rolling resistance torque, QSY5 <br> Load based camber squared rolling resistance torque, QSY6 <br> Normal load rolling resistance coefficient, QSY7 <br> Pressure load rolling resistance coefficient, QSY8 <br> Rolling resistance scaling factor, lam_My |
| Mapped torque | Spin axis velocity breakpoints, VxMy <br> Normal force breakpoints, FzMy <br> Rolling resistance torque map, MyMap |

## Vertical Motion - Vertical Motion

None (default) | Mapped stiffness and damping
To calculate vertical motion, specify one of these Vertical Motion parameters.

| Setting | Block Implementation |
| :--- | :--- |
| None | Block passes the applied chassis forces directly through to <br> the rolling resistance and longitudinal force calculations. |
| Mapped stiffness and damping | Vertical motion depends on wheel stiffness and damping. <br> Stiffness is a function of tire sidewall displacement and <br> pressure. Damping is a function of tire sidewall velocity and <br> pressure. |

## Dependencies

Setting Vertical Motion to Mapped stiffness and damping enables these parameters:

| Setting | Parameters Enabled |
| :---: | :---: |
| Mapped stiffness and damping | - Wheel mass, MASS <br> - Initial tire displacement, zo <br> - Initial velocity, zdoto <br> - Initial wheel vertical velocity (wheel fixed frame), zdoto <br> - Vertical deflection breakpoints, $\mathbf{z F z}$ <br> - Pressure breakpoints, pFz <br> - Force due to deflection, Fzz <br> - Vertical velocity breakpoints, zdotFz <br> - Force due to velocity, Fzzdot |

## Longitudinal and Lateral

Longitudinal stiffness, Ckappa - Longitudinal stiffness
1e7 (default) | scalar | $N$-by-1 vector
Longitudinal stiffness, $C_{K}$, specified as a scalar or $N$-by-1 vector, in N. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other longitudinal and lateral parameters.
$N$ is the number of wheels and must match the input signal dimensions.
Lateral stiffness per slip angle, Calpha - Lateral stiffness
4.5 e 4 (default) | scalar | $N$-by-1 vector

Lateral stiffness per slip angle, $C_{\alpha}$, specified as a scalar or $N$-by- 1 vector, in $N /$ rad. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other longitudinal and lateral parameters.
$N$ is the number of wheels and must match the input signal dimensions.

## Camber stiffness, Cgamma - Camber stiffness

1e3 (default) | scalar | $N$-by-1 vector
Camber stiffness, $C_{\gamma}$, specified as a scalar or $N$-by- 1 vector, in $\mathrm{N} /$ rad. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other longitudinal and lateral parameters.
$N$ is the number of wheels and must match the input signal dimensions.
Kinematic friction, muMin - Kinematic friction
0.8 (default) | scalar | $N$-by-1 vector

Kinematic friction, $\mu_{k}$, specified as a scalar or $N$-by- 1 vector, dimensionless. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other longitudinal and lateral parameters.
$N$ is the number of wheels and must match the input signal dimensions.
Static friction, muMax - Static friction
1 (default) | scalar | $N$-by- 1 vector
Static friction, $\mu_{s}$, specified as a scalar or $N$-by- 1 vector, dimensionless. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other longitudinal and lateral parameters.
$N$ is the number of wheels and must match the input signal dimensions.
Longitudinal relaxation length, Lrelx - Longitudinal relaxation length
0.05 (default) | scalar | $N$-by-1 vector

Longitudinal relaxation length, $L_{\text {relx }}$, specified as a scalar or $N$-by- 1 vector, in $m$. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other longitudinal and lateral parameters.
$N$ is the number of wheels and must match the input signal dimensions.
Lateral relaxation length, Lrely - Lateral relaxation length
0.15 (default) | scalar | $N$-by-1 vector

Lateral relaxation length, $L_{\text {rely }}$, in $\mathrm{m} / \mathrm{rad}$.
Lateral relaxation length, $L_{\text {rely }}$, specified as a scalar or $N$-by-1 vector, in m/rad. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other longitudinal and lateral parameters.
$N$ is the number of wheels and must match the input signal dimensions.

## Rolling

Rotational damping, br - Rotational damping
scalar | $N$-by- 1 vector
Rotational damping, specified as a scalar or $N$-by-1 vector, in $N \cdot m \cdot s / r a d$. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other rotational parameters.
$N$ is the number of wheels and must match the input signal dimensions.
Rotational inertia (rolling axis), IYY - Rotational inertia
scalar | N-by-1 vector

Rotational inertia (rolling axis), specified as a scalar or $N$-by-1 vector, in $\mathrm{kg} \cdot \mathrm{m}^{2}$. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other rotational parameters.
$N$ is the number of wheels and must match the input signal dimensions.
Initial rotational velocity, omegao - Initial rotational velocity
scalar | $N$-by-1 vector
Initial rotational velocity, specified as a scalar or $N$-by-1 vector, in rad/s. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other rotational parameters.
$N$ is the number of wheels and must match the input signal dimensions.
Unloaded radius, UNLOADED_RADIUS - Unloaded radius
0.309384029954441 (default) $\mid$ scalar

Unloaded radius, in m.

## Pressure and Velocity

Velocity independent force coefficient, $\mathbf{a M y}$ - Velocity-independent force coefficient
8e-4 (default) | scalar
Velocity-independent force coefficient, $a$, in $\mathrm{s} / \mathrm{m}$.

## Dependencies

To enable this parameter, set Rolling Resistance to Pressure and velocity.
Linear velocity force component, bMy - Linear velocity force component
0.001 (default) | scalar

Linear velocity force component, $b$, in $\mathrm{s} / \mathrm{m}$.

## Dependencies

To enable this parameter, set Rolling Resistance to Pressure and velocity.
Quadratic velocity force component, cMy - Quadratic velocity force component 1.6e-4 (default) | scalar

Quadratic velocity force component, $c$, in $\mathrm{s}^{\wedge} 2 / \mathrm{m}^{\wedge} 2$.

## Dependencies

To enable this parameter, set Rolling Resistance to Pressure and velocity.
Tire pressure exponent, alphaMy - Tire pressure exponent

- 0.003 (default) | scalar

Tire pressure exponent, $\alpha$, dimensionless.
Dependencies
To enable this parameter, set Rolling Resistance to Pressure and velocity.

Normal force exponent, betaMy - Normal force exponent

### 0.97 (default) | scalar

Normal force exponent, $\beta$, dimensionless.

## Dependencies

To enable this parameter, set Rolling Resistance to Pressure and velocity.
ISO 28580
Parasitic losses force, FpI - Parasitic force loss
10 (default) | scalar
Parasitic force loss, $F_{p l}$ in N.

## Dependencies

To enable this parameter, set Rolling Resistance to ISO 28580.
Rolling resistance constant, $\mathbf{C r}$ - Rolling resistance constant
1e-3 (default) | scalar
Rolling resistance constant, $C_{r}$, in $\mathrm{N} / \mathrm{kN}$. ISO 28580 specifies the rolling resistance unit as one newton of tractive resistance for every kilonewtons of normal load.

## Dependencies

To enable this parameter, set Rolling Resistance to ISO 28580.
Thermal correction factor, $\mathbf{K t}$ - Thermal correction factor
0.008 (default) | scalar

Thermal correction factor, $K_{t}$, in $1 /$ degC.

## Dependencies

To enable this parameter, set Rolling Resistance to ISO 28580.
Measured temperature, Tmeas - Temperature during testing
298.15 (default) | scalar

Measured ambient temperature, $T_{\text {meas }}$, near tire during tire testing, in K.

## Dependencies

To enable this parameter, set Rolling Resistance to ISO 28580.
Ambient temperature, Tamb - Temperature in application environment 298.15 (default) | scalar

Measured ambient temperature, $T_{\text {amb }}$, near tire in application environment, in K. For example, the measured ambient temperature is the ambient temperature near the tire when the vehicle is on the road.

## Dependencies

To enable this parameter, set Rolling Resistance to ISO 28580.

Input ambient temperature - Option to input ambient temperature
off (default) | on
Select to create input port Tamb to input the measured ambient temperature.
The measured ambient temperature, $T_{a m b}$, is the temperature near tire in application environment, in K. For example, the measured ambient temperature is the ambient temperature near the tire when the vehicle is on the road.

## Dependencies

To enable this parameter, set Rolling Resistance to IS0 28580.

## Magic Formula

Rolling resistance torque coefficient, QSY1 - Torque coefficient

### 0.007 (default) | scalar

Rolling resistance torque coefficient, dimensionless.

## Dependencies

To enable this parameter, set Rolling Resistance to Magic Formula.
Longitudinal force rolling resistance coefficient, QSY2 - Force resistance coefficient
0 (default) | scalar
Longitudinal force rolling resistance coefficient, dimensionless.

## Dependencies

To enable this parameter, set Rolling Resistance to Magic Formula.
Linear rotational speed rolling resistance coefficient, QSY3 - Linear speed coefficient 0.0015 (default) | scalar

Linear rotational speed rolling resistance coefficient, dimensionless.

## Dependencies

To enable this parameter, set Rolling Resistance to Magic Formula.
Quartic rotational speed rolling resistance coefficient, QSY4 - Quartic speed coefficient 8.5e-05 (default) | scalar

Quartic rotational speed rolling resistance coefficient, dimensionless.

## Dependencies

To enable this parameter, set Rolling Resistance to Magic Formula.
Camber squared rolling resistance torque, QSY5 - Camber resistance torque
0 (default) | scalar
Camber squared rolling resistance torque, in $1 / \mathrm{rad}^{\wedge} 2$.

## Dependencies

To enable this parameter, set Rolling Resistance to Magic Formula.

Load based camber squared rolling resistance torque, QSY6 - Load resistance torque 0 (default) | scalar

Load based camber squared rolling resistance torque, in $1 / \mathrm{rad}^{\wedge} 2$.

## Dependencies

To enable this parameter, set Rolling Resistance to Magic Formula.
Normal load rolling resistance coefficient, QSY7 - Normal resistance coefficient 0.9 (default) | scalar

Normal load rolling resistance coefficient, dimensionless.

## Dependencies

To enable this parameter, set Rolling Resistance to Magic Formula.
Pressure load rolling resistance coefficient, QSY8 - Pressure resistance coefficient
-0.4 (default) | scalar
Pressure load rolling resistance coefficient, dimensionless.

## Dependencies

To enable this parameter, set Rolling Resistance to Magic Formula.
Rolling resistance scaling factor, lam_My - Scaling factor
1 (default) | scalar
Rolling resistance scaling factor, dimensionless.

## Dependencies

To enable this parameter, set Rolling Resistance to Magic Formula.

## Mapped

Spin axis velocity breakpoints, $\mathbf{V x M y}$ - Spin axis velocity breakpoints
-20:1:20 (default) | vector
Spin axis velocity breakpoints, in $\mathrm{m} / \mathrm{s}$.

## Dependencies

To enable this parameter, set Rolling Resistance to Mapped torque.
Normal force breakpoints, FzMy - Normal force breakpoints
0:200:1e4 (default) | vector
Normal force breakpoints, in N.

## Dependencies

To enable this parameter, set Rolling Resistance to Mapped torque.
Rolling resistance torque map, MyMap - Rolling resistance torque map array

Rolling resistance torque versus axle speed and normal force, in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

To enable this parameter, set Rolling Resistance to Mapped torque.

## Aligning

Wheel width, WIDTH - Wheel width
scalar
Wheel width, WIDTH, in m .
Linear yaw rate resistance, bMz - Linear yaw rate resistance
0 | scalar
Linear yaw rate resistance, $b_{M z}$, in $\mathrm{N} \cdot \mathrm{m} \cdot \mathrm{s} / \mathrm{rad}$.

## Brake

Static friction coefficient, mu_static - Static friction coefficient
0.3 (default) | scalar | $N$-by-1 vector

Static friction coefficient, specified as a scalar or $N$-by-1 vector, dimensionless. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other brake parameters.
$N$ is the number of wheels and must match the input signal dimensions.

## Dependencies

To enable this parameter, set Brake Type to Disc, Drum, or Mapped
Kinetic friction coefficient, mu_kinetic - Kinetic friction

## 0.2 (default) | scalar | $N$-by-1 vector

Kinematic friction coefficient, specified as a scalar or $N$-by-1 vector, dimensionless. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other brake parameters.
$N$ is the number of wheels and must match the input signal dimensions.

## Dependencies

To enable this parameter, set Brake Type to Disc, Drum, or Mapped
Disc
Disc brake actuator bore, disc_abore - Bore distance
0.05 (default) | scalar | $N$-by-1 vector

Disc brake actuator bore, specified as a scalar or $N$-by-1 vector, in m . If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other brake parameters.
$N$ is the number of wheels and must match the input signal dimensions.

## Dependencies

To enable this parameter, set Brake Type to Disc.
Brake pad mean radius, Rm - Radius
0.177 (default) | scalar | N-by-1 vector

Brake pad mean radius, specified as a scalar or $N$-by-1 vector, in $m$. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other brake parameters.
$N$ is the number of wheels and must match the input signal dimensions.

## Dependencies

To enable this parameter, set Brake Type to Disc.
Number of brake pads, num_pads - Number of brake pads
2 (default) | scalar $\mid N$-by-1 vector
Number of brake pads, specified as a scalar or $N$-by-1 vector, dimensionless. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other brake parameters.
$N$ is the number of wheels and must match the input signal dimensions.

## Dependencies

To enable this parameter, set Brake Type to Disc.

## Drum

## Drum brake actuator bore, disc_abore - Bore distance 0.0508 (default) | scalar | $N$-by-1 vector

Drum brake actuator bore, specified as a scalar or $N$-by-1 vector, in m. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other brake parameters.
$N$ is the number of wheels and must match the input signal dimensions.

## Dependencies

To enable this parameter, set Brake Type to Drum.
Shoe pin to drum center distance, drum_a - Shoe pin to drum center distance
0.123 (default) | scalar

Shoe pin to drum center distance, in $m$.

## Dependencies

To enable this parameter, set Brake Type to Drum.
Shoe pin center to force application point distance, drum_c - Shoe pin center to force application point distance
0.212 (default) | scalar

Shoe pin center to force application point distance, in $m$.

## Dependencies

To enable this parameter, set Brake Type to Drum.
Drum internal radius, drum_r - Drum internal radius
0.15 (default) | scalar

Drum internal radius, in $m$.

## Dependencies

To enable this parameter, set Brake Type to Drum.
Shoe pin to pad start angle, drum_thetal - Shoe pin to pad start angle 0 (default) | scalar

Shoe pin to pad start angle, in deg.
Dependencies
To enable this parameter, set Brake Type to Drum.
Shoe pin to pad end angle, drum_theta2 - Shoe pin to pad end angle
126 (default) | scalar
Shoe pin to pad end angle, in deg.

## Dependencies

To enable this parameter, set Brake Type to Drum.
Mapped
Brake actuator pressure breakpoints, brake_p_bpt - Brake actuator pressure breakpoints vector

Brake actuator pressure breakpoints, in bar.

## Dependencies

To enable this parameter, set Brake Type to Mapped.
Wheel speed breakpoints, brake_n_bpt - Wheel speed breakpoints
vector
Wheel speed breakpoints, in rpm.

## Dependencies

To enable this parameter, set Brake Type to Mapped.
Brake torque map, f_brake_t - Lookup table for brake torque array

The lookup table for the brake torque, $f_{\text {brake }}(P, N)$, is a function of applied brake pressure and wheel speed, where:

- $T$ is brake torque, in $\mathrm{N} \cdot \mathrm{m}$.
- $\quad P$ is applied brake pressure, in bar.
- $N$ is wheel speed, in rpm.



## Dependencies

To enable this parameter, set Brake Type to Mapped.

## Vertical

Wheel mass, m - Wheel mass
9.46491996974568 (default) | scalar | $N$-by-1 vector

Wheel mass, specified as a scalar or $N$-by- 1 vector, in kg. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other vertical parameters.
$N$ is the number of wheels and must match the input signal dimensions.

## Dependencies

To enable this parameter, set Vertical Motion to Mapped stiffness and damping.
Initial tire deflection, zo - Initial tire deflection
0 (default) | scalar $\mid N$-by- 1 vector
Initial tire displacement, specified as a scalar or $N$-by-1 vector, in m. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other vertical parameters.
$N$ is the number of wheels and must match the input signal dimensions.

## Dependencies

To enable this parameter, set Vertical Motion to Mapped stiffness and damping.
Initial wheel vertical velocity (wheel fixed frame), zdoto - Initial wheel velocity
0 (default) | scalar $\mid N$-by- 1 vector
Initial wheel vertical velocity, specified as a scalar or $N$-by-1 vector, in $\mathrm{m} / \mathrm{s}$. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other vertical parameters.
$N$ is the number of wheels and must match the input signal dimensions.

## Dependencies

To enable this parameter, set Vertical Motion to Mapped stiffness and damping.
Gravitational acceleration, GRAVITY - Gravitational acceleration
-9.81 (default) | scalar
Gravitational acceleration, in m/s^2.

## Dependencies

To enable this parameter, set Vertical Motion to Mapped stiffness and damping.

## Mapped Stiffness and Damping

Vertical deflection breakpoints, zFz - Vertical deflection breakpoints
[0 . 01 .1] (default) | vector
Vector of sidewall deflection breakpoints corresponding to the force table, in m .

## Dependencies

To enable this parameter, set Vertical Motion to Mapped stiffness and damping.
Pressure breakpoints, pFz - Pressure breakpoints
[10000 1000000] (default) | vector
Vector of pressure data points corresponding to the force table, in Pa.

## Dependencies

To enable this parameter, set Vertical Motion to Mapped stiffness and damping.
Force due to deflection, Fzz - Force due to deflection
[0 1e3 1e4; 0 le4 1e5] (default)|vector
Force due to sidewall deflection and pressure along wheel-fixed $z$-axis, in N .

## Dependencies

To enable this parameter, set Vertical Motion to Mapped stiffness and damping.
Vertical velocity breakpoints, zdotFz - Vertical velocity breakpoints
[-20 0 20] (default) | scalar
Vector of sidewall velocity breakpoints corresponding to the force due to velocity table, in m.

## Dependencies

To enable this parameter, set Vertical Motion to Mapped stiffness and damping.
Force due to velocity, Fzzdot - Force due to velocity
[500 0-500;250 0-250] (default) | array
Force due to sidewall velocity and pressure along wheel-fixed $z$-axis, in N .

## Dependencies

To enable this parameter, set Vertical Motion to Mapped stiffness and damping.

## Simulation

Maximum normal force, FZMAX - Maximum normal force
10000 (default) | scalar
Maximum normal force, in N. Used with all vertical force calculations.
Minimum normal force, FZMIN - Minimum normal force
0 (default) | scalar
Minimum normal force, in N. Used with all vertical force calculations.
Maximum pressure, PRESMAX - Maximum pressure
1003118 (default) | scalar
Maximum pressure, PRESMAX, in Pa.
Minimum pressure, PRESMIN - Minimum pressure
9982 (default) | scalar
Minimum pressure, PRESMIN, in Pa.
Max allowable slip ratio (absolute), KPUMAX - Max allowable slip ratio
0.999 (default) | scalar

Max allowable slip ratio (absolute), KPUMAX, dimensionless.
Minimum allowable slip ratio (absolute), KPUMIN - Minimum allowable slip ratio
-0.999 (default) | scalar
Minimum allowable slip ratio (absolute), KPUMIN, dimensionless.
Max allowable slip angle (absolute), ALPMAX - Max allowable slip angle
1.5708 (default) | scalar

Max allowable slip angle (absolute), ALPMAX, in rad.
Minimum allowable slip angle (absolute), ALPMIN - Minimum allowable slip angle - 1.5708 (default) | scalar

Minimum allowable slip angle (absolute), ALPMIN, in rad.
Maximum allowable camber angle, CAMMAX - Maximum allowable camber angle 0.173 | scalar

Maximum allowable camber angle CAMMAX, in rad.
Minimum allowable camber angle, CAMMIN - Minimum allowable camber angle -0.173 | scalar

Minimum allowable camber angle, CAMMIN, in rad.

Minimum ambient temperature, TMIN - Minimum ambient temperature 0 (default) | scalar

Minimum ambient temperature, $T_{\text {MIN }}$, in K .

## Dependencies

To enable this parameter, set Rolling Resistance to ISO 28580.
Maximum ambient temperature, TMAX - Maximum ambient temperature 400 (default) | scalar

Maximum ambient temperature, $T_{\text {MAX }}$, in K .

## Dependencies

To enable this parameter, set Rolling Resistance to ISO 28580.

## Version History

Introduced in R2019a

## R2022b: Specify Brake and Tire Parameters for Each Wheel

Behavior changed in R2022b
Starting from R2022b, you can to use the Fiala Wheel 2DOF block to specify brake and tire characteristics for each wheel on your vehicle. Specifically, the block allows $N$-by- 1 vectors for these parameters:

- Static friction coefficient, mu_static
- Kinetic friction coefficient, mu_kinetic
- Disc brake actuator bore, disc_abore
- Brake pad mean radius, Rm
- Number of brake pads, num_pads
- Drum brake actuator bore, disc_abore
- Initial rotational velocity, omegao
- Rotational damping, br
- Wheel mass, m
- Rotational inertia (rolling axis), IYY
- Initial tire displacement, zo
- Initial wheel vertical velocity (wheel fixed frame), zdoto
- Longitudinal stiffness, Ckappa
- Lateral stiffness per slip angle, Calpha
- Camber stiffness, Cgamma
- Kinematic friction, muMin
- Static friction, muMax
- Longitudinal relaxation length, Lrelx
- Lateral relaxation length, Lrely
$N$ is the number of wheels and must match the input signal dimensions.


## References

[1] Fiala, E. "Seitenkrafte am Rollenden Luftreifen." VDI Zeitschrift, V.D.I.. Vol 96, 1954.
[2] Highway Tire Committee. Stepwise Coastdown Methodology for Measuring Tire Rolling Resistance. Standard J2452_199906. Warrendale, PA: SAE International, June 1999.
[3] ISO 28580:2018. Passenger car, truck and bus tyre rolling resistance measurement method Single point test and correlation of measurement results. ISO (International Organization for Standardization), 2018.
[4] Pacejka, H. B. Tire and Vehicle Dynamics. 3rd ed. Oxford, UK: SAE and Butterworth-Heinemann, 2012.

## Extended Capabilities

C/C++ Code Generation
Generate C and C++ code using Simulink ${ }^{\circledR}$ Coder ${ }^{\mathrm{TM}}$.

## See Also

Combined Slip Wheel 2DOF | Combined Slip Wheel 2DOF CPI | Combined Slip Wheel 2DOF STI | Longitudinal Wheel | Dugoff Wheel 2DOF

Topics
"Coordinate Systems in Vehicle Dynamics Blockset"

## Combined Slip Wheel CPI

Combined slip wheel compliant with CPI Tydex standard


## Libraries:

Vehicle Dynamics Blockset / Wheels and Tires

## Description

The Combined Slip Wheel CPI block implements the longitudinal and lateral behavior of a wheel characterized by the Magic Formula ${ }^{1,2}$ that complies with the contact point interface (CPI) Tyre Data Exchange Format (TYDEX) ${ }^{3}$ standard. You can import your own tire data or use fitted tire data sets provided by the Global Center for Automotive Performance Simulation (GCAPS). Use the block in driveline and vehicle simulations where low-frequency tire-road interactions are required to determine vehicle acceleration, braking, and wheel-rolling resistance. The block is suitable for applications that require combined lateral slip, for example, in lateral motion and yaw stability studies.

Based on the wheel rotational velocity, longitudinal and lateral velocity, wheel camber angle, and inflation pressure, the block determines the vertical motion, forces, and moments in all six degrees of freedom (DOF). Use the vertical DOF to study tire-suspension resonances from road profiles or chassis motion.

Use the Tire type parameter to select the source of the tire data.

| Goal | Action |
| :--- | :--- |
| Implement the Magic Formula using <br> empirical equations <br> use fitting coefficients that equations <br> correspond to the block parameters. | Update the block parameters with fitting coefficients from a <br> file: |
|  | 1Set Tire type to External file.  <br> $\mathbf{2}$ On the External tire source pane, Click Select file. <br> $\mathbf{3}$ Select the tire coefficient file. <br> $\mathbf{4}$ Click Update mask values from file. In the dialog box <br> that prompts you for confirmation, click OK. The block  <br> updates the parameters.  |
|  | $\mathbf{5} \quad$ Click Apply. |


| Goal | Action |
| :---: | :---: |
| Implement fitted tire data sets provided by the Global Center for Automotive Performance Simulation (GCAPS). | Update the applicable block parameters with GCAPS fitted tire data: <br> 1 Set Tire type to the tire that you want to implement. Options include: <br> - Light passenger car 205/60R15 <br> - Mid-size passenger car 235/45R18 <br> - Performance car 225/40R19 <br> - SUV 265/50R20 <br> - Light truck 275/65R18 <br> - Commercial truck 295/75R22.5 <br> 2 Click Update applicable Tire Parameters with tire type values. On the Tire Parameters tab, the block updates the applicable parameters, including Wheel width, Rim radius, and Wheel mass. <br> Click Apply. |

## Rotational Wheel Dynamics

The block calculates the inertial response of the wheel subject to:

- Axle losses
- Tire rolling resistance
- Ground contact through the tire-road interface

To implement the Magic Formula, the block uses these equations from the cited references:

| Calculation | Equations |
| :--- | :--- |
| Longitudinal force | Tire and Vehicle Dynamics ${ }^{2}$ equations 4.E9 through 4.E57 |
| Lateral force - pure <br> sideslip | Tire and Vehicle Dynamics ${ }^{2}$ equations 4.E19 through 4.E30 |
| Lateral force - combined <br> slip | Tire and Vehicle Dynamics ${ }^{2}$ equations 4.E58 through 4.E67 |
| Vertical dynamics | Tire and Vehicle Dynamics ${ }^{2}$ equations 4.E68, 4.E1, 4.E2a, and 4.E2b |
| Overturning couple | Tire and Vehicle Dynamics ${ }^{2}$ equation 4.E69 |
| Rolling resistance | - An improved Magic Formula/Swift tyre model that can handle inflation $_{\text {pressure changes }{ }^{1} \text { equation 6.1.2 }}$ <br> Tire and Vehicle Dynamics ${ }^{2}$ equation 4.E70 |
| Aligning moment  <br> Aligning torque - Tire and Vehicle Dynamics ${ }^{2}$ equation 4.E31 through 4.E49Tire and Vehicle Dynamics ${ }^{2}$ equation 4.E71 through 4.E78 <br> If you clear Include turn slip, the block sets some of these equations to 1. |  |

## CPI Tire Coordinate System

The block uses tire coordinate system axes $\left(X_{T}, Y_{T}, Z_{T}\right)$ that are fixed in a reference frame attached to the tire. The origin is at the tire contact with the ground.

The CPI tire coordinate system is shown in red.

Note The CPI tire coordinate system (red) is equivalent to the TYDEX wheel-axis coordinate system.

3


| Axis | Description |
| :--- | :--- |
| $X_{T}$ | $X_{T}$ and $Y_{T}$ are parallel to the road plane. The intersection of the wheel plane and <br> the road plane define the orientation of the $X_{T}$ axis. |
| $Y_{T}$ | $Y_{T}$ is the projection of the wheel spin axis on the ground. |
| $Z_{T}$ | $Z_{T}$ points upward. |

## Ports

## Input

Omega - Rotational velocity
scalar | N-by-1 vector
Tire rotational velocity, $\omega$, about wheel spin axis, in rad/s.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

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Vx - Longitudinal velocity
scalar | $N$-by-1 vector
Axle longitudinal velocity, $V_{x}$, along tire-fixed $x$-axis, in $\mathrm{m} / \mathrm{s}$.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.
$\mathbf{V y}$ - Lateral velocity
scalar | $N$-by-1 vector
Axle lateral velocity, $V_{y}$, along tire-fixed $y$-axis, in $\mathrm{m} / \mathrm{s}$.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

Camber - Inclination angle
scalar | $N$-by-1 vector
Camber angle, $\gamma$, or inclination angle, $\varepsilon$, in rad.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

YawRate - Tire angular velocity
scalar | $N$-by-1 vector
Tire angular velocity, $r$, about the tire-fixed $z$-axis (yaw rate), in rad/s.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

Fext - Axle force applied to tire scalar | $N$-by-1 vector

Axle force applied to tire, $F_{\text {ext }}$, along vehicle-fixed $z$-axis (positive input compresses the tire), in N .
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

## ScaleFctrs - Road friction scale factors

2-by-N array
Magic formula road friction scale factor array. Array dimensions are 2 by the number of wheels, $N$.
The Magic Formula equations use scale factors to account for static or simulation run-time variations. Nominally, most are set to 1 .

| Array Element | Variable | Scale Factor |
| :--- | :--- | :--- |
| ScaleFctrs $(1,1)$ | lam_mux | Longitudinal peak friction coefficient |
| ScaleFctrs $(2,1)$ | lam_muy | Lateral peak friction coefficient |

Prs - Tire inflation pressure scalar | N-by-1 vector

Tire inflation pressure, $p_{i}$, in Pa.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

## Dependencies

To create this port, select Input tire pressure.

## Output

## Info - Block data

bus
Block data, returned as a bus signal containing these block values.

| Signal | Description | Units |
| :--- | :--- | :--- |
| Omega | Wheel angular velocity about wheel-fixed $y$-axis | $\mathrm{rad} / \mathrm{s}$ |
| Fx | Longitudinal vehicle force along tire-fixed $x$-axis | N |
| Fy | Lateral vehicle force along tire-fixed $y$-axis | N |
| Fz | Vertical vehicle force along tire-fixed $z$-axis | N |
| Mx | Overturning moment about tire-fixed $x$-axis | $\mathrm{N} \cdot \mathrm{m}$ |
| My | Rolling resistance torque about tire-fixed $y$-axis | $\mathrm{N} \cdot \mathrm{m}$ |
| Mz | Aligning moment about tire-fixed $z$-axis | $\mathrm{N} \cdot \mathrm{m}$ |
| Vx | Vehicle longitudinal velocity along tire-fixed $x$-axis | $\mathrm{m} / \mathrm{s}$ |
| Vy | Vehicle lateral velocity along tire-fixed $y$-axis | $\mathrm{m} / \mathrm{s}$ |
| Re | Loaded effective radius | m |
| Kappa | Longitudinal slip ratio | NA |
| Alpha | Side slip angle | rad |
| a | Contact patch half length | m |
| b | Contact patch half width | m |
| Gamma | Camber angle | rad |
| psidot | Tire angular velocity about the tire-fixed $z$-axis (yaw <br> rate) | $\mathrm{rad} / \mathrm{s}$ |
| rhoz | Axle vertical displacement along tire-fixed $z$-axis | m |
| FNormal | Vertical sidewall force on ground along tire-fixed $z$-axis | N |
| Prs | Tire inflation pressure | Pa |

## Fx - Longitudinal axle force

scalar | N-by-1 vector
Longitudinal force acting on axle, $F_{x}$, along tire-fixed $x$-axis, in N. Positive force acts to move the vehicle forward.

Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

Fy - Lateral axle force
scalar | $N$-by-1 vector
Lateral force acting on axle, $F_{y}$, along tire-fixed $y$-axis, in $N$.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

Fz - Vertical axle force
scalar $\mid N$-by-1 vector
Vertical force acting on axle, $F_{z}$, along tire-fixed $z$-axis, in N .
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

Mx - Overturning moment
scalar | $N$-by-1 vector
Longitudinal moment acting on axle, $M_{x}$, about tire-fixed $x$-axis, in $\mathrm{N} \cdot \mathrm{m}$.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

My - Rolling resistive moment
scalar | $N$-by-1 vector
Lateral moment acting on axle, $M_{y}$, about tire-fixed $y$-axis, in $\mathrm{N} \cdot \mathrm{m}$.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

Mz - Aligning moment
scalar | $N$-by-1 vector
Vertical moment acting on axle, $M_{z}$, about tire-fixed $z$-axis, in $\mathrm{N} \cdot \mathrm{m}$.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

## Parameters

## Block Options

Tire type - Type
External file (default)| Light passenger car 205/60R15|Mid-size passenger car 235/45R18|Performance car 225/40R19|SUV 265/50R20|Light truck 275/65R18| Commercial truck 295/75R22.5

Use the Tire type parameter to select the source of the tire data.

| Goal | Action |
| :---: | :---: |
| Implement the Magic Formula using empirical equations ${ }^{1,2}$. The equations use fitting coefficients that correspond to the block parameters. | Update the block parameters with fitting coefficients from a file: <br> Set Tire type to External file. <br> On the External tire source pane, Click Select file. <br> Select the tire coefficient file. <br> Click Update mask values from file. In the dialog box that prompts you for confirmation, click $\mathbf{O K}$. The block updates the parameters. <br> 5 Click Apply. |
| Implement fitted tire data sets provided by the Global Center for Automotive Performance Simulation (GCAPS). | Update the applicable block parameters with GCAPS fitted tire data: <br> 1 Set Tire type to the tire that you want to implement. Options include: <br> - Light passenger car 205/60R15 <br> - Mid-size passenger car 235/45R18 <br> - Performance car 225/40R19 <br> - SUV 265/50R20 <br> - Light truck 275/65R18 <br> - Commercial truck 295/75R22.5 <br> 2 Click Update applicable Tire Parameters with tire type values. On the Tire Parameters tab, the block updates the applicable parameters, including Wheel width, Rim radius, and Wheel mass. <br> 3 Click Apply. |

## Tire file or object, tireParamSet - Tire file

.mat|.tir|.txt
Tire file .tir or object containing empirical data to model tire longitudinal and lateral behavior with the Magic Formula. If you provide an .txt file, make sure the file contains names that correspond to the block parameters.

Update the block parameters with fitting coefficients from a file:

- Set Tire type to External file.
- On the External tire source pane, select Select file.
- Select the tire coefficient file.
- Select Update mask values from file. In the dialog box that prompts you for confirmation, click $\mathbf{O K}$. The block updates the parameters.
- Select Apply.

Tire side - Select tire side
Right (default) | Left | Symmetric

Specify the tire side.
Tire pressure - Pressure 220000 (default) | scalar

Tire inflation pressure, $p$, in Pa.

## Dependencies

To enable this parameter, clear Input tire pressure.
Ply steer - Include ply steer
on (default) | off
Select to include ply steer in the Magic Formula equations.
By default, the blocks include ply steer and turn slip in the Magic Formula equations. The equations are fit to flat-belt test data and predict a number of tire effects, including ply steer and turn slip. Consider removing the effects if your:

- Test data does not include ply steer or turn slip data.
- Analysis does not require ply steer or turn slip effects.

If you clear Ply steer, the block internally sets these parameters to 0 :

- Vertical shift of overturning moment, QSX1
- Combined slip Fx shift factor reduction, RHX1
- Efy curvature constant camber dependency, PEY3
- SHY horizontal shift at FZNOM, PHY1
- SHY variation with load, PHY2
- Svy/Fz vertical shift at FZNOM, PVY1
- Svy/Fz variation with load, PVY2
- Fy shift reduction with slip angle, RBY3
- Slip ratio side force Svyk/Muy*Fz at FZNOM, RVY1
- Side force Svyk/Muy*Fz variation with load, RVY2
- Bpt slope variation with camber, QBZ4
- Dpt peak trail variation with camber, QDZ3
- Dmr peak residual torque, QDZ6
- Dmr peak residual torque variation with load, QDZ7
- Ept variation with sign of alpha-t, QEZ4
- Sht horizontal trail shift at FZNOM, QHZ1
- Sht variation with load, QHZ2
- Nominal value of s/R0: effect of Fx on Mz, SSZ1

Turn slip - Include turn slip
on (default) | off
Select to include ply steer in Magic Formula equations.

By default, the blocks include ply steer and turn slip in the Magic Formula equations. The equations are fit to flat-belt test data and predict a number of tire effects, including ply steer and turn slip. Consider removing the effects if your:

- Test data does not include ply steer or turn slip data.
- Analysis does not require ply steer or turn slip effects.

If you clear Turn slip, the block internally:

- Sets the Magic Formula turn slip equations to 1. Specifically, equations 4.E77, 4.E79, 4.E81, 4.E83, 4.E84, 4.E92, 4.E102, 4.E101, and 4.E105. ${ }^{2}$.
- Uses Magic Formula terms that effect horizontal shift.
- Uses Magic Formula small turn slip values in 4.E27².


## Simulation

Maximum pressure, PRESMAX - Maximum pressure 1003118 (default) | scalar

Maximum pressure, PRESMAX, in Pa.
Minimum pressure, PRESMIN - Minimum pressure
9982 (default) | scalar
Minimum pressure, PRESMIN, in Pa.
Maximum normal force, FZMAX - Force
scalar
Maximum normal force, FZMAX, in N.
Minimum normal force, FZMIN - Force
scalar
Minimum normal force, FZMIN, in N.
Velocity tolerance used to handle low velocity situations, VXLOW - Tolerance
scalar
Velocity tolerance used to handle low-velocity situations, VXLOW, in m/s.
Max allowable slip ratio (absolute), KPUMAX - Max allowable slip ratio
0.999 (default) | scalar

Max allowable slip ratio (absolute), KPUMAX, dimensionless.
Minimum allowable slip ratio (absolute), KPUMIN - Minimum allowable slip ratio -0. 999 (default) | scalar

Minimum allowable slip ratio (absolute), KPUMIN, dimensionless.
Max allowable slip angle (absolute), ALPMAX - Max allowable slip angle 1.5708 (default) | scalar

Max allowable slip angle (absolute), $A L P M A X$, in rad.

Minimum allowable slip angle (absolute), ALPMIN - Minimum allowable slip angle - 1.5708 (default) | scalar

Minimum allowable slip angle (absolute), ALPMIN, in rad.
Maximum allowable camber angle, CAMMAX - Maximum allowable camber angle 0.173 | scalar

Maximum allowable camber angle $C A M M A X$, in rad.
Minimum allowable camber angle, CAMMIN - Minimum allowable camber angle -0. 173 | scalar

Minimum allowable camber angle, CAMMIN, in rad.
Nominal longitudinal speed, LONGVL - Speed scalar

Nominal longitudinal speed, $L O N G V L$, in $\mathrm{m} / \mathrm{s}$.
Default tyre side, tyreside - Side
'Right' (default)|char
Default tyre side, tyreside, dimensionless.
Wheel
Initial rotational velocity, omegao - Velocity
scalar
Initial rotational velocity, specified as a scalar, in rad/s.
Rotational damping, br - Damping
scalar
Rotational damping, specified as a scalar, in $\mathrm{N} \cdot \mathrm{m} \cdot \mathrm{s} / \mathrm{rad}$.
Unloaded radius, UNLOADED_RADIUS - Radius
scalar
Unloaded radius, UNLOADED_RADIUS, in m .
Nominal pressure, NOMPRES - Pressure
scalar
Nominal pressure, NOMPRES, in Pa.
Nominal normal force, FNOMIN - Force scalar

Nominal normal force, FNOMIN, in N.
Wheel width, WIDTH - Width
scalar
Wheel width, WIDTH, in m.

## Rim radius, RIM_RADIUS - Radius

scalar
Rim radius, RIM_RADIUS, in m.
Nominal aspect ratio, ASPECT_RATIO - Ratio
scalar
Nominal aspect ratio, ASPECT_RATIO, dimensionless.
Inertial
Wheel mass, MASS - Mass
scalar
Wheel mass, specified as a scalar, in kg.
Rotational inertia (rolling axis), IYY - Inertia
scalar
Rotational inertia (rolling axis), specified as a scalar, in $\mathrm{kg} \cdot \mathrm{m}^{2}$.
Gravity, GRAVITY - Gravity
scalar
Gravity, GRAVITY, in m/s^2.

## Vertical

Initial tire displacement, zo - Displacement scalar

Initial tire displacement, $z o$, in m .
Initial wheel vertical velocity (wheel fixed frame), zdoto - Velocity scalar

Initial wheel vertical velocity (wheel fixed frame), $z$ doto, in $\mathrm{m} / \mathrm{s}$.
Effective rolling radius at low load stiffness, BREFF - Stiffness
scalar
Effective rolling radius at low load stiffness, BREFF, dimensionless.
Effective rolling radius peak value, DREFF - Radius
scalar
Effective rolling radius peak value, $D R E F F$, dimensionless.
Effective rolling radius at high load stiffness, FREFF - Radius scalar

Effective rolling radius at high load stiffness, FREFF, dimensionless.
Unloaded to nominal rolling radius ratio, Q_REO - Ratio scalar

Unloaded to nominal rolling radius ratio, $Q_{-} R E 0$, dimensionless.
Radius rotational speed dependence, Q_V1 - Speed scalar

Radius rotational speed dependence, $Q_{-}$V1, dimensionless.
Stiffness rotational speed dependence, Q_V2 - Speed scalar

Stiffness rotational speed dependence, $Q_{-} V 2$, dimensionless.
Linear load change with deflection, Q_FZ1 - Load change scalar

Linear load change with deflection, $Q_{-} F Z 1$, dimensionless.
Quadratic load change with deflection, Q_FZ2 - Load change scalar

Quadratic load change with deflection, Q_FZ2, dimensionless.
Linear load change with deflection and quadratic camber, Q_FZ3 - Load change scalar

Linear load change with deflection and quadratic camber, $Q_{-} F Z 3$, dimensionless.
Load response to longitudinal force, Q_FCX - Force scalar

Load response to longitudinal force, $Q_{-} F C X$, dimensionless.
Load response to lateral force, Q_FCY - Force scalar

Load response to lateral force, $Q_{-} F C Y$, dimensionless.
Vertical stiffness change due to lateral load dependency on lateral stiffness, Q_FCY2 Stiffness
scalar
Vertical stiffness change due to lateral load dependency on lateral stiffness, Q_FCY2, dimensionless.
Stiffness response to pressure, PFZ1 - Stiffness
scalar
Stiffness response to pressure, PFZ1, dimensionless.

## Vertical tire stiffness, VERTICAL_STIFFNESS - Stiffness

scalar
Vertical tire stiffness, VERTICAL_STIFFNESS, in N/m.

## Vertical tire damping, VERTICAL_DAMPING - Damping scalar

Vertical tire damping, VERTICAL_DAMPING, in $\mathrm{N} \cdot \mathrm{s} / \mathrm{m}$.
Rim bottoming out offset, BOTTOM_OFFST - Offset scalar

Rim bottoming out offset, BOTTOM_OFFST, in m.

## Bottoming out stiffness, BOTTOM_STIFF - Stiffness

 scalarBottoming out stiffness, BOTTOM_STIFF, in N/m.
Linear load dependent camber angle influence on vertical stiffness, Q_CAM1 - Stiffness scalar

Linear load dependent camber angle influence on vertical stiffness, Q_CAM1, dimensionless.
Quadratic load dependent camber angle influence on vertical stiffness, Q_CAM2 - Stiffness scalar

Quadratic load dependent camber angle influence on vertical stiffness, $Q_{-} C A M 2$, dimensionless.
Linear load and camber angle dependent reduction on vertical stiffness, Q_CAM3 - Stiffness scalar

Linear load and camber angle dependent reduction on vertical stiffness, $Q_{-} C A M 3$, dimensionless.

## Structural

Longitudinal stiffness, LONGITUDINAL_STIFFNESS - Stiffness
scalar
Longitudinal stiffness, LONGITUDINAL_STIFFNESS, in N/m.
Lateral stiffness, LATERAL_STIF FNESS - Stiffness
scalar
Longitudinal stiffness, LATERAL_STIFFNESS, in N/m.
Linear vertical deflection influence on longitudinal stiffness, PCFX1 - Deflection influence scalar

Linear vertical deflection influence on longitudinal stiffness, PCFX1, dimensionless.
Quadratic vertical deflection influence on longitudinal stiffness, PCFX2 - Deflection influence scalar

Quadratic vertical deflection influence on longitudinal stiffness, PCFX2, dimensionless.
Pressure dependency on longitudinal stiffness, PCFX3 - Pressure dependency scalar

Pressure dependency on longitudinal stiffness, PCFX3, dimensionless.
Linear vertical deflection influence on lateral stiffness, PCFY1 - Deflection influence scalar

Linear vertical deflection influence on lateral stiffness, PCFY1, dimensionless.
Quadratic vertical deflection influence on lateral stiffness, PCFY2 - Deflection influence scalar

Quadratic vertical deflection influence on lateral stiffness, PCFY2, dimensionless.
Pressure dependency on longitudinal stiffness, PCFY3 - Pressure dependency scalar

Pressure dependency on longitudinal stiffness, PCFY3, dimensionless.

## Contact Patch

Contact length square root term, Q_RA1 - Length term

## scalar

Contact length square root term, $Q \_$RA1, dimensionless.
Contact length linear term, Q_RA2 - Length term
scalar
Contact length linear term, Q_RA2, dimensionless.
Contact width root term, Q_RB1 - Width term
scalar
Contact width root term, Q_RB1, dimensionless.
Contact width linear term, Q_RB2 - Width term
scalar
Contact width linear term, $Q_{-} R B 2$, dimensionless.

## Longitudinal

Cfx shape factor, PCX1 - Shape factor
scalar
Shape factor, $C_{f x}, P C X 1$, dimensionless.
Longitudinal friction at nominal normal load, PDX1 - Friction scalar

Longitudinal friction at nominal normal load, PDX1, dimensionless.
Frictional variation with load, PDX2 - Friction variation scalar

Frictional variation with load, $P D X 2$, dimensionless.
Frictional variation with camber, PDX3 - Friction variation scalar

Frictional variation with camber, $P D X 3$, in $1 / \mathrm{rad}^{\wedge} 2$.

## Longitudinal curvature at nominal normal load, PEX1 - Curvature

 scalarLongitudinal curvature at nominal normal load, PEX1, dimensionless.
Variation of curvature factor with load, PEX2 - Curvature variation scalar

Variation of curvature factor with load, PEX2, dimensionless.
Variation of curvature factor with square of load, PEX3 - Curvature variation scalar

Variation of curvature factor with square of load, PEX3, dimensionless.
Longitudinal curvature factor with slip, PEX4 - Curvature scalar

Longitudinal curvature factor with slip, PEX4, dimensionless.
Longitudinal slip stiffness at nominal normal load, PKX1 - Stiffness
scalar
Longitudinal slip stiffness at nominal normal load, PKX1, dimensionless.
Variation of slip stiffness with load, PKX2 - Stiffness variation
scalar
Variation of slip stiffness with load, $P K X 2$, dimensionless.
Slip stiffness exponent factor, PKX3 - Slip stiffness
scalar
Slip stiffness exponent factor, $P K X 3$, dimensionless.
Horizontal shift in slip ratio at nominal normal load, PHX1 - Slip ratio shift scalar

Horizontal shift in slip ratio at nominal normal load, PHX1, dimensionless.
Variation of horizontal slip ratio with load, PHX2 - Slip variation scalar

Variation of horizontal slip ratio with load, PHX2, dimensionless.
Vertical shift in load at nominal normal load, PVX1 - Load shift scalar

Vertical shift in load at nominal normal load, PVX1, dimensionless.
Variation of vertical shift with load, PVX2 - Load variation scalar

Variation of vertical shift with load, $P V X 2$, dimensionless.

Linear variation of longitudinal slip stiffness with tire pressure, PPX1 - Stiffness variation scalar

Linear variation of longitudinal slip stiffness with tire pressure, $P$ PX1, dimensionless.
Quadratic variation of longitudinal slip stiffness with tire pressure, PPX2 - Stiffness variation scalar

Quadratic variation of longitudinal slip stiffness with tire pressure, PPX2, dimensionless.
Linear variation of peak longitudinal friction with tire pressure, PPX3 - Friction variation scalar

Linear variation of peak longitudinal friction with tire pressure, $\operatorname{PPX} 3$, dimensionless.
Quadratic variation of peak longitudinal friction with tire pressure, PPX4 - Friction variation scalar

Quadratic variation of peak longitudinal friction with tire pressure, PPX4, dimensionless.
Combined slip Fx slope factor reduction, RBX1 - Combined slip longitudinal force slope factor reduction
scalar
Combined slip longitudinal force, $F_{x}$, slope factor reduction, $R B X 1$, dimensionless.
Slip ratio Fx slope reduction variation, RBX2 - Slip ratio longitudinal force slope reduction variation
scalar
Slip ratio longitudinal force, $F_{x}$, slope reduction variation, $R B X 2$, dimensionless.
Camber influence on combined slip Fx stiffness, RBX3 - Camber influence on combined slip longitudinal force stiffness
scalar
Camber influence on combined slip longitudinal force, $F_{x}$, stiffness, $R B X 3$, dimensionless.
Shape factor for combined slip Fx reduction, RCX1 - Shape factor for combined slip longitudinal force reduction
scalar
Shape factor for combined slip longitudinal force, $F_{x}$, reduction, RCX1, dimensionless.
Combined Fx curvature factor, REX1 - Combined longitudinal force curvature factor scalar

Combined longitudinal force, $F_{x}$, curvature factor, REX1, dimensionless.
Combined Fx curvature factor with load, REX2 - Combined longitudinal force curvature factor scalar

Combined longitudinal force, $F_{x}$, curvature factor with load, REX2, dimensionless.
Combined slip Fx shift factor reduction, RHX1 - Combined slip longitudinal force slip factor scalar

Combined slip longitudinal force, $F_{x}$, shift factor reduction, RHX1, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.

## Overturning

Vertical shift of overturning moment, QSX1 - Overturning moment scalar

Vertical shift of overturning moment, QSX1, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Overturning moment due to camber, QSX2 - Overturning moment due to camber scalar

Overturning moment due to camber, QSX2, dimensionless.
Overturning moment due to Fy, QSX3 - Overturning moment due to lateral force scalar

Overturning moment due to lateral force, QSX3, dimensionless.
Mx combined lateral force load and camber, QSX4 - Overturning moment scalar

Overturning moment, $M_{x}$, combined lateral force load and camber, QSX4, dimensionless.
Mx load effect due to lateral force and camber, QSX5 - Overturning moment scalar

Overturning moment, $M_{x}$, load effect due to lateral force and camber, QSX5, dimensionless.
Mx load effect due to B-factor, QSX6 - Overturning moment scalar

Overturning moment, $M_{x}$, load effect due to B-factor, QSX6, dimensionless.
Mx due to camber and load, QSX7 - Overturning moment scalar

Overturning moment, $M_{x}$, due to camber and load, QSX7, dimensionless.
Mx due to lateral force and load, QSX8 - Overturning moment scalar

Overturning moment, $M_{x}$, due to lateral force and load, QSX8, dimensionless.
Mx due to B-factor of lateral force and load, QSX9 - Overturning moment scalar

Overturning moment, $M_{x}$, due to B-factor of lateral force and load, QSX9, dimensionless.

## Mx due to vertical force and camber, QSX10 - Overturning moment scalar

Overturning moment, $M_{x}$, due to vertical force and camber, QSX10, dimensionless.
Mx due to B-factor of vertical force and camber, QSX11 - Overturning moment scalar

Overturning moment, $M_{x}$, due to B-factor of vertical force and camber, QSX11, dimensionless.
Mx due to squared camber, QSX12 - Overturning moment
scalar
Overturning moment, $M_{x}$, due to squared camber, QSX12, dimensionless.
Mx due to lateral force, QSX13 - Overturning moment
scalar
Overturning moment, $M_{x}$, due to lateral force, QSX13, dimensionless.
Mx due to lateral force with camber, QSX14 - Overturning moment scalar

Overturning moment, $M_{x}$, due to lateral force with camber, QSX14, dimensionless.
Mx due to inflation pressure, PPMX1 - Overturning moment due to pressure scalar

Overturning moment, $M_{x}$, due to inflation pressure, PPMX1, dimensionless.

## Lateral

Cfy shape factor for lateral force, PCY1 - Lateral force shape factor scalar

Shape factor for lateral force, $C_{f y}$, PCY1, dimensionless.
Lateral friction muy, PDY1 - Lateral friction
scalar
Lateral friction, $\mu_{y}$, PDY1, dimensionless.
Lateral friction variation of muy with load, PDY2 - Lateral friction variation scalar

Variation of lateral friction, $\mu_{y}$, with load, PDY2, dimensionless.
Lateral friction variation of muy with squared camber, PDY3 - Lateral friction variation scalar

Variation of lateral friction, $\mu_{y}$, with squared camber, PDY3, dimensionless.
Efy lateral curvature at nominal force FZNOM, PEY1 - Lateral curvature at nominal force scalar

Lateral curvature, $E f_{y}$, at nominal force, $F_{Z N O M}$, PEY1, dimensionless.

Efy curvature variation with load, PEY2 - Lateral curvature variation scalar

Lateral curvature, $E f_{y}$, variation with load, PEY2, dimensionless.
Efy curvature constant camber dependency, PEY3 - Lateral curvature constant scalar

Lateral curvature, $E f_{y}$, constant camber dependency, PEY3, dimensionless.
Dependencies
If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Efy curvature variation with camber, PEY4 - Lateral curvature variation scalar

Lateral curvature, $E f_{y}$, variation with camber, PEY4, dimensionless.
Efy curvature variation with camber squared, PEY5 - Lateral curvature variation scalar

Lateral curvature, $E f_{y}$, variation with camber squared, $P E Y 5$, dimensionless.
Maximum KFy/FZNOM stiffness, PKY1 - Maximum stiffness

## scalar

Maximum lateral force stiffness, $K F_{y}$, to nominal force, $F_{Z N O M}$, ratio, $P K Y 1$, dimensionless.
Load at maximum KFy/FZNOM stiffness, PKY2 - Load
scalar
Load at maximum lateral force stiffness, $K F_{y}$, to nominal force, $F_{Z N O M}$, ratio, $P K Y 2$, dimensionless.
KFy/FZNOM stiffness variation with camber, PKY3 - Stiffness variation scalar

Lateral force stiffness, $K F_{y}$, to nominal force, $F_{Z N O M}$, stiffness variation with camber, $P K Y 3$, dimensionless.

KFy curvature, PKY4 - Lateral force stiffness curvature scalar

Lateral force stiffness, $K F_{y}$ curvature, $P K Y 4$, dimensionless.
Variation of peak stiffness with squared camber, PKY5 - Stiffness variation scalar

Variation of peak stiffness with squared camber, PKY5, dimensionless.
Fy camber stiffness factor, PKY6 - Lateral force camber stiffness factor scalar

Lateral force, $F_{y}$, camber stiffness factor, $P K Y 6$, dimensionless.
Camber stiffness vertical load dependency, PKY7 - Stiffness
scalar

Camber stiffness vertical load dependency, PKY7, dimensionless.
SHY horizontal shift at FZNOM, PHY1 - Horizontal shift at nominal force scalar

Horizontal shift, $S_{H Y}$, at nominal force, $F_{Z N O M}$, PHY1, dimensionless.
Dependencies
If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
SHY variation with load, PHY2 - Horizontal shift variation
scalar
Horizontal shift, $S_{H Y}$, variation with load, PHY2, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Svy/Fz vertical shift at FZNOM, PVY1 - Vertical shift at nominal force scalar

Vertical shift, $S_{v y}$, at nominal force, $F_{Z N O M}, P V Y 1$, dimensionless.
Dependencies
If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Svy/Fz variation with load, PVY2 - Vertical shift variation with load scalar

Vertical shift, $S_{v y}$, variation with load, $P V Y 2$, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Svy/Fz variation with camber, PVY3 - Vertical shift variation with camber scalar

Vertical shift, $S_{v y}$, variation with camber, $P V Y 3$, dimensionless.
Svy/Fz variation with load and camber, PVY4 - Vertical shift variation with load and camber scalar

Vertical shift, $S_{v y}$, variation with load and camber, $P V Y 4$, dimensionless.
Cornering stiffness variation with inflation pressure, PPY1 - Stiffness variation with pressure scalar

Cornering stiffness variation with inflation pressure, PPY1, dimensionless.
Cornering stiffness variation with inflation pressure induced nominal load dependency, PPY2 - Stiffness variation with pressure scalar

Cornering stiffness variation with inflation pressure induced nominal load dependency, PPY2, dimensionless.

## Linear inflation pressure on peak lateral friction, PPY3 - Pressure scalar

Linear inflation pressure on peak lateral friction, $P P Y 3$, dimensionless.
Quadratic inflation pressure on peak lateral friction, PPY4 - Pressure scalar

Quadratic inflation pressure on peak lateral friction, PPY4, dimensionless.
Inflation pressure effect on camber stiffness, PPY5 - Pressure scalar

Inflation pressure effect on camber stiffness, PPY5, dimensionless.
Combined Fy reduction slope factor, RBY1 - Combined lateral force reduction slope factor scalar

Combined lateral force, $F_{y}$, reduction slope factor, RBY1, dimensionless.
Fy slope reduction with slip angle, RBY2 - Lateral force slope reduction with slip angle scalar

Lateral force, $F_{y}$, slope reduction with slip angle, RBY2, dimensionless.
Fy shift reduction with slip angle, RBY3 - Lateral force shift reduction with slip angle scalar

Lateral force, $F_{y}$, shift reduction with slip angle, RBY3, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Fy combined stiffness variation from camber, RBY4 - Lateral force combined stiffness variation from camber
scalar
Lateral force, $F_{y}$, combined stiffness variation from camber, RBY4, dimensionless.
Fy combined reduction shape factor, RCY1 - Lateral force combined reduction shape factor scalar

Lateral force, $F_{y}$, combined reduction shape factor, RCY1, dimensionless.
Fy combined curvature factor, REY1 - Lateral force combined curvature factor scalar

Lateral force, $F_{y}$, combined curvature factor, REY1, dimensionless.
Fy combined curvature factor with load, REY2 - Lateral force combined curvature factor with load
scalar

Lateral force, $F_{y}$, combined curvature factor with load, REY2, dimensionless.
Fy combined reduction shift factor, RHY1 - Lateral force combined reduction shift factor scalar

Lateral force, $F_{y}$, combined reduction shift factor, RHY1, dimensionless.
Fy combined reduction shift factor with load, RHY2 - Lateral force combined reduction shift factor with load
scalar
Lateral force, $F_{y}$, combined reduction shift factor with load, RHY2, dimensionless.
Slip ratio side force Svyk/Muy*Fz at FZNOM, RVY1 - Slip ratio slide force at nominal force scalar

Slip ratio side force at nominal force, $F_{\text {ZNOM }}, R V Y 1$, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Side force Svyk/Muy*Fz variation with load, RVY2 - Side force variation with load scalar

Side force variation with load, RVY2, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Side force Svyk/Muy*Fz variation with camber, RVY3 - Side force variation with camber scalar

Side force variation with camber, $R V Y 3$, dimensionless.
Side force Svyk/Muy*Fz variation with slip angle, RVY4 - Side force variation with slip angle scalar

Side force variation with slip angle, $R V Y 4$, dimensionless.
Side force Svyk/Muy*Fz variation with slip ratio, RVY5 - Side force variation with slip ratio scalar

Side force variation with slip ratio, $R V Y 5$, dimensionless.
Side force Svyk/Muy*Fz variation with slip ratio arctangent, RVY6 - Side force variation with slip ratio arctangent scalar

Side force variation with slip ratio arctangent, $R V Y 6$, dimensionless.

## Rolling

Torque resistance coefficient, QSY1 - Torque resistance scalar

Torque resistance coefficient, QSY1, dimensionless.
Torque resistance due to Fx, QSY2 - Torque resistance due to longitudinal force scalar

Torque resistance due to longitudinal force, $F_{x}$, QSY2, dimensionless.
Torque resistance due to speed, QSY3 - Torque resistance due to speed scalar

Torque resistance due to speed, QSY3, dimensionless.
Torque resistance due to speed^4, QSY4 - Torque resistance due to speed scalar

Torque resistance due to speed^ ${ }^{\wedge}$, $Q S Y 4$, dimensionless.
Torque resistance due to square of camber, QSY5 - Torque resistance due to camber scalar

Torque resistance due to square of camber, QSY5, dimensionless.
Torque resistance due to square of camber and load, QSY6 - Torque resistance due to camber and load
scalar
Torque resistance due to square of camber and load, QSY6, dimensionless.
Torque resistance due to load, QSY7 - Torque resistance due to load scalar

Torque resistance due to load, QSY7, dimensionless.
Torque resistance due to pressure, QSY8 - Torque resistance due to pressure scalar

Torque resistance due to pressure, QSY8, dimensionless.
Aligning
Trail slope factor for trail Bpt at FZNOM, QBZ1 - Trail slope factor at nominal force scalar

Trail slope factor for trail $B p t$ at nominal force, $F_{\text {ZNOM }}, Q B Z 1$, dimensionless.
Bpt slope variation with load, QBZ2 - Slope variation with load
scalar
Slope variation with load, QBZ2, dimensionless.
Bpt slope variation with square of load, QBZ3 - Slope variation with load scalar

Slope variation with square of load, $Q B Z 3$, dimensionless.

Bpt slope variation with camber, QBZ4 - Slope variation with camber scalar

Slope variation with camber, QBZ4, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Bpt slope variation with absolute value of camber, QBZ5 - Slope variation with camber scalar

Slope variation with absolute value of camber, QBZ5, dimensionless.
Bpt slope variation with square of camber, QBZ6 - Slope variation with camber scalar

Slope variation with square of camber, QBZ6, dimensionless.
Br of Mzr slope scaling factor, QBZ9 - Slope scaling factor scalar

Slope scaling factor, QBZ9, dimensionless.
Br of Mzr cornering stiffness factor, QBZ10 - Cornering stiffness factor
0 (default) | scalar
$B r$ of $M z r$ cornering stiffness factor, $Q B Z 10$, dimensionless.
Cpt pneumatic trail shape factor, QCZ1 - Pneumatic trail shape factor scalar

Pneumatic trail shape factor, $C_{p t}$, $Q C Z 1$, dimensionless.
Dpt peak trail, QDZ1 - Peak trail
scalar
Peak trail, $D_{p t}$ QDZ1, dimensionless.
Dpt peak trail variation with load, QDZ2 - Peak trail variation with load scalar

Peak trail, $D_{p t}$, variation with load, QDZ2, dimensionless.
Dpt peak trail variation with camber, QDZ3 - Peak trail variation with camber scalar

Peak trail, $D_{p t}$, variation with camber, $Q D Z 3$, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Dpt peak trail variation with square of camber, QDZ4 - Peak trail variation with camber scalar

Peak trail, $D_{p t}$, variation with square of camber, $Q D Z 4$, dimensionless.

Dmr peak residual torque, QDZ6 - Peak residual torque scalar

Peak residual torque, $D_{m r}, Q D Z 6$, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Dmr peak residual torque variation with load, QDZ7 - Peak residual torque variation with load scalar

Peak residual torque, $D_{m r}$, variation with load, $Q D Z 7$, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Dmr peak residual torque variation with camber, QDZ8 - Peak residual torque variation with camber
scalar
Peak residual torque, $D_{m r}$, variation with camber, $Q D Z 8$, dimensionless.
Dmr peak residual torque variation with camber and load, QDZ9 - Peak residual torque variation with camber and load scalar

Peak residual torque, $D_{m r}$, variation with camber and load, $Q D Z 9$, dimensionless.
Dmr peak residual torque variation with square of camber, QDZ10 - Peak residual torque variation with camber scalar

Peak residual torque, $D_{m r}$, variation with square of camber, $Q D Z 10$, dimensionless.
Dmr peak residual torque variation with square of load, QDZ11 - Peak residual torque variation with load scalar

Peak residual torque, $D_{m r}$, variation with square of load, $Q D Z 11$, dimensionless.
Ept trail curvature at FZNOM, QEZ1 - Trail curvature at nominal force scalar

Trail curvature, $E_{p t}$, at nominal force, $F_{Z N O M}, Q E Z 1$, dimensionless.
Ept variation with load, QEZ2 - Trail curvature variation with load scalar

Trail curvature, $E_{p t}$ variation with load, QEZ2, dimensionless.
Ept variation with square of load, QEZ3 - Trail curvature variation with load scalar

Trail curvature, $E_{p t}$ variation with square of load, $Q E Z 3$, dimensionless.

## Ept variation with sign of alpha-t, QEZ4 - Trail curvature variation <br> scalar

Trail curvature, $E_{p t}$ variation with sign of alpha-t, QEZ4, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.

## Ept variation with sign of alpha-t and camber, QEZ5 - Variation <br> scalar

Trail curvature, $E_{p t}$ variation with sign of alpha-t and camber, $Q E Z 5$, dimensionless.
Sht horizontal trail shift at FZNOM, QHZ1 - Horizontal trail shift at nominal load scalar

Horizontal trail shift, $S h_{t}$, at nominal load, $F_{\text {ZNOM }}, Q H Z 1$, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Sht variation with load, QHZ2 - Horizontal trail shift variation with load

## scalar

Horizontal trail shift, $S h_{t}$, variation with load, $Q H Z 2$, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Sht variation with camber, QHZ3 - Horizontal trail shift variation with camber scalar

Horizontal trail shift, $S h_{t}$, variation with camber, $Q H Z 3$, dimensionless.
Sht variation with load and camber, QHZ4 - Horizontal trail shift variation with load and camber scalar

Horizontal trail shift, $S h_{t}$, variation with load and camber, QHZ4, dimensionless.
Inflation pressure influence on trail length, PPZ1 - Pressure influence on trail length scalar

Inflation pressure influence on trail length, PPZ1, dimensionless.
Inflation pressure influence on residual aligning torque, PPZ2 - Pressure influence on aligning torque
scalar
Inflation pressure influence on residual aligning torque, $P$ PZZ2, dimensionless.
Nominal value of s/R0: effect of Fx on Mz, SSZ1 - Effect of longitudinal force on aligning torque scalar

Nominal value of $\mathrm{s} / \mathrm{R} 0$ : effect of longitudinal force, $F_{x}$, on aligning torque, $M_{z}$, SSZ1, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
s/R0 variation with lateral to nominal force ratio, SSZ2 - Variation with lateral to nominal force ratio
scalar
Variation with lateral to nominal force ratio, SSZ2, dimensionless.
s/R0 variation with camber, SSZ3 - Variation with camber
scalar
Variation with camber, SSZ3, dimensionless.
s/R0 variation with camber and load, SSZ4 - Variation with camber and load

## scalar

Variation with camber and load, SSZ4, dimensionless.

## Turnslip

Fx peak reduction due to spin, PDXP1 - Longitudinal force peak reduction due to spin scalar

Longitudinal force, $F_{x}$, peak reduction due to spin, $P D X P 1$, dimensionless.
Fx peak reduction due to spin with varying load, PDXP2 - Longitudinal force peak reduction due to spin
scalar
Longitudinal force, $F_{x}$, peak reduction due to spin with varying load, $P D X P 2$, dimensionless.
Fx peak reduction due to spin with slip ratio, PDXP3 - Longitudinal force peak reduction due to spin
scalar
Longitudinal force, $F_{x}$, peak reduction due to spin with slip ratio, PDXP3, dimensionless.
Cornering stiffness reduction due to spin, PKYP1 - Stiffness reduction due to spin scalar

Cornering stiffness reduction due to spin, PKYP1, dimensionless.
Fy peak reduction due to spin, PDYP1 - Lateral force peak reduction due to spin scalar

Lateral force, $F_{y}$, peak reduction due to spin, PDYP1, dimensionless.
Fy peak reduction due to spin with varying load, PDYP2 - Lateral force peak reduction due to spin scalar

Lateral force, $F_{y}$, peak reduction due to spin with varying load, $P D Y P 2$, dimensionless.

Fy peak reduction due to spin with slip angle, PDYP3 - Lateral force peak reduction due to spin scalar

Lateral force, $F_{y}$, peak reduction due to spin with slip angle, PDYP3, dimensionless.
Fy peak reduction due to square root of spin, PDYP4 - Lateral force peak reduction due to spin scalar

Lateral force, $F_{y}$, peak reduction due to square root of spin, PDYP4, dimensionless.
Fy vs. slip angle response lateral shift limit, PHYP1 - Lateral force versus slip angle response scalar

Lateral force, $F_{y}$, versus slip angle response lateral shift limit, PHYP1, dimensionless.
Fy vs. slip angle response max lateral shift limit, PHYP2 - Lateral force versus slip angle response
scalar
Lateral force, $F_{y}$, versus slip angle response max lateral shift limit, PHYP2, dimensionless.
Fy vs. slip angle response max lateral shift limit with load, PHYP3 - Lateral force versus slip angle response
scalar
Lateral force, $F_{y}$, versus slip angle response max lateral shift limit with load, PHYP3, dimensionless.
Fy vs. slip angle response lateral shift curvature factor, PHYP4 - Lateral force versus slip angle response
scalar
Lateral force, $F_{y}$, versus slip angle response lateral shift curvature factor, PHYP4, dimensionless.
Camber stiffness reduction due to spin, PECP1 - Camber stiffness reduction scalar

Camber stiffness reduction due to spin, PECP1, dimensionless.
Camber stiffness reduction due to spin with load, PECP2 - Camber stiffness reduction scalar

Camber stiffness reduction due to spin with load, PECP2, dimensionless.
Turn slip pneumatic trail reduction factor, QDTP1 - Turn slip pneumatic trail reduction factor scalar

Turn slip pneumatic trail reduction factor, QDTP1, dimensionless.
Turn moment for constant turning and zero longitudinal speed, QCRP1 - Turn moment for constant turning scalar

Turn moment for constant turning and zero longitudinal speed, QCRP1, dimensionless.
Turn slip moment increase with spin at 90deg slip angle, QCRP2 - Turn slip moment scalar

Turn slip moment increase with spin at 90-degree slip angle, QCRP2, dimensionless.
Residual spin torque reduction from side slip, QBRP1 - Residual spin torque reduction scalar

Residual spin torque reduction from side slip, QBRP1, dimensionless.
Turn slip moment peak magnitude, QDRP1 - Turn slip moment peak magnitude scalar

Turn slip moment peak magnitude, $Q D R P 1$, dimensionless.
Turn slip moment curvature, QDRP2 - Turn slip moment curvature
scalar
Turn slip moment curvature, QDRP2, dimensionless.

## Version History

Introduced in R2021b
R2022b: New Ply steer and Turn slip Parameters
Behavior changed in R2022b
Starting from R2022b, the Combined Slip Wheel CPI block includes Ply steer and Turn slip parameters. To remove ply steer and turn slip from the Magic Formula implementation of these blocks, clear the Ply steer and Turn slip parameters.

## References

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[2] Pacejka, Hans B. Tire and Vehicle Dynamics. 3rd ed. Oxford, United Kingdom: SAE and Butterworth-Heinemann, 2012.
[3] Bohm, F., and H. P. Willumeit, "Tyre Models for Vehicle Dynamic Analysis: Proceedings of the 2nd International Colloquium on Tyre Models for Vehicle Dynamics Analysis, Held at the Technical University of Berlin, Germany, February 20-21, 1997." Vehicle System Dynamics International Journal of Vehicle Mechanics and Mobility 27, sup. 1, 343-45. https://doi.org/ 0.1080/00423119708969669.
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## Extended Capabilities

C/C++ Code Generation
Generate C and $\mathrm{C}++$ code using Simulink $®$ Coder $^{\mathrm{TM}}$.

## See Also

Combined Slip Wheel 2DOF | Combined Slip Wheel 2DOF STI | Fiala Wheel 2DOF | Longitudinal Wheel | Dugoff Wheel 2DOF

Topics
"Coordinate Systems in Vehicle Dynamics Blockset"

## Combined Slip Wheel STI

Combined slip wheel compliant with STI Tydex standard


## Libraries:

Vehicle Dynamics Blockset / Wheels and Tires

## Description

The Combined Slip Wheel STI block implements the longitudinal and lateral behavior of a wheel characterized by the Magic Formula ${ }^{1,2}$ that complies with the standard tire interface (STI) Tyre Data Exchange Format (TYDEX) ${ }^{3}$ standard. You can import your own tire data or use fitted tire data sets provided by the Global Center for Automotive Performance Simulation (GCAPS). Use the block in driveline and vehicle simulations where low-frequency tire road interactions are required to determine vehicle acceleration and wheel-rolling resistance. The block is suitable for applications that require combined lateral slip, for example, in lateral motion and yaw stability studies.

Based on the wheel rotational velocity, longitudinal and lateral velocity, wheel camber angle, and inflation pressure, the block determines the vertical motion, forces, and moments in all six degrees of freedom (DOF). Use the vertical DOF to study tire-suspension resonances from road profiles or chassis motion.

Use the Tire type parameter to select the source of the tire data.

| Goal |
| :--- |
| Implement the Magic Formula using <br> empirical equations <br> use fitting coefficients the equations <br> correspond to the block parameters. |

## Action <br> Update the block parameters with fitting coefficients from a file: <br> 1 Set Tire type to External file. <br> 2 On the External tire source pane, Click Select file. <br> 3 Select the tire coefficient file. <br> 4 Click Update mask values from file. In the dialog box that prompts you for confirmation, click OK. The block updates the parameters.

5 Click Apply.

| Goal | Action |
| :---: | :---: |
| Implement fitted tire data sets provided by the Global Center for Automotive Performance Simulation (GCAPS). | Update the applicable block parameters with GCAPS fitted tire data: <br> 1 Set Tire type to the tire that you want to implement. Options include: <br> - Light passenger car 205/60R15 <br> - Mid-size passenger car 235/45R18 <br> - Performance car 225/40R19 <br> - SUV 265/50R20 <br> - Light truck 275/65R18 <br> - Commercial truck 295/75R22.5 <br> 2 Click Update applicable Tire Parameters with tire type values. On the Tire Parameters tab, the block updates the applicable parameters, including Wheel width, Rim radius, and Wheel mass. <br> Click Apply. |

## Rotational Wheel Dynamics

The block calculates the inertial response of the wheel subject to:

- Axle losses
- Tire rolling resistance
- Ground contact through the tire-road interface

To implement the Magic Formula, the block uses these equations from the cited references:

| Calculation | Equations |
| :--- | :--- |
| Longitudinal force | Tire and Vehicle Dynamics ${ }^{2}$ equations 4.E9 through 4.E57 |
| Lateral force - pure <br> sideslip | Tire and Vehicle Dynamics ${ }^{2}$ equations 4.E19 through 4.E30 |
| Lateral force - combined <br> slip | Tire and Vehicle Dynamics ${ }^{2}$ equations 4.E58 through 4.E67 |
| Vertical dynamics | Tire and Vehicle Dynamics ${ }^{2}$ equations 4.E68, 4.E1, 4.E2a, and 4.E2b |
| Overturning couple | Tire and Vehicle Dynamics ${ }^{2}$ equation 4.E69 |
| Rolling resistance | - An improved Magic Formula/Swift tyre model that can handle inflation $_{\text {pressure changes }{ }^{1} \text { equation 6.1.2 }}$ <br> Tire and Vehicle Dynamics ${ }^{2}$ equation 4.E70 |
| Aligning moment  <br> Aligning torque - Tire and Vehicle Dynamics ${ }^{2}$ equation 4.E31 through 4.E49Tire and Vehicle Dynamics ${ }^{2}$ equation 4.E71 through 4.E78 <br> If you clear Include turn slip, the block sets some of these equations to 1. |  |

## STI Wheel Coordinate System

The block uses wheel coordinate system axes ( $X_{W}, Y_{W}, Z_{W}$ ) that are fixed in a reference frame attached to the wheel. The origin is at the wheel center.

The STI wheel coordinate system is shown in blue.

Note The STI wheel coordinate system (blue) is equivalent to the TYDEX centre-axis coordinate system.

4


| Axis | Description |
| :--- | :--- |
| $X_{W}$ | $X_{W}$ and $Y_{W}$ are parallel to the wheel plane: |
| $Y_{W}$ | - $\quad X_{W}$ is parallel to the local road plane. <br>  <br>  <br> $Z_{W} \quad Y_{W}$ is parallel to the wheel-spin axis. <br> $Z_{W}$ points upward. |

## Ports

## Input

Xe - Wheel position in inertial reference frame
N -by-3 vector
Wheel position along inertial-fixed $X$-, $Y$-, $Z$-axes, respectively, in m .
Vector is the number of wheels, $N$, by 3.

[^3] without prior permission from SAE.

DCM - Direction cosine matrix
3-by-3 vector
Transformation matrix from the wheel coordinate system to the Earth-fixed inertial coordinate system.

Ang - Rotation angle of the rim
3-by-3 vector
Rotation angle of rim with respect to the wheel center, in rad.
Ve - Wheel velocity in inertial reference frame
N -by-3 vector
Wheel velocity along inertial-fixed $X$-, $Y$-, and $Z$-axes, respectively, in m .
Vector is the number of wheels, $N$, by 3.
Omega - Rotational velocity
N -by-3 vector
Wheel rotational velocity along inertial-fixed $X$-, $Y$-, and $Z$-axes, respectively, in m.
Vector is the number of wheels, $N$, by 3.
OmegaWc - Rim rotational velocity
scalar
Rim rotational velocity, $\omega$, about wheel spin axis, in rad/s.
Road - Wheel position, rotation matrix, velocity
1-by-18 vector
Vector containing wheel position, rotation, and velocity with respect to the Earth-fixed inertial coordinate system.

| Vector Element | Description |
| :--- | :--- |
| $\operatorname{Road}(1,1)$ | Wheel position along inertial-fixed $X$-, $Y$-, and $Z$-axes, <br> respectively, in $m$. |
| $\operatorname{Road}(1,2)$ |  |
| $\operatorname{Road}(1,3)$ |  |


| Vector Element | Description |
| :--- | :--- |
| $\operatorname{Road}(1,4)$ | Transformation matrix from the wheel coordinate system to the <br> Earth-fixed inertial coordinate system. |
| $\operatorname{Road}(1,6)$ |  |
| $\operatorname{Road}(1,7)$ |  |
| $\operatorname{Road}(1,8)$ |  |
| $\operatorname{Road}(1,9)$ |  |
| $\operatorname{Road}(1,10)$ |  |
| $\operatorname{Road}(1,11)$ |  |
| $\operatorname{Road}(1,12)$ | Wheel velocity along inertial-fixed $X$-, $Y$-, and $Z$-axes, <br> respectively, in m/s. |
| $\operatorname{Road}(1,13)$ <br> $\operatorname{Road}(1,15)$ | Wheel angular velocity along inertial-fixed $X$-, $Y$-, and $Z$-axes, <br> respectively, in rad/s. |
| $\operatorname{Road}(1,16)$ |  |
| $\operatorname{Road}(1,17)$ | $\operatorname{Road}(1,18)$ |

ScaleFctrs - Road friction scale factors
2-by-N array
Magic formula road friction scale factor array. Array dimensions are 2 by the number of wheels, $N$.
The Magic Formula equations use scale factors to account for static or simulation run-time variations. Nominally, most are set to 1 .

| Array Element | Variable | Scale Factor |
| :--- | :--- | :--- |
| ScaleFctrs $(1,1)$ | lam_mux | Longitudinal peak friction coefficient |
| ScaleFctrs $(2,1)$ | lam_muy | Lateral peak friction coefficient |

Prs - Tire inflation pressure
scalar | N-by-1 vector
Tire inflation pressure, $p_{i}$, in Pa .
Vector is the number of wheels, $N$, by 1. If you provide a scalar value, the block assumes that number of wheels is one.

## Dependencies

To create this port, select Input tire pressure.

## Output

Info - Block data
bus
Block data, returned as a bus signal containing these block values.

| Signal |  | Description | Units |
| :---: | :---: | :---: | :---: |
| CPI_info | Omega | Wheel angular velocity about wheel-fixed $y$ axis | rad/s |
|  | FX | Longitudinal vehicle force along tire-fixed $x$ axis | N |
|  | Fy | Lateral vehicle force along tire-fixed $y$-axis | N |
|  | Fz | Vertical vehicle force along tire-fixed $z$-axis | N |
|  | Mx | Overturning moment about tire-fixed $x$-axis | $\mathrm{N} \cdot \mathrm{m}$ |
|  | My | Rolling resistance torque about tire-fixed $y$ axis | $\mathrm{N} \cdot \mathrm{m}$ |
|  | Mz | Aligning moment about tire-fixed $z$-axis | $\mathrm{N} \cdot \mathrm{m}$ |
|  | Vx | Vehicle longitudinal velocity along tire-fixed x-axis | $\mathrm{m} / \mathrm{s}$ |
|  | Vy | Vehicle lateral velocity along tire-fixed $y$-axis | $\mathrm{m} / \mathrm{s}$ |
|  | Re | Loaded effective radius | m |
|  | Kappa | Longitudinal slip ratio | NA |
|  | Alpha | Side slip angle | rad |
|  | a | Contact patch half length | m |
|  | b | Contact patch half width | m |
|  | Gamma | Camber angle | rad |
|  | psidot | Tire angular velocity about the tire-fixed $z$ axis (yaw rate) | rad/s |
|  | rhoz | Axle vertical displacement along tire-fixed $z$ axis | m |
|  | FNormal | Vertical sidewall force on ground along tirefixed $z$-axis | N |
|  | Prs | Tire inflation pressure | Pa |
| DCM |  | Transformation matrix from the wheel coordinate system to the Earth-fixed inertial coordinate system | NA |
| Xe |  | Wheel position along inertial-fixed $X$-, $Y$-, $Z$ axes, respectively | m |
| Ang |  | Rotation angle of the rim with respect to the wheel center | rad |
| Omega |  | Tire rotational velocity, $\omega$, about wheel spin axis | rad/s |


| Signal | Description | Units |
| :--- | :--- | :--- |
| Ve | Wheel velocity along inertial-fixed $X-, Y-, Z-$ <br> axes, respectively | $\mathrm{m} / \mathrm{s}$ |
| OmegaWc | Rim rotational velocity, $\omega$, about wheel spin <br> axis | $\mathrm{rad} / \mathrm{s}$ |
| Road | Vector containing wheel position, rotation, <br> and velocity with respect to the Earth-fixed <br> inertial coordinate system | NA |

Fwc - Force at wheel center
1-by-3 vector
Force applied at wheel center by tire along wheel-fixed $x$-, $y$-, $z$-axes, respectively, in $N$.
Mwc - Moment at wheel center
1-by-3 vector
Moment applied at wheel center by tire about wheel-fixed $x$-, $y$-, $z$-axes, respectively, in $\mathrm{N} \cdot \mathrm{m}$.

## Parameters

## Block Options

## Tire type - Select type

External file (default)| Light passenger car 205/60R15|Mid-size passenger car 235/45R18|Performance car 225/40R19|SUV 265/50R20|Light truck 275/65R18| Commercial truck 295/75R22.5

Use the Tire type parameter to select the source of the tire data.

| Goal | A |
| :--- | :--- |
| Implement the Magic Formula using | Up |
| empirical equations ${ }^{1,2}$. The equations |  |
| use fitting coefficients that | fil |
| correspond to the block parameters. | $\mathbf{1}$ |
|  | 2 |
|  | 3 |
|  | 4 |
|  |  |

## Action

Update the block parameters with fitting coefficients from a file:

1 Set Tire type to External file.
2 On the External tire source pane, Click Select file.
3 Select the tire coefficient file.
4 Click Update mask values from file. In the dialog box that prompts you for confirmation, click OK. The block updates the parameters.
5 Click Apply.

| Goal |
| :--- |
| Implement fitted tire data sets |
| provided by the Global Center for |
| Automotive Performance Simulation |
| (GCAPS). |

## Action

Update the applicable block parameters with GCAPS fitted tire data:

1 Set Tire type to the tire that you want to implement. Options include:

- Light passenger car 205/60R15
- Mid-size passenger car 235/45R18
- Performance car 225/40R19
- SUV 265/50R20
- Light truck 275/65R18
- Commercial truck 295/75R22.5

2 Click Update applicable Tire Parameters with tire type values. On the Tire Parameters tab, the block updates the applicable parameters, including Wheel width, Rim radius, and Wheel mass.
3 Click Apply.

Tire file or object, tireParamSet - Tire file
.mat|.tir|.txt
Tire file .tir or object containing empirical data to model tire longitudinal and lateral behavior with the Magic Formula. If you provide an .txt file, make sure the file contains names that correspond to the block parameters.

Update the block parameters with fitting coefficients from a file:
1 Set Tire type to External file.
2 On the External tire source pane, click Select file.
3 Select the tire coefficient file.
4 Click Update mask values from file. In the dialog box that prompts you for confirmation, click OK. The block updates the parameters.
5 Click Apply.
Tire side - Select tire side
Right (default) | Left | Symmetric
Specify the tire side.
Tire pressure - Select tire side
220000 (default) | scalar
Tire inflation pressure, $p$, in Pa.

## Dependencies

To enable this parameter, clear Input tire pressure.
Ply steer - Include ply steer
on (default) | off

Select to include ply steer in the Magic Formula equations.
By default, the blocks include ply steer and turn slip in the Magic Formula equations. The equations are fit to flat-belt test data and predict a number of tire effects, including ply steer and turn slip. Consider removing the effects if your:

- Test data does not include ply steer or turn slip data.
- Analysis does not require ply steer or turn slip effects.

If you clear Ply steer, the block internally sets these parameters to 0 :

- Vertical shift of overturning moment, QSX1
- Combined slip Fx shift factor reduction, RHX1
- Efy curvature constant camber dependency, PEY3
- SHY horizontal shift at FZNOM, PHY1
- SHY variation with load, PHY2
- Svy/Fz vertical shift at FZNOM, PVY1
- Svy/Fz variation with load, PVY2
- Fy shift reduction with slip angle, RBY3
- Slip ratio side force Svyk/Muy*Fz at FZNOM, RVY1
- Side force Suyk/Muy*Fz variation with load, RVY2
- Bpt slope variation with camber, QBZ4
- Dpt peak trail variation with camber, QDZ3
- Dmr peak residual torque, QDZ6
- Dmr peak residual torque variation with load, QDZ7
- Ept variation with sign of alpha-t, QEZ4
- Sht horizontal trail shift at FZNOM, QHZ1
- Sht variation with load, QHZ2
- Nominal value of s/R0: effect of Fx on Mz, SSZ1

Turn slip - Include turn slip
on (default) | off
Select to include ply steer in Magic Formula equations.
By default, the blocks include ply steer and turn slip in the Magic Formula equations. The equations are fit to flat-belt test data and predict a number of tire effects, including ply steer and turn slip. Consider removing the effects if your:

- Test data does not include ply steer or turn slip data.
- Analysis does not require ply steer or turn slip effects.

If you clear Turn slip, the block internally:

- Sets the Magic Formula turn slip equations to 1. Specifically, equations 4.E77, 4.E79, 4.E81, 4.E83, 4.E84, 4.E92, 4.E102, 4.E101, and 4.E105. ${ }^{2}$.
- Uses Magic Formula terms that effect horizontal shift.
- Uses Magic Formula small turn slip values in 4.E27².


## Simulation

Maximum pressure, PRESMAX - Maximum pressure 1003118 (default) | scalar

Maximum pressure, PRESMAX, in Pa.
Minimum pressure, PRESMIN - Minimum pressure
9982 (default) | scalar
Minimum pressure, PRESMIN, in Pa.
Maximum normal force, FZMAX - Force
scalar
Maximum normal force, FZMAX, in N.
Minimum normal force, FZMIN - Force
scalar
Minimum normal force, FZMIN, in N.
Velocity tolerance used to handle low velocity situations, VXLOW - Tolerance scalar

Velocity tolerance used to handle low-velocity situations, VXLOW, in m/s.
Max allowable slip ratio (absolute), KPUMAX - Max allowable slip ratio 0.999 (default) | scalar

Max allowable slip ratio (absolute), KPUMAX, dimensionless.
Minimum allowable slip ratio (absolute), KPUMIN - Minimum allowable slip ratio -0. 999 (default) | scalar

Minimum allowable slip ratio (absolute), KPUMIN, dimensionless.
Max allowable slip angle (absolute), ALPMAX - Max allowable slip angle 1.5708 (default) | scalar

Max allowable slip angle (absolute), ALPMAX, in rad.
Minimum allowable slip angle (absolute), ALPMIN - Minimum allowable slip angle - 1.5708 (default) | scalar

Minimum allowable slip angle (absolute), ALPMIN, in rad.
Maximum allowable camber angle, CAMMAX - Maximum allowable camber angle 0.173 | scalar

Maximum allowable camber angle CAMMAX, in rad.
Minimum allowable camber angle, CAMMIN - Minimum allowable camber angle
-0.173 | scalar

Minimum allowable camber angle, CAMMIN, in rad.
Nominal longitudinal speed, LONGVL - Speed
scalar
Nominal longitudinal speed, $L O N G V L$, in $\mathrm{m} / \mathrm{s}$.
Default tyre side, tyreside - Side
'Right' (default)|char
Default tyre side, tyreside, dimensionless.
Wheel
Initial rotational velocity, omegao - Velocity
scalar
Initial rotational velocity, specified as a scalar, in rad/s.
Rotational damping, br - Damping
scalar
Rotational damping, specified as a scalar, in $\mathrm{N} \cdot \mathrm{m} \cdot \mathrm{s} / \mathrm{rad}$.
Unloaded radius, UNLOADED_RADIUS - Radius
scalar
Unloaded radius, UNLOADED_RADIUS, in m.
Nominal pressure, NOMPRES - Pressure
scalar
Nominal pressure, NOMPRES, in Pa.
Nominal normal force, FNOMIN - Force
scalar
Nominal normal force, FNOMIN, in N.
Wheel width, WIDTH - Width
scalar
Wheel width, WIDTH, in m.
Rim radius, RIM_RADIUS - Radius
scalar
Rim radius, RIM_RADIUS, in m.
Nominal aspect ratio, ASPECT_RATIO - Ratio scalar

Nominal aspect ratio, ASPECT_RATIO, dimensionless.

```
Inertial
Wheel mass, MASS - Mass
scalar
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Wheel mass, specified as a scalar, in kg .
Rotational inertia (rolling axis), IYY - Inertia
scalar
Rotational inertia (rolling axis), specified as a scalar, in $\mathrm{kg} \cdot \mathrm{m}^{2}$.
Gravity, GRAVITY - Gravity
scalar
Gravity, GRAVITY, in m/s^2.

## Vertical

Initial tire displacement, zo - Displacement
scalar
Initial tire displacement, $z o$, in m .
Initial wheel vertical velocity (wheel fixed frame), zdoto - Velocity scalar

Initial wheel vertical velocity (wheel fixed frame), $z$ doto, in $\mathrm{m} / \mathrm{s}$.
Effective rolling radius at low load stiffness, BREFF - Stiffness
scalar
Effective rolling radius at low load stiffness, BREFF, dimensionless.
Effective rolling radius peak value, DREFF - Radius
scalar
Effective rolling radius peak value, $D R E F F$, dimensionless.
Effective rolling radius at high load stiffness, FREFF - Radius
scalar
Effective rolling radius at high load stiffness, FREFF, dimensionless.
Unloaded to nominal rolling radius ratio, Q_REO - Ratio scalar

Unloaded to nominal rolling radius ratio, $Q_{-}$REO, dimensionless.
Radius rotational speed dependence, Q_V1 - Speed scalar

Radius rotational speed dependence, $Q_{-}$V1, dimensionless.
Stiffness rotational speed dependence, Q_V2 - Speed scalar

Stiffness rotational speed dependence, $Q_{-} V 2$, dimensionless.
Linear load change with deflection, Q_FZ1 - Load change scalar

Linear load change with deflection, Q_FZ1, dimensionless.
Quadratic load change with deflection, Q_FZ2 - Load change scalar

Quadratic load change with deflection, Q_FZ2, dimensionless.
Linear load change with deflection and quadratic camber, Q_FZ3 - Load change scalar

Linear load change with deflection and quadratic camber, Q_FZ3, dimensionless.
Load response to longitudinal force, Q_FCX - Force scalar

Load response to longitudinal force, $Q_{-} F C X$, dimensionless.
Load response to lateral force, Q_FCY - Force scalar

Load response to lateral force, $Q_{-} F C Y$, dimensionless.
Vertical stiffness change due to lateral load dependency on lateral stiffness, Q_FCY2 Stiffness
scalar
Vertical stiffness change due to lateral load dependency on lateral stiffness, $Q_{-} F C Y 2$, dimensionless.
Stiffness response to pressure, PFZ1 - Stiffness
scalar
Stiffness response to pressure, PFZ1, dimensionless.
Vertical tire stiffness, VERTICAL_STIFFNESS - Stiffness
scalar
Vertical tire stiffness, VERTICAL_STIFFNESS, in N/m.
Vertical tire damping, VERTICAL_DAMPING - Damping
scalar
Vertical tire damping, VERTICAL_DAMPING, in $\mathrm{N} \cdot \mathrm{s} / \mathrm{m}$.
Rim bottoming out offset, BOTTOM_OFFST - Offset
scalar
Rim bottoming out offset, BOTTOM_OFFST, in m.
Bottoming out stiffness, BOTTOM_STIFF - Stiffness
scalar

Bottoming out stiffness, BOTTOM_STIFF, in N/m.
Linear load dependent camber angle influence on vertical stiffness, Q_CAM1 - Stiffness scalar

Linear load dependent camber angle influence on vertical stiffness, Q_CAM1, dimensionless.
Quadratic load dependent camber angle influence on vertical stiffness, Q_CAM2 - Stiffness scalar

Quadratic load dependent camber angle influence on vertical stiffness, Q_CAM2, dimensionless.
Linear load and camber angle dependent reduction on vertical stiffness, Q_CAM3 - Stiffness scalar

Linear load and camber angle dependent reduction on vertical stiffness, $Q_{-} C A M 3$, dimensionless.

## Structural

Longitudinal stiffness, LONGITUDINAL_STIFFNESS - Stiffness
scalar
Longitudinal stiffness, LONGITUDINAL_STIFFNESS, in N/m.
Lateral stiffness, LATERAL_STIFFNESS - Stiffness
scalar
Longitudinal stiffness, LATERAL_STIFFNESS, in N/m.
Linear vertical deflection influence on longitudinal stiffness, PCFX1 - Deflection influence scalar

Linear vertical deflection influence on longitudinal stiffness, PCFX1, dimensionless.
Quadratic vertical deflection influence on longitudinal stiffness, PCFX2 - Deflection influence scalar

Quadratic vertical deflection influence on longitudinal stiffness, PCFX2, dimensionless.
Pressure dependency on longitudinal stiffness, PCFX3 - Pressure dependency scalar

Pressure dependency on longitudinal stiffness, PCFX3, dimensionless.
Linear vertical deflection influence on lateral stiffness, PCFY1 - Deflection influence scalar

Linear vertical deflection influence on lateral stiffness, PCFY1, dimensionless.
Quadratic vertical deflection influence on lateral stiffness, PCFY2 - Deflection influence scalar

Quadratic vertical deflection influence on lateral stiffness, PCFY2, dimensionless.
Pressure dependency on longitudinal stiffness, PCFY3 - Pressure dependency scalar

Pressure dependency on longitudinal stiffness, PCFY3, dimensionless.

## Contact Patch

Contact length square root term, Q_RA1 - Length term scalar

Contact length square root term, $Q \_R A 1$, dimensionless.
Contact length linear term, Q_RA2 - Length term
scalar
Contact length linear term, $Q_{-} R A 2$, dimensionless.
Contact width root term, Q_RB1 - Width term
scalar
Contact width root term, $Q_{-} R B 1$, dimensionless.
Contact width linear term, Q_RB2 - Width term
scalar
Contact width linear term, $Q_{-} R B 2$, dimensionless.

## Longitudinal

Cfx shape factor, PCX1 - Shape factor
scalar
Shape factor, $C_{f x}, P C X 1$, dimensionless.
Longitudinal friction at nominal normal load, PDX1 - Friction
scalar
Longitudinal friction at nominal normal load, PDX1, dimensionless.
Frictional variation with load, PDX2 - Friction variation

## scalar

Frictional variation with load, $P D X 2$, dimensionless.
Frictional variation with camber, PDX3 - Friction variation scalar

Frictional variation with camber, $P D X 3$, in $1 / \mathrm{rad}^{\wedge} 2$.

## Longitudinal curvature at nominal normal load, PEX1 - Curvature scalar

Longitudinal curvature at nominal normal load, PEX1, dimensionless.
Variation of curvature factor with load, PEX2 - Curvature variation scalar

Variation of curvature factor with load, PEX2, dimensionless.

Variation of curvature factor with square of load, PEX3 - Curvature variation scalar

Variation of curvature factor with square of load, PEX3, dimensionless.
Longitudinal curvature factor with slip, PEX4 - Curvature
scalar
Longitudinal curvature factor with slip, PEX4, dimensionless.
Longitudinal slip stiffness at nominal normal load, PKX1 - Stiffness
scalar
Longitudinal slip stiffness at nominal normal load, PKX1, dimensionless.
Variation of slip stiffness with load, PKX2 - Stiffness variation scalar

Variation of slip stiffness with load, $P K X 2$, dimensionless.
Slip stiffness exponent factor, PKX3 - Slip stiffness
scalar
Slip stiffness exponent factor, $P K X 3$, dimensionless.
Horizontal shift in slip ratio at nominal normal load, PHX1 - Slip ratio shift scalar

Horizontal shift in slip ratio at nominal normal load, PHX1, dimensionless.
Variation of horizontal slip ratio with load, PHX2 - Slip variation scalar

Variation of horizontal slip ratio with load, PHX 2 , dimensionless.
Vertical shift in load at nominal normal load, PVX1 - Load shift scalar

Vertical shift in load at nominal normal load, $P V X 1$, dimensionless.
Variation of vertical shift with load, PVX2 - Load variation
scalar
Variation of vertical shift with load, PVX2, dimensionless.
Linear variation of longitudinal slip stiffness with tire pressure, PPX1 - Stiffness variation scalar

Linear variation of longitudinal slip stiffness with tire pressure, PPX1, dimensionless.
Quadratic variation of longitudinal slip stiffness with tire pressure, PPX2 - Stiffness variation scalar

Quadratic variation of longitudinal slip stiffness with tire pressure, PPX2, dimensionless.

Linear variation of peak longitudinal friction with tire pressure, PPX3 - Friction variation scalar

Linear variation of peak longitudinal friction with tire pressure, $P P X 3$, dimensionless.
Quadratic variation of peak longitudinal friction with tire pressure, PPX4 - Friction variation scalar

Quadratic variation of peak longitudinal friction with tire pressure, PPX4, dimensionless.
Combined slip Fx slope factor reduction, RBX1 - Combined slip longitudinal force slope factor reduction
scalar
Combined slip longitudinal force, $F_{x}$, slope factor reduction, $R B X 1$, dimensionless.
Slip ratio Fx slope reduction variation, RBX2 - Slip ratio longitudinal force slope reduction variation
scalar
Slip ratio longitudinal force, $F_{x}$, slope reduction variation, $R B X 2$, dimensionless.
Camber influence on combined slip Fx stiffness, RBX3 - Camber influence on combined slip longitudinal force stiffness
scalar
Camber influence on combined slip longitudinal force, $F_{x}$, stiffness, $R B X 3$, dimensionless.
Shape factor for combined slip Fx reduction, RCX1 - Shape factor for combined slip longitudinal force reduction
scalar
Shape factor for combined slip longitudinal force, $F_{x}$, reduction, $R C X 1$, dimensionless.
Combined Fx curvature factor, REX1 - Combined longitudinal force curvature factor scalar

Combined longitudinal force, $F_{x}$, curvature factor, REX1, dimensionless.
Combined Fx curvature factor with load, REX2 - Combined longitudinal force curvature factor scalar

Combined longitudinal force, $F_{x}$, curvature factor with load, REX2, dimensionless.
Combined slip Fx shift factor reduction, RHX1 - Combined slip longitudinal force slip factor scalar

Combined slip longitudinal force, $F_{x}$, shift factor reduction, RHX1, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.

## Overturning

Vertical shift of overturning moment, QSX1 - Overturning moment scalar

Vertical shift of overturning moment, QSX1, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Overturning moment due to camber, QSX2 - Overturning moment due to camber scalar

Overturning moment due to camber, QSX2, dimensionless.
Overturning moment due to Fy, QSX3 - Overturning moment due to lateral force scalar

Overturning moment due to lateral force, QSX3, dimensionless.
Mx combined lateral force load and camber, QSX4 - Overturning moment scalar

Overturning moment, $M_{x}$, combined lateral force load and camber, QSX4, dimensionless.
Mx load effect due to lateral force and camber, QSX5 - Overturning moment scalar

Overturning moment, $M_{x}$, load effect due to lateral force and camber, QSX5, dimensionless.
Mx load effect due to B-factor, QSX6 - Overturning moment scalar

Overturning moment, $M_{x}$, load effect due to B-factor, QSX6, dimensionless.
Mx due to camber and load, QSX7 - Overturning moment
scalar
Overturning moment, $M_{x}$, due to camber and load, QSX7, dimensionless.
Mx due to lateral force and load, QSX8 - Overturning moment
scalar
Overturning moment, $M_{x}$, due to lateral force and load, QSX8, dimensionless.
Mx due to B-factor of lateral force and load, QSX9 - Overturning moment scalar

Overturning moment, $M_{x}$, due to B-factor of lateral force and load, QSX9, dimensionless.
Mx due to vertical force and camber, QSX10 - Overturning moment scalar

Overturning moment, $M_{x}$, due to vertical force and camber, QSX10, dimensionless.
Mx due to B-factor of vertical force and camber, QSX11 - Overturning moment scalar

Overturning moment, $M_{x}$, due to B-factor of vertical force and camber, QSX11, dimensionless.

Mx due to squared camber, QSX12 - Overturning moment scalar

Overturning moment, $M_{x}$, due to squared camber, QSX12, dimensionless.
Mx due to lateral force, QSX13 - Overturning moment
scalar
Overturning moment, $M_{x}$, due to lateral force, QSX13, dimensionless.
Mx due to lateral force with camber, QSX14 - Overturning moment scalar

Overturning moment, $M_{x}$, due to lateral force with camber, QSX14, dimensionless.
Mx due to inflation pressure, PPMX1 - Overturning moment due to pressure scalar

Overturning moment, $M_{x}$, due to inflation pressure, PPMX1, dimensionless.

## Lateral

Cfy shape factor for lateral force, PCY1 - Lateral force shape factor scalar

Shape factor for lateral force, $C_{f y}, P C Y 1$, dimensionless.
Lateral friction muy, PDY1 - Lateral friction
scalar
Lateral friction, $\mu_{y}$ PDY1, dimensionless.
Lateral friction variation of muy with load, PDY2 - Lateral friction variation scalar

Variation of lateral friction, $\mu_{y}$, with load, PDY2, dimensionless.
Lateral friction variation of muy with squared camber, PDY3 - Lateral friction variation scalar

Variation of lateral friction, $\mu_{y}$, with squared camber, PDY3, dimensionless.
Efy lateral curvature at nominal force FZNOM, PEY1 - Lateral curvature at nominal force scalar

Lateral curvature, $E f_{y}$, at nominal force, $F_{Z N O M}, P E Y 1$, dimensionless.
Efy curvature variation with load, PEY2 - Lateral curvature variation scalar

Lateral curvature, $E f_{y}$, variation with load, $P E Y 2$, dimensionless.
Efy curvature constant camber dependency, PEY3 - Lateral curvature constant scalar

Lateral curvature, $E f_{y}$, constant camber dependency, PEY3, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Efy curvature variation with camber, PEY4 - Lateral curvature variation scalar

Lateral curvature, $E f_{y}$, variation with camber, $P E Y 4$, dimensionless.
Efy curvature variation with camber squared, PEY5 - Lateral curvature variation scalar

Lateral curvature, $E f_{y}$, variation with camber squared, PEY5, dimensionless.
Maximum KFy/FZNOM stiffness, PKY1 - Maximum stiffness scalar

Maximum lateral force stiffness, $K F_{y}$, to nominal force, $F_{Z N O M}$, ratio, $P K Y 1$, dimensionless.
Load at maximum KFy/FZNOM stiffness, PKY2 - Load
scalar
Load at maximum lateral force stiffness, $K F_{y}$, to nominal force, $F_{Z N O M}$, ratio, $P K Y 2$, dimensionless.
KFy/FZNOM stiffness variation with camber, PKY3 - Stiffness variation scalar

Lateral force stiffness, $K F_{y}$, to nominal force, $F_{Z N O M}$, stiffness variation with camber, PKY3, dimensionless.

KFy curvature, PKY4 - Lateral force stiffness curvature scalar

Lateral force stiffness, $K F_{y}$ curvature, $P K Y 4$, dimensionless.
Variation of peak stiffness with squared camber, PKY5 - Stiffness variation scalar

Variation of peak stiffness with squared camber, $P K Y 5$, dimensionless.
Fy camber stiffness factor, PKY6 - Lateral force camber stiffness factor scalar

Lateral force, $F_{y}$, camber stiffness factor, PKY6, dimensionless.
Camber stiffness vertical load dependency, PKY7 - Stiffness
scalar
Camber stiffness vertical load dependency, PKY7, dimensionless.
SHY horizontal shift at FZNOM, PHY1 - Horizontal shift at nominal force scalar

Horizontal shift, $S_{H Y}$, at nominal force, $F_{Z N O M}$, PHY1, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
SHY variation with load, PHY2 - Horizontal shift variation
scalar
Horizontal shift, $S_{H Y}$, variation with load, $P H Y 2$, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Svy/Fz vertical shift at FZNOM, PVY1 - Vertical shift at nominal force scalar

Vertical shift, $S_{v y}$, at nominal force, $F_{Z N O M}, P V Y 1$, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Svy/Fz variation with load, PVY2 - Vertical shift variation with load scalar

Vertical shift, $S_{v y}$, variation with load, $P V Y 2$, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Svy/Fz variation with camber, PVY3 - Vertical shift variation with camber scalar

Vertical shift, $S_{v y}$, variation with camber, PVY3, dimensionless.
Svy/Fz variation with load and camber, PVY4 - Vertical shift variation with load and camber scalar

Vertical shift, $S_{v y}$, variation with load and camber, $P V Y 4$, dimensionless.
Cornering stiffness variation with inflation pressure, PPY1 - Stiffness variation with pressure scalar

Cornering stiffness variation with inflation pressure, PPY1, dimensionless.
Cornering stiffness variation with inflation pressure induced nominal load dependency, PPY2 - Stiffness variation with pressure
scalar
Cornering stiffness variation with inflation pressure induced nominal load dependency, PPY2, dimensionless.

## Linear inflation pressure on peak lateral friction, PPY3 - Pressure

scalar
Linear inflation pressure on peak lateral friction, $P P Y 3$, dimensionless.

## Quadratic inflation pressure on peak lateral friction, PPY4 - Pressure

 scalarQuadratic inflation pressure on peak lateral friction, $P P Y 4$, dimensionless.
Inflation pressure effect on camber stiffness, PPY5 - Pressure scalar

Inflation pressure effect on camber stiffness, PPY5, dimensionless.
Combined Fy reduction slope factor, RBY1 - Combined lateral force reduction slope factor scalar

Combined lateral force, $F_{y}$, reduction slope factor, RBY1, dimensionless.
Fy slope reduction with slip angle, RBY2 - Lateral force slope reduction with slip angle scalar

Lateral force, $F_{y}$, slope reduction with slip angle, $R B Y 2$, dimensionless.
Fy shift reduction with slip angle, RBY3 - Lateral force shift reduction with slip angle scalar

Lateral force, $F_{y}$, shift reduction with slip angle, $R B Y 3$, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Fy combined stiffness variation from camber, RBY4 - Lateral force combined stiffness variation from camber
scalar
Lateral force, $F_{y}$, combined stiffness variation from camber, RBY4, dimensionless.
Fy combined reduction shape factor, RCY1 - Lateral force combined reduction shape factor scalar

Lateral force, $F_{y}$, combined reduction shape factor, RCY1, dimensionless.
Fy combined curvature factor, REY1 - Lateral force combined curvature factor scalar

Lateral force, $F_{y}$, combined curvature factor, REY1, dimensionless.
Fy combined curvature factor with load, REY2 - Lateral force combined curvature factor with load scalar

Lateral force, $F_{y}$, combined curvature factor with load, REY2, dimensionless.
Fy combined reduction shift factor, RHY1 - Lateral force combined reduction shift factor scalar

Lateral force, $F_{y}$ combined reduction shift factor, RHY1, dimensionless.

Fy combined reduction shift factor with load, RHY2 - Lateral force combined reduction shift factor with load
scalar
Lateral force, $F_{y}$, combined reduction shift factor with load, RHY2, dimensionless.
Slip ratio side force Svyk/Muy*Fz at FZNOM, RVY1 - Slip ratio slide force at nominal force scalar

Slip ratio side force at nominal force, $F_{Z N O M}, R V Y 1$, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Side force Svyk/Muy*Fz variation with load, RVY2 - Side force variation with load scalar

Side force variation with load, RVY2, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Side force Svyk/Muy*Fz variation with camber, RVY3 - Side force variation with camber scalar

Side force variation with camber, $R V Y 3$, dimensionless.
Side force Svyk/Muy*Fz variation with slip angle, RVY4 - Side force variation with slip angle scalar

Side force variation with slip angle, RVY4, dimensionless.
Side force Svyk/Muy*Fz variation with slip ratio, RVY5 - Side force variation with slip ratio scalar

Side force variation with slip ratio, $R V Y 5$, dimensionless.
Side force Svyk/Muy*Fz variation with slip ratio arctangent, RVY6 - Side force variation with slip ratio arctangent
scalar
Side force variation with slip ratio arctangent, RVY6, dimensionless.

## Rolling

Torque resistance coefficient, QSY1 - Torque resistance scalar

Torque resistance coefficient, QSY1, dimensionless.
Torque resistance due to Fx, QSY2 - Torque resistance due to longitudinal force scalar

Torque resistance due to longitudinal force, $F_{x}$, $Q S Y 2$, dimensionless.

Torque resistance due to speed, QSY3 - Torque resistance due to speed scalar

Torque resistance due to speed, QSY3, dimensionless.
Torque resistance due to speed^4, QSY4 - Torque resistance due to speed scalar

Torque resistance due to speed^ ${ }^{\wedge}$, $Q S Y 4$, dimensionless.
Torque resistance due to square of camber, QSY5 - Torque resistance due to camber scalar

Torque resistance due to square of camber, QSY5, dimensionless.
Torque resistance due to square of camber and load, QSY6 - Torque resistance due to camber and load
scalar
Torque resistance due to square of camber and load, QSY6, dimensionless.
Torque resistance due to load, QSY7 - Torque resistance due to load scalar

Torque resistance due to load, QSY7, dimensionless.
Torque resistance due to pressure, QSY8 - Torque resistance due to pressure scalar

Torque resistance due to pressure, QSY8, dimensionless.
Aligning
Trail slope factor for trail Bpt at FZNOM, QBZ1 - Trail slope factor at nominal force scalar

Trail slope factor for trail Bpt at nominal force, $F_{\text {ZNOM }}, Q B Z 1$, dimensionless.
Bpt slope variation with load, QBZ2 - Slope variation with load scalar

Slope variation with load, QBZ2, dimensionless.
Bpt slope variation with square of load, QBZ3 - Slope variation with load scalar

Slope variation with square of load, $Q B Z 3$, dimensionless.
Bpt slope variation with camber, QBZ4 - Slope variation with camber scalar

Slope variation with camber, QBZ4, dimensionless.
Dependencies
If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.

Bpt slope variation with absolute value of camber, QBZ5 - Slope variation with camber scalar

Slope variation with absolute value of camber, QBZ5, dimensionless.
Bpt slope variation with square of camber, QBZ6 - Slope variation with camber scalar

Slope variation with square of camber, QBZ6, dimensionless.
Br of Mzr slope scaling factor, QBZ9 - Slope scaling factor
scalar
Slope scaling factor, QBZ9, dimensionless.
Br of Mzr cornering stiffness factor, QBZ10 - Cornering stiffness factor 0 (default) | scalar
$B r$ of $M z r$ cornering stiffness factor, $Q B Z 10$, dimensionless.
Cpt pneumatic trail shape factor, QCZ1 - Pneumatic trail shape factor scalar

Pneumatic trail shape factor, $C_{p t}$, $Q C Z 1$, dimensionless.
Dpt peak trail, QDZ1 - Peak trail
scalar
Peak trail, $D_{p t}$ QDZ1, dimensionless.
Dpt peak trail variation with load, QDZ2 - Peak trail variation with load scalar

Peak trail, $D_{p t}$, variation with load, $Q D Z 2$, dimensionless.
Dpt peak trail variation with camber, QDZ3 - Peak trail variation with camber scalar

Peak trail, $D_{p t}$, variation with camber, $Q D Z 3$, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Dpt peak trail variation with square of camber, QDZ4 - Peak trail variation with camber scalar

Peak trail, $D_{p t}$, variation with square of camber, $Q D Z 4$, dimensionless.
Dmr peak residual torque, QDZ6 - Peak residual torque scalar

Peak residual torque, $D_{m r}$, QDZ6, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.

Dmr peak residual torque variation with load, QDZ7 - Peak residual torque variation with load scalar

Peak residual torque, $D_{m r}$, variation with load, $Q D Z 7$, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Dmr peak residual torque variation with camber, QDZ8 - Peak residual torque variation with camber
scalar
Peak residual torque, $D_{m r}$, variation with camber, QDZ8, dimensionless.
Dmr peak residual torque variation with camber and load, QDZ9 - Peak residual torque variation with camber and load
scalar
Peak residual torque, $D_{m r}$, variation with camber and load, $Q D Z 9$, dimensionless.
Dmr peak residual torque variation with square of camber, QDZ10 - Peak residual torque variation with camber
scalar
Peak residual torque, $D_{m r}$, variation with square of camber, QDZ10, dimensionless.
Dmr peak residual torque variation with square of load, QDZ11 - Peak residual torque variation with load
scalar
Peak residual torque, $D_{m r}$, variation with square of load, $Q D Z 11$, dimensionless.
Ept trail curvature at FZNOM, QEZ1 - Trail curvature at nominal force scalar

Trail curvature, $E_{p t}$, at nominal force, $F_{Z N O M}$, QEZ1, dimensionless.
Ept variation with load, QEZ2 - Trail curvature variation with load scalar

Trail curvature, $E_{p t}$ variation with load, $Q E Z 2$, dimensionless.
Ept variation with square of load, QEZ3 - Trail curvature variation with load scalar

Trail curvature, $E_{p t}$ variation with square of load, QEZ3, dimensionless.
Ept variation with sign of alpha-t, QEZ4 - Trail curvature variation scalar

Trail curvature, $E_{p t}$ variation with sign of alpha-t, QEZ4, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.

## Ept variation with sign of alpha-t and camber, QEZ5 - Variation <br> scalar

Trail curvature, $E_{p t}$ variation with sign of alpha-t and camber, $Q E Z 5$, dimensionless.
Sht horizontal trail shift at FZNOM, QHZ1 - Horizontal trail shift at nominal load scalar

Horizontal trail shift, $S h_{t}$, at nominal load, $F_{Z N O M}, Q H Z 1$, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Sht variation with load, QHZ2 - Horizontal trail shift variation with load scalar

Horizontal trail shift, $S h_{t}$, variation with load, $Q H Z 2$, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
Sht variation with camber, QHZ3 - Horizontal trail shift variation with camber scalar

Horizontal trail shift, $S h_{t}$, variation with camber, $Q H Z 3$, dimensionless.
Sht variation with load and camber, QHZ4 - Horizontal trail shift variation with load and camber scalar

Horizontal trail shift, $S h_{t}$, variation with load and camber, QHZ4, dimensionless.
Inflation pressure influence on trail length, PPZ1 - Pressure influence on trail length scalar

Inflation pressure influence on trail length, $P P Z 1$, dimensionless.
Inflation pressure influence on residual aligning torque, PPZ2 - Pressure influence on aligning torque
scalar
Inflation pressure influence on residual aligning torque, PPZ2, dimensionless.
Nominal value of s/R0: effect of Fx on Mz, SSZ1 - Effect of longitudinal force on aligning torque scalar

Nominal value of $\mathrm{s} / \mathrm{R} 0$ : effect of longitudinal force, $F_{x}$, on aligning torque, $M_{z}$, SSZ1, dimensionless.

## Dependencies

If you clear Ply steer, the block internally sets this parameter to 0 in the Magic Formula equations.
$\mathbf{s / R 0}$ variation with lateral to nominal force ratio, SSZ2 - Variation with lateral to nominal force ratio
scalar

Variation with lateral to nominal force ratio, SSZ2, dimensionless.
s/R0 variation with camber, SSZ3 - Variation with camber
scalar
Variation with camber, SSZ3, dimensionless.
s/R0 variation with camber and load, SSZ4 - Variation with camber and load scalar

Variation with camber and load, SSZ4, dimensionless.

## Turnslip

Fx peak reduction due to spin, PDXP1 - Longitudinal force peak reduction due to spin scalar

Longitudinal force, $F_{x}$, peak reduction due to spin, PDXP1, dimensionless.
Fx peak reduction due to spin with varying load, PDXP2 - Longitudinal force peak reduction due to spin
scalar
Longitudinal force, $F_{x}$, peak reduction due to spin with varying load, $P D X P 2$, dimensionless.
Fx peak reduction due to spin with slip ratio, PDXP3 - Longitudinal force peak reduction due to spin
scalar
Longitudinal force, $F_{x}$, peak reduction due to spin with slip ratio, PDXP3, dimensionless.
Cornering stiffness reduction due to spin, PKYP1 - Stiffness reduction due to spin scalar

Cornering stiffness reduction due to spin, PKYP1, dimensionless.
Fy peak reduction due to spin, PDYP1 - Lateral force peak reduction due to spin scalar

Lateral force, $F_{y}$, peak reduction due to spin, PDYP1, dimensionless.
Fy peak reduction due to spin with varying load, PDYP2 - Lateral force peak reduction due to spin
scalar
Lateral force, $F_{y}$, peak reduction due to spin with varying load, PDYP2, dimensionless.
Fy peak reduction due to spin with slip angle, PDYP3 - Lateral force peak reduction due to spin scalar

Lateral force, $F_{y}$, peak reduction due to spin with slip angle, PDYP3, dimensionless.
Fy peak reduction due to square root of spin, PDYP4 - Lateral force peak reduction due to spin scalar

Lateral force, $F_{y}$, peak reduction due to square root of spin, PDYP4, dimensionless.

Fy vs. slip angle response lateral shift limit, PHYP1 - Lateral force versus slip angle response scalar

Lateral force, $F_{y}$, versus slip angle response lateral shift limit, PHYP1, dimensionless.
Fy vs. slip angle response max lateral shift limit, PHYP2 - Lateral force versus slip angle response scalar

Lateral force, $F_{y}$, versus slip angle response max lateral shift limit, PHYP2, dimensionless.
Fy vs. slip angle response max lateral shift limit with load, PHYP3 - Lateral force versus slip angle response
scalar
Lateral force, $F_{y}$, versus slip angle response max lateral shift limit with load, PHYP3, dimensionless.
Fy vs. slip angle response lateral shift curvature factor, PHYP4 - Lateral force versus slip angle response
scalar
Lateral force, $F_{y}$, versus slip angle response lateral shift curvature factor, PHYP4, dimensionless.
Camber stiffness reduction due to spin, PECP1 - Camber stiffness reduction scalar

Camber stiffness reduction due to spin, PECP1, dimensionless.
Camber stiffness reduction due to spin with load, PECP2 - Camber stiffness reduction scalar

Camber stiffness reduction due to spin with load, $P E C P 2$, dimensionless.
Turn slip pneumatic trail reduction factor, QDTP1 - Turn slip pneumatic trail reduction factor scalar

Turn slip pneumatic trail reduction factor, QDTP1, dimensionless.
Turn moment for constant turning and zero longitudinal speed, QCRP1 - Turn moment for constant turning scalar

Turn moment for constant turning and zero longitudinal speed, QCRP1, dimensionless.
Turn slip moment increase with spin at 90deg slip angle, QCRP2 - Turn slip moment scalar

Turn slip moment increase with spin at 90 -degree slip angle, QCRP2, dimensionless.
Residual spin torque reduction from side slip, QBRP1 - Residual spin torque reduction scalar

Residual spin torque reduction from side slip, QBRP1, dimensionless.
Turn slip moment peak magnitude, QDRP1 - Turn slip moment peak magnitude scalar

Turn slip moment peak magnitude, QDRP1, dimensionless.
Turn slip moment curvature, QDRP2 - Turn slip moment curvature scalar

Turn slip moment curvature, QDRP2, dimensionless.

## Version History

Introduced in R2021b

## R2022b: New Ply steer and Turn slip Parameters

Behavior changed in R2022b
Starting from R2022b, the Combined Slip Wheel STI block includes Ply steer and Turn slip parameters. To remove ply steer and turn slip from the Magic Formula implementation of these blocks, clear the Ply steer and Turn slip parameters.

## References

[1] Besselink, Igo, Antoine J. M. Schmeitz, and Hans B. Pacejka, "An improved Magic Formula/Swift tyre model that can handle inflation pressure changes," Vehicle System Dynamics International Journal of Vehicle Mechanics and Mobility 48, sup. 1 (2010): 337-52, https:// doi.org/10.1080/00423111003748088.
[2] Pacejka, Hans B. Tire and Vehicle Dynamics. 3rd ed. Oxford, United Kingdom: SAE and Butterworth-Heinemann, 2012.
[3] Bohm, F., and H. P. Willumeit, "Tyre Models for Vehicle Dynamic Analysis: Proceedings of the 2nd International Colloquium on Tyre Models for Vehicle Dynamics Analysis, Held at the Technical University of Berlin, Germany, February 20-21, 1997." Vehicle System Dynamics International Journal of Vehicle Mechanics and Mobility 27, sup. 1, 343-45. https://doi.org/ 0.1080/00423119708969669.
[4] Schmid, Steven R., Bernard J. Hamrock, and Bo O. Jacobson. Fundamentals of Machine Elements, SI Version. 3rd ed. Boca Raton: CRC Press, 2014.

## Extended Capabilities

C/C++ Code Generation
Generate C and C++ code using Simulink $\circledR_{\circledR}$ Coder ${ }^{\text {TM }}$.

## See Also

Combined Slip Wheel 2DOF | Combined Slip Wheel 2DOF CPI | Fiala Wheel 2DOF | Longitudinal Wheel \| Dugoff Wheel 2DOF

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"

## Dugoff Wheel 2DOF

Dugoff Wheel 2DOF wheel with disc, drum, or mapped brake


## Libraries:

Vehicle Dynamics Blockset / Wheels and Tires

## Description

The Dugoff Wheel 2DOF block implements a simplified tire with lateral and longitudinal slip capability based on the H. Dugoff model ${ }^{[1]}$. The block uses a translational friction model to calculate the forces and moments during combined longitudinal and lateral slip, requiring fewer parameters than the Combined Slip Wheel 2DOF block. If you do not have the tire coefficients needed by the Magic Formula, consider using this block for studies that do not involve extensive nonlinear combined lateral slip or lateral dynamics. If your study does require nonlinear combined slip or lateral dynamics, consider using the Combined Slip Wheel 2DOF block.

The block determines the wheel rotation rate, vertical motion, and forces and moments in all six degrees-of-freedom (DOFs) based on the driveline torque, brake pressure, road height, wheel camber angle, and inflation pressure. You can use this block for these types of analyses:

- Driveline and vehicle simulations that require low frequency tire-road and braking forces for vehicle acceleration, braking, and wheel rolling resistance calculations with minimal tire parameters.
- Wheel interaction with an idealized road surface.
- Ride and handling maneuvers for vehicles undergoing mild combined slip. For this analysis, you can connect the block to driveline and chassis components such as differentials, suspension, and vehicle body systems.
- Yaw stability. For this analyses, you can connect this block to more detailed braking system models.
- Tire stiffness and unsprung mass interactions with ground variations, load transfer, or chassis motion using the block vertical DOF.

The block integrates rotational wheel, vertical mass, and braking dynamics models.
Use the Tire Type parameter to select slip type.

| Action | Tire Type Setting |
| :--- | :--- |
| Calculate longitudinal and lateral <br> forces under nominal slip conditions | Nominal slip |


| Action | Tire Type Setting |
| :--- | :--- |
| Calculate longitudinal and lateral <br> forces with additional correction <br> factors for a more accurate response <br> at higher slip ratios | Extended slip |

Use the Brake Type parameter to select the brake.

| Action | Brake Type Setting |
| :--- | :--- |
| No braking | None |
| Implement brake that converts the <br> brake cylinder pressure into a <br> braking force | Disc |
| Implement simplex drum brake that <br> converts the applied force and brake <br> geometry into a net braking torque | Drum |
| Implement lookup table that is a <br> function of the wheel speed and <br> applied brake pressure | Mapped |

To calculate the rolling resistance torque, specify one of these Rolling Resistance parameters.

| Setting | Block Implementation |
| :--- | :--- |
| None | None |
| Pressure and velocity | Method in Stepwise Coastdown Methodology for Measuring <br> Tire Rolling Resistance. The rolling resistance is a function of <br> tire pressure, normal force, and velocity. |
| ISO 28580 | Method specified in ISO 28580:2018, Passenger car, truck <br> and bus tyre rolling resistance measurement method - <br> Single point test and correlation of measurement results. |
| Magic Formula | Magic formula equations from 4.E70 in Tire and Vehicle <br> Dynamics. The magic formula is an empirical equation based <br> on fitting coefficients. |
| Mapped torque | Lookup table that is a function of the normal force and spin <br> axis longitudinal velocity. |

To calculate vertical motion, specify one of these Vertical Motion parameters.

| Setting | Block Implementation |
| :--- | :--- |
| None | Block passes the applied chassis forces directly through to <br> the rolling resistance and longitudinal force calculations. |
| Mapped stiffness and damping | Vertical motion depends on wheel stiffness and damping. <br> Stiffness is a function of tire sidewall displacement and <br> pressure. Damping is a function of tire sidewall velocity and <br> pressure. |

## Rotational Wheel Dynamics

The block calculates the inertial response of the wheel subject to:

- Axle losses
- Brake and drive torque
- Tire rolling resistance
- Ground contact through the tire-road interface

The input torque is the summation of the applied axle torque, braking torque, and moment arising from the combined tire torque.

$$
T_{i}=T_{a}-T_{b}+T_{d}
$$

For the moment arising from the combined tire torque, the block implements tractive wheel forces and rolling resistance with first-order dynamics. The rolling resistance has a time constant parameterized in terms of a relaxation length.

$$
T_{d}(s)=\frac{1}{\frac{L_{e}}{|\omega| R_{e}} s+1}+\left(F_{x} R_{e}+M_{y}\right)
$$

To calculate the rolling resistance torque, you can specify one of these Rolling Resistance parameters.

| Setting | Block Implementation |
| :--- | :--- |
| None | Block sets rolling resistance, $M_{y}$, to zero. |
| Pressure and <br> velocity | Block uses the method in SAE Stepwise Coastdown Methodology for Measuring <br> Tire Rolling Resistance. The rolling resistance is a function of tire pressure, <br> normal force, and velocity, specifically, <br>  <br> $M_{y}=R_{e}\left\{a+b\left\|V_{x}\right\|+c V_{x}{ }^{2}\right\}\left\{F_{z} \beta p_{i} \alpha\right\} \tanh \left(4 V_{x}\right)$ |
| IS0 28580 | Block uses the method specified in ISO 28580:2018, Passenger car, truck and <br> bus tyre rolling resistance measurement method - Single point test and <br> correlation of measurement results. The method accounts for normal load, <br> parasitic loss, and thermal corrections from test conditions, specifically, |
| $\quad M_{y}=R_{e}\left(\frac{F_{z} C_{r}}{1+K_{t}\left(T_{a m b}-T_{\text {meas }}\right)}-F_{p l}\right)$ tanh $(\omega)$ |  |

If the brakes are enabled, the block determines the braking locked or unlocked condition based on an idealized dry clutch friction model. Based on the lock-up condition, the block implements these friction and dynamic models.

| Equation | Lock-Up Condition | Friction Model | Dynamic Model |
| :---: | :---: | :---: | :---: |
| $\omega \neq 0$ <br> or $\left\|T_{S}<\left\|T_{i}+T_{f}-\omega b\right\|\right.$ | Unlocked | $T_{f}=T_{k},$ <br> where $\begin{aligned} & T_{k}=F_{c} R_{e f f} \mu_{k} \tanh \left[4\left(-\omega_{d}\right)\right] \\ & T_{s}=F_{C} R_{e f f} \mu_{S} \\ & R_{e f f}=\frac{2\left(R_{o}^{3}-R_{i}^{3}\right)}{3\left(R_{o}{ }^{2}-R_{i}^{2}\right)} \end{aligned}$ | $\dot{\omega} J=-\omega b+T_{i}+T_{o}$ |
| $\begin{aligned} & \omega=0 \\ & \text { and } \\ & T_{S} \geq\left\|T_{i}+T_{f}-\omega b\right\| \end{aligned}$ | Locked | $T_{f}=T_{S}$ | $\omega=0$ |

The equations use these variables.

| Variable | Value |
| :--- | :--- |
| $\omega$ | Wheel angular velocity |
| $a$ | Velocity-independent force component |
| $b$ | Linear velocity force component |
| $c$ | Quadratic velocity force component |
| $L_{e}$ | Tire relaxation length |
| $J$ | Moment of inertia |
| $M_{y}$ | Rolling resistance torque |
| $T_{a}$ | Applied axle torque |
| $T_{b}$ | Braking torque |
| $T_{d}$ | Combined tire torque |
| $T_{f}$ | Frictional torque |
| $T_{i}$ | Net input torque |
| $T_{k}$ | Kinetic frictional torque |
| $T_{o}$ | Net output torque |
| $T_{s}$ | Static frictional torque |
| $F_{c}$ | Applied clutch force |
| $F_{x}$ | Longitudinal force developed by the tire road interface due to slip |
| $R_{e f f}$ | Effective clutch radius |
| $R_{o}$ | Annular disk outer radius |
| $R_{i}$ | Annular disk inner radius |
| $R_{e}$ | Effective tire radius while under load and for a given pressure |
| $V_{x}$ | Longitudinal axle velocity |
| $F_{z}$ | Vehicle normal force |
| $C_{r}$ | Rolling resistance constant |
| $T_{a m b}$ | Ambient temperature |


| Variable | Value |
| :--- | :--- |
| $T_{\text {meas }}$ | Measured temperature for rolling resistance constant |
| $F_{p l}$ | Parasitic force loss |
| $K_{t}$ | Thermal correction factor |
| $\alpha$ | Tire pressure exponent |
| $\beta$ | Normal force exponent |
| $p_{i}$ | Tire pressure |
| $\mu_{s}$ | Coefficient of static friction |
| $\mu_{k}$ | Coefficient of kinetic friction |

## Longitudinal Force

The block implements the longitudinal force as a function of wheel slip relative to the road surface using these equations.

| Calculation | Equation |
| :---: | :---: |
| Nominal Slip | $F_{X}=\frac{C_{k} K}{1-K} f(z),$ <br> where $\begin{aligned} & f(z)= \begin{cases}z(2-z) & \text { when } z<1 \\ 1 & \text { when } z \geq 1\end{cases} \\ & z=\frac{\mu F_{z}(1-\kappa)}{2 \sqrt{\left(C_{k} K\right)^{2}+\left(C_{\alpha} \tan (\alpha)\right)^{2}}} \end{aligned}$ |
| Extended | $F_{X}=\frac{C_{k} K}{1-K} f(z) g_{x}$ <br> where $\begin{aligned} & f(z)= \begin{cases}z(2-z) & \text { when } z<1 \\ 1 & \text { when } z \geq 1\end{cases} \\ & z=\frac{\mu F_{z}(1-\kappa)}{2 \sqrt{\left(C_{k} K\right)^{2}+\left(C_{\alpha} \tan (\alpha)\right)^{2}}} \\ & \left.g_{x}=\left(g_{x 1}+g_{x 2} \mu\right)\right)^{2}-\left(g_{x 3}+g_{x 4} \mu\right) K+g_{x 5} \end{aligned}$ |
| Friction coefficient | $\mu=\mu_{0}\left(1-A_{s} V_{s}\right),$ <br> where $V_{S}=u \sqrt{K^{2}+\tan ^{2}(\alpha)}$ |

The equations use these variables.

| Variable | Value |
| :--- | :--- |
| $F_{\chi}$ | Longitudinal force acting on axle along tire-fixed $x$-axis |
| $C_{K}$ | Longitudinal stiffness |
| $C_{\alpha}$ | Lateral stiffness per slip angle |


| Variable | Value |
| :--- | :--- |
| $k$ | Longitudinal slip ratio of tires |
| $F_{z}$ | Vertical contact patch normal force along tire-fixed $z$-axis |
| $u$ | Velocity component in the wheel plane |
| $\mu$ | Maximum friction coefficient |
| $\mu_{0}$ | Maximum friction scaling coefficient |
| $A_{s}$ | Friction reduction factor |
| $V_{s}$ | Friction reduction magnitude |
| $\alpha$ | Side slip angle of tires |
| $g_{x}$ | Longitudinal correction factor |
| $g_{\times 1}$ | Longitudinal squared slip correction factor |
| $g_{\times 2}$ | Longitudinal squared slip friction correction factor |
| $g_{\times 3}$ | Longitudinal linear slip correction factor |
| $g_{\times 4}$ | Longitudinal linear slip friction correction factor |
| $g_{\times 5}$ | Longitudinal offset correction factor |

## Lateral Force

The block implements the lateral force as a function of wheel slip angle state using these equations.

| Calculation | Equation |
| :---: | :---: |
| Nominal Slip | $F_{y}=\frac{C_{\alpha} \tan (\alpha)}{1-K} f(z)+\gamma C_{\gamma},$ <br> where $\begin{aligned} & f(z)= \begin{cases}z(2-z) & \text { when } z<1 \\ 1 & \text { when } z \geq 1\end{cases} \\ & z=\frac{\mu F_{z}(1-K)}{2 \sqrt{\left(C_{k} K\right)^{2}+\left(C_{\alpha} \tan (\alpha)\right)^{2}}} \end{aligned}$ |
| Extended Slip | $F_{y}=\frac{C_{\alpha} \tan (\alpha)}{1-K} f(z) g_{y}+\gamma C_{\gamma},$ <br> where $\begin{aligned} & f(z)= \begin{cases}z(2-z) & \text { when } z<1 \\ 1 & \text { when } z \geq 1\end{cases} \\ & z=\frac{\mu F_{z}(1-\kappa)}{2 \sqrt{\left(C_{k} K\right)^{2}+\left(C_{\alpha} \tan (\alpha)\right)^{2}}} \\ & g_{y}=\left(\mu+g_{y 1}\right) \tan (\alpha)+g_{y 2} \end{aligned}$ |
| Friction Coefficient | $\mu=\mu_{0}\left(1-A_{s} V_{s}\right),$ <br> where $V_{S}=u \sqrt{\kappa^{2}+\tan ^{2}(\alpha)}$ |

The equations use these variables.

| Variable | Value |
| :--- | :--- |
| $\alpha$ | Side slip angle of tires |
| $F_{y}$ | Lateral force acting on axle along tire-fixed $y$-axis |
| $F_{z}$ | Vertical contact patch normal force along tire-fixed $z$-axis |
| $\gamma$ | Camber angle |
| $C_{\gamma}$ | Camber stiffness |
| $C_{\alpha}$ | Lateral stiffness per angle slip |
| $C_{k}$ | Longitudinal stiffness |
| $k$ | Longitudinal slip ratio of tires |
| $u$ | Velocity component in the wheel plane |
| $\mu$ | Maximum friction coefficient |
| $\mu_{0}$ | Maximum friction scaling coefficient |
| $V_{s}$ | Friction reduction magnitude |
| $A_{s}$ | Friction reduction factor |
| $g_{y}$ | Lateral correction factor |
| $g_{y 1}$ | Lateral maximum friction correction factor |
| $g_{y 2}$ | Lateral offset correction factor |

## Vertical Dynamics

The block implements these equations for the vertical dynamics.

| Calculation | Equation |
| :--- | :--- |
| Vertical response | $\ddot{z} m=F_{z t i r e}+m g-F z$ |
| Tire normal force | $F_{z t i r e}=\rho_{z} k-b \dot{z}$ |
| Vertical sidewall deflection | $\rho_{z}=z_{\text {gnd }}-z, z \geq 0$ |

The equations use these variables.

| Variable | Value |
| :--- | :--- |
| $z$ | Tire deflection along tire-fixed $z$-axis |
| $z_{\text {gnd }}$ | Ground displacement along tire-fixed $z$-axis |
| $F_{\text {ztire }}$ | Tire normal force along tire-fixed $z$-axis |
| $F_{z}$ | Vertical force acting on axle along tire-fixed $z$-axis |
| $\rho_{z}$ | Vertical sidewall deflection along tire-fixed $z$-axis |
| $k$ | Vertical sidewall stiffness |
| $b$ | Vertical sidewall damping |

## Overturning, Aligning, and Scaling

This table summarizes the overturning, aligning, and scaling implementation.

| Calculation | Implementation |
| :--- | :--- |
| Overturning moment | The Dugoff model does not define an overturning moment. The <br> block implements this equation, requiring minimal parameters. <br> $M_{x}=F_{y} R_{e} \cos (\gamma)$ |
| Aligning moment | The block implements the aligning moment as a combination of yaw <br> rate damping and slip angle state. |
|  | $M_{z}= \begin{cases}\dot{\psi} b_{M_{z}} & \text { when }\left\|\alpha^{\prime}\right\|>\alpha^{\prime} \text { Critical } \\ \tanh \left(4 \alpha^{\prime}\right) w \mu\left\|F_{z}\right\|(1-\xi) \xi^{3}+\dot{\psi} b_{M_{z}} & \text { when }\left\|\alpha^{\prime}\right\| \leq \alpha_{C r i t i c a l ~}^{\prime}\end{cases}$ |
|  | $\xi=1-\frac{C_{a}\left\|\tan \left(\alpha^{\prime}\right)\right\|}{3 \mu\left\|F_{z}\right\|}$ |

The equations use these variables.

| Variable | Value |
| :--- | :--- |
| $M_{x}$ | Overturning moment acting on axle about tire-fixed $x$-axis |
| $M_{z}$ | Aligning moment acting on axle about tire-fixed $z$-axis |
| $R_{e}$ | Effective contact patch to wheel carrier radial distance |
| $\gamma$ | Camber angle |
| $k$ | Vertical sidewall stiffness |
| $b$ | Vertical sidewall damping |
| $\dot{\psi}$ | Tire angular velocity about the tire-fixed $z$-axis (yaw rate) |
| $w$ | Tire width |
| $\alpha^{\prime}$ | Slip angle state |
| $b_{M z}$ | Linear yaw rate resistance |
| $F_{y}$ | Lateral force acting on axle along tire-fixed $y$-axis |
| $C_{\gamma}$ | Camber stiffness |
| $C_{\alpha}$ | Lateral stiffness per slip angle |
| $\mu$ | Friction coefficient |
| $F_{z}$ | Vertical contact patch normal force along tire-fixed $z$-axis |

## Tire and Wheel Coordinate Systems

To resolve the forces and moments, the block uses the Z-Up orientation of the tire and wheel coordinate systems.

- Tire coordinate system axes $\left(X_{T}, Y_{T}, Z_{T}\right)$ are fixed in a reference frame attached to the tire. The origin is at the tire contact with the ground.
- Wheel coordinate system axes ( $X_{W}, Y_{W}, Z_{W}$ ) are fixed in a reference frame attached to the wheel. The origin is at the wheel center.


## Z-Up Orientation ${ }^{5}$



## Brakes

## Disc

If you specify the Brake Type parameter as Disc, the block implements a disc brake. This figure shows the side and front views of a disc brake.


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A disc brake converts brake cylinder pressure from the brake cylinder into force. The disc brake applies the force at the brake pad mean radius.

The block uses these equations to calculate brake torque for the disc brake.

$$
\begin{aligned}
& T= \begin{cases}\frac{\mu P_{\pi B} B_{a} R_{m} N_{\text {pads }}}{4} & \text { when } N \neq 0 \\
\frac{\mu_{\text {static }} P_{\Pi B} B_{a} 2 R_{m} N_{\text {pads }}}{4} & \text { when } N=0\end{cases} \\
& R m=\frac{R o+R i}{2}
\end{aligned}
$$

The equations use these variables.

| Variable | Value |
| :--- | :--- |
| $T$ | Brake torque |
| $P$ | Applied brake pressure |
| $N$ | Wheel speed |
| $N_{\text {pads }}$ | Number of brake pads in disc brake assembly |
| $\mu_{\text {static }}$ | Disc pad-rotor coefficient of static friction |
| $\mu$ | Disc pad-rotor coefficient of kinetic friction |
| $B_{a}$ | Brake actuator bore diameter |
| $R_{m}$ | Mean radius of brake pad force application on brake rotor |
| $R_{o}$ | Outer radius of brake pad |
| $R_{i}$ | Inner radius of brake pad |

## Drum

If you specify the Brake Type parameter as Drum, the block implements a static (steady-state) simplex drum brake. A simplex drum brake consists of a single two-sided hydraulic actuator and two brake shoes. The brake shoes do not share a common hinge pin.

The simplex drum brake model uses the applied force and brake geometry to calculate a net torque for each brake shoe. The drum model assumes that the actuators and shoe geometry are symmetrical for both sides, allowing a single set of geometry and friction parameters to be used for both shoes.

The block implements equations that are derived from these equations in Fundamentals of Machine Elements.

$$
\begin{aligned}
& T_{\text {rshoe }}=\left(\frac{\pi \mu c r\left(\cos \theta_{2}-\cos \theta_{1}\right) B_{a}{ }^{2}}{2 \mu\left(2 r\left(\cos \theta_{2}-\cos \theta_{1}\right)+a\left(\cos ^{2} \theta_{2}-\cos ^{2} \theta_{1}\right)\right)+a r\left(2 \theta_{1}-2 \theta_{2}+\sin 2 \theta_{2}-\sin 2 \theta_{1}\right)}\right) P \\
& T_{\text {lshoe }}=\left(\frac{\pi \mu c r\left(\cos \theta_{2}-\cos \theta_{1}\right) B_{a}^{2}}{-2 \mu\left(2 r\left(\cos \theta_{2}-\cos \theta_{1}\right)+a\left(\cos ^{2} \theta_{2}-\cos ^{2} \theta_{1}\right)\right)+a r\left(2 \theta_{1}-2 \theta_{2}+\sin 2 \theta_{2}-\sin 2 \theta_{1}\right)}\right) P \\
& T= \begin{cases}T_{\text {rshoe }}+T_{\text {lshoe }} & \text { when } N \neq 0 \\
\left(T_{\text {rshoe }}+T_{\text {lshoe }}\right) \frac{\mu_{\text {static }}}{\mu} & \text { when } N=0\end{cases}
\end{aligned}
$$



The equations use these variables.

| Variable | Value |
| :--- | :--- |
| $T$ | Brake torque |
| $P$ | Applied brake pressure |
| $N$ | Wheel speed |
| $\mu_{\text {static }}$ | Disc pad-rotor coefficient of static friction |
| $\mu$ | Disc pad-rotor coefficient of kinetic friction |
| $T_{\text {rshoe }}$ | Right shoe brake torque |
| $T_{\text {lshoe }}$ | Left shoe brake torque |
| $a$ | Distance from drum center to shoe hinge pin center |
| $C$ | Distance from shoe hinge pin center to brake actuator connection on brake shoe |
| $r$ | Drum internal radius |
| $B_{a}$ | Brake actuator bore diameter |
| $\Theta_{1}$ | Angle from shoe hinge pin center to start of brake pad material on shoe |
| $\Theta_{2}$ | Angle from shoe hinge pin center to end of brake pad material on shoe |

## Mapped

If you specify the Brake Type parameter as Mapped, the block uses a lookup table to determine the brake torque.

$$
T=\left\{\begin{array}{lr}
f_{\text {brake }}(P, N) & \text { when } N \neq 0 \\
\left(\frac{\mu_{\text {static }}}{\mu}\right) f_{\text {brake }}(P, N) & \text { when } N=0
\end{array}\right.
$$

The equations use these variables.

| Variable | Value |
| :--- | :--- |
| $T$ | Brake torque |
| $f_{\text {brake }}(P, N)$ | Brake torque lookup table |
| $P$ | Applied brake pressure |
| $N$ | Wheel speed |
| $\mu_{\text {static }}$ | Friction coefficient of drum pad-face interface under static conditions |
| $\mu$ | Friction coefficient of disc pad-rotor interface |

The lookup table for the brake torque, $f_{\text {brake }}(P, N)$, is a function of applied brake pressure and wheel speed, where:

- $T$ is brake torque, in $\mathrm{N} \cdot \mathrm{m}$.
- $P$ is applied brake pressure, in bar.
- $N$ is wheel speed, in rpm.



## Ports

Input
BrkPrs - Brake pressure
scalar | $N$-by- 1 vector
Brake pressure, in Pa.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

## Dependencies

To enable this port, set the Brake Type parameter, to one of these types:

- Disc
- Drum
- Mapped

AxITrq - Axle torque
scalar | $N$-by- 1 vector

Axle torque, $T_{a}$, about wheel spin axis, in $\mathrm{N} \cdot \mathrm{m}$.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

Vx - Longitudinal velocity
scalar | $N$-by-1 vector
Axle longitudinal velocity, $V_{x}$, along tire-fixed $x$-axis, in $\mathrm{m} / \mathrm{s}$.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.
$\mathbf{V y}$ - Lateral velocity
scalar | $N$-by- 1 vector
Axle lateral velocity, $V_{y}$, along tire-fixed $y$-axis, in $\mathrm{m} / \mathrm{s}$.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

Camber - Inclination angle
scalar | N-by-1 vector
Camber angle, $\gamma$, or inclination angle, $\varepsilon$, in rad.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

YawRate - Tire angular velocity
scalar | $N$-by-1 vector
Tire angular velocity, $r$, about the tire-fixed $z$-axis (yaw rate), in rad/s.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

Prs - Tire inflation pressure
scalar | N-by-1 vector
Tire inflation pressure, $p_{i}$, in Pa.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

Gnd - Ground displacement
scalar | $N$-by-1 vector
Ground displacement along tire-fixed $z$-axis, in m . Positive input produces wheel lift.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

Fext - Axle force applied to tire
scalar | $N$-by- 1 vector

Axle force applied to tire, $F_{\text {ext }}$, along vehicle-fixed $z$-axis (positive input compresses the tire), in N .
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

ScaleFctrs - Scale factor
scalar | $N$-by-1 vector
Scale factor to account for variations in the coefficient of friction.

Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

## Output

Info - Block data
bus

Block data, returned as a bus signal containing these block values.

| Signal | Description | Units |
| :--- | :--- | :--- |
| AxlTrq | Axle torque about wheel-fixed $y$-axis | $\mathrm{N} \cdot \mathrm{m}$ |
| Omega | Wheel angular velocity about wheel-fixed $y$-axis | $\mathrm{rad} / \mathrm{s}$ |
| Fx | Longitudinal vehicle force along tire-fixed $x$-axis | N |
| Fy | Lateral vehicle force along tire-fixed $y$-axis | N |
| Fz | Vertical vehicle force along tire-fixed $z$-axis | N |
| Mx | Overturning moment about tire-fixed $x$-axis | $\mathrm{N} \cdot \mathrm{m}$ |
| My | Rolling resistance torque about tire-fixed $y$-axis | $\mathrm{N} \cdot \mathrm{m}$ |
| Mz | Aligning moment about tire-fixed $z$-axis | $\mathrm{N} \cdot \mathrm{m}$ |
| Vx | Vehicle longitudinal velocity along tire-fixed $x$-axis | $\mathrm{m} / \mathrm{s}$ |
| Vy | Vehicle lateral velocity along tire-fixed $y$-axis | $\mathrm{m} / \mathrm{s}$ |
| Re | Loaded effective radius | m |
| Kappa | Longitudinal slip ratio | NA |
| Alpha | Side slip angle | rad |
| a | Contact patch half length | m |
| b | Contact patch half width | m |
| Gamma | Camber angle | rad |
| psidot | Tire angular velocity about the tire-fixed $z$-axis $($ yaw <br> rate $)$ | $\mathrm{rad} / \mathrm{s}$ |
| BrkTrq | Brake torque about the vehicle-fixed $y$-axis | $\mathrm{N} \cdot \mathrm{m}$ |
| BrkPrs | Brake pressure | Pa |
| z | Axle vertical displacement along tire-fixed $z$-axis | m |
| zdot | Axle vertical velocity along tire-fixed $z$-axis | $\mathrm{m} / \mathrm{s}$ |


| Signal | Description | Units |
| :--- | :--- | :--- |
| Gnd | Ground displacement along tire-fixed $z$-axis (positive <br> input produces wheel lift) | m |
| GndFz | Vertical sidewall force on ground along tire-fixed $z$-axis | N |
| Prs | Tire inflation pressure | Pa |

Omega - Wheel angular velocity
scalar | $N$-by-1 vector
Wheel angular velocity, $\omega$, about wheel-fixed $y$-axis, in rad/s.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

Fx - Longitudinal axle force
scalar | $N$-by-1 vector
Longitudinal force acting on axle, $F_{x}$, along tire-fixed $x$-axis, in N. Positive force acts to move the vehicle forward.

Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

## Fy - Lateral axle force

scalar | $N$-by-1 vector
Lateral force acting on axle, $F_{y}$, along tire-fixed $y$-axis, in N .
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

## Fz - Vertical axle force

scalar | $N$-by-1 vector
Vertical force acting on axle, $F_{z}$, along tire-fixed $z$-axis, in N .
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

Mx - Overturning moment
scalar | $N$-by-1 vector
Longitudinal moment acting on axle, $M_{x}$, about tire-fixed x-axis, in $\mathrm{N} \cdot \mathrm{m}$.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

My - Rolling resistive moment
scalar | $N$-by- 1 vector
Lateral moment acting on axle, $M_{y}$, about tire-fixed $y$-axis, in $\mathrm{N} \cdot \mathrm{m}$.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

Mz - Aligning moment
scalar | $N$-by-1 vector
Vertical moment acting on axle, $M_{z}$, about tire-fixed $z$-axis, in $\mathrm{N} \cdot \mathrm{m}$.
Vector is the number of wheels, $N$, by 1 . If you provide a scalar value, the block assumes that number of wheels is one.

## Parameters

## Block Options

Tire type - Slip type
Nominal slip|Extended slip
Use the Tire Type parameter to select slip type.

| Action | Tire Type Setting |
| :--- | :--- |
| Calculate longitudinal and lateral <br> forces under nominal slip conditions | Nominal slip |
| Calculate longitudinal and lateral <br> forces with additional correction <br> factors for a more accurate response <br> at higher slip ratios | Extended slip |

## Dependencies

Setting Tire type to Extended slip enables these parameters:

| Setting | Parameters Enabled |
| :---: | :---: |
| Extended slip | - Longitudinal squared slip correction factor, $\mathbf{g x 1}$ |
|  | - Longitudinal squared slip friction correction factor, $\mathbf{g x} 2$ |
|  | - Longitudinal linear slip correction factor, gx3 |
|  | - Longitudinal linear slip friction correction factor, gx4 |
|  | - Longitudinal offset correction factor, gx5 |
|  | - Lateral maximum friction correction factor, gy1 |
|  | - Lateral offset correction factor, gy2 |

## Brake type - Brake type

None | Disc | Drum | Mapped
Use the Brake Type parameter to select the brake.

| Action | Brake Type Setting |
| :--- | :--- |
| No braking | None |
| Implement brake that converts the <br> brake cylinder pressure into a <br> braking force | Disc |
| Implement simplex drum brake that <br> converts the applied force and brake <br> geometry into a net braking torque | Drum |
| Implement lookup table that is a <br> function of the wheel speed and <br> applied brake pressure | Mapped |

Rolling Resistance - Rolling resistance torque
None (default) | Pressure and velocity | ISO 28580|Magic Formula|Mapped torque
To calculate the rolling resistance torque, specify one of these Rolling Resistance parameters.

| Setting | Block Implementation |
| :--- | :--- |
| None | None |
| Pressure and velocity | Method in Stepwise Coastdown Methodology for Measuring <br> Tire Rolling Resistance. The rolling resistance is a function of <br> tire pressure, normal force, and velocity. |
| ISO 28580 | Method specified in ISO 28580:2018, Passenger car, truck <br> and bus tyre rolling resistance measurement method <br> Single point test and correlation of measurement results. |
| Magic Formula | Magic formula equations from 4.E70 in Tire and Vehicle <br> Dynamics. The magic formula is an empirical equation based <br> on fitting coefficients. |
| Mapped torque | Lookup table that is a function of the normal force and spin <br> axis longitudinal velocity. |

## Dependencies

Each Rolling Resistance setting enables additional parameters.

| Setting | Parameters Enabled |
| :--- | :--- |
| Pressure and velocity | - Velocity independent force coefficient, aMy |
|  | - Linear velocity force component, bMy |
|  | - Quadratic velocity force component, cMy |
|  | - Tire pressure exponent, alphaMy |
|  | - $\quad$ Normal force exponent, betaMy |


| Setting | Parameters Enabled |
| :--- | :--- |
| ISO 28580 | - |
|  | Parasitic losses force, Fpl |
|  | Rolling resistance constant, Cr |
|  | - Thermal correction factor, Kt |
|  | Measured temperature, Tmeas |
|  | - |
|  | Ambitic losses force, Fpl |
|  | Rolling resistance torque coefficient, QSY |
|  | Longitudinal force rolling resistance coefficient, QSY2 |
|  | Linear rotational speed rolling resistance coefficient, |
|  | QSY3 |
|  | Quartic rotational speed rolling resistance coefficient, |
| QSY4 |  |
|  | Camber squared rolling resistance torque, QSY5 |
|  | Load based camber squared rolling resistance torque, |
|  | QSY6 |
|  | Normal load rolling resistance coefficient, QSY7 |
|  | Pressure load rolling resistance coefficient, QSY8 |
|  | Rolling resistance scaling factor, lam_My |
| Mapped torque | Spin axis velocity breakpoints, VxMy |
|  | Normal force breakpoints, FzMy |
|  | Rolling resistance torque map, MyMap |

## Vertical Motion - Vertical Motion

None (default)|Mapped stiffness and damping
To calculate vertical motion, specify one of these Vertical Motion parameters.

| Setting | Block Implementation |
| :--- | :--- |
| None | Block passes the applied chassis forces directly through to <br> the rolling resistance and longitudinal force calculations. |
| Mapped stiffness and damping | Vertical motion depends on wheel stiffness and damping. <br> Stiffness is a function of tire sidewall displacement and <br> pressure. Damping is a function of tire sidewall velocity and <br> pressure. |

## Dependencies

Setting Vertical Motion to Mapped stiffness and damping enables these parameters:

| Setting | Parameters Enabled |
| :---: | :---: |
| Mapped stiffness and damping | - Wheel mass, MASS <br> - Initial tire displacement, zo <br> - Initial velocity, zdoto <br> - Initial wheel vertical velocity (wheel fixed frame), zdoto <br> - Vertical deflection breakpoints, $\mathbf{z F z}$ <br> - Pressure breakpoints, pFz <br> - Force due to deflection, Fzz <br> - Vertical velocity breakpoints, zdotFz <br> - Force due to velocity, Fzzdot |

## Longitudinal and Lateral

Longitudinal stiffness, Ckappa - Longitudinal stiffness
1e7 (default) | scalar | $N$-by-1 vector
Longitudinal stiffness, $C_{K}$, specified as a scalar or $N$-by-1 vector, in N. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other longitudinal and lateral parameters.
$N$ is the number of wheels and must match the input signal dimensions.
Lateral stiffness per slip angle, Calpha - Lateral stiffness
4.5 e 4 (default) | scalar | $N$-by-1 vector

Lateral stiffness per slip angle, $C_{\alpha}$, specified as a scalar or $N$-by- 1 vector, in $N /$ rad. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other longitudinal and lateral parameters.
$N$ is the number of wheels and must match the input signal dimensions.
Camber stiffness, Cgamma - Camber stiffness
1e3 (default) | scalar | $N$-by-1 vector
Camber stiffness, $C_{\gamma}$, specified as a scalar or $N$-by- 1 vector, in $\mathrm{N} /$ rad. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other longitudinal and lateral parameters.
$N$ is the number of wheels and must match the input signal dimensions.
Maximum friction scaling coefficient, mu0 - Maximum friction scaling coefficient
0.8 (default) | scalar | $N$-by-1 vector

Maximum friction scaling coefficient, $\mu_{0}$, specified as a scalar or $N$-by-1 vector, dimensionless. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other longitudinal and lateral parameters.
$N$ is the number of wheels and must match the input signal dimensions.
Friction reduction factor, As - Friction reduction factor
0.01 (default) | scalar | $N$-by-1 vector

Friction reduction factor, $A_{s}$, specified as a scalar or $N$-by-1 vector, dimensionless. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other longitudinal and lateral parameters.
$N$ is the number of wheels and must match the input signal dimensions.
Longitudinal relaxation length, Lrelx - Longitudinal relaxation length
0.05 (default) | scalar | $N$-by-1 vector

Longitudinal relaxation length, $L_{\text {relx }}$, specified as a scalar or $N$-by- 1 vector, in $m$. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other longitudinal and lateral parameters.
$N$ is the number of wheels and must match the input signal dimensions.
Lateral relaxation length, Lrely - Lateral relaxation length
0.15 (default) | scalar | $N$-by-1 vector

Lateral relaxation length, $L_{\text {rely }}$, specified as a scalar or $N$-by- 1 vector, in $\mathrm{m} / \mathrm{rad}$. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other longitudinal and lateral parameters.
$N$ is the number of wheels and must match the input signal dimensions.

## Extended slip

Lateral offset correction factor, gy2 - Lateral offset correction factor
1.5 (default) | scalar

Lateral offset correction factor, $g_{y 2}$, dimensionless.

## Dependencies

To enable this parameter, set Tire type to Extended slip.
Lateral maximum friction correction factor, gy1 - Lateral maximum friction correction factor

- 1.6 (default) | scalar

Lateral maximum friction correction factor, $g_{y 1}$, dimensionless.

## Dependencies

To enable this parameter, set Tire type to Extended slip.
Longitudinal offset correction factor, $\mathbf{g x 5}$ - Longitudinal offset correction factor
1.5 (default) | scalar

Longitudinal offset correction factor, $g_{\times 5}$, dimensionless.

## Dependencies

To enable this parameter, set Tire type to Extended slip.
Longitudinal linear slip friction correction factor, $\mathbf{g x 4}$ - Longitudinal linear slip friction correction factor

- 0.75 (default) | scalar

Longitudinal linear slip friction correction factor, $g_{x 4}$, dimensionless.

## Dependencies

To enable this parameter, set Tire type to Extended slip.
Longitudinal linear slip correction factor, gx3 - Longitudinal linear slip correction factor 1.63 (default) | scalar

Longitudinal linear slip correction factor, $g_{x 3}$, dimensionless.

## Dependencies

To enable this parameter, set Tire type to Extended slip.
Longitudinal squared slip friction correction factor, gx2 - Longitudinal squared slip friction correction factor

- 0.75 (default) | scalar

Longitudinal squared slip friction correction factor, $g_{x 2}$, dimensionless.

## Dependencies

To enable this parameter, set Tire type to Extended slip.
Longitudinal squared slip correction factor, gx1 - Longitudinal squared slip correction factor 1.14 (default) | scalar

Longitudinal squared slip correction factor, $g_{x 1}$, dimensionless.

## Dependencies

To enable this parameter, set Tire type to Extended slip.

## Rolling

Rotational damping, br - Rotational damping
scalar | $N$-by-1 vector
Rotational damping, specified as a scalar or $N$-by-1 vector, in $N \cdot m \cdot s / r a d$. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other rotational parameters.
$N$ is the number of wheels and must match the input signal dimensions.
Rotational inertia (rolling axis), IYY - Rotational inertia
scalar | $N$-by-1 vector
Rotational inertia (rolling axis), specified as a scalar or $N$-by- 1 vector, in $\mathrm{kg} \cdot \mathrm{m}^{2}$. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other rotational parameters.
$N$ is the number of wheels and must match the input signal dimensions.
Initial rotational velocity, omegao - Initial rotational velocity
scalar | $N$-by-1 vector

Initial rotational velocity, specified as a scalar or $N$-by-1 vector, in rad/s. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other rotational parameters.
$N$ is the number of wheels and must match the input signal dimensions.
Unloaded radius, UNLOADED_RADIUS - Unloaded radius 0.309384029954441 (default) | scalar

Unloaded radius, in $m$.
Pressure and Velocity
Velocity independent force coefficient, aMy - Velocity-independent force coefficient 8e-4 (default) | scalar

Velocity-independent force coefficient, $a$, in $\mathrm{s} / \mathrm{m}$.

## Dependencies

To enable this parameter, set Rolling Resistance to Pressure and velocity.
Linear velocity force component, bMy - Linear velocity force component
0.001 (default) | scalar

Linear velocity force component, $b$, in s/m.

## Dependencies

To enable this parameter, set Rolling Resistance to Pressure and velocity.
Quadratic velocity force component, cMy - Quadratic velocity force component 1.6e-4 (default) | scalar

Quadratic velocity force component, $c$, in $\mathrm{s}^{\wedge} 2 / \mathrm{m}^{\wedge} 2$.

## Dependencies

To enable this parameter, set Rolling Resistance to Pressure and velocity.
Tire pressure exponent, alphaMy - Tire pressure exponent
-0.003 (default) | scalar
Tire pressure exponent, $\alpha$, dimensionless.

## Dependencies

To enable this parameter, set Rolling Resistance to Pressure and velocity.
Normal force exponent, betaMy - Normal force exponent
0.97 (default) | scalar

Normal force exponent, $\beta$, dimensionless.

## Dependencies

To enable this parameter, set Rolling Resistance to Pressure and velocity.

ISO 28580
Parasitic losses force, Fpl — Parasitic force loss
10 (default) | scalar
Parasitic force loss, $F_{p l}$, in N .

## Dependencies

To enable this parameter, set Rolling Resistance to ISO 28580.
Rolling resistance constant, $\mathbf{C r}$ - Rolling resistance constant
1e-3 (default) | scalar
Rolling resistance constant, $C_{r}$, in $\mathrm{N} / \mathrm{kN}$. ISO 28580 specifies the rolling resistance unit as one newton of tractive resistance for every kilonewtons of normal load.

## Dependencies

To enable this parameter, set Rolling Resistance to ISO 28580.
Thermal correction factor, $\mathbf{K t}$ - Thermal correction factor
0.008 (default) | scalar

Thermal correction factor, $K_{t}$, in $1 /$ degC.
Dependencies
To enable this parameter, set Rolling Resistance to ISO 28580.
Measured temperature, Tmeas - Temperature during testing
298.15 (default) | scalar

Measured ambient temperature, $T_{\text {meas }}$, near tire during tire testing, in K .

## Dependencies

To enable this parameter, set Rolling Resistance to ISO 28580.
Ambient temperature, Tamb - Temperature in application environment 298.15 (default) | scalar

Measured ambient temperature, $T_{\text {amb }}$, near tire in application environment, in K. For example, the measured ambient temperature is the ambient temperature near the tire when the vehicle is on the road.

## Dependencies

To enable this parameter, set Rolling Resistance to ISO 28580.
Input ambient temperature - Option to input ambient temperature
off (default) | on
Select to create input port Tamb to input the measured ambient temperature.
The measured ambient temperature, $T_{\text {amb }}$, is the temperature near tire in application environment, in K. For example, the measured ambient temperature is the ambient temperature near the tire when the vehicle is on the road.

## Dependencies

To enable this parameter, set Rolling Resistance to ISO 28580.

## Magic Formula

Rolling resistance torque coefficient, QSY1 - Torque coefficient 0.007 (default) | scalar

Rolling resistance torque coefficient, dimensionless.

## Dependencies

To enable this parameter, set Rolling Resistance to Magic Formula.
Longitudinal force rolling resistance coefficient, QSY2 - Force resistance coefficient 0 (default) | scalar

Longitudinal force rolling resistance coefficient, dimensionless.

## Dependencies

To enable this parameter, set Rolling Resistance to Magic Formula.
Linear rotational speed rolling resistance coefficient, QSY3 - Linear speed coefficient 0.0015 (default) | scalar

Linear rotational speed rolling resistance coefficient, dimensionless.

## Dependencies

To enable this parameter, set Rolling Resistance to Magic Formula.
Quartic rotational speed rolling resistance coefficient, QSY4 - Quartic speed coefficient 8.5e-05 (default) | scalar

Quartic rotational speed rolling resistance coefficient, dimensionless.

## Dependencies

To enable this parameter, set Rolling Resistance to Magic Formula.
Camber squared rolling resistance torque, QSY5 - Camber resistance torque
0 (default) | scalar
Camber squared rolling resistance torque, in $1 / \mathrm{rad}^{\wedge} 2$.

## Dependencies

To enable this parameter, set Rolling Resistance to Magic Formula.
Load based camber squared rolling resistance torque, QSY6 - Load resistance torque 0 (default) | scalar

Load based camber squared rolling resistance torque, in $1 / \mathrm{rad}^{\wedge} 2$.

## Dependencies

To enable this parameter, set Rolling Resistance to Magic Formula.

Normal load rolling resistance coefficient, QSY7 - Normal resistance coefficient 0.9 (default) | scalar

Normal load rolling resistance coefficient, dimensionless.

## Dependencies

To enable this parameter, set Rolling Resistance to Magic Formula.
Pressure load rolling resistance coefficient, QSY8 - Pressure resistance coefficient -0. 4 (default) | scalar

Pressure load rolling resistance coefficient, dimensionless.

## Dependencies

To enable this parameter, set Rolling Resistance to Magic Formula.
Rolling resistance scaling factor, lam_My - Scaling factor
1 (default) | scalar
Rolling resistance scaling factor, dimensionless.

## Dependencies

To enable this parameter, set Rolling Resistance to Magic Formula.

## Mapped

Spin axis velocity breakpoints, VxMy - Spin axis velocity breakpoints
-20:1:20 (default) | vector
Spin axis velocity breakpoints, in m/s.

## Dependencies

To enable this parameter, set Rolling Resistance to Mapped torque.
Normal force breakpoints, FzMy - Normal force breakpoints
0:200:1e4 (default) | vector
Normal force breakpoints, in N.

## Dependencies

To enable this parameter, set Rolling Resistance to Mapped torque.
Rolling resistance torque map, MyMap - Rolling resistance torque map array

Rolling resistance torque versus axle speed and normal force, in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

To enable this parameter, set Rolling Resistance to Mapped torque.

## Aligning

Wheel width, WIDTH - Wheel width
scalar
Wheel width, WIDTH, in m.

## Linear yaw rate resistance, bMz - Linear yaw rate resistance

0 | scalar
Linear yaw rate resistance, $b_{M z}$, in $\mathrm{N} \cdot \mathrm{m} \cdot \mathrm{s} / \mathrm{rad}$.

## Brake

Static friction coefficient, mu_static - Static friction coefficient
0.3 (default) | scalar | $N$-by-1 vector

Static friction coefficient, specified as a scalar or $N$-by-1 vector, dimensionless. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other brake parameters.
$N$ is the number of wheels and must match the input signal dimensions.

## Dependencies

To enable this parameter, set Brake Type to Disc, Drum, or Mapped
Kinetic friction coefficient, mu_kinetic - Kinetic friction
0.2 (default) | scalar | $N$-by-1 vector

Kinematic friction coefficient, specified as a scalar or $N$-by-1 vector, dimensionless. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other brake parameters.
$N$ is the number of wheels and must match the input signal dimensions.

## Dependencies

To enable this parameter, set Brake Type to Disc, Drum, or Mapped

## Disc

Disc brake actuator bore, disc_abore - Bore distance
0.05 (default) | scalar | $N$-by-1 vector

Disc brake actuator bore, specified as a scalar or $N$-by- 1 vector, in $m$. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other brake parameters.
$N$ is the number of wheels and must match the input signal dimensions.

## Dependencies

To enable this parameter, set Brake Type to Disc.
Brake pad mean radius, Rm - Radius
0.177 (default) | scalar | $N$-by-1 vector

Brake pad mean radius, specified as a scalar or $N$-by- 1 vector, in m. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other brake parameters.
$N$ is the number of wheels and must match the input signal dimensions.

## Dependencies

To enable this parameter, set Brake Type to Disc.
Number of brake pads, num_pads - Number of brake pads
2 (default) | scalar $\mid N$-by- 1 vector
Number of brake pads, specified as a scalar or $N$-by- 1 vector, dimensionless. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other brake parameters.
$N$ is the number of wheels and must match the input signal dimensions.

## Dependencies

To enable this parameter, set Brake Type to Disc.

## Drum

## Drum brake actuator bore, disc_abore - Bore distance

0.0508 (default) | scalar | $N$-by-1 vector

Drum brake actuator bore, specified as a scalar or $N$-by-1 vector, in m. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other brake parameters.
$N$ is the number of wheels and must match the input signal dimensions.

## Dependencies

To enable this parameter, set Brake Type to Drum.
Shoe pin to drum center distance, drum_a - Shoe pin to drum center distance 0.123 (default) | scalar

Shoe pin to drum center distance, in $m$.

## Dependencies

To enable this parameter, set Brake Type to Drum.
Shoe pin center to force application point distance, drum_c - Shoe pin center to force application point distance
0.212 (default) | scalar

Shoe pin center to force application point distance, in $m$.

## Dependencies

To enable this parameter, set Brake Type to Drum.

Drum internal radius, drum_r - Drum internal radius
0.15 (default) | scalar

Drum internal radius, in $m$.

## Dependencies

To enable this parameter, set Brake Type to Drum.
Shoe pin to pad start angle, drum_thetal - Shoe pin to pad start angle
0 (default) | scalar
Shoe pin to pad start angle, in deg.

## Dependencies

To enable this parameter, set Brake Type to Drum.
Shoe pin to pad end angle, drum_theta 2 - Shoe pin to pad end angle 126 (default) | scalar

Shoe pin to pad end angle, in deg.

## Dependencies

To enable this parameter, set Brake Type to Drum.
Mapped
Brake actuator pressure breakpoints, brake_p_bpt - Brake actuator pressure breakpoints vector

Brake actuator pressure breakpoints, in bar.

## Dependencies

To enable this parameter, set Brake Type to Mapped.
Wheel speed breakpoints, brake_n_bpt - Wheel speed breakpoints
vector
Wheel speed breakpoints, in rpm.

## Dependencies

To enable this parameter, set Brake Type to Mapped.
Brake torque map, f_brake_t - Lookup table for brake torque array

The lookup table for the brake torque, $f_{\text {brake }}(P, N)$, is a function of applied brake pressure and wheel speed, where:

- $\quad T$ is brake torque, in $\mathrm{N} \cdot \mathrm{m}$.
- $P$ is applied brake pressure, in bar.
- $N$ is wheel speed, in rpm.



## Dependencies

To enable this parameter, set Brake Type to Mapped.

## Vertical

Wheel mass, $\mathbf{m}$ - Wheel mass
9.46491996974568 (default) | scalar | $N$-by-1 vector

Wheel mass, specified as a scalar or $N$-by- 1 vector, in kg . If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other vertical parameters.
$N$ is the number of wheels and must match the input signal dimensions.

## Dependencies

To enable this parameter, set Vertical Motion to Mapped stiffness and damping.
Initial tire deflection, zo - Initial tire deflection
0 (default) | scalar | $N$-by-1 vector
Initial tire displacement, specified as a scalar or $N$-by-1 vector, in $m$. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other vertical parameters.
$N$ is the number of wheels and must match the input signal dimensions.

## Dependencies

To enable this parameter, set Vertical Motion to Mapped stiffness and damping.
Initial wheel vertical velocity (wheel fixed frame), zdoto - Initial wheel vertical velocity
0 (default) | scalar | $N$-by-1 vector
Initial wheel vertical velocity, specified as a scalar or $N$-by- 1 vector, in m/s. If you specify a scalar, the block uses that value for all wheels. If you specify a vector, you must specify vectors for the other vertical parameters.
$N$ is the number of wheels and must match the input signal dimensions.

## Dependencies

To enable this parameter, set Vertical Motion to Mapped stiffness and damping.

## Gravitational acceleration, GRAVITY - Gravitational acceleration

## -9.81 (default) | scalar

Gravitational acceleration, in $\mathrm{m} / \mathrm{s}^{\wedge} 2$.

## Dependencies

To enable this parameter, set Vertical Motion to Mapped stiffness and damping.

## Mapped Stiffness and Damping

Vertical deflection breakpoints, zFz - Vertical deflection breakpoints
[0 . 01 .1] (default) | vector
Vector of sidewall deflection breakpoints corresponding to the force table, in $m$.

## Dependencies

To enable this parameter, set Vertical Motion to Mapped stiffness and damping.
Pressure breakpoints, pFz - Pressure breakpoints
[10000 1000000] (default) | vector
Vector of pressure data points corresponding to the force table, in Pa.

## Dependencies

To enable this parameter, set Vertical Motion to Mapped stiffness and damping.
Force due to deflection, Fzz - Force due to deflection
[0 le3 1e4; 0 le4 1e5] (default)|vector
Force due to sidewall deflection and pressure along wheel-fixed $z$-axis, in N .

## Dependencies

To enable this parameter, set Vertical Motion to Mapped stiffness and damping.
Vertical velocity breakpoints, zdotFz - Vertical velocity breakpoints
[-20 0 20] (default)|scalar
Vector of sidewall velocity breakpoints corresponding to the force due to velocity table, in m .

## Dependencies

To enable this parameter, set Vertical Motion to Mapped stiffness and damping.
Force due to velocity, Fzzdot - Force due to velocity
[500 0-500;250 0-250] (default) | array
Force due to sidewall velocity and pressure along wheel-fixed $z$-axis, in N .

## Dependencies

To enable this parameter, set Vertical Motion to Mapped stiffness and damping.

## Simulation Setup

Maximum normal force, FZMAX - Maximum normal force
10000 (default) | scalar
Maximum normal force, in N. Used with all vertical force calculations.
Minimum normal force, FZMIN - Minimum normal force
0 (default) | scalar
Minimum normal force, in N. Used with all vertical force calculations.
Maximum pressure, PRESMAX - Maximum pressure
1003118 (default) | scalar
Maximum pressure, PRESMAX, in Pa.
Minimum pressure, PRESMIN - Minimum pressure
9982 (default) | scalar
Minimum pressure, PRESMIN, in Pa.
Max allowable slip ratio (absolute), KPUMAX - Max allowable slip ratio
0.999 (default) | scalar

Max allowable slip ratio (absolute), KPUMAX, dimensionless.
Minimum allowable slip ratio (absolute), KPUMIN - Minimum allowable slip ratio -0.999 (default) | scalar

Minimum allowable slip ratio (absolute), KPUMIN, dimensionless.
Max allowable slip angle (absolute), ALPMAX - Max allowable slip angle 1.5708 (default) | scalar

Max allowable slip angle (absolute), ALPMAX, in rad.
Minimum allowable slip angle (absolute), ALPMIN - Minimum allowable slip angle - 1.5708 (default) | scalar

Minimum allowable slip angle (absolute), ALPMIN, in rad.
Maximum allowable camber angle, CAMMAX - Maximum allowable camber angle 0.173 | scalar

Maximum allowable camber angle CAMMAX, in rad.
Minimum allowable camber angle, CAMMIN - Minimum allowable camber angle -0. 173 | scalar

Minimum allowable camber angle, CAMMIN, in rad.
Minimum ambient temperature, TMIN - Minimum ambient temperature 0 (default) | scalar

Minimum ambient temperature, $T_{\text {MIN }}$, in K .

## Dependencies

To enable this parameter, set Rolling Resistance to ISO 28580.
Maximum ambient temperature, TMAX - Maximum ambient temperature 400 (default) | scalar

Maximum ambient temperature, $T_{M A X}$, in K .
Dependencies
To enable this parameter, set Rolling Resistance to ISO 28580.

## Version History

## Introduced in R2023a

## References

[1] Bhoraskar, A. and P. Sakthivel. "A Review and a Comparison of Dugoff and Modified Dugoff Formula with Magic Formula." 2017 International Conference on Nascent Technologies in Engineering (ICNTE)(2017): 1-4. https://doi.org/10.1109/ICNTE.2017.7947898.
[2] Highway Tire Committee. Stepwise Coastdown Methodology for Measuring Tire Rolling Resistance. Standard J2452_199906. Warrendale, PA: SAE International, June 1999.
[3] International Organization for Standardization. Passenger car, truck and bus tyre rolling resistance measurement method - Single point test and correlation of measurement results. ISO 28580: 2018. https://www.iso.org/standard/67531.html.
[4] Pacejka, H. B. Tire and Vehicle Dynamics, 3rd ed. Oxford, UK: SAE and Butterworth-Heinemann, 2012.

## Extended Capabilities

C/C++ Code Generation
Generate C and C++ code using Simulink ${ }^{\circledR}$ Coder ${ }^{\mathrm{TM}}$.

## See Also

Combined Slip Wheel 2DOF | Combined Slip Wheel 2DOF CPI | Combined Slip Wheel 2DOF STI |
Longitudinal Wheel | Fiala Wheel 2DOF
Topics
"Coordinate Systems in Vehicle Dynamics Blockset" Propulsion Blocks

## Simple Engine

Simplified engine model using lookup tables


## Libraries:

Powertrain Blockset / Propulsion / Combustion Engines
Vehicle Dynamics Blockset / Powertrain / Propulsion

## Description

The Simple Engine block implements a simplified engine model using a maximum torque vs engine speed table, two scalar fuel mass properties, and one scalar engine efficiency parameter to estimate engine torque and fuel flow. You can use the block for:

- Hardware-in-the-loop (HIL) engine control design
- Vehicle-level fuel economy and performance simulations


## Ports

## Input

TrqCmd - Commanded torque
scalar
Torque, in $\mathrm{N} \cdot \mathrm{m}$.
EngSpd - Engine speed
scalar
Engine speed, in rpm.

## Output

Info - Bus signal
bus
Bus signal containing these block calculations.

| Signal | Description | Units |
| :--- | :--- | :--- |
| IntkGasMassFlw (zeroed out intentionally) | Engine air mass flow output | $\mathrm{kg} / \mathrm{s}$ |
| NrmlzdAirChrg (zeroed out intentionally) | Normalized engine cylinder air mass | $\mathrm{N} / \mathrm{A}$ |
| Afr (zeroed out intentionally) | Air-fuel ratio (AFR) | $\mathrm{N} / \mathrm{A}$ |
| FuelMassFlw | Engine fuel flow output | $\mathrm{kg} / \mathrm{s}$ |
| FuelVolFlw | Volumetric fuel flow | $\mathrm{m}^{3} / \mathrm{s}$ |
| ExhManGasTemp (zeroed out intentionally) | Engine exhaust gas temperature | K |


| Signal |  |  | Description | Units |
| :---: | :---: | :---: | :---: | :---: |
| EngTrq |  |  | Engine torque output | $\mathrm{N} \cdot \mathrm{m}$ |
| EngSpd |  |  | Engine speed | rpm |
| CrkAng (zeroed out intentionally) |  |  | Engine crankshaft absolute angle $\int_{0}^{(360) C p s} E n g S p d \frac{180}{30} d \theta$ <br> where Cps is crankshaft revolutions per power stroke. | degrees crank angle |
| Bsfc |  |  | Engine brake-specific fuel consumption (BSFC) | $\mathrm{g} / \mathrm{kWh}$ |
| EoHC (zeroed out intentionally) |  |  | Engine out hydrocarbon emission mass flow | kg/s |
| EoC0 (zeroed out intentionally) |  |  | Engine out carbon monoxide emission mass flow rate | kg/s |
| EoN0x (zeroed out intentionally) |  |  | Engine out nitric oxide and nitrogen dioxide emissions mass flow | kg/s |
| EoC02 (zeroed out intentionally) |  |  | Engine out carbon dioxide emission mass flow | kg/s |
| EoPM (zeroed out intentionally) |  |  | Engine out particulate matter emission mass flow | kg/s |
| PwrInfo | PwrTrnsfrd | PwrCrkshft | Crankshaft power | W |
|  | PwrNotTrnsfrd | PwrFuel | Fuel input power | W |
|  |  | PwrLoss | Power loss | W |
|  | PwrStored |  | Not used |  |

EngTrq - Engine brake torque
scalar
Engine brake torque, in $\mathrm{N} \cdot \mathrm{m}$.

## Parameters

Engine maximum torque, f_tqmax - Breakpoints

```
[75.679776480773256 75.679776480773256 97.173658538143172 116.84042599160529
152.21029882684542 175 174.99889520597083 174.99996520122858 175 175 175 175
175 175 175 175] (default)
```

Breakpoints, in $\mathrm{N} \cdot \mathrm{m}$.
Breakpoints for engine speed input, f_tqmax_n_bpt - Breakpoints

Breakpoints, in rpm.
Fuel lower heating value, Lhv - Heating value
4. 6E+7 (default)

Fuel lower heating value, in J/kg.
Fuel specific gravity, Sg - Specific gravity
0.745 (default)

Specific gravity of fuel, dimensionless.
Average brake specific fuel consumption, BsfcAvg - Average brake specific fuel consumption 350 (default)

Average brake specific fuel consumption, in $\mathrm{g} / \mathrm{kwh}$.

## Version History

Introduced in R2021b

## Extended Capabilities

C/C++ Code Generation
Generate C and $\mathrm{C}++$ code using Simulink ${ }^{\circledR}$ Coder $^{\text {™ }}$.

## Mapped Motor

Mapped motor and drive electronics operating in torque-control mode


## Libraries:

Powertrain Blockset / Propulsion / Electric Motors and Inverters
Vehicle Dynamics Blockset / Powertrain / Propulsion

## Description

The Mapped Motor block implements a mapped motor and drive electronics operating in torquecontrol mode. The output torque tracks the torque reference demand and includes a motor-response and drive-response time constant. Use the block for fast system-level simulations when you do not know detailed motor parameters, for example, for motor power and torque tradeoff studies. The block assumes that the speed fluctuations due to mechanical load do not affect the motor torque tracking.

You can specify:

- Port configuration - Input torque or speed.
- Electrical torque range - Torque speed envelope or maximum motor power and torque.
- Electrical loss - Single operating point, measured efficiency, or measured loss. If you have ModelBased Calibration Toolbox ${ }^{\mathrm{TM}}$, you can virtually calibrate the measured loss tables.


## Electrical Torque

To specify the range of torque and speed that the block allows, on the Electrical Torque tab, for Parametrized by, select one of these options.

| Setting | Block Implementation |
| :--- | :--- |
| Tabulated torque-speed <br> envelope | Range specified as a set of speed data points and corresponding <br> maximum torque values. |
| Maximum torque and power | Range specified with maximum torque and maximum power. |

For either method, the block implements an envelope similar to this.


## Electrical Losses

To specify the electrical losses, on the Electrical Losses tab, for Parameterize losses by, select one of these options.

| Setting | Block Implementation |
| :---: | :---: |
| Single efficiency measurement | Sum of these terms, measured at a single measurement point: <br> - Fixed losses independent of torque and speed, $P_{0}$. Use $P_{0}$ to account for fixed converter losses. <br> - A torque-dependent electrical loss $k \tau^{2}$, where $k$ is a constant and $\tau$ is the torque. Represents ohmic losses in the copper windings. <br> - A speed-dependent electrical loss $k_{\mathrm{w}} \omega^{2}$, where $k_{\mathrm{w}}$ is a constant and $\omega$ is the speed. Represents iron losses due to eddy currents. |
| Tabulated loss data | Loss lookup table that is a function of motor speeds and load torques. <br> If you have Model-Based Calibration Toolbox, click Calibrate Maps to virtually calibrate the 2D lookup tables using measured data. |
| Tabulated loss data with temperature | Loss lookup table that is a function of motor speeds, load torques, and operating temperature. <br> If you have Model-Based Calibration Toolbox, click Calibrate Maps to virtually calibrate the 3D lookup tables using measured data. |
| Tabulated efficiency data | 2D efficiency lookup table that is a function of motor speeds and load torques: <br> - Converts the efficiency values you provide into losses and uses the tabulated losses for simulation. <br> - Ignores efficiency values you provide for zero speed or zero torque. Losses are assumed zero when either torque or speed is zero. <br> - Uses linear interpolation to determine losses. Provide tabulated data for low speeds and low torques, as required, to get the desired level of accuracy for lower power conditions. <br> - Does not extrapolate loss values for speed and torque magnitudes that exceed the range of the table. |


| Setting | Block Implementation |
| :--- | :--- |
| Tabulated efficiency data <br> with temperature | 3D efficiency lookup table that is a function of motor speeds, load <br> torques, and operating temperature: |
|  | -Converts the efficiency values you provide into losses and uses <br> the tabulated losses for simulation. <br> Ignores efficiency values you provide for zero speed or zero <br> torque. Losses are assumed zero when either torque or speed <br> is zero. <br>  <br>  <br>  <br>  <br>  <br> - Uses linear interpolation to determine losses. Provide <br> tabulated data for low speeds and low torques, as required, to <br> get the desired level of accuracy for lower power conditions. <br> Does not extrapolate loss values for speed, torque, or <br> temperature magnitudes that exceed the range of the table. |

For best practice, use Tabulated loss data instead of Tabulated efficiency data:

- Efficiency becomes ill defined for zero speed or zero torque.
- You can account for fixed losses that are still present for zero speed or torque.

Note Due to system losses, the motor can draw a current when the motor torque is zero.

## Virtual Calibration

If you have Model-Based Calibration Toolbox, you can virtually calibrate the measured loss lookup tables.

1 On the Electrical Losses tab, set Parameterize losses by to either:

- Tabulated loss data
- Tabulated loss data with temperature


## 2 Click Calibrate Maps.

The dialog box steps through these tasks.

| Task | Description |  |
| :---: | :---: | :---: |
| Import Loss Data | Import this loss data from a file. For example, open <matlabroot>/toolbox/ autoblks/autoblksshared/mbctemplates/MappedMotorDataset.xlsx. <br> For more information, see "Using Data" (Model-Based Calibration Toolbox). |  |
|  | Parameterize losses by | Required Data |
|  | Tabulated loss data | - Motor speed, rad/s - - Potor torquer loss, W |
|  | Tabulated loss data with temperature | - Motor speed, rad/s <br> - Motor torque, $\mathrm{N} \cdot \mathrm{m}$ <br> - Motor temperature, K <br> - Power loss, W |
|  | Collect motor data at steady-state operating conditions. Data should cover the motor speed, torque, and temperature operating range. <br> To filter or edit the data, select Edit in Application. The Model-Based Calibration Toolbox Data Editor opens. |  |
| Generate Response Models | Model-Based Calibration Toolbox uses test plans to fit data to Gaussian process models (GPMs). <br> To assess or adjust the response model fit, select Edit in Application. The Model-Based Calibration Toolbox Model Browser opens. For more information, see "Model Assessment" (Model-Based Calibration Toolbox). |  |
| Generate Calibration | Model-Based Calibration Toolbox calibrates the response models and generates calibrated tables. <br> To assess or adjust the calibration, select Edit in Application. The ModelBased Calibration Toolbox CAGE Browser opens. For more information, see "Calibration Lookup Tables" (Model-Based Calibration Toolbox). |  |


| Task | Description |  |
| :---: | :---: | :---: |
| Update block parameters | Update these parameters with the calibration. |  |
|  | Parameterize losses by | Parameters |
|  | Tabulated loss data | - Vector of speeds(w) for tabulated losses, w_eff_bp <br> - Vector of torques (T) for tabulated losses, T_eff_bp <br> - Corresponding losses, losses_table |
|  | Tabulated loss data with temperature | - Vector of speeds(w) for tabulated losses, w_eff_bp <br> - Vector of torques ( $\mathbf{T}$ ) for tabulated losses, T_eff_bp <br> Vector of temperatures for tabulated losses, Temp_eff_bp <br> - Corresponding losses, losses_table_3d |

## Battery Current

The block calculates the battery current using the mechanical power, power loss, and battery voltage. Positive current indicates battery discharge. Negative current indicates battery charge.

$$
\text { BattAmp }=\frac{\text { MechPwr }+ \text { PwrLoss }}{\text { BattVolt }}
$$

The equation uses these variables.

## BattVolt Battery voltage

MechPwr Mechanical power
PwrLoss Power loss
BattCurr Battery current

## Power Accounting

For the power accounting, the block implements these equations.

| Bus Signal |  |  | Description | Variable | Equations |
| :---: | :---: | :---: | :---: | :---: | :---: |
| PwrIn fo | PwrTrnsfrd <br> - Positive signals indicate power flow into the block. <br> - Negative signals indicate power flow out of the block. | PwrMtr | Mechanical power | $P_{\text {mot }}$ | $P_{\text {mot }}=\omega_{m} T_{e}$ |
|  |  | PwrBus | Electrical power | $P_{\text {bus }}$ | $P_{\text {bus }}=P_{\text {mot }}+P_{\text {loss }}$ |
|  | PwrNotTrnsfrd <br> - Negative signals indicate power loss. | PwrLoss | Motor power loss | $P_{\text {loss }}$ | ${ }_{\text {stored }}=\omega_{m} \dot{\omega}_{m} J$ |


| Bus Signal |  | Description | Variable | Equations |
| :--- | :--- | :--- | :--- | :--- | :--- |
| PwrStored <br> -Positive signals indicate <br> power gain. | PwrStor <br> edShft | Motor power <br> stored | $P_{\text {str }}$ | $P_{\text {loss }}=\quad-\left(P_{\text {mot }}\right.$ <br> $\left.+P_{\text {loss }}-\quad P_{\text {stored }}\right)$ |

The equations use these variables.

| $T_{e}$ | Motor output shaft torque |
| :--- | :--- |
| $\omega$ | Motor shaft speed |
| $J$ | Motor inertia |

## Ports

Input
BattVolt - Battery voltage
scalar
Battery voltage, BattVolt, in V.
TrqCmd - Commanded motor torque
scalar
Commanded motor torque, $\mathrm{Trq}_{\text {cmd }}$, in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

To create this input port, for the Port configuration, select Torque.
MtrSpd - Motor output shaft speed
scalar
Motor shaft speed, $M t r_{\text {spd }}$, in rad/s.

## Dependencies

To create this input port, for the Port configuration, select Speed.

## Output

Info - Bus signal
bus
The bus signal contains these block calculations.

| Signal |  | Description | Units |
| :--- | :--- | :--- | :--- |
| MechPwr |  | Mechanical power | W |
| PwrLoss | Internal inverter and motor power loss | $\mathrm{N} \cdot \mathrm{m}$ |  |
| PwrInfo | PwrTrnsfrd | PwrMtr | Mechanical power |
|  | PwrBus | Electrical power | W |


| Signal |  | Description | Units |  |
| :--- | :--- | :--- | :--- | :--- |
|  | PwrNotTrnsfrd | PwrLoss | Motor power loss | W |
|  | PwrStored | PwrStored <br> Shft | Motor power stored | W |

## BattCurr - Battery current scalar

Battery current draw or demand, $I_{\text {batt, }}$ in A.
MtrTrq - Motor torque
scalar
Motor output shaft torque, $\mathrm{Mtr}_{\text {trq, }}$, in $\mathrm{N} \cdot \mathrm{m}$.
MtrSpd - Motor shaft speed
scalar
Motor shaft speed, $M t r_{s p d}$, in rad/s.

## Dependencies

To create this output port, for the Port configuration, select Torque.

## Parameters

## Block Options

Port configuration - Select port configuration
Torque (default) | Speed
This table summarizes the port configurations.

| Port Configuration | Creates Ports |
| :--- | :--- |
| Torque | Outpost MtrSpd |
| Speed | Input Mt rSpd |

Calibrate Maps - Calibrate tables with measured data selection

If you have Model-Based Calibration Toolbox, you can virtually calibrate the measured loss lookup tables.

1 On the Electrical Losses tab, set Parameterize losses by to either:

- Tabulated loss data
- Tabulated loss data with temperature


## 2 Click Calibrate Maps.

The dialog box steps through these tasks.

| Task | Description |  |
| :---: | :---: | :---: |
| Import Loss Data | Import this loss data from a file. For example, open <matlabroot>/toolbox/ autoblks/autoblksshared/mbctemplates/MappedMotorDataset.xlsx. <br> For more information, see "Using Data" (Model-Based Calibration Toolbox). |  |
|  | Parameterize losses by | Required Data |
|  | Tabulated loss data | - Motor speed, rad/s - - Potor torquer loss, W |
|  | Tabulated loss data with temperature | - Motor speed, rad/s <br> - Motor torque, $\mathrm{N} \cdot \mathrm{m}$ <br> - Motor temperature, K <br> - Power loss, W |
|  | Collect motor data at steady-state operating conditions. Data should cover the motor speed, torque, and temperature operating range. <br> To filter or edit the data, select Edit in Application. The Model-Based Calibration Toolbox Data Editor opens. |  |
| Generate Response Models | Model-Based Calibration Toolbox uses test plans to fit data to Gaussian process models (GPMs). <br> To assess or adjust the response model fit, select Edit in Application. The Model-Based Calibration Toolbox Model Browser opens. For more information, see "Model Assessment" (Model-Based Calibration Toolbox). |  |
| Generate Calibration | Model-Based Calibration Toolbox calibrates the response models and generates calibrated tables. <br> To assess or adjust the calibration, select Edit in Application. The ModelBased Calibration Toolbox CAGE Browser opens. For more information, see "Calibration Lookup Tables" (Model-Based Calibration Toolbox). |  |


| Task | Description |  |
| :---: | :---: | :---: |
| Update block parameters | Update these parameters with the calibration. |  |
|  | Parameterize losses by | Parameters |
|  | Tabulated loss data | - Vector of speeds(w) for tabulated losses, w_eff_bp <br> - Vector of torques (T) for tabulated losses, T_eff_bp <br> - Corresponding losses, losses_table |
|  | ```Tabulated loss data with temperature``` | - Vector of speeds(w) for tabulated losses, w_eff_bp <br> - Vector of torques (T) for tabulated losses, T_eff_bp <br> - Vector of temperatures for tabulated losses, Temp_eff_bp <br> - Corresponding losses, losses_table_3d |

## Electrical Torque

Parameterized by - Select type
Tabulated torque-speed envelope (default)|Maximum torque and power

| Setting | Block Implementation |
| :--- | :--- |
| Tabulated torque-speed <br> envelope | Range specified as a set of speed data points and corresponding <br> maximum torque values. |
| Maximum torque and power | Range specified with maximum torque and maximum power. |

For either method, the block implements an envelope similar to this.


Vector of rotational speeds, w_t - Rotational speeds

## [0 375750 800] (default) | vector

Rotational speeds for permissible steady-state operation, in rad/s. To avoid poor performance due to an infinite slope in the torque-speed curve, specify a vector of rotational speeds that does not contain duplicate consecutive values.

## Dependencies

To create this parameter, for the Parameterized by parameter, select Tabulated torque-speed envelope.

Vector of maximum torque values, $\mathbf{T}_{-} \mathbf{t}$ - Torque
[0.09 0.08 0.07 0] (default)|vector
Maximum torque values for permissible steady state, in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

To create this parameter, for the Parameterized by parameter, select Tabulated torque-speed envelope.

Maximum torque, torque_max - Torque
. 1 (default) | scalar
The maximum permissible motor torque, in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

To create this parameter, for the Parameterized by parameter, select Maximum torque and power.

Maximum power, power_max - Power
30 (default) | scalar
The maximum permissible motor power, in W .

## Dependencies

To create this parameter, for the Parameterized by parameter, select Maximum torque and power.

Torque control time constant, Tc - Time constant
0.02 (default) | scalar

Time constant with which the motor driver tracks a torque demand, in s.

## Electrical Losses

Parameterize losses by - Select type
Single efficiency measurement (default)|Tabulated loss data|Tabulated efficiency data

| Setting | Block Implementation |
| :---: | :---: |
| Single efficiency measurement | Sum of these terms, measured at a single measurement point: <br> - Fixed losses independent of torque and speed, $P_{0}$. Use $P_{0}$ to account for fixed converter losses. <br> - A torque-dependent electrical loss $k \tau^{2}$, where $k$ is a constant and $\tau$ is the torque. Represents ohmic losses in the copper windings. <br> - A speed-dependent electrical loss $k_{\mathrm{w}} \omega^{2}$, where $k_{\mathrm{w}}$ is a constant and $\omega$ is the speed. Represents iron losses due to eddy currents. |
| Tabulated loss data | Loss lookup table that is a function of motor speeds and load torques. <br> If you have Model-Based Calibration Toolbox, click Calibrate Maps to virtually calibrate the 2D lookup tables using measured data. |
| Tabulated loss data with temperature | Loss lookup table that is a function of motor speeds, load torques, and operating temperature. <br> If you have Model-Based Calibration Toolbox, click Calibrate Maps to virtually calibrate the 3D lookup tables using measured data. |
| Tabulated efficiency data | 2D efficiency lookup table that is a function of motor speeds and load torques: <br> - Converts the efficiency values you provide into losses and uses the tabulated losses for simulation. <br> - Ignores efficiency values you provide for zero speed or zero torque. Losses are assumed zero when either torque or speed is zero. <br> - Uses linear interpolation to determine losses. Provide tabulated data for low speeds and low torques, as required, to get the desired level of accuracy for lower power conditions. <br> - Does not extrapolate loss values for speed and torque magnitudes that exceed the range of the table. |


| Setting | Block Implementation |
| :--- | :--- |
| Tabulated efficiency data <br> with temperature | 3D efficiency lookup table that is a function of motor speeds, load <br> torques, and operating temperature: <br> - <br> Converts the efficiency values you provide into losses and uses <br> the tabulated losses for simulation. |
|  | - Ignores efficiency values you provide for zero speed or zero <br> torque. Losses are assumed zero when either torque or speed <br> is zero. |
|  | Uses linear interpolation to determine losses. Provide <br> tabulated data for low speeds and low torques, as required, to <br> get the desired level of accuracy for lower power conditions. <br> Does not extrapolate loss values for speed, torque, or <br> temperature magnitudes that exceed the range of the table. |

For best practice, use Tabulated loss data instead of Tabulated efficiency data:

- Efficiency becomes ill defined for zero speed or zero torque.
- You can account for fixed losses that are still present for zero speed or torque.

Note Due to system losses, the motor can draw a current when the motor torque is zero.

## Motor and drive overall efficiency, eff - Efficiency

100 (default) | scalar
The block defines overall efficiency as:

$$
\eta=100 \frac{\tau_{0} \omega_{0}}{\tau_{0} \omega_{0}+P_{0}+k \tau_{0}^{2}+k_{w} \omega_{0}^{2}}
$$

The equation uses these variables.
$\tau_{0} \quad$ Torque at which efficiency is measured
$\omega_{0} \quad$ Speed at which efficiency is measured
$P_{0} \quad$ Fixed losses independent of torque or speed
$k \tau_{0}^{2} \quad$ Torque-dependent electrical losses
$k_{w} \omega^{2} \quad$ Speed-dependent iron losses
At initialization, the block solves the efficiency equation for $k$. The block neglects losses associated with the rotor damping.

## Dependencies

To create this parameter, for the Parameterize losses by parameter, select Single efficiency measurement.

## Speed at which efficiency is measured, w_eff - Speed

375 (default) | scalar
Speed at which efficiency is measured, in rad/s.

## Dependencies

To create this parameter, for the Parameterize losses by parameter, select Single efficiency measurement.

Torque at which efficiency is measured, T_eff - Torque
0.08 (default)| scalar

Torque at which efficiency is measured, in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

To create this parameter, for the Parameterize losses by parameter, select Single efficiency measurement.

Iron losses, Piron - Power
0 (default) | scalar
Iron losses at the speed and torque at which efficiency is defined, in W.
Dependencies
To create this parameter, for the Parameterize losses by parameter, select Single efficiency measurement.

Fixed losses independent of torque and speed, Pbase - Power
0 (default) | scalar
Fixed electrical loss associated with the driver when the motor current and torque are zero, in W.

## Dependencies

To create this parameter, for the Parameterize losses by parameter, select Single efficiency measurement.

Vector of speeds (w) for tabulated losses, w_eff_bp - Breakpoints
[-8000-4000 04000 8000] (default)| 1-by-M vector
Speed breakpoints for lookup table when calculating losses, in rad/s. Array dimensions are 1 by the number of speed breakpoints, M.

## Dependencies

To create this parameter, for the Parameterize losses by parameter, select one of these:

- Tabulated loss data
- Tabulated loss data with temperature
- Tabulated efficiency data
- Tabulated efficiency data with temperature

Vector of torques (T) for tabulated losses, T_eff_bp - Breakpoints
[0 0.03 0.06 0.09] (default)| 1-by-N vector
Torque breakpoints for lookup table when calculating losses, in $N \cdot m$. Array dimensions are 1 by the number of torque breakpoints, N .

## Dependencies

To create this parameter, for the Parameterize losses by parameter, select one of these:

- Tabulated loss data
- Tabulated loss data with temperature
- Tabulated efficiency data
- Tabulated efficiency data with temperature

Vector of temperatures for tabulated losses, Temp_eff_bp - Breakpoints
[233.15 293.15 373.15] (default)| 1-by-L vector
Temperature breakpoints for lookup table when calculating losses, in K. Array dimensions are 1 by the number of temperature breakpoints, $L$.

Dependencies
To create this parameter, for the Parameterize losses by parameter, select one of these:

- Tabulated loss data with temperature
- Tabulated efficiency data with temperature

Corresponding losses, losses_table - 2D lookup table
M-by-N matrix
Array of values for electrical losses as a function of speed and torque, in W. Each value specifies the losses for a specific combination of speed and torque. The array dimensions must match the speed, M, and torque, N , breakpoint vector dimensions.

## Dependencies

To create this parameter, for the Parameterize losses by parameter, select Tabulated loss data.

## Corresponding losses, losses_table_3d - 3D lookup table

M-by-N-by-L array
Array of values for electrical losses as a function of speed, torque, and temperature, in W. Each value specifies the losses for a specific combination of speed, torque, and temperature. The array dimensions must match the speed, $M$, torque, $N$, and temperature, $L$, breakpoint vector dimensions.

## Dependencies

To create this parameter, for the Parameterize losses by parameter, select Tabulated loss data with temperature.

## Corresponding efficiency, efficiency_table - 2D lookup table

M-by-N matrix
Array of efficiency as a function of speed and torque, in \%. Each value specifies the losses for a specific combination of speed and torque. The array dimensions must match the speed, $M$, and torque, N , breakpoint vector dimensions.

The block ignores efficiency values for zero speed or zero torque. Losses are zero when either torque or speed is zero. The block uses linear interpolation.

To get the desired level of accuracy for lower power conditions, you can provide tabulated data for low speeds and low torques.

## Dependencies

To create this parameter, for the Parameterize losses by parameter, select Tabulated efficiency data.

Corresponding efficiency, efficiency_table_3d - 3D lookup table
M-by-N-by-L array
Array of efficiency as a function of speed and torque, in \%. Each value specifies the losses for a specific combination of speed and torque. The array dimensions must match the speed, M , torque, N , and temperature, $L$, breakpoint vector dimensions.

The block ignores efficiency values for zero speed or zero torque. Losses are zero when either torque or speed is zero. The block uses linear interpolation.

To get the desired level of accuracy for lower power conditions, you can provide tabulated data for low speeds and low torques.

## Dependencies

To create this parameter, for the Parameterize losses by parameter, select Tabulated efficiency data.

Mechanical
Rotor inertia, J - Inertia
5e-6 (default) | scalar
Rotor resistance to change in motor motion, in $\mathrm{kg}^{*} \mathrm{~m}^{2}$. The value can be zero.

## Dependencies

To create this parameter, for the Port configuration parameter, select Torque.
Rotor damping, b - Damping
le-5 (default) | scalar
Rotor damping, in $\mathrm{N} \cdot \mathrm{m} /(\mathrm{rad} / \mathrm{s})$. The value can be zero.

## Dependencies

To create this parameter, for the Port configuration parameter, select Torque.
Initial rotor speed, omega_o - Speed
0 (default) | scalar
Rotor speed at the start of the simulation, in rad/s.

## Dependencies

To create this parameter, for the Port configuration parameter, select Torque.

## Version History

Introduced in R2017a

## Extended Capabilities

C/C++ Code Generation
Generate C and C++ code using Simulink ${ }^{\circledR}$ Coder $^{\mathrm{TM}}$.

## See Also

Open Differential

## Mapped CI Engine

Compression-ignition engine model using lookup tables


## Libraries:

Powertrain Blockset / Propulsion / Combustion Engines
Vehicle Dynamics Blockset / Powertrain / Propulsion

## Description

The Mapped CI Engine block implements a mapped compression-ignition (CI) engine model using power, air mass flow, fuel flow, exhaust temperature, efficiency, and emission performance lookup tables. You can use the block for:

- Hardware-in-the-loop (HIL) engine control design
- Vehicle-level fuel economy and performance simulations

The lookup tables, developed with the Model-Based Calibration Toolbox, are functions of injected fuel mass, $F$, engine torque, $T$, engine speed, $N$, and engine temperature, $T e m p_{\text {Eng }}$.

| Input Command Setting | Input Engine Temperature <br> Parameter Setting | Lookup Tables |
| :--- | :--- | :--- |
| Fuel mass | off | $f(F, N)$ |
|  | on | $f\left(F, N, T e m p_{\text {Eng }}\right)$ |
| Torque | off | $f(T, N)$ |
|  | on | $f\left(T, N, T e m p_{\text {Eng }}\right)$ |

The block enables you to specify lookup tables for these engine characteristics:

- Power
- Air
- Fuel
- Temperature
- Efficiency
- Hydrocarbon (HC) emissions
- Carbon monoxide (CO) emissions
- Nitric oxide and nitrogen dioxide (NOx) emissions
- Carbon dioxide $\left(\mathrm{CO}_{2}\right)$ emissions
- Particulate matter (PM) emissions

To bound the Mapped CI Engine block output, the block does not extrapolate the lookup table data.

## Virtual Calibration

If you have Model-Based Calibration Toolbox, click Calibrate Maps to virtually calibrate the 2D lookup tables using measured data. The dialog box steps through these tasks.

| Task | Description |  |  |
| :---: | :---: | :---: | :---: |
| Import firing data | Import this loss data from a file. For example, open <matlabroot>/ toolbox/mbc/mbctraining/CiEngineData.xlsx. <br> For more information, see "Using Data" (Model-Based Calibration Toolbox). |  |  |
|  | Input command | Required Data | Optional Data |
|  | Fuel mass | - Engine speed, rpm <br> - Commanded fuel mass per injection, mg <br> - Engine torque, $\mathrm{N} \cdot \mathrm{m}$ | - Air mass flow rate, kg/s <br> - Brake specific fuel consumption, $\mathrm{g} /(\mathrm{kW} \cdot \mathrm{h})$ <br> - CO2 mass flow rate, $\mathrm{kg} / \mathrm{s}$ |
|  | Torque | - Engine speed, rpm | - CO mass flow rate, $\mathrm{kg} / \mathrm{s}$ <br> - Exhaust temperature, K <br> - Fuel mass flow rate, kg/s <br> - HC mass flow rate, $\mathrm{kg} / \mathrm{s}$ <br> - NOx mass flow rate, kg/s <br> - Particulate matter mass flow rate, $\mathrm{kg} / \mathrm{s}$ |
|  | Collect firing data at steady-state operating conditions when injectors deliver the fuel. Data should cover the engine speed and torque operating range. Model-Based Calibration Toolbox uses the firing data boundary as the maximum torque. <br> To filter or edit the data, select Edit in Application. The Model-Based Calibration Toolbox Data Editor opens. |  |  |
| Import non-firing data | Import this non-firing data from a file. For example, open <matlabroot>/ toolbox/mbc/mbctraining/CiEngineData.xlsx. <br> - Engine speed, rpm <br> - Engine torque, $\mathrm{N} \cdot \mathrm{m}$ <br> Collect non-firing (motoring) data at steady-state operating conditions when fuel is cut off. All non-firing torque points must be less than zero. Non-firing data is a function of engine speed only. |  |  |
| Generate response models | For both firing and non-firing data, the Model-Based Calibration Toolbox uses test plans to fit data to Gaussian process models (GPMs). <br> To assess or adjust the response model fit, select Edit in Application. The Model-Based Calibration Toolbox Model Browser opens. For more information, see "Model Assessment" (Model-Based Calibration Toolbox). |  |  |


| Task | Description |
| :--- | :--- |
| Generate <br> calibration | Model-Based Calibration Toolbox calibrates the firing and non-firing response <br> models and generates calibrated tables. <br> To assess or adjust the calibration, select Edit in Application. The Model- <br> Based Calibration Toolbox CAGE Browser opens. For more information, see <br> "Calibration Lookup Tables" (Model-Based Calibration Toolbox). |
| Update block <br> parameters | Update the block lookup table and breakpoint parameters with the calibration. |

## Cylinder Air Mass

The block calculates the normalized cylinder air mass using these equations.

$$
\begin{aligned}
& M_{\text {Nom }}=\frac{P_{\text {std }} V_{d}}{N_{\text {cyl }} R_{\text {air }} T_{\text {std }}} \\
& L=\frac{\left(\frac{60 s}{\mathrm{~min}}\right) C p s \cdot \dot{m}_{a i r}}{\left(\frac{1000 g}{\mathrm{Kg}}\right) N_{\text {cyl }} \cdot N \cdot M_{\text {Nom }}}
\end{aligned}
$$

The equations use these variables.
$L \quad$ Normalized cylinder air mass
$M_{\text {Nom }} \quad$ Nominal engine cylinder air mass at standard temperature and pressure, piston at bottom dead center (BDC) maximum volume, in kg
Cps Crankshaft revolutions per power stroke, rev/stroke
$P_{s t d} \quad$ Standard pressure
$T_{\text {std }} \quad$ Standard temperature
$R_{\text {air }} \quad$ Ideal gas constant for air and burned gas mixture
$V_{d} \quad$ Displaced volume
$N_{\text {cyl }} \quad$ Number of engine cylinders
$N \quad$ Engine speed
$\dot{m}_{\text {intk }} \quad$ Engine air mass flow, in $\mathrm{g} / \mathrm{s}$

## Turbocharger Lag

To model turbocharger lag, select Include turbocharger lag effect. Turbocharger lag limits the maximum fuel mass per injection. To model the maximum fuel mass per injection, the block uses a first-order system with a time constant. At low torque, the engine does not require boost to provide sufficient air flow. When the requested fuel mass requires boost, the block uses a time constant to determine the maximum fuel mass per injection. The block uses these equations for the specified Input command setting.

| Calculation | Input command Parameter Setting |  |
| :---: | :---: | :---: |
|  | Fuel mass | Torque |
| Dynamic torque | $\frac{d F_{\max }}{d t}=\frac{1}{\tau_{e n g}}\left(F_{c m d}-F_{\max }\right)$ | $\frac{d T_{\max }}{d t}=\frac{1}{\tau_{e n g}}\left(T_{c m d}-T_{\max }\right)$ |
| Fuel mass per injection or torque - with turbocharger lag | $\begin{aligned} & F= \\ & \begin{cases}F_{c m d} & \text { when } F_{c m d}<F_{\max } \\ F_{\max } & \text { when } F_{c m d} \geq F_{\max }\end{cases} \end{aligned}$ | $\begin{aligned} & T_{\text {target }}= \\ & \begin{cases}T_{c m d} & \text { when } T_{c m d}<T_{\max } \\ T_{\max } & \text { when } T_{c m d} \geq T_{\max }\end{cases} \end{aligned}$ |
| Fuel mass per injection or torque- without turbocharger lag | $F=F_{\text {cmd }}=F_{\text {max }}$ | $T_{\text {target }}=T_{\text {cmd }}=T_{\text {max }}$ |
| Boost time constant | $\begin{aligned} & \tau_{b s t}= \\ & \begin{cases}\tau_{\text {bst, } \text { rising }} & \text { when } F_{c m d}>F_{\mathrm{max}} \\ \tau_{b s t, \text { falling }} & \text { when } F_{c m d} \leq F_{\mathrm{max}}\end{cases} \end{aligned}$ | $\begin{aligned} & \tau_{b s t}= \\ & \begin{cases}\tau_{\text {bst, } \text { rising }} & \text { when } T_{c m d}>T_{\max } \\ \tau_{\text {bst }, \text { falling }} & \text { when } T_{c m d} \leq T_{\max }\end{cases} \end{aligned}$ |
| Final time constant | $\tau_{\text {eng }}= \begin{cases}\tau_{\text {nat }} & \text { when } T_{\text {brake }}<f_{\text {bst }}(N) \\ \tau_{\text {bst }} & \text { when } T_{\text {brake }} \geq f_{\text {bst }}(N)\end{cases}$ |  |

The equations use these variables.

| $T_{\text {brake }}$ | Brake torque |
| :--- | :--- |
| $F$ | Fuel mass per injection |
| $F_{\text {cmd }}, F_{\text {max }}$ | Commanded and maximum fuel mass per injection, respectively |
| $T_{\text {target, }}, T_{\text {cmd }}, T_{\text {max }}$ | Target, commanded, and maximum torque, respectively |
| $\tau_{\text {bst }}$ | Boost time constant |
| $\tau_{\text {bst,rising, }}, \tau_{\text {bst,falling }}$ | Boost rising and falling time constant, respectively |
| $\tau_{\text {eng }}$ | Final time constant |
| $\tau_{\text {nat }}$ | Time constant below the boost torque speed line |
| $f_{\text {bst }}(N)$ | Boost torque/speed line |
| $N$ | Engine speed |

## Fuel Flow

To calculate the fuel economy for high-fidelity models, the block uses the volumetric fuel flow.

$$
Q_{f u e l}=\frac{\dot{m}_{\text {fuel }}}{\left(\frac{100 \mathrm{~kg}}{\mathrm{~m}^{3}}\right) S g_{\text {fuel }}}
$$

The equation uses these variables.
$\dot{m}_{\text {fuel }} \quad$ Fuel mass flow
$S g_{\text {fuel }} \quad$ Specific gravity of fuel
$Q_{\text {fuel }} \quad$ Volumetric fuel flow

## Power Accounting

For the power accounting, the block implements these equations.

| Bus Signal |  |  | Description | Equations |
| :---: | :---: | :---: | :---: | :---: |
| PwrInf <br> 0 | PwrTrnsfrd - Power transferred between blocks <br> - Positive signals indicate flow into block <br> - Negative signals indicate flow out of block | PwrCrkshft | Crankshaft power | $-\tau_{\text {eng }} \omega$ |
|  | PwrNotTrnsfrd - Power crossing the block boundary, but not transferred | PwrFuel | Fuel input power | $\dot{m}_{\text {fuel }} L H V$ |
|  | - Positive signals indicate an input <br> - Negative signals indicate a loss | PwrLoss | Power loss | $\left\lvert\, \begin{aligned} & \tau_{e n g} \omega \\ & -\dot{m}_{\text {fuel }} L H V \end{aligned}\right.$ |
|  | PwrStored - Stored energy rate of cha <br> - Positive signals indicate an increase <br> - Negative signals indicate a decrease |  | Not used |  |

The equations use these variables.

| LHV | Fuel lower heating value |
| :--- | :--- |
| $\omega$ | Engine speed, rad/s |
| $\dot{m}_{\text {fuel }}$ | Fuel mass flow |
| $\tau_{\text {eng }}$ | Fuel mass per injection time constant |

## Ports

## Input

FuelMassCmd - Injected fuel mass command
scalar
Injected fuel mass command, $F$, in mg/inj.

## Dependencies

To enable this port, for Input command, select Fuel mass.
TrqCmd - Torque command
scalar
Torque command, $T$, in $N \cdot m$.

## Dependencies

To enable this port, for Input command, select Torque.

EngSpd - Engine speed
scalar
Engine speed, $N$, in rpm.
EngTemp - Engine temperature
scalar
Engine temperature, $\mathrm{Temp}_{\text {Eng, }}$, in K .

## Dependencies

To enable this port, select Input engine temperature.

## Output

Info - Bus signal
bus
Bus signal containing these block calculations.

| Signal | Description | Units |
| :--- | :--- | :--- |
| IntkGasMassFlw | Engine air mass flow output | $\mathrm{kg} / \mathrm{s}$ |
| NrmlzdAirChrg | Normalized engine cylinder air mass | $\mathrm{N} / \mathrm{A}$ |
| Afr | Air-fuel ratio (AFR) | $\mathrm{N} / \mathrm{A}$ |
| FuelMassFlw | Engine fuel flow output | $\mathrm{kg} / \mathrm{s}$ |
| FuelVolFlw | Volumetric fuel flow | $\mathrm{m}^{3} / \mathrm{s}$ |
| ExhManGasTemp | Engine exhaust gas temperature | K |
| EngTrq | Engine torque output | $\mathrm{N} \cdot \mathrm{m}$ |
| EngSpd | Engine speed | rpm |
| CrkAng | Engine crankshaft absolute angle <br> $(360) C p s$ | degrees <br> crank angle |
| Bsfc | 0 <br> where Cps is crankshaft revolutions per <br> power stroke. | Eng |
| EoHC | Engine brake-specific fuel consumption <br> (BSFC) | $\mathrm{g} / \mathrm{kWh}$ |
| EoCO | Engine out hydrocarbon emission mass <br> flow | $\mathrm{kg} / \mathrm{s}$ |
| EoNOx | Engine out carbon monoxide emission <br> mass flow rate | $\mathrm{kg} / \mathrm{s}$ |
| EoC02 | Engine out nitric oxide and nitrogen <br> dioxide emissions mass flow | $\mathrm{kg} / \mathrm{s}$ |


| Signal |  | Description | Units |
| :--- | :--- | :--- | :--- |
| EoPM | Engine out particulate matter emission <br> mass flow | $\mathrm{kg} / \mathrm{s}$ |  |
| PwrInfo | PwrTrnsfrd | PwrCrkshft | Crankshaft power |
|  | PwrNotTrnsfr <br> d | PwrFuel | Fuel input power |
|  | PwrLoss | Power loss | W |
|  | PwrStored | Not used | W |

## EngTrq - Power <br> scalar

Engine power, $T_{\text {brake }}$, in $\mathrm{N} \cdot \mathrm{m}$.

## Parameters

## Block Options

Input command - Table functions
Fuel mass (default)|Torque
The lookup tables, developed with the Model-Based Calibration Toolbox, are functions of injected fuel mass, $F$, engine torque, $T$, engine speed, $N$, and engine temperature, $T e m p_{\text {Eng }}$.

| Input Command Setting | Input Engine Temperature <br> Parameter Setting | Lookup Tables |
| :--- | :--- | :--- |
| Fuel mass | off | $f(F, N)$ |
|  | on | $f\left(F, N, T e m p_{\text {Eng }}\right)$ |
| Torque | off | $f(T, N)$ |
|  | on | $f\left(T, N, T e m p_{\text {Eng }}\right)$ |

## Dependencies

- Selecting Fuel mass enables Breakpoints for commanded fuel mass input, f_tbrake_f_bpt.
- Selecting Torque enables Breakpoints for commanded torque input, f_tbrake_t_bpt.
- Selecting Input engine temperature enables Breakpoints for temperature input, f_tbrake_engtmp_bpt.

Include turbocharger lag effect - Increase time constant
off (default)
To model turbocharger lag, select Include turbocharger lag effect. Turbocharger lag limits the maximum fuel mass per injection. To model the maximum fuel mass per injection, the block uses a first-order system with a time constant. At low torque, the engine does not require boost to provide sufficient air flow. When the requested fuel mass requires boost, the block uses a time constant to determine the maximum fuel mass per injection. The block uses these equations for the specified Input command setting.

| Calculation | Input command Parameter Setting |  |
| :---: | :---: | :---: |
|  | Fuel mass | Torque |
| Dynamic torque | $\frac{d F_{\max }}{d t}=\frac{1}{\tau_{e n g}}\left(F_{c m d}-F_{\max }\right)$ | $\frac{d T_{\max }}{d t}=\frac{1}{\tau_{e n g}}\left(T_{c m d}-T_{\max }\right)$ |
| Fuel mass per injection or torque - with turbocharger lag | $\begin{aligned} & F= \\ & \begin{cases}F_{c m d} & \text { when } F_{c m d}<F_{\max } \\ F_{\max } & \text { when } F_{c m d} \geq F_{\max }\end{cases} \end{aligned}$ | $\begin{aligned} & T_{\text {target }}= \\ & \begin{cases}T_{\text {cmd }} & \text { when } T_{c m d}<T_{\max } \\ T_{\max } & \text { when } T_{c m d} \geq T_{\max }\end{cases} \end{aligned}$ |
| Fuel mass per injection or torque- without turbocharger lag | $F=F_{\text {cmd }}=F_{\text {max }}$ | $T_{\text {target }}=T_{\text {cmd }}=T_{\text {max }}$ |
| Boost time constant | $\begin{aligned} & \tau_{b s t} \\ & \begin{cases}\tau_{\text {bst, } \text { rising }} & \text { when } F_{c m d}>F_{\mathrm{max}} \\ \tau_{\text {bst }, \text { falling }} & \text { when } F_{c m d} \leq F_{\mathrm{max}}\end{cases} \end{aligned}$ | $\begin{aligned} & \tau_{\text {bst }}= \\ & \begin{cases}\tau_{\text {bst }, \text { rising }} & \text { when } T_{c m d}>T_{\max } \\ \tau_{\text {bst }, \text { falling }} & \text { when } T_{c m d} \leq T_{\max }\end{cases} \end{aligned}$ |
| Final time constant | $\tau_{\text {eng }}= \begin{cases}\tau_{\text {nat }} & \text { when } T_{\text {brake }}<f_{\text {bst }}(N) \\ \tau_{\text {bst }} & \text { when } T_{\text {brake }} \geq f_{\text {bst }}(N)\end{cases}$ |  |

The equations use these variables.

| $T_{\text {brake }}$ | Brake torque |
| :--- | :--- |
| $F$ | Fuel mass per injection |
| $F_{\text {cmd }}, F_{\text {max }}$ | Commanded and maximum fuel mass per injection, respectively |
| $T_{\text {target },}, T_{\text {cmd }}, T_{\text {max }}$ | Target, commanded, and maximum torque, respectively |
| $\tau_{\text {bst }}$ | Boost time constant |
| $\tau_{\text {bst }, \text { rising, }}, \tau_{\text {bst,falling }}$ | Boost rising and falling time constant, respectively |
| $\tau_{\text {eng }}$ | Final time constant |
| $\tau_{\text {nat }}$ | Time constant below the boost torque speed line |
| $f_{\text {bst }}(N)$ | Boost torque/speed line |
| $N$ | Engine speed |
| Dependencies |  |

Selecting Include turbocharger lag effect enables these parameters:

- Boost torque line, f_tbrake_bst
- Time constant below boost line, tau_nat
- Rising maximum fuel mass boost time constant, tau_bst_rising
- Falling maximum fuel mass boost time constant, tau_bst_falling

Input engine temperature - Create input port
off (default) | on
Select this to create the EngTemp input port.

The lookup tables, developed with the Model-Based Calibration Toolbox, are functions of injected fuel mass, $F$, engine torque, $T$, engine speed, $N$, and engine temperature, $T e m p_{\text {Eng }}$.

| Input Command Setting | Input Engine Temperature <br> Parameter Setting | Lookup Tables |
| :--- | :--- | :--- |
| Fuel mass | off | $f(F, N)$ |
|  | on | $f\left(F, N, T e m p_{\text {Eng }}\right)$ |
| Torque | off | $f(T, N)$ |
|  | on | $f\left(T, N, T e m p_{\text {Eng }}\right)$ |

## Configuration

## Calibrate Maps - Calibrate tables with measured data

selection
If you have Model-Based Calibration Toolbox, click Calibrate Maps to virtually calibrate the 2D lookup tables using measured data. The dialog box steps through these tasks.

| Task | Description |  |  |
| :---: | :---: | :---: | :---: |
| Import firing data | Import this loss data from a file. For example, open <matlabroot>/ toolbox/mbc/mbctraining/CiEngineData.xlsx. <br> For more information, see "Using Data" (Model-Based Calibration Toolbox). |  |  |
|  | Input command | Required Data | Optional Data |
|  | Fuel mass | - Engine speed, rpm <br> - Commanded fuel mass per injection, mg <br> - Engine torque, $\mathrm{N} \cdot \mathrm{m}$ | - Air mass flow rate, kg/s <br> - Brake specific fuel consumption, $\mathrm{g} /(\mathrm{kW} \cdot \mathrm{h})$ <br> - CO2 mass flow rate, $\mathrm{kg} / \mathrm{s}$ |
|  | Torque | - Engine speed, rpm <br> - Engine torque, $\mathrm{N} \cdot \mathrm{m}$ | - CO mass flow rate, $\mathrm{kg} / \mathrm{s}$ <br> - Exhaust temperature, K <br> - Fuel mass flow rate, kg/s <br> - HC mass flow rate, kg/s <br> - NOx mass flow rate, $\mathrm{kg} / \mathrm{s}$ <br> - Particulate matter mass flow rate, $\mathrm{kg} / \mathrm{s}$ |

Collect firing data at steady-state operating conditions when injectors deliver the fuel. Data should cover the engine speed and torque operating range. Model-Based Calibration Toolbox uses the firing data boundary as the maximum torque.

To filter or edit the data, select Edit in Application. The Model-Based Calibration Toolbox Data Editor opens.

| Task | Description |
| :--- | :--- |
| Import non-firing <br> data | Import this non-firing data from a file. For example, open <matlabroot>/ <br> toolbox/mbc/mbct raining/CiEngineData.xlsx. <br> - Engine speed, rpm <br> - Engine torque, N•m <br> Collect non-firing (motoring) data at steady-state operating conditions when <br> fuel is cut off. All non-firing torque points must be less than zero. Non-firing <br> data is a function of engine speed only. |
| Generate response <br> models | For both firing and non-firing data, the Model-Based Calibration Toolbox uses <br> test plans to fit data to Gaussian process models (GPMs). <br> To assess or adjust the response model fit, select Edit in Application. The <br> Model-Based Calibration Toolbox Model Browser opens. For more information, <br> see "Model Assessment" (Model-Based Calibration Toolbox). |
| Generate <br> calibration | Model-Based Calibration Toolbox calibrates the firing and non-firing response <br> models and generates calibrated tables. <br> To assess or adjust the calibration, select Edit in Application. The Model- <br> Based Calibration Toolbox CAGE Browser opens. For more information, see <br> "Calibration Lookup Tables" (Model-Based Calibration Toolbox). |
| Update block <br> parameters | Update the block lookup table and breakpoint parameters with the calibration. |

## Dependencies

To enable this parameter, clear Input engine temperature.

## Breakpoints for commanded fuel mass input, f_tbrake_f_bpt - Breakpoints

1-by-M vector
Breakpoints, in mg/inj.

## Dependencies

Setting Input command to Fuel mass enables this parameter.

## Breakpoints for commanded torque input, f_tbrake_t_bpt - Breakpoints

1-by-M vector
Breakpoints, in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

Setting Input command to Torque enables this parameter.

## Breakpoints for engine speed input, f_tbrake_n_bpt - Breakpoints

1-by-N vector
Breakpoints, in rpm.
Breakpoints for temperature input, f_tbrake_engtmp_bpt - Breakpoints
[233.15 273.15 373.15] (default) | 1-by-L vector

Breakpoints, in K.
Dependencies
To enable this parameter, select Input engine temperature.
Number of cylinders, NCyI - Number
4 (default) | scalar
Number of cylinders.
Crank revolutions per power stroke, Cps - Crank revolutions
2 (default) | scalar
Crank revolutions per power stroke.
Total displaced volume, Vd - Volume
0.0015 (default) | scalar

Volume displaced by engine, in $\mathrm{m} \wedge 3$.
Fuel lower heating value, Lhv - Heating value
45e6 (default) | scalar
Fuel lower heating value, $L H V$, in $\mathrm{J} / \mathrm{kg}$.
Fuel specific gravity, $\mathbf{S g}$ - Specific gravity
0.832 (default) | scalar

Specific gravity of fuel, $S g_{\text {fuel }}$, dimensionless.
Ideal gas constant air, Rair - Constant
287 (default) | scalar
Ideal gas constant of air and residual gas entering the engine intake port, in $\mathrm{J} /(\mathrm{kg} \cdot \mathrm{K})$.
Air standard pressure, Pstd - Pressure
101325 (default) | scalar
Standard air pressure, in Pa.
Air standard temperature, Tstd - Temperature
293.15 (default) | scalar

Standard air temperature, in K.
Boost torque line, f_tbrake_bst - Boost lag
[90, $95,95,95,96,100,104,104,104,100,95,85,75,67,60,55]$ (default) | 1-by-M vector
Boost torque line, $f_{\text {bst }}(N)$, in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

To enable this parameter, select Include turbocharger lag effect.
Time constant below boost line - Time constant below
0.1 (default) | scalar

Time constant below boost line, $\tau_{\text {nat }}$, in s .
Dependencies
To enable this parameter, select Include turbocharger lag effect.
Rising maximum fuel mass boost time constant, tau_bst_rising - Rising time constant 1.0 (default) | scalar

Rising maximum fuel mass boost time constant, $\tau_{\text {bst,rising }}$, in s .
Dependencies
To enable this parameter, select Include turbocharger lag effect.
Falling maximum fuel mass boost time constant, tau_bst_falling - Falling time constant 0.7 (default) | scalar

Falling maximum fuel mass boost time constant, $\tau_{\text {bst,falling }}$ in s .
Dependencies
To enable this parameter, select Include turbocharger lag effect.
Turbocharger time constant blend fuel mass fraction, f_blend_frac - Time constant 0.01 (default)| scalar

Turbocharger time constant blend fuel mass fraction, in s.
Dependencies
To enable this parameter, select Include turbocharger lag effect.

## Power

Brake torque map, f_tbrake - 2D lookup table
M-by-N matrix

| Input Command Setting | Description |
| :---: | :---: |
| Fuel mass | The engine brake torque lookup table is a function of commanded fuel mass and engine speed, $T_{\text {brake }}=f(F, N)$, where: <br> - $T_{\text {brake }}$ is engine torque, in $\mathrm{N} \cdot \mathrm{m}$. <br> - $F$ is commanded fuel mass, in mg per injection. <br> - $N$ is engine speed, in rpm. |
| Torque | The engine brake torque lookup table is a function of target torque and engine speed, $T_{\text {brake }}=\mathrm{f}\left(T_{\text {target, }}, N\right)$, where: <br> - $\quad T_{\text {brake }}$ is engine torque, in $\mathrm{N} \cdot \mathrm{m}$. <br> - $T_{\text {target }}$ is target torque, in $\mathrm{N} \cdot \mathrm{m}$. <br> - $N$ is engine speed, in rpm. |

## Dependencies

To enable this parameter, clear Input engine temperature.
Plot brake torque map - Plot table
button
Click to plot table.

## Dependencies

To enable this parameter, clear Input engine temperature.
Brake torque map, f_tbrake_3d - 3D lookup table
M-by-N-by-L array

| Input Command Setting | Description |
| :---: | :---: |
| Fuel mass | The engine brake torque lookup table is a function of commanded fuel mass and engine speed, $T_{\text {brake }}=f\left(F, N, T e m p_{\text {Eng }}\right)$, where: <br> - $T_{\text {brake }}$ is engine torque, in $\mathrm{N} \cdot \mathrm{m}$. <br> - $F$ is commanded fuel mass, in mg per injection. <br> - $\mathrm{Temp}_{\text {Eng }}$ is engine temperature, in K . |


| Input Command Setting | Description |
| :---: | :---: |
| Torque | The engine brake torque lookup table is a function of target torque and engine speed, $T_{\text {brake }}=f\left(T_{\text {target }}, N, T e m p_{\text {Eng }}\right)$, where: <br> - $T_{\text {brake }}$ is engine torque, in $\mathrm{N} \cdot \mathrm{m}$. <br> - $T_{\text {target }}$ is target torque, in $\mathrm{N} \cdot \mathrm{m}$. <br> - $N$ is engine speed, in rpm. <br> - Temp $_{\text {Eng }}$ is engine temperature, in K . |

## Dependencies

To enable this parameter, select Input engine temperature.
Air
Air mass flow map, f_air - 2D lookup table
M-by-N matrix

| Input Command Setting | Description |
| :---: | :---: |
| Fuel mass | The air mass flow lookup table is a function of commanded fuel mass and engine speed, $\dot{m}_{\text {intk }}=\mathrm{f}\left(F_{\text {max }}, N\right)$, where: <br> - $\dot{m}_{\text {intk }}$ is engine air mass flow, in $\mathrm{kg} / \mathrm{s}$. <br> - $F_{\text {max }}$ is commanded fuel mass, in mg per injection. <br> - $N$ is engine speed, in rpm. |
| Torque | The air mass flow lookup table is a function of maximum torque and engine speed, $\dot{m}_{\text {intk }}=f\left(T_{\max }, N\right)$, where: <br> - $\dot{m}_{\text {intk }}$ is engine air mass flow, in $\mathrm{kg} / \mathrm{s}$. <br> - $T_{\max }$ is maximum torque, in $\mathrm{N} \cdot \mathrm{m}$. <br> - $N$ is engine speed, in rpm. |

## Dependencies

To enable this parameter, clear Input engine temperature.
Plot air mass map - Plot table
button

Click to plot table.

## Dependencies

To enable this parameter, clear Input engine temperature.
Air mass flow map, f_air_3d - 3D lookup table
M-by-N-by-L array

## Input Command Setting Description

| Fuel mass | The air mass flow lookup table is a function of commanded fuel mass and engine speed, $\dot{m}_{\text {intk }}=f\left(F_{\text {max }}, N, T e m p_{\text {Eng }}\right)$, where: <br> - $\dot{m}_{\text {intk }}$ is engine air mass flow, in $\mathrm{kg} / \mathrm{s}$. <br> - $F_{\max }$ is commanded fuel mass, in mg per injection. <br> - $N$ is engine speed, in rpm. <br> - $T e m p_{\text {Eng }}$ is engine temperature, in K . |
| :---: | :---: |
| Torque | The air mass flow lookup table is a function of maximum torque and engine speed, $\dot{m}_{\text {intk }}=f\left(T_{\text {max }}, N, T e m p_{\text {Eng }}\right)$, where: |

- $\dot{m}_{i n t k}$ is engine air mass flow, in $\mathrm{kg} / \mathrm{s}$.
- $T_{\max }$ is maximum torque, in $\mathrm{N} \cdot \mathrm{m}$.
- $\quad N$ is engine speed, in rpm.
- $\mathrm{Temp}_{\text {Eng }}$ is engine temperature, in K .


## Dependencies

To enable this parameter, select Input engine temperature.

## Fuel

Fuel flow map, f_fuel - 2D lookup table
M-by-N matrix

| Input Command Setting | Description |
| :---: | :---: |
| Fuel mass | The engine fuel flow lookup table is a function of commanded fuel mass and engine speed, MassFlow $=f(F, N)$, where: <br> - MassFlow is engine fuel mass flow, in $\mathrm{kg} / \mathrm{s}$. <br> - $F$ is commanded fuel mass, in mg per injection. <br> - $N$ is engine speed, in rpm. <br> Commanded Fuel (mg/inj) |
| Torque | The engine fuel flow lookup table is a function of target torque and engine speed, MassFlow $=f\left(T_{\text {target }}, N\right)$, where: <br> - MassFlow is engine fuel mass flow, in $\mathrm{kg} / \mathrm{s}$. <br> - $T_{\text {target }}$ is target torque, in $\mathrm{N} \cdot \mathrm{m}$. <br> - $N$ is engine speed, in rpm. |

## Dependencies

To enable this parameter, clear Input engine temperature.

## Plot fuel flow map - Plot table

## button

Click to plot table.

## Dependencies

To enable this parameter, clear Input engine temperature.
Fuel flow map, f_fuel_3d - 3D lookup table
M-by-N-by-L array

| Input Command Setting | Description |
| :---: | :---: |
| Fuel mass | The engine fuel flow lookup table is a function of commanded fuel mass, engine speed, and engine temperature, MassFlow $=f\left(F, N, T e m p_{\text {Eng }}\right)$, where: <br> - MassFlow is engine fuel mass flow, in $\mathrm{kg} / \mathrm{s}$. <br> - $F$ is commanded fuel mass, in mg per injection. <br> - $N$ is engine speed, in rpm. <br> - $T e m p_{\text {Eng }}$ is engine temperature, in K . |
| Torque | The engine fuel flow lookup table is a function of target torque and engine speed, and engine temperature, MassFlow $=f\left(T_{\text {target, }}, N, T e m p_{\text {Eng }}\right)$, where: <br> - MassFlow is engine fuel mass flow, in $\mathrm{kg} / \mathrm{s}$. <br> - $T_{\text {target }}$ is target torque, in $\mathrm{N} \cdot \mathrm{m}$. <br> - $N$ is engine speed, in rpm. <br> - $T e m p_{\text {Eng }}$ is engine temperature, in K. |

## Dependencies

To enable this parameter, select Input engine temperature.

## Temperature

Exhaust temperature map, f_texh - 2D lookup table
M-by-N matrix

| Input Command Setting | Description |
| :---: | :---: |
| Fuel mass | The engine exhaust temperature table is a function of commanded fuel mass and engine speed, $T_{\text {exh }}=f(F, N)$, where: <br> - $T_{e x h}$ is exhaust temperature, in K. <br> - $F$ is commanded fuel mass, in mg per injection. <br> - $N$ is engine speed, in rpm. |


| Input Command Setting | Description |
| :---: | :---: |
| Torque | The engine exhaust temperature table is a function of target torque and engine speed, $T_{\text {exh }}=f\left(T_{\text {target }}, N\right)$, where: <br> - $T_{\text {exh }}$ is exhaust temperature, in K . <br> - $T_{\text {target }}$ is target torque, in $\mathrm{N} \cdot \mathrm{m}$. <br> - $N$ is engine speed, in rpm. |

## Dependencies

To enable this parameter, clear Input engine temperature.
Plot exhaust temperature map - Plot table
button
Click to plot table.

## Dependencies

To enable this parameter, clear Input engine temperature.
Exhaust temperature map, f_texh_3d - 3D lookup table
M-by-N-by-L array

| Input Command Setting | Description |
| :---: | :---: |
| Fuel mass | The engine exhaust temperature table is a function of commanded fuel mass and engine speed, $T_{\text {exh }}=f\left(F, N, T e m p_{\text {Eng }}\right)$, where: <br> - $T_{\text {exh }}$ is exhaust temperature, in K. <br> - $F$ is commanded fuel mass, in mg per injection. <br> - $N$ is engine speed, in rpm. <br> - $T e m p_{\text {Eng }}$ is engine temperature, in K . |
| Torque | The engine exhaust temperature table is a function of target torque and engine speed, $T_{\text {exh }}=f\left(T_{\text {target, }}, N, T e m p_{\text {Eng }}\right)$, where: <br> - $T_{\text {exh }}$ is exhaust temperature, in K . <br> - $T_{\text {target }}$ is target torque, in $\mathrm{N} \cdot \mathrm{m}$. <br> - $N$ is engine speed, in rpm. <br> - Temp $_{\text {Eng }}$ is engine temperature, in K . |

## Dependencies

To enable this parameter, select Input engine temperature.

## Efficiency

BSFC map, f_eff - 2D lookup table
M-by-N matrix

| Input Command Setting | Description |
| :---: | :---: |
| Fuel mass | The brake-specific fuel consumption (BSFC) efficiency is a function of commanded fuel mass and engine speed, $B S F C=f(F, N)$, where: <br> - BSFC is BSFC, in $\mathrm{g} / \mathrm{kWh}$. <br> - $F$ is commanded fuel mass, in mg per injection. <br> - $N$ is engine speed, in rpm. <br> Commanded Fuel (mg/inj) |
| Torque | The brake-specific fuel consumption (BSFC) efficiency is a function of target torque and engine speed, $B S F C=f\left(T_{\text {target }}, N\right)$, where: <br> - BSFC is BSFC, in $\mathrm{g} / \mathrm{kWh}$. <br> - $T_{\text {target }}$ is target torque, in $\mathrm{N} \cdot \mathrm{m}$. <br> - $N$ is engine speed, in rpm. |

## Dependencies

To enable this parameter, clear Input engine temperature.
Plot BSFC map - Plot table
button
Click to plot table.

## Dependencies

To enable this parameter, clear Input engine temperature.
BSFC map, f_eff_3d - 3D lookup table
M-by-N-by-L array

| Input Command Setting | Description |
| :---: | :---: |
| Fuel mass | The brake-specific fuel consumption (BSFC) efficiency is a function of commanded fuel mass and engine speed, $B S F C=f\left(F, N, T e m p_{\text {Eng }}\right)$, where: <br> - BSFC is BSFC, in $\mathrm{g} / \mathrm{kWh}$. <br> - $F$ is commanded fuel mass, in mg per injection. <br> - $N$ is engine speed, in rpm. <br> - $T e m p_{\text {Eng }}$ is engine temperature, in K . |


| Input Command Setting | Description |
| :--- | :--- |


| Torque | The brake-specific fuel consumption (BSFC) efficiency is a function of target torque and engine speed, $B S F C=f\left(T_{\text {target }}, N, T e m p_{\text {Eng }}\right)$, where: <br> - $B S F C$ is BSFC , in $\mathrm{g} / \mathrm{kWh}$. <br> - $T_{\text {target }}$ is target torque, in $\mathrm{N} \cdot \mathrm{m}$. <br> - $N$ is engine speed, in rpm. <br> - Temp $_{\text {Eng }}$ is engine temperature, in K . |
| :---: | :---: |

## Dependencies

To enable this parameter, select Input engine temperature.
HC
EO HC map, f_hc - 2D lookup table
M-by-N matrix

| Input Command Setting | Description |
| :---: | :---: |
| Fuel mass | The engine-out hydrocarbon emissions are a function of commanded fuel mass and engine speed, $E O H C=f(F, N)$, where: <br> - EO HC is engine-out hydrocarbon emissions, in kg/s. <br> - $F$ is commanded fuel mass, in mg per injection. <br> - $N$ is engine speed, in rpm. |
| Torque | The engine-out hydrocarbon emissions are a function of target torque and engine speed, EO HC $=f\left(T_{\text {target }}, N\right)$, where: <br> - EO HC is engine-out hydrocarbon emissions, in $\mathrm{kg} / \mathrm{s}$. <br> - $T_{\text {target }}$ is target torque, in $\mathrm{N} \cdot \mathrm{m}$. <br> - $N$ is engine speed, in rpm. |

## Dependencies

To enable this parameter, clear Input engine temperature.
Plot EO HC map - Plot table
button

Click to plot table.

## Dependencies

To enable this parameter, clear Input engine temperature.
EO HC map, f_hc_3d - 3D lookup table
M-by-N-by-L array

| Input Command Setting | Description |
| :---: | :---: |
| Fuel mass | The engine-out hydrocarbon emissions are a function of commanded fuel mass and engine speed, $E O H C=f\left(F, N, T e m p_{\text {Eng }}\right)$, where: <br> - EO HC is engine-out hydrocarbon emissions, in kg/s. <br> - $F$ is commanded fuel mass, in mg per injection. <br> - $N$ is engine speed, in rpm. <br> - Temp $_{\text {Eng }}$ is engine temperature, in K . |
| Torque | The engine-out hydrocarbon emissions are a function of target torque and engine speed, $E O H C=f\left(T_{\text {target }}, N, T e m p_{\text {Eng }}\right)$, where: <br> - EO HC is engine-out hydrocarbon emissions, in kg/s. <br> - $T_{\text {target }}$ is target torque, in $\mathrm{N} \cdot \mathrm{m}$. <br> - $N$ is engine speed, in rpm. <br> - $T e m p_{\text {Eng }}$ is engine temperature, in K . |

## Dependencies

To enable this parameter, select Input engine temperature.

## CO

EO CO map, f_co - 2D lookup table
M-by-N matrix

| Input Command Setting | Description |
| :---: | :---: |
| Fuel mass | The engine-out carbon monoxide emissions are a function of commanded fuel mass and engine speed, $E O C O=f(F, N)$, where: <br> - EO CO is engine-out carbon monoxide emissions, in $\mathrm{kg} / \mathrm{s}$. <br> - $F$ is commanded fuel mass, in mg per injection. <br> - $N$ is engine speed, in rpm. |
| Torque | The engine-out carbon monoxide emissions are a function of target torque and engine speed, $E O C O=f\left(T_{\text {target }}, N\right)$, where: <br> - EO CO is engine-out carbon monoxide emissions, in $\mathrm{kg} / \mathrm{s}$. <br> - $T_{\text {target }}$ is target torque, in $\mathrm{N} \cdot \mathrm{m}$. <br> - $N$ is engine speed, in rpm. |

## Dependencies

To enable this parameter, clear Input engine temperature.

## Plot EO CO map - Plot table

button
Click to plot table.

## Dependencies

To enable this parameter, clear Input engine temperature.
EO CO map, f_co_3d - 3D lookup table
M-by-N-by-L array

| Input Command Setting | Description |
| :---: | :---: |
| Fuel mass | The engine-out carbon monoxide emissions are a function of commanded fuel mass and engine speed, $E O C O=f\left(F, N, T e m p_{\text {Eng }}\right)$, where: <br> - EO CO is engine-out carbon monoxide emissions, in $\mathrm{kg} / \mathrm{s}$. <br> - $F$ is commanded fuel mass, in mg per injection. <br> - $N$ is engine speed, in rpm. <br> - $T e m p_{\text {Eng }}$ is engine temperature, in K . |
| Torque | The engine-out carbon monoxide emissions are a function of target torque and engine speed, $E O C O=f\left(T_{\text {target, }}, N, T e m p_{\text {Eng }}\right)$, where: <br> - EO CO is engine-out carbon monoxide emissions, in $\mathrm{kg} / \mathrm{s}$. <br> - $T_{\text {target }}$ is target torque, in $\mathrm{N} \cdot \mathrm{m}$. <br> - $N$ is engine speed, in rpm. <br> - $T e m p_{\text {Eng }}$ is engine temperature, in K . |

## Dependencies

To enable this parameter, select Input engine temperature.
NOx
EO NOx map, f_nox - 2D lookup table
M-by-N matrix

| Input Command Setting | Description |
| :---: | :---: |
| Fuel mass | The engine-out nitric oxide and nitrogen dioxide emissions are a function of commanded fuel mass and engine speed, $E O$ NOx $=f(F, N)$, where: <br> - EO NOx is engine-out nitric oxide and nitrogen dioxide emissions, in $\mathrm{kg} / \mathrm{s}$. <br> - $F$ is commanded fuel mass, in mg per injection. <br> - $N$ is engine speed, in rpm. |


| Input Command Setting |
| :--- |
| Torque |
|  |
|  |
|  |

## Description

The engine-out nitric oxide and nitrogen dioxide emissions are a function of target torque and engine speed, EO NOx $=f\left(T_{\text {target }}, N\right)$, where:

- EO NOx is engine-out nitric oxide and nitrogen dioxide emissions, in $\mathrm{kg} / \mathrm{s}$.
- $T_{\text {target }}$ is target torque, in $\mathrm{N} \cdot \mathrm{m}$.
- $N$ is engine speed, in rpm.


## Dependencies

To enable this parameter, clear Input engine temperature.
Plot EO NOx map - Plot table
button
Click to plot table.

## Dependencies

To enable this parameter, clear Input engine temperature.
EO NOx map, f_nox_3d - 3D lookup table
M-by-N-by-L array

| Input Command Setting | Description |
| :---: | :---: |
| Fuel mass | The engine-out nitric oxide and nitrogen dioxide emissions are a function of commanded fuel mass, engine speed, and engine temperature, EO $N O x=f\left(F, N, T e m p_{\text {Eng }}\right)$, where: <br> - EO NOx is engine-out nitric oxide and nitrogen dioxide emissions, in kg/s. <br> - $F$ is commanded fuel mass, in mg per injection. <br> - $N$ is engine speed, in rpm. <br> - $T e m p_{\text {Eng }}$ is engine temperature, in K . |
| Torque | The engine-out nitric oxide and nitrogen dioxide emissions are a function of target torque, engine speed, and engine temperature, EO NOx = $\mathrm{f}\left(T_{\text {target }}, N, \operatorname{Temp}_{\text {Eng }}\right)$, where: <br> - EO NOx is engine-out nitric oxide and nitrogen dioxide emissions, in $\mathrm{kg} / \mathrm{s}$. <br> - $T_{\text {target }}$ is target torque, in $\mathrm{N} \cdot \mathrm{m}$. <br> - $N$ is engine speed, in rpm. <br> - $T e m p_{\text {Eng }}$ is engine temperature, in K . |

## Dependencies

To enable this parameter, select Input engine temperature.

CO2
EO CO2 map, f_co2 - 2D lookup table
M-by-N matrix

| Input Command Setting | Description |
| :---: | :---: |
| Fuel mass | The engine-out carbon dioxide emissions are a function of commanded fuel mass and engine speed, $E O C O 2=f(F, N)$, where: <br> - EO CO2 is engine-out carbon dioxide emissions, in $\mathrm{kg} / \mathrm{s}$. <br> - $F$ is commanded fuel mass, in mg per injection. <br> - $N$ is engine speed, in rpm. |
| Torque | The engine-out carbon dioxide emissions are a function of target torque and engine speed, EO CO2 $=f\left(T_{\text {target }}, N\right)$, where: <br> - EO CO2 is engine-out carbon dioxide emissions, in $\mathrm{kg} / \mathrm{s}$. <br> - $T_{\text {target }}$ is target torque, in $\mathrm{N} \cdot \mathrm{m}$. <br> - $N$ is engine speed, in rpm. |

## Dependencies

To enable this parameter, clear Input engine temperature.
Plot CO2 map - Plot table
button
Click to plot table.

## Dependencies

To enable this parameter, clear Input engine temperature.
EO CO2 map, f_co2_3d - 3D lookup table
M-by-N-by-L array

| Input Command Setting | Description |
| :---: | :---: |
| Fuel mass | The engine-out carbon dioxide emissions are a function of commanded fuel mass, engine speed, and engine temperature, $E O C O 2=f(F, N$, Temp $p_{\text {Eng }}$ ), where: <br> - EO CO2 is engine-out carbon dioxide emissions, in $\mathrm{kg} / \mathrm{s}$. <br> - $F$ is commanded fuel mass, in mg per injection. <br> - $N$ is engine speed, in rpm. <br> - $T e m p_{\text {Eng }}$ is engine temperature, in K. |
| Torque | The engine-out carbon dioxide emissions are a function of target torque, engine speed, and engine temperature, EO CO2 $=\mathrm{f}\left(T_{\text {target, }}, N, T e m p_{\text {Eng }}\right)$, where: <br> - EO CO2 is engine-out carbon dioxide emissions, in $\mathrm{kg} / \mathrm{s}$. <br> - $T_{\text {target }}$ is target torque, in $\mathrm{N} \cdot \mathrm{m}$. <br> - $N$ is engine speed, in rpm. <br> - $\mathrm{Temp}_{\text {Eng }}$ is engine temperature, in K . |

## Dependencies

To enable this parameter, select Input engine temperature.
PM
EO PM map, f_pm - 2D lookup table
M-by-N matrix

| Input Command Setting | Description |
| :---: | :---: |
| Fuel mass | The engine-out PM emissions are a function of commanded fuel mass and engine speed, where: <br> - EO PM is engine-out PM emissions, in $\mathrm{kg} / \mathrm{s}$. <br> - $F$ is commanded fuel mass, in mg per injection. <br> - $N$ is engine speed, in rpm. |
| Torque | The engine-out PM emissions are a function of target torque and engine speed, EO PM $=f\left(T_{\text {target, }}, N\right)$, where: <br> - EO PM is engine-out PM emissions, in kg/s. <br> - $T_{\text {target }}$ is target torque, in $\mathrm{N} \cdot \mathrm{m}$. <br> - $N$ is engine speed, in rpm. |

## Dependencies

To enable this parameter, clear Input engine temperature.
Plot EO PM map - Plot table
button
Click to plot table.

## Dependencies

To enable this parameter, clear Input engine temperature.
EO PM map, f_pm_3d - 3D lookup table
M-by-N-by-L array

| Input Command Setting | Description |
| :---: | :---: |
| Fuel mass | The engine-out PM emissions are a function of commanded fuel mass, engine speed, and engine temperature, where: <br> - EO PM is engine-out PM emissions, in kg/s. <br> - $F$ is commanded fuel mass, in mg per injection. <br> - $N$ is engine speed, in rpm. <br> - $T e m p_{\text {Eng }}$ is engine temperature, in K. |
| Torque | The engine-out PM emissions are a function of target torque, engine speed, and engine temperature, $E O P M=f\left(T_{\text {target }}, N, T\right)$, where: <br> - EO PM is engine-out PM emissions, in $\mathrm{kg} / \mathrm{s}$. <br> - $T_{\text {target }}$ is target torque, in $\mathrm{N} \cdot \mathrm{m}$. <br> - $N$ is engine speed, in rpm. <br> - $T e m p_{\text {Eng }}$ is engine temperature, in K . |

## Dependencies

To enable this parameter, select Input engine temperature.

## Version History

## Introduced in R2017a

## Extended Capabilities

C/C++ Code Generation
Generate C and C++ code using Simulink ${ }^{\circledR}$ Coder ${ }^{\mathrm{TM}}$.

## See Also

Mapped Motor | Mapped SI Engine

## Topics

"Engine Calibration Maps"
"Model-Based Calibration Toolbox"

## Mapped SI Engine

Spark-ignition engine model using lookup tables


## Libraries:

Powertrain Blockset / Propulsion / Combustion Engines
Vehicle Dynamics Blockset / Powertrain / Propulsion

## Description

The Mapped SI Engine block implements a mapped spark-ignition (SI) engine model using power, air mass flow, fuel flow, exhaust temperature, efficiency, and emission performance lookup tables. You can use the block for:

- Hardware-in-the-loop (HIL) engine control design
- Vehicle-level fuel economy and performance simulations

The block enables you to specify lookup tables for these engine characteristics. The lookup tables, developed with the Model-Based Calibration Toolbox, are functions of commanded torque, $T_{\text {cmd }}$, brake torque, $T_{\text {brake }}$, and engine speed, $N$. If you select Input engine temperature, the tables are also a function of engine temperature, $\mathrm{Temp}_{\text {Eng }}$.

| Table | Input Engine Temperature Parameter Setting |  |
| :---: | :---: | :---: |
|  | off | on |
| Power | $f\left(T_{\text {cmd }}, N\right)$ | $f\left(T_{\text {cmd }}, N, T e m p_{\text {Eng }}\right)$ |
| Air | $f\left(T_{\text {brake }}, N\right)$ | $f\left(T_{\text {brake }}, N\right.$, Temp $\left._{\text {Eng }}\right)$ |
| Fuel |  |  |
| Temperature |  |  |
| Efficiency |  |  |
| HC |  |  |
| CO |  |  |
| NOx |  |  |
| CO2 |  |  |
| PM |  |  |

To bound the Mapped SI Engine block output, the block does not extrapolate the lookup table data.

## Virtual Calibration

If you have Model-Based Calibration Toolbox, click Calibrate Maps to virtually calibrate the 2D lookup tables using measured data. The dialog box steps through these tasks.

| Task | Description |  |
| :---: | :---: | :---: |
| Import firing data | Import this loss data from a file. For example, open <matlabroot>/ toolbox/mbc/mbctraining/SiEngineData.xlsx. <br> For more information, see "Using Data" (Model-Based Calibration Toolbox). |  |
|  | Required Data | Optional D |
|  | $\begin{array}{ll}\text { - Engine speed, } \mathrm{rpm} \\ \text { - } & \text { Engine torque, } \mathrm{N} \cdot \mathrm{m}\end{array}$ | - Air mass flow rate, kg/s <br> - Brake specific fuel consumption, $\mathrm{g} /(\mathrm{kW} \cdot \mathrm{h})$ <br> - CO2 mass flow rate, $\mathrm{kg} / \mathrm{s}$ <br> - CO mass flow rate, $\mathrm{kg} / \mathrm{s}$ <br> - Exhaust temperature, K <br> - Fuel mass flow rate, kg/s <br> - HC mass flow rate, $\mathrm{kg} / \mathrm{s}$ <br> - NOx mass flow rate, $\mathrm{kg} / \mathrm{s}$ <br> - Particulate matter mass flow rate, $\mathrm{kg} / \mathrm{s}$ |
|  | Collect firing data at steady-state operating conditions when injectors deliver the fuel. Data should cover the engine speed and torque operating range. Model-Based Calibration Toolbox uses the firing data boundary as the maximum torque. <br> To filter or edit the data, select Edit in Application. The Model-Based Calibration Toolbox Data Editor opens. |  |
| Import non-firing data | Import this non-firing data from a file. For example, open <matlabroot>/ toolbox/mbc/mbctraining/SiEngineData.xlsx. <br> - Engine speed, rpm <br> - Engine torque, $\mathrm{N} \cdot \mathrm{m}$ <br> Collect non-firing (motoring) data at steady-state operating conditions when fuel is cut off. All non-firing torque points must be less than zero. Non-firing data is a function of engine speed only. |  |
| Generate response models | For both firing and non-firing data, the Model-Based Calibration Toolbox uses test plans to fit data to Gaussian process models (GPMs). <br> To assess or adjust the response model fit, select Edit in Application. The Model-Based Calibration Toolbox Model Browser opens. For more information, see "Model Assessment" (Model-Based Calibration Toolbox). |  |
| Generate calibration | Model-Based Calibration Toolbox calibrates the firing and non-firing response models and generates calibrated tables. <br> To assess or adjust the calibration, select Edit in Application. The ModelBased Calibration Toolbox CAGE Browser opens. For more information, see "Calibration Lookup Tables" (Model-Based Calibration Toolbox). |  |
| Update block parameters | Update the block lookup table and breakpoint parameters with the calibration. |  |

## Cylinder Air Mass

The block calculates the normalized cylinder air mass using these equations.

$$
\begin{aligned}
& M_{\text {Nom }}=\frac{P_{\text {std }} V_{d}}{N_{\text {cyl }} R_{\text {air }} T_{\text {std }}} \\
& L=\frac{\left(\frac{60 s}{m i n}\right) C p s \cdot \dot{m}_{\text {air }}}{\left(\frac{1000 g}{K g}\right) N_{\text {cyl }} \cdot N \cdot M_{\text {Nom }}}
\end{aligned}
$$

The equations use these variables.
$L \quad$ Normalized cylinder air mass
$M_{\text {Nom }} \quad$ Nominal engine cylinder air mass at standard temperature and pressure, piston at bottom dead center (BDC) maximum volume, in kg
Cps Crankshaft revolutions per power stroke, rev/stroke
$P_{s t d} \quad$ Standard pressure
$T_{\text {std }} \quad$ Standard temperature
$R_{\text {air }} \quad$ Ideal gas constant for air and burned gas mixture
$V_{d} \quad$ Displaced volume
$N_{\text {cyl }} \quad$ Number of engine cylinders
$N \quad$ Engine speed
$\dot{m}_{\text {intk }} \quad$ Engine air mass flow, in $\mathrm{g} / \mathrm{s}$

## Turbocharger Lag

To model turbocharger lag, select Include turbocharger lag effect. During throttle control, the time constant models the manifold filling and emptying dynamics. When the torque request requires a turbocharger boost, the block uses a larger time constant to represent the turbocharger lag. The block uses these equations.

| Dynamic torque | $\frac{d T_{\text {brake }}}{d t}=\frac{1}{\tau_{\text {eng }}}\left(T_{\text {stdy }}-T_{\text {brake }}\right)$ |
| :--- | :---: |
| Boost time constant | $\tau_{\text {bst }}=\left\{\begin{array}{ll\|}\tau_{\text {bst, rising }} & \text { when } T_{\text {stdy }}>T_{\text {brake }} \\ \tau_{\text {bst, falling }} & \text { when } T_{\text {stdy }} \leq T_{\text {brake }}\end{array}\right.$ |
| Final time constant | $\tau_{\text {eng }}= \begin{cases}\tau_{\text {thr }} & \text { when } T_{\text {brake }}<f_{\text {bst }}(N) \\ \tau_{\text {bst }} & \text { when } T_{\text {brake }} \geq f_{\text {bst }}(N)\end{cases}$ |

The equations use these variables.

| $T_{\text {brake }}$ | Brake torque |
| :--- | :--- |
| $T_{\text {stdy }}$ | Steady-state target torque |
| $\tau_{\text {bst }}$ | Boost time constant |
| $\tau_{\text {bst,rising, }}$ | Boost rising and falling time constant, respectively |
| $\tau_{\text {bst,falling }}$ |  |


| $\tau_{\text {eng }}$ | Final time constant |
| :--- | :--- |
| $\tau_{\text {thr }}$ | Time constant during throttle control |
| $f_{\text {bst }}(N)$ | Boost torque speed line |
| $N$ | Engine speed |

## Fuel Flow

To calculate the fuel economy for high-fidelity models, the block uses the volumetric fuel flow.

$$
Q_{\text {fuel }}=\frac{\dot{m}_{\text {fuel }}}{\left(\frac{1000 \mathrm{~kg}}{\mathrm{~m}^{3}}\right) S g_{f u e l}}
$$

The equation uses these variables.

| $\dot{m}_{\text {fuel }}$ | Fuel mass flow |
| :--- | :--- |
| $S g_{\text {fuel }}$ | Specific gravity of fuel |
| $Q_{\text {fuel }}$ | Volumetric fuel flow |

## Power Accounting

For the power accounting, the block implements these equations.

| Bus Signal |  |  | Description | Equations |
| :---: | :---: | :---: | :---: | :---: |
| PwrInf 0 | PwrTrnsfrd - Power transferred between blocks <br> - Positive signals indicate flow into block <br> - Negative signals indicate flow out of block | PwrCrkshft | Crankshaft power | $-\tau_{\text {eng }} \omega$ |
|  | PwrNotTrnsfrd - Power crossing the block boundary, but not transferred | PwrFuel | Fuel input power | $\dot{m}_{\text {fuel }}$ LHV |
|  | - Positive signals indicate an input <br> - Negative signals indicate a loss | PwrLoss | Power loss | $\begin{aligned} & \tau_{\text {eng }} \omega \\ & -\dot{m}_{\text {fuel }} L H V \end{aligned}$ |
|  | PwrStored - Stored energy rate of chan <br> - Positive signals indicate an increase <br> - Negative signals indicate a decrease |  | Not used |  |

The equations use these variables.

| LHV | Fuel lower heating value |
| :--- | :--- |
| $\omega$ | Engine speed, rad/s |
| $\dot{m}_{\text {fuel }}$ | Fuel mass flow |
| $\tau_{\text {eng }}$ | Fuel mass per injection time constant |

## Ports

## Input

TrqCmd - Commanded torque
scalar
Torque, $T_{\text {cmd }}$, in $\mathrm{N} \cdot \mathrm{m}$.
EngSpd - Engine speed
scalar
Engine speed, $N$, in rpm.
EngTemp - Engine temperature
scalar
Engine temperature, $\operatorname{Temp}_{\text {Eng, }}$, in K .

## Dependencies

To enable this port, select Input engine temperature.

## Output

Info - Bus signal
bus
Bus signal containing these block calculations.

| Signal | Description | Units |
| :--- | :--- | :--- |
| IntkGassMassFlw | Engine air mass flow output | $\mathrm{kg} / \mathrm{s}$ |
| NrmlzdAirChrg | Normalized engine cylinder air mass | $\mathrm{N} / \mathrm{A}$ |
| Afr | Air-fuel ratio (AFR) | $\mathrm{N} / \mathrm{A}$ |
| FuelMassFlw | Engine fuel flow output | $\mathrm{kg} / \mathrm{s}$ |
| FuelVolFlw | Volumetric fuel flow | $\mathrm{m} / \mathrm{s}$ |
| ExhManGasTemp | Engine exhaust gas temperature | K |
| EngTrq | Engine torque output | $\mathrm{N} \cdot \mathrm{m}$ |
| EngSpd | Engine speed | rpm |
| CrkAng | Engine crankshaft absolute angle <br> $(360) C p s$ <br> $\int_{0}$ EngSpd $\frac{180}{30} d \theta$ <br> where $C p s$ is crankshaft revolutions per | degrees <br> crank <br> angle |
| power stroke. |  |  |


| Signal | Description | Units |
| :--- | :--- | :--- |
| EoHC |  | Engine out hydrocarbon emission mass <br> flow |
| EoC0 | Engine out carbon monoxide emission <br> mass flow rate | $\mathrm{kg} / \mathrm{s}$ |
| EoN0x | Engine out nitric oxide and nitrogen <br> dioxide emissions mass flow | $\mathrm{kg} / \mathrm{s}$ |
| EoC02 |  | Engine out carbon dioxide emission mass <br> flow |
| EoPM | Engine out particulate matter emission <br> mass flow | $\mathrm{kg} / \mathrm{s}$ |
| PwrInfo | PwrTrnsfrd | PwrCrkshft | Crankshaft power $\quad \mathrm{W}$.

EngTrq - Engine brake torque scalar

Engine brake torque, $T_{\text {brake }}$, in $\mathrm{N} \cdot \mathrm{m}$.

## Parameters

## Block Options

Include turbocharger lag effect - Increase time constant
off (default)

To model turbocharger lag, select Include turbocharger lag effect. During throttle control, the time constant models the manifold filling and emptying dynamics. When the torque request requires a turbocharger boost, the block uses a larger time constant to represent the turbocharger lag. The block uses these equations.

| Dynamic torque | $\frac{d T_{\text {brake }}}{d t}=\frac{1}{\tau_{\text {eng }}}\left(T_{\text {stdy }}-T_{\text {brake }}\right)$ |
| :--- | :---: |
| Boost time constant | $\tau_{\text {bst }}=\left\{\begin{array}{ll\|}\tau_{\text {bst, rising }} & \text { when } T_{\text {stdy }}>T_{\text {brake }} \\ \tau_{\text {bst, falling }} & \text { when } T_{\text {stdy }} \leq T_{\text {brake }}\end{array}\right.$ |
| Final time constant | $\tau_{\text {eng }}= \begin{cases}\tau_{\text {thr }} & \text { when } T_{\text {brake }}<f_{\text {bst }}(N) \\ \tau_{\text {bst }} & \text { when } T_{\text {brake }} \geq f_{\text {bst }}(N)\end{cases}$ |

The equations use these variables.

| $T_{\text {brake }}$ | Brake torque |
| :--- | :--- |
| $T_{\text {stdy }}$ | Steady-state target torque |
| $\tau_{\text {bst }}$ | Boost time constant |


| $\tau_{\text {bst,rising }}$ | Boost rising and falling time constant, respectively |
| :--- | :--- |
| $\tau_{\text {bst,falling }}$ |  |
| $\tau_{\text {eng }}$ | Final time constant |
| $\tau_{\text {thr }}$ | Time constant during throttle control |
| $f_{\text {bst }}(N)$ | Boost torque speed line |
| $N$ | Engine speed |
| Dependencies |  |

Selecting Include turbocharger lag effect enables these parameters:

- Boost torque line, f_tbrake_bst
- Time constant below boost line, tau_thr
- Rising torque boost time constant, tau_bst_rising
- Falling torque boost time constant, tau_bst_falling

Input engine temperature - Create input port
off (default) | on
Select this to create the EngTemp input port.
The block enables you to specify lookup tables for these engine characteristics. The lookup tables, developed with the Model-Based Calibration Toolbox, are functions of commanded torque, $T_{\text {cmd }}$, brake torque, $T_{\text {brake }}$, and engine speed, $N$. If you select Input engine temperature, the tables are also a function of engine temperature, $\mathrm{Temp}_{\text {Eng }}$.

| Table | Input Engine Temperature Parameter Setting |  |
| :--- | :--- | :--- |
|  | off | on |
| Power | $f\left(T_{\text {cmd }}, N\right)$ | $f\left(T_{\text {cmd }}, N, T e m p_{\text {Eng }}\right)$ |
| Air | $f\left(T_{\text {brake }}, N\right)$ | $f\left(T_{\text {brake }}, N, T e m p_{\text {Eng }}\right)$ |
| Fuel |  |  |
| Temperature |  |  |
| Efficiency |  |  |
| HC |  |  |
| CO |  |  |
| NOx |  |  |
| CO2 |  |  |
| PM |  |  |

## Configuration

Calibrate Maps - Calibrate tables with measured data selection

If you have Model-Based Calibration Toolbox, click Calibrate Maps to virtually calibrate the 2D lookup tables using measured data. The dialog box steps through these tasks.

| Task | Description |  |
| :---: | :---: | :---: |
| Import firing data | Import this loss data from a file. For example, open <matlabroot>/ toolbox/mbc/mbctraining/SiEngineData.xlsx. <br> For more information, see "Using Data" (Model-Based Calibration Toolbox). |  |
|  | Required Data | Optional D |
|  | $\begin{array}{ll}\text { - Engine speed, } \mathrm{rpm} \\ \text { - } & \text { Engine torque, } \mathrm{N} \cdot \mathrm{m}\end{array}$ | - Air mass flow rate, kg/s <br> - Brake specific fuel consumption, $\mathrm{g} /(\mathrm{kW} \cdot \mathrm{h})$ <br> - CO2 mass flow rate, $\mathrm{kg} / \mathrm{s}$ <br> - CO mass flow rate, $\mathrm{kg} / \mathrm{s}$ <br> - Exhaust temperature, K <br> - Fuel mass flow rate, kg/s <br> - HC mass flow rate, $\mathrm{kg} / \mathrm{s}$ <br> - NOx mass flow rate, $\mathrm{kg} / \mathrm{s}$ <br> - Particulate matter mass flow rate, $\mathrm{kg} / \mathrm{s}$ |
|  | Collect firing data at steady-state operating conditions when injectors deliver the fuel. Data should cover the engine speed and torque operating range. Model-Based Calibration Toolbox uses the firing data boundary as the maximum torque. <br> To filter or edit the data, select Edit in Application. The Model-Based Calibration Toolbox Data Editor opens. |  |
| Import non-firing data | Import this non-firing data from a file. For example, open <matlabroot>/ toolbox/mbc/mbctraining/SiEngineData.xlsx. <br> - Engine speed, rpm <br> - Engine torque, $\mathrm{N} \cdot \mathrm{m}$ <br> Collect non-firing (motoring) data at steady-state operating conditions when fuel is cut off. All non-firing torque points must be less than zero. Non-firing data is a function of engine speed only. |  |
| Generate response models | For both firing and non-firing data, the Model-Based Calibration Toolbox uses test plans to fit data to Gaussian process models (GPMs). <br> To assess or adjust the response model fit, select Edit in Application. The Model-Based Calibration Toolbox Model Browser opens. For more information, see "Model Assessment" (Model-Based Calibration Toolbox). |  |
| Generate calibration | Model-Based Calibration Toolbox calibrates the firing and non-firing response models and generates calibrated tables. <br> To assess or adjust the calibration, select Edit in Application. The ModelBased Calibration Toolbox CAGE Browser opens. For more information, see "Calibration Lookup Tables" (Model-Based Calibration Toolbox). |  |
| Update block parameters | Update the block lookup table and breakpoint parameters with the calibration. |  |

## Dependencies

To enable this parameter, clear Input engine temperature.
Breakpoints for commanded torque, f_tbrake_t_bpt - Breakpoints
1-by-M vector
Breakpoints, in $\mathrm{N} \cdot \mathrm{m}$.
Breakpoints for engine speed input, f_tbrake_n_bpt - Breakpoints
1-by-N vector
Breakpoints, in rpm.
Breakpoints for temperature input, f_tbrake_engtmp_bpt - Breakpoints
[233.15 273.15 373.15] (default) | $\overline{1}$-by-L vector
Breakpoints, in K.
Dependencies
To enable this parameter, select Input engine temperature.
Number of cylinders, NCyI - Number
4 (default) | scalar
Number of cylinders.
Crank revolutions per power stroke, Cps - Crank revolutions
2 (default) | scalar
Crank revolutions per power stroke.
Total displaced volume, Vd - Volume
0.0015 (default) | scalar

Volume displaced by engine, in $\mathrm{m}^{\wedge} 3$.
Fuel lower heating value, Lhv - Heating value
45e6 (default) | scalar
Fuel lower heating value, $L H V$, in $\mathrm{J} / \mathrm{kg}$.
Fuel specific gravity, $\mathbf{S g}$ - Specific gravity
0.745 (default) | scalar

Specific gravity of fuel, $S g_{\text {fuel }}$, dimensionless.

## Ideal gas constant air, Rair - Constant

287 (default) | scalar
Ideal gas constant of air and residual gas entering the engine intake port, in $\mathrm{J} /(\mathrm{kg} * \mathrm{~K})$.
Air standard pressure, Pstd - Pressure
101325 (default) | scalar
Standard air pressure, in Pa.

Air standard temperature, Tstd - Temperature
293. 15 (default) | scalar

Standard air temperature, in K.
Boost torque line, f_tbrake_bst - Boost lag
1-by-M vector
Boost torque line, $f_{b s t}(N)$, in $N \cdot \mathrm{~m}$.

## Dependencies

To enable this parameter, select Include turbocharger lag effect.
Time constant below boost line - Time constant below
0.2 (default) | scalar

Time constant below boost line, $\tau_{t h r}$, in s .
Dependencies
To enable this parameter, select Include turbocharger lag effect.
Rising torque boost time constant, tau_bst_rising - Rising time constant
1.5 (default) | scalar

Rising torque boost time constant, $\tau_{\text {bst,rising }}$, in s .
Dependencies
To enable this parameter, select Include turbocharger lag effect.
Falling torque boost time constant, tau_bst_falling - Falling time constant
1 (default) | scalar
Falling torque boost time constant, $\tau_{\text {bst,falling }}$, in s.
Dependencies
To enable this parameter, select Include turbocharger lag effect.

## Power

Brake torque map, f_tbrake - 2D lookup table
M-by-N matrix
The engine torque lookup table is a function of commanded engine torque and engine speed, $T=$ $f\left(T_{c m d}, N\right)$, where:

- $T$ is engine torque, in $\mathrm{N} \cdot \mathrm{m}$.
- $T_{c m d}$ is commanded engine torque, in $\mathrm{N} \cdot \mathrm{m}$.
- $\quad N$ is engine speed, in rpm.


Plot brake torque map - Plot table
button
Click to plot table.

## Dependencies

To enable this parameter, clear Input engine temperature.
Brake torque map, f_tbrake_3d - 3D lookup table
M-by-N-by-L array
The engine torque lookup table is a function of commanded engine torque, engine speed, and engine temperature, $T=f\left(T_{c m d}, N, T e m p_{\text {Eng }}\right)$, where:

- $T$ is engine torque, in $\mathrm{N} \cdot \mathrm{m}$.
- $T_{c m d}$ is commanded engine torque, in $\mathrm{N} \cdot \mathrm{m}$.
- $N$ is engine speed, in rpm.
- $\mathrm{Temp}_{\text {Eng }}$ is engine temperature, in K .


## Dependencies

To enable this parameter, select Input engine temperature.

## Air

Air mass flow map, f_air - 2D lookup table
M-by-N matrix
The engine air mass flow lookup table is a function of commanded engine torque and engine speed, $\dot{m}_{\text {intk }}=f\left(T_{\text {cmd }}, N\right)$, where:

- $\dot{m}_{\text {intk }}$ is engine air mass flow, in $\mathrm{kg} / \mathrm{s}$.
- $T_{c m d}$ is commanded engine torque, in $\mathrm{N} \cdot \mathrm{m}$.
- $N$ is engine speed, in rpm.



## Dependencies

To enable this parameter, clear Input engine temperature.
Plot air mass map - Plot table
button
Click to plot table.

## Dependencies

To enable this parameter, clear Input engine temperature.

## Air mass flow map, f_air_3d - 3D lookup table

M-by-N-by-L array
The engine air mass flow lookup table is a function of commanded engine torque, engine speed, and engine temperature, $\dot{m}_{\text {intk }}=f\left(T_{\text {cmd }}, N, T e m p_{\text {Eng }}\right)$, where:

- $\dot{m}_{\text {intk }}$ is engine air mass flow, in $\mathrm{kg} / \mathrm{s}$.
- $T_{c m d}$ is commanded engine torque, in $\mathrm{N} \cdot \mathrm{m}$.
- $N$ is engine speed, in rpm.
- $T e m p_{\text {Eng }}$ is engine temperature, in K .


## Dependencies

To enable this parameter, select Input engine temperature.

## Fuel

Fuel flow map, f_fuel - 2D lookup table
M-by-N matrix
The engine fuel mass flow lookup table is a function of commanded engine torque and engine speed, MassFlow $=f\left(T_{\text {cmd }}, N\right)$, where:

- MassFlow is engine fuel mass flow, in $\mathrm{kg} / \mathrm{s}$.
- $T_{\text {cmd }}$ is commanded engine torque, in $\mathrm{N} \cdot \mathrm{m}$.
- $N$ is engine speed, in rpm.



## Dependencies

To enable this parameter, clear Input engine temperature.
Plot fuel flow map - Plot table
button
Click to plot table.

## Dependencies

To enable this parameter, clear Input engine temperature.
Fuel flow map, f_fuel_3d - 3D lookup table

## M-by-N-by-L array

The engine fuel mass flow lookup table is a function of commanded engine torque, engine speed, and engine temperature, MassFlow $=f\left(T_{\text {cmd }}, N, T e m p_{\text {Eng }}\right)$, where:

- MassFlow is engine fuel mass flow, in $\mathrm{kg} / \mathrm{s}$.
- $T_{c m d}$ is commanded engine torque, in $\mathrm{N} \cdot \mathrm{m}$.
- $N$ is engine speed, in rpm.
- Temp $p_{\text {Eng }}$ is engine temperature, in K .


## Dependencies

To enable this parameter, select Input engine temperature.

## Temperature

Exhaust temperature map, f_texh - 2D lookup table
M-by-N matrix
The engine exhaust temperature lookup table is a function of commanded engine torque and engine speed, $T_{\text {exh }}=f\left(T_{c m d}, N\right)$, where:

- $T_{\text {exh }}$ is exhaust temperature, in K.
- $T_{c m d}$ is commanded engine torque, in $\mathrm{N} \cdot \mathrm{m}$.
- $N$ is engine speed, in rpm.



## Dependencies

To enable this parameter, clear Input engine temperature.

## Plot exhaust temperature map - Plot table

## button

Click to plot table.

## Dependencies

To enable this parameter, clear Input engine temperature.
Exhaust temperature map, f_texh_3d - 3D lookup table array

The engine exhaust temperature lookup table is a function of commanded engine torque, engine speed, and engine temperature, $T_{\text {exh }}=f\left(T_{\text {cmd }}, N, T e m p_{\text {Eng }}\right)$, where:

- $T_{\text {exh }}$ is exhaust temperature, in $K$.
- $T_{c m d}$ is commanded engine torque, in $\mathrm{N} \cdot \mathrm{m}$.
- $N$ is engine speed, in rpm.
- $T e m p_{\text {Eng }}$ is engine temperature, in K .


## Dependencies

To enable this parameter, select Input engine temperature.

## Efficiency

BSFC map, f_eff - 2D lookup table
M-by-N-by-L array
The brake-specific fuel consumption (BSFC) efficiency is a function of commanded engine torque and engine speed, $B S F C=f\left(T_{\text {cmd }}, N\right)$, where:

- BSFC is BSFC, in $\mathrm{g} / \mathrm{kWh}$.
- $T_{c m d}$ is commanded engine torque, in $\mathrm{N} \cdot \mathrm{m}$.
- $N$ is engine speed, in rpm.



## Dependencies

To enable this parameter, clear Input engine temperature.
Plot BSFC map - Plot table
button
Click to plot table.

## Dependencies

To enable this parameter, clear Input engine temperature.
BSFC map, f_eff_3d - 3D lookup table

## M-by-N-by-L array

The brake-specific fuel consumption (BSFC) efficiency is a function of commanded engine torque, engine speed, and engine temperature, $B S F C=f\left(T_{c m d}, N, T e m p_{\text {Eng }}\right)$, where:

- $B S F C$ is BSFC, in $\mathrm{g} / \mathrm{kWh}$.
- $T_{c m d}$ is commanded engine torque, in $\mathrm{N} \cdot \mathrm{m}$.
- $N$ is engine speed, in rpm.
- $T_{e m p}^{\text {Eng }}$ is engine temperature, in K .


## Dependencies

To enable this parameter, select Input engine temperature.
HC
EO HC map, f_hc - 2D lookup table

## M-by-N matrix

The engine-out hydrocarbon emissions are a function of commanded engine torque and engine speed, EO HC $=f\left(T_{\text {cmd }}, N\right)$, where:

- EO HC is engine-out hydrocarbon emissions, in $\mathrm{kg} / \mathrm{s}$.
- $T_{c m d}$ is commanded engine torque, in $\mathrm{N} \cdot \mathrm{m}$.
- $N$ is engine speed, in rpm.



## Dependencies

To enable this parameter, clear Input engine temperature.

## Plot EO HC map - Plot table

button
Click to plot table.

## Dependencies

To enable this parameter, clear Input engine temperature.
EO HC map, f_hc_3d - 3D lookup table
M-by-N-by-L array
The engine-out hydrocarbon emissions are a function of commanded engine torque, engine speed, and engine temperature, EO HC $=f\left(T_{\text {cmd }}, N, T e m p_{\text {Eng }}\right)$, where:

- EO HC is engine-out hydrocarbon emissions, in $\mathrm{kg} / \mathrm{s}$.
- $T_{\text {cmd }}$ is commanded engine torque, in $\mathrm{N} \cdot \mathrm{m}$.
- $N$ is engine speed, in rpm.
- $T e m p_{\text {Eng }}$ is engine temperature, in K .


## Dependencies

To enable this parameter, select Input engine temperature.
CO
EO CO map, f_co - 2D lookup table
M-by-N matrix
The engine-out carbon monoxide emissions are a function of commanded engine torque and engine speed, $E O C O=f\left(T_{c m d}, N\right)$, where:

- EO CO is engine-out carbon monoxide emissions, in $\mathrm{kg} / \mathrm{s}$.
- $T_{c m d}$ is commanded engine torque, in $\mathrm{N} \cdot \mathrm{m}$.
- $N$ is engine speed, in rpm.



## Dependencies

To enable this parameter, clear Input engine temperature.
Plot EO CO map - Plot table
button
Click to plot table.

## Dependencies

To enable this parameter, clear Input engine temperature.
EO HC map, f_hc_3d - 3D lookup table
M-by-N-by-L array
The engine-out hydrocarbon emissions are a function of commanded engine torque, engine speed, and engine temperature, EO HC $=f\left(T_{c m d}, N, T e m p_{\text {Eng }}\right)$, where:

- EO HC is engine-out hydrocarbon emissions, in $\mathrm{kg} / \mathrm{s}$.
- $T_{c m d}$ is commanded engine torque, in $\mathrm{N} \cdot \mathrm{m}$.
- $N$ is engine speed, in rpm.
- $T e m p_{\text {Eng }}$ is engine temperature, in K .


## Dependencies

To enable this parameter, select Input engine temperature.

## NOx

EO NOx map, f_nox - 2D lookup table
M-by-N matrix
The engine-out nitric oxide and nitrogen dioxide emissions are a function of commanded engine torque and engine speed, $E O N O x=f\left(T_{\text {cmd }}, N\right)$, where:

- EO NOx is engine-out nitric oxide and nitrogen dioxide emissions, in kg/s.
- $T_{c m d}$ is commanded engine torque, in $\mathrm{N} \cdot \mathrm{m}$.
- $N$ is engine speed, in rpm.



## Dependencies

To enable this parameter, clear Input engine temperature.
Plot EO NOx map - Plot table
button
Click to plot table.

## Dependencies

To enable this parameter, clear Input engine temperature.
EO NOx map, f_nox_3d - 3D lookup table
M-by-N-by-L array
The engine-out nitric oxide and nitrogen dioxide emissions are a function of commanded engine torque, engine speed, and engine temperature, EO NOx $=f\left(T_{c m d}, N, T e m p_{E n g}\right)$, where:

- EO NOX is engine-out nitric oxide and nitrogen dioxide emissions, in $\mathrm{kg} / \mathrm{s}$.
- $T_{\text {cmd }}$ is commanded engine torque, in $\mathrm{N} \cdot \mathrm{m}$.
- $N$ is engine speed, in rpm.
- $T e m p_{\text {Eng }}$ is engine temperature, in K .


## Dependencies

To enable this parameter, select Input engine temperature.
CO2
EO CO2 map, f_co2 - 2D lookup table
M-by-N matrix
The engine-out carbon dioxide emissions are a function of commanded engine torque and engine speed, $E O$ CO2 $=f\left(T_{\text {cmd }}, N\right)$, where:

- EO CO2 is engine-out carbon dioxide emissions, in $\mathrm{kg} / \mathrm{s}$.
- $T_{c m d}$ is commanded engine torque, in $\mathrm{N} \cdot \mathrm{m}$.
- $N$ is engine speed, in rpm.



## Dependencies

To enable this parameter, clear Input engine temperature.
Plot CO2 map - Plot table
button
Click to plot table.

## Dependencies

To enable this parameter, clear Input engine temperature.

## EO CO2 map, f_co2_3d - 3D lookup table

## M-by-N-by-L array

The engine-out carbon dioxide emissions are a function of commanded engine torque, engine speed, and engine temperature, EO CO2 $=f\left(T_{c m d}, N, T e m p_{\text {Eng }}\right)$, where:

- EO CO2 is engine-out carbon dioxide emissions, in $\mathrm{kg} / \mathrm{s}$.
- $T_{c m d}$ is commanded engine torque, in $\mathrm{N} \cdot \mathrm{m}$.
- $N$ is engine speed, in rpm.
- $T e m p_{\text {Eng }}$ is engine temperature, in K.


## Dependencies

To enable this parameter, select Input engine temperature.

## PM

EO PM map, f_pm - 2D lookup table
M-by-N matrix
The engine-out particulate matter emissions are a function of commanded engine torque and engine speed, where:

- EO PM is engine-out PM emissions, in kg/s.
- $T_{c m d}$ is commanded engine torque, in $\mathrm{N} \cdot \mathrm{m}$.
- $N$ is engine speed, in rpm.


## Dependencies

To enable this parameter, clear Input engine temperature.

Plot EO PM map - Plot table

## button

Click to plot table.

## Dependencies

To enable this parameter, clear Input engine temperature.
EO PM map, f_pm_3d - 3D lookup table
M-by-N-by-L array
The engine-out particulate matter emissions are a function of commanded engine torque, engine speed, and engine temperature, where:

- EO PM is engine-out PM emissions, in $\mathrm{kg} / \mathrm{s}$.
- $T_{c m d}$ is commanded engine torque, in $\mathrm{N} \cdot \mathrm{m}$.
- $\quad N$ is engine speed, in rpm.
- $T e m p_{\text {Eng }}$ is engine temperature, in K .


## Dependencies

To enable this parameter, select Input engine temperature.

## Version History

Introduced in R2017a

## Extended Capabilities

C/C++ Code Generation
Generate C and C++ code using Simulink ${ }^{\circledR}$ Coder ${ }^{\mathrm{TM}}$.

## See Also

Mapped Motor | Mapped CI Engine
Topics
"Engine Calibration Maps"
"Model-Based Calibration Toolbox"

## Vehicle Dynamics Blocks

## Vehicle Body Total Road Load

Vehicle motion using coast-down testing coefficients


## Libraries:

Powertrain Blockset / Vehicle Dynamics
Vehicle Dynamics Blockset / Vehicle Body

## Description

The Vehicle Body Total Road Load block implements a one degree-of-freedom (1DOF) rigid vehicle model using coast-down testing coefficients. You can use this block in a vehicle model to represent the load that the driveline and chassis applies to a transmission or engine. It is suitable for systemlevel performance, component sizing, fuel economy, or drive cycle tracking studies. The block calculates the dynamic powertrain load with minimal parameterization or computational cost.

You can configure the block for kinematic, force, or total power input.

- Kinematic - Block uses the vehicle longitudinal velocity and acceleration to calculate the tractive force and power.
- Force - Block uses the tractive force to calculate the vehicle longitudinal displacement and velocity.
- Power - Block uses the engine or transmission power to calculate the vehicle longitudinal displacement and velocity.


## Dynamics

To calculate the total road load acting on the vehicle, the block implements this equation.

$$
F_{\text {road }}=a+b \dot{x}+c \dot{x}^{2}+m g \sin (\theta)
$$

To determine the coefficients $a, b$, and $c$, you can use a test procedure similar to the one described in Road Load Measurement and Dynamometer Simulation Using Coastdown Techniques. You can also use Simulink ${ }^{\circledR}$ Design Optimization ${ }^{\text {TM }}$ to fit the coefficients to measured data.

To calculate the vehicle motion, the block uses Newton's law for rigid bodies.

$$
F_{\text {total }}=m \ddot{x}+F_{\text {road }}
$$

Total power input is a product of the total force and longitudinal velocity. Power due to road and gravitational forces is a product of the road force and longitudinal velocity.

$$
\begin{aligned}
& P_{\text {total }}=F_{\text {total }} \dot{x} \\
& P_{\text {road }}=F_{\text {road }} \dot{x}
\end{aligned}
$$

## Power Accounting

For the power accounting, the block implements these equations.

| Bus Signal |  |  | Description | Variable | Equations |
| :---: | :---: | :---: | :---: | :---: | :---: |
| PwrInfo | PwrTrnsfrd - Power transferred between blocks <br> - Positive signals indicate flow into block <br> - Negative signals indicate flow out of block | $\begin{aligned} & \text { PwrFxE } \\ & \text { xt } \end{aligned}$ | Externally applied force power | $P_{\text {FXEXt }}$ | $P_{\text {FxExt }}=F_{\text {total }} \dot{x}$ |
|  | PwrNotTrnsfrd - Power crossing the block boundary, but not transferred <br> - Positive signals indicate an input <br> - Negative signals indicate a loss | $\begin{aligned} & \text { PwrFxD } \\ & \text { rag } \end{aligned}$ | Drag force power | $P_{D}$ | $P_{d}=-\left(a+b \dot{x}+c \dot{x}^{2}\right) \dot{x}$ |
|  | PwrStored - Stored energy rate of change <br> - Positive signals indicate an increase | wrStor edGrvt Y | Rate change in gravitational potential energy | $P_{g}$ | $P_{g}=-m g \dot{Z}$ |
|  | - Negative signals indicate a decrease | PwrSto redxdo t | Rate in change of longitudinal kinetic energy | $P_{\text {xdot }}$ | $P_{\dot{\chi}}=m \ddot{\chi} \dot{\chi}$ |

The equations use these variables.

| $a$ | Steady-state rolling resistance coefficient |
| :--- | :--- |
| $b$ | Viscous driveline and rolling resistance coefficient |
| $c$ | Aerodynamic drag coefficient |
| $g$ | Gravitational acceleration |
| $x$ | Vehicle longitudinal displacement with respect to ground, in the vehicle-fixed |
| $\dot{x}$ | frame |
| $\ddot{\chi}$ | Vehicle longitudinal velocity with respect to ground, in the vehicle-fixed frame |
| $m$ | Vehicle longitudinal acceleration with respect to ground, vehicle-fixed frame |
| $\Theta$ | Vehicle body mass |
| $F_{\text {total }}$ | Road grade angle |
| $F_{\text {road }}$ | Total force acting on vehicle |
| $P_{\text {total }}$ | Resistive road load due to losses and gravitational load |
| $P_{\text {road }}$ | Total tractive input power |
| $\dot{Z}$ | Total power due to losses and gravitational load |

## Ports

## Input

xdot - Vehicle longitudinal velocity
scalar
Vehicle total longitudinal velocity, $\dot{x}$, in $\mathrm{m} / \mathrm{s}$.

## Dependencies

To enable this port, for the Input Mode parameter, select Kinematic.
xddot - Vehicle longitudinal acceleration
scalar
Vehicle total longitudinal acceleration, $\ddot{x}$, in $\mathrm{m} / \mathrm{s}^{\wedge} 2$.

## Dependencies

To enable this port, for the Input Mode parameter, select Kinematic.
PwrTot - Tractive input power
scalar
Tractive input power, $P_{\text {total }}$, in W.

## Dependencies

To enable this port, for the Input Mode parameter, select Power.
ForceTot - Tractive input force
scalar
Tractive input force, $F_{\text {total }}$, in N .

## Dependencies

To enable this port, for the Input Mode parameter, select Force.
Grade - Road grade angle
scalar
Road grade angle, $\Theta$, in deg.

## Output

Info - Bus signal
bus
Bus signal containing these block calculations.

| Signal |  | Description | Value | Units |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| In <br> er | Cg | Disp | X | Vehicle CG displacement along earth- <br> fixed X-axis | Computed |


| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \mathrm{tF} \\ & \mathrm{rm} \end{aligned}$ |  |  | Y | Vehicle CG displacement along earthfixed $Y$-axis | 0 | m |
|  |  |  | Z | Vehicle CG displacement along earthfixed Z-axis | Computed | m |
|  |  | Vel | Xdot | Vehicle CG velocity along earth-fixed X-axis | Computed | m/s |
|  |  |  | Ydot | Vehicle CG velocity along earth-fixed Y-axis | 0 | m/s |
|  |  |  | Zdot | Vehicle CG velocity along earth-fixed Z-axis | Computed | m/s |
|  |  | Ang | phi | Rotation of vehicle-fixed frame about the earth-fixed X-axis (roll) | 0 | rad |
|  |  |  | theta | Rotation of vehicle-fixed frame about the earth-fixed Y -axis (pitch) | Computed | rad |
|  |  |  | psi | Rotation of vehicle-fixed frame about the earth-fixed Z-axis (yaw) | 0 | rad |
| $\begin{aligned} & \mathrm{Bd} \\ & \mathrm{yF} \\ & \mathrm{rm} \end{aligned}$ | Cg | Disp | x | Vehicle CG displacement along the vehicle-fixed x-axis | Computed | m |
|  |  |  | y | Vehicle CG displacement along the vehicle-fixed $y$-axis | 0 | m |
|  |  |  | z | Vehicle CG displacement along the vehicle-fixed $z$-axis | 0 | m |
|  |  | Vel | xdot | Vehicle CG velocity along the vehiclefixed $x$-axis | Computed | m/s |
|  |  |  | ydot | Vehicle CG velocity along the vehiclefixed y-axis | 0 | m/s |
|  |  |  | zdot | Vehicle CG velocity along the vehiclefixed $z$-axis | 0 | m/s |
|  |  | Acc | ax | Vehicle CG acceleration along the vehicle-fixed $x$-axis | Computed | gn |
|  |  |  | ay | Vehicle CG acceleration along the vehicle-fixed $y$-axis | 0 | gn |
|  |  |  | az | Vehicle CG acceleration along the vehicle-fixed $z$-axis | 0 | gn |
|  | Forc es | Body | Fx | Net force on vehicle CG along the vehicle-fixed x -axis | Computed | N |
|  |  |  | Fy | Net force on vehicle CG along the vehicle-fixed $y$-axis | 0 | N |
|  |  |  | Fz | Net force on vehicle CG along the vehicle-fixed $z$-axis | 0 | N |
|  |  | Ext | FX | External force on vehicle CG along the vehicle-fixed $x$-axis | Computed | N |


| Signal |  | Description | Value | Units |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  |  |  | Fy | External force on vehicle CG along the <br> vehicle-fixed y-axis | 0 |
|  |  |  | Fz | External force on vehicle CG along the <br> vehicle-fixed z-axis | 0 |

xdot - Vehicle longitudinal velocity
scalar
Vehicle total longitudinal velocity, $\dot{x}$, in $\mathrm{m} / \mathrm{s}$.

## Dependencies

To enable this port, for the Input Mode parameter, select Power or Force.
ForceTot - Tractive input force
scalar
Tractive input force, $F_{\text {total }}$, in N .

## Dependencies

To enable this port, for the Input Mode parameter, select Kinematic.

## Parameters

Input Mode - Specify input mode
Kinematic (default) | Force | Power
Specify the input type.

- Kinematic - Block uses the vehicle longitudinal velocity and acceleration to calculate the tractive force and power. Use this configuration for powertrain, driveline, and braking system design, or component sizing.
- Force - Block uses the tractive force to calculate the vehicle longitudinal displacement and velocity. Use this configuration for system-level performance, fuel economy, or drive cycle tracking studies.
- Power - Block uses the engine or transmission power to calculate the vehicle longitudinal displacement and velocity. Use this configuration for system-level performance, fuel economy, or drive cycle tracking studies.


## Dependencies

This table summarizes the port and input mode configurations.

| Input Mode | Creates Ports |
| :--- | :--- |
| Kinematic | xdot |
|  | xddot |
| Force | Force |
| Power | Power |

Mass - Vehicle body mass
1200 (default) | scalar
Vehicle body mass, $m$, in kg .
Rolling resistance coefficient, a-Rolling
196 (default) | scalar
Steady-state rolling resistance coefficient, $a$, in N .
Rolling and driveline resistance coefficient, $\mathbf{b}$ - Rolling and driveline
2.232 (default) | scalar

Viscous driveline and rolling resistance coefficient, $b$, in $\mathrm{N}^{*} \mathrm{~s} / \mathrm{m}$.

## Aerodynamic drag coefficient, c - Drag

0.389 (default) | scalar

Aerodynamic drag coefficient, $c$, in $\mathrm{N} \cdot \mathrm{s}^{\wedge} 2 / \mathrm{m}$.
Gravitational acceleration, g - Gravity
9.81 (default) | scalar

Gravitational acceleration, $g$, in $\mathrm{m} / \mathrm{s}^{\wedge} 2$.

Initial position, x_o - Position
0 (default) | scalar
Vehicle longitudinal initial position, in $m$.
Initial velocity, xdot_o - Velocity
0 (default) | scalar
Vehicle longitudinal initial velocity with respect to ground, in m/s.

## Version History

Introduced in R2017a

## References

[1] Gillespie, Thomas. Fundamentals of Vehicle Dynamics. Warrendale, PA: Society of Automotive Engineers (SAE), 1992.
[2] Light Duty Vehicle Performance And Economy Measure Committee. Road Load Measurement and Dynamometer Simulation Using Coastdown Techniques. Standard J1263_201003. SAE International, March 2010.

## Extended Capabilities

C/C++ Code Generation
Generate C and $\mathrm{C}++$ code using Simulink ${ }_{\circledR}$ Coder $^{\mathrm{TM}}$.

## See Also

Drive Cycle Source | Vehicle Body 1DOF Longitudinal | Vehicle Body 3DOF Longitudinal
Topics
"Coordinate Systems in Vehicle Dynamics Blockset"

## Vehicle Body 1DOF Longitudinal

Two-axle vehicle in forward and reverse motion


## Libraries:

Powertrain Blockset / Vehicle Dynamics
Vehicle Dynamics Blockset / Vehicle Body

## Description

The Vehicle Body 1DOF Longitudinal block implements a one degree-of-freedom (1DOF) rigid vehicle body with constant mass undergoing longitudinal (that is, forward and reverse) motion. Use the block:

- In powertrain and fuel economy studies to represent the vehicle inertial and drag loads when weight transfer from vertical and pitch motions are negligible.
- To determine the engine torque and power required for the vehicle to follow a specified drive cycle.

You can select block options to create input ports for external forces, moments, air temperature, and wind speed.

| Block Option <br> Setting | External Input <br> Ports | Description |
| :--- | :--- | :--- |
| External forces | FExt | External force applied to vehicle CG in the vehicle-fixed frame. |
| External <br> moments | MExt | External moment about vehicle CG in the vehicle-fixed frame. |
| Air <br> temperature | AirTemp | Ambient air temperature. Consider this option if you want to <br> vary the temperature during run-time. |
| Wind $\mathbf{X , Y , Z}$ | WindXYZ | Wind speed along earth-fixed $X$-, $Y$-, and $Z$-axes. <br> If you do not select this option, the block implements input port <br> WindX - Longitudinal wind speed along the earth-fixed $X$-axis. |

## Vehicle Body Model

The vehicle axles are parallel and form a plane. The longitudinal direction lies in this plane and is perpendicular to the axles. If the vehicle is traveling on an inclined slope, the normal direction is not parallel to gravity but is always perpendicular to the axle-longitudinal plane.

The block uses the net effect of all the forces and torques acting on it to determine the vehicle motion. The longitudinal tire forces push the vehicle forward or backward. The weight of the vehicle acts through its center of gravity (CG). The grade angle changes the direction of the resolved gravitational force acting on the vehicle CG. Similarly, the block resolves the resistive aerodynamic drag force on the vehicle CM.


The Vehicle Body 1DOF Longitudinal block implements these equations.

$$
\begin{aligned}
& F_{b}=m \ddot{x} \\
& F_{b}=F_{\chi F}+F_{\chi R}-F_{d, x}+F_{e x t, x}-m g \sin \gamma
\end{aligned}
$$

Zero normal acceleration and zero pitch torque determine the normal force on each front and rear axles.

$$
\begin{aligned}
& F_{z F}=\frac{-M_{e x t, y}-M_{d, y}+b\left(F_{d, z}+F_{e x t, z}+m g \cos \gamma\right)-h\left(-F_{e x t, x}+F_{d, x}+m g \sin \gamma+m \ddot{x}\right)}{N_{F}(a+b)} \\
& F_{z R}=\frac{M_{e x t, y}+M_{d, y}+a\left(F_{d, z}+F_{e x t, z}+m g \cos \gamma\right)+h\left(-F_{e x t, x}+F_{d, x}+m g \sin \gamma+m \ddot{x}\right)}{N_{R}(a+b)}
\end{aligned}
$$

The wheel normal forces satisfy this equation.

$$
N_{F} F_{z F}+N_{R} F_{z R}-F_{e x t, z}=m g \cos \gamma
$$

## Wind and Drag Forces

The block subtracts the wind speeds from the vehicle velocity components to obtain a net relative airspeed. To calculate the drag force and moments acting on the vehicle, the block uses the net relative airspeed.

$$
\begin{aligned}
& F_{d, x}=\frac{1}{2 T R} C_{d} A_{f} P_{a b s}{ }^{\dot{X}} \\
& F_{d, z}=\frac{1}{2 T R} C_{l} A_{f} P_{a b s}{ }^{\dot{x}} \\
& M_{d, y}=\frac{1}{2 T R} C_{p m} A_{f} P_{a b s}\left(^{\dot{x}}(a+b)\right.
\end{aligned}
$$

By default, to calculate the wind speed along the vehicle-fixed $x$-axis, the block uses the longitudinal wind speed along the earth-fixed $X$-axis. If you select WindX,Y,Z, the block uses the wind speed along the earth-fixed $X$-, $Y$-, $Z$-axes.

## Power Accounting

For the power accounting, the block implements these equations.

| Bus Signal |  |  | Description | Equations |
| :---: | :---: | :---: | :---: | :---: |
| PwrInf 0 | PwrTrnsfrd Power transferred between blocks | PwrFxExt | Externally applied force power | $P_{\text {FxExt }}=F_{\chi E x t} \dot{\chi}$ |
|  | between blocks <br> - Positive signals indicate flow | PwrFwFx | Longitudinal force power applied at the front axle | $P_{F w F X}=F_{w F \bar{X}}$ |
|  | into block <br> - Negative signals indicate flow out of block | PwrFwRx | Longitudinal force power applied at the rear axle | $P_{F w R \chi}=F_{w R} \dot{X}$ |
|  | PwrNotTrnsfrd Power crossing the block boundary, but not transferred <br> - Positive signals indicate an input <br> - Negative signals indicate a loss | PwrFxDrag | Drag force power | $P_{d}=-\frac{0.5 C_{d} A_{f} P_{a b s}\left(\dot{x}^{2}-w_{x}\right)^{2}}{287.058 T} \dot{x}$ |
|  | PwrStored Stored energy rate of change | wrStoredGrvty | Rate change in gravitational potential energy | $P_{g}=-m g \dot{Z}$ |
|  | - Positive signals indicate an increase <br> - Negative signals indicate a decrease | PwrStoredxdot | Rate in change of longitudinal kinetic energy | $P_{\dot{\chi}}=m \ddot{x} \dot{\chi}$ |

The equations use these variables.
$F_{x f}, F_{x r} \quad$ Longitudinal forces on each wheel at the front and rear ground contact points, respectively

| $F_{z f}, F_{z r}$ | Normal load forces on each wheel at the front and rear ground contact points, respectively |
| :---: | :---: |
| $F_{w F}, F_{w R}$ | Longitudinal force on front and rear axles along vehicle-fixed $x$-axis |
| $F_{\chi E x t}, F_{w R}$ | External force along the vehicle-fixed $x$-axis |
| $F_{d, \chi}, F_{d, z}$ | Longitudinal and normal drag force on vehicle CG |
| $M_{d, y}$ | Torque due to drag on vehicle about the vehicle-fixed $y$-axis |
| $F_{d}$ | Aerodynamic drag force |
| $V_{\chi}$ | Velocity of the vehicle. When $V_{x}>0$, the vehicle moves forward. When $V_{x}<0$, the vehicle moves backward. |
| $N_{f}, N_{r}$ | Number of wheels on front and rear axle, respectively |
| $\gamma$ | Angle of road grade |
| m | Vehicle body mass |
| $a, b$ | Distance of front and rear axles, respectively, from the normal projection point of vehicle CG onto the common axle plane |
| h | Height of vehicle CG above the axle plane |
| $C_{\text {d }}$ | Frontal air drag coefficient |
| $A_{f}$ | Frontal area |
| $P_{a b s}$ | Absolute pressure |
| $\rho$ | Mass density of air |
| $x, \dot{\chi}, \ddot{\chi}$ | Vehicle longitudinal position, velocity, and acceleration along the vehicle-fixed $x$ axis |
| $w_{x}$ | Wind speed along the vehicle-fixed $x$-axis |
| $\dot{Z}$ | Vehicle vertical velocity along the vehicle-fixed $z$-axis |

## Limitations

The Vehicle Body 1DOF Longitudinal block lets you model only longitudinal dynamics, parallel to the ground and oriented along the direction of motion. The vehicle is assumed to be in pitch and normal equilibrium. The block does not model pitch or vertical movement. To model a vehicle with three degrees-of-freedom (DOF), use the Vehicle Body 3DOF Longitudinal.

## Ports

Input
FExt - External force on vehicle CG
array
External forces applied to vehicle CG, $F_{\text {xext }}, F_{\text {yext }}, F_{\text {zext }}$, in vehicle-fixed frame, in N. Signal vector dimensions are [ $1 \times 3$ ] or [3x1].

## Dependencies

To enable this port, select External forces.

MExt - External moment about vehicle CG
array
External moment about vehicle CG, $M_{x}, M_{y}, M_{z}$, in the vehicle-fixed frame, in $\mathrm{N} \cdot \mathrm{m}$. Signal vector dimensions are [1×3] or [3×1].

Dependencies
To enable this port, select External moments.
FwF - Total longitudinal force on front axle scalar

Longitudinal force on the front axle, $F_{x f}$, along vehicle-fixed x-axis, in N .
FwR - Total longitudinal force on rear axle
scalar
Longitudinal force on the rear axle, $F w_{R}$, along vehicle-fixed x-axis, in N.
Grade - Road grade angle scalar

Road grade angle, $\gamma$, in deg.
WindX - Longitudinal wind speed
scalar
Longitudinal wind speed, $W_{w}$, along earth-fixed X-axis, in m/s.

## Dependencies

To enable this port, clear Wind $X, Y, Z$ components.
WindXYZ - Wind speed
array
Wind speed, $W_{w}, W_{w Y}, W_{w Z}$ along inertial $X$-, $Y$-, and $Z$-axes, in $\mathrm{m} / \mathrm{s}$. Signal vector dimensions are [1×3] or [3x1].

## Dependencies

To enable this port, select Wind $\mathbf{X}, \mathbf{Y}, \mathbf{Z}$ components.
AirTemp - Ambient air temperature
scalar
Ambient air temperature, $T_{\text {air }}$, in K . Considering this option if you want to vary the temperature during run-time.

## Dependencies

To enable this port, select Air temperature.

## Output

Info - Bus signal
bus

Bus signal containing these block values.

| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| InertFrm | Cg | Disp | X | Vehicle CG displacement along earth-fixed X -axis | Computed | m |
|  |  |  | Y | Vehicle CG displacement along earth-fixed $Y$-axis | 0 | m |
|  |  |  | Z | Vehicle CG displacement along earth-fixed Z-axis | Computed | m |
|  |  | Vel | Xdot | Vehicle CG velocity along earth-fixed X-axis | Computed | m/s |
|  |  |  | Ydot | Vehicle CG velocity along earth-fixed $Y$-axis | 0 | m/s |
|  |  |  | Zdot | Vehicle CG velocity along earth-fixed Z-axis | Computed | m/s |
|  |  | Ang | phi | Rotation of vehicle-fixed frame about the earth-fixed X-axis (roll) | 0 | rad |
|  |  |  | theta | Rotation of vehicle-fixed frame about the earth-fixed Y -axis (pitch) | Computed (input grade angle) | rad |
|  |  |  | psi | Rotation of vehicle-fixed frame about the earth-fixed Z-axis (yaw) | 0 | rad |
|  | FrntAxl | Disp | X | Front axle displacement along the earth-fixed X -axis | Computed | m |
|  |  |  | Y | Front axle displacement along the earth-fixed Y -axis | 0 | m |
|  |  |  | Z | Front axle displacement along the earth-fixed Z-axis | Computed | m |
|  |  | Vel | Xdot | Front axle velocity along the earth-fixed X -axis | Computed | m/s |
|  |  |  | Ydot | Front axle velocity along the earth-fixed Y -axis | 0 | m/s |
|  |  |  | Zdot | Front axle velocity along the earth-fixed Z-axis | Computed | m/s |
|  | RearAxl | Disp | X | Rear axle displacement along the earth-fixed X-axis | Computed | m |
|  |  |  | Y | Rear axle displacement along the earth-fixed $Y$-axis | 0 | m |
|  |  |  | Z | Rear axle displacement along the earth-fixed Z-axis | Computed | m |





| Signal |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Fz | External moment on vehicle CG about the vehicle-fixed z-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
| FrntAxl | Disp | x | Front axle displacement along the vehicle-fixed x axis | Computed | m |
|  |  | y | Front axle displacement along the vehicle-fixed $y$ axis | 0 | m |
|  |  | z | Front axle displacement along the vehicle-fixed $z$ axis | Computed | m |
|  | Vel | xdot | Front axle velocity along the vehicle-fixed $x$-axis | Computed | m/s |
|  |  | ydot | Front axle velocity along the vehicle-fixed $y$-axis | 0 | m/s |
|  |  | zdot | Front axle velocity along the vehicle-fixed $z$-axis | Computed | m/s |
|  | Steer | WhlAngFL | Front left wheel steering angle | Computed | rad |
|  |  | WhlAngFR | Front right wheel steering angle | Computed | rad |
| RearAxl | Disp | x | Rear axle displacement along the vehicle-fixed $x$ axis | Computed | m |
|  |  | y | Rear axle displacement along the vehicle-fixed $y$ axis | 0 | m |
|  |  | z | Rear axle displacement along the vehicle-fixed z axis | Computed | m |
|  | Vel | xdot | Rear axle velocity along the vehicle-fixed x-axis | Computed | m/s |
|  |  | ydot | Rear axle velocity along the vehicle-fixed y-axis | 0 | m/s |
|  |  | zdot | Rear axle velocity along the vehicle-fixed $z$-axis | Computed | m/s |
|  | Steer | WhlAngRL | Rear left wheel steering angle | Computed | rad |
|  |  | WhlAngRR | Rear right wheel steering angle | Computed | rad |
| Pwr | PwrExt |  | Applied external power | Computed | W |
|  | Drag |  | Power loss due to drag | Computed | W |


| Signal |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: |
| PwrInfo | PwrTrns frd | PwrFxExt | Externally applied force power | Computed | W |
|  |  | PwrFwFx | Longitudinal force power applied at the front axle | Computed | W |
|  |  | PwrFwRx | Longitudinal force power applied at the rear axle | Computed | W |
|  | PwrNotT rnsfrd | PwrFxDrag | Drag force power | Computed | W |
|  | PwrStor ed | wrStoredGrvty | Rate change in gravitational potential energy | Computed | W |
|  |  | PwrStoredxdot | Rate in change of longitudinal kinetic energy | Computed | W |

xdot - Vehicle body longitudinal velocity
scalar
Vehicle body longitudinal velocity along the vehicle-fixed reference frame $x$-axis, in $m / s$.
FzF - Front axle normal force
scalar
Normal load force on the front axle, $F_{z f}$, along vehicle-fixed z-axis, in N .
FzR - Rear axle normal force
scalar
Normal force on rear axle, $F_{z r}$, along the vehicle-fixed z-axis, in N .

## Parameters

## Options

External forces - FExt input port
off (default) | on
Specify to create input port FExt.
External moments - MExt input port
off (default) |on
Specify to create input port MExt.
Air temperature - AirTemp input port
off (default) |on
Specify to create input port AirTemp.
Wind $\mathbf{X}, \mathbf{Y}, \mathbf{Z}$ components - WindXYZ input port
off (default) |on

Specify to create input port WindXYZ.

## Longitudinal

Number of wheels on front axle, NF - Front wheel count
2 (default) | scalar
Number of wheels on front axle, $N_{F}$. The value is dimensionless.
Number of wheels on rear axle, NR - Rear wheel count
2 (default) | scalar
Number of wheels on rear axle, $N_{R}$. The value is dimensionless.
Mass, m - Vehicle mass
1500 (default) | scalar
Vehicle mass, $M$, in kg.
Horizontal distance from CG to front axle, a - Front axle distance 1.4 (default) | scalar

Horizontal distance $a$ from the vehicle CG to the front wheel axle, in $m$.
Horizontal distance from CG to rear axle, b-Rear axle distance
1.8 (default) | scalar

Horizontal distance $b$ from the vehicle CG to the rear wheel axle, in $m$.
CG height above axles, $\mathbf{h}$ - Height
. 35 (default) | scalar
Height of vehicle CG above the ground, $h$, in $m$.
Longitudinal drag coefficient, Cd - Drag
. 3 (default) | scalar
Air drag coefficient, $C_{d}$. The value is dimensionless.
Longitudinal lift coefficient, CI - Lift
0 (default) | scalar
Air lift coefficient, $C_{l}$. The value is dimensionless.
Longitudinal drag pitch moment, Cpm - Pitch drag
0 (default) | scalar
Pitch drag moment coefficient, $C_{p m}$. The value is dimensionless.

## Frontal area, Af - Area

4 (default) | scalar
Effective vehicle cross-sectional area, $A$, to calculate the aerodynamic drag force on the vehicle, in $\mathrm{m}^{2}$.

Initial position, x_o - Position
0 (default) | scalar

Vehicle body longitudinal initial position along the vehicle-fixed x -axis, $\chi_{0}$, in m .
Initial velocity, xdot_o - Velocity
0 (default) | scalar
Vehicle body longitudinal initial velocity along the vehicle-fixed $x$-axis, $\dot{x}_{0}$, in $\mathrm{m} / \mathrm{s}$.

## Environment

Absolute air pressure, Pabs - Pressure
101325 (default) | scalar
Environmental air absolute pressure, $P_{a b s}$, in Pa .
Air temperature, $\mathbf{T}$ - Ambient air temperature
273 (default) | scalar
Ambient air temperature, $T_{\text {air }}$, in K .
Dependencies
To enable this parameter, clear Air temperature.
Gravitational acceleration, g - Gravity
9.81 (default) | scalar

Gravitational acceleration, $g$, in $\mathrm{m} / \mathrm{s}^{2}$.

## Version History <br> Introduced in R2017a

## Extended Capabilities

C/C++ Code Generation
Generate C and C++ code using Simulink ${ }^{\circledR}$ Coder $^{\mathrm{TM}}$.

## See Also

Vehicle Body 3DOF Longitudinal | Vehicle Body Total Road Load

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"

## Vehicle Body 3DOF Longitudinal

3DOF rigid vehicle body to calculate longitudinal, vertical, and pitch motion


## Libraries:

Powertrain Blockset / Vehicle Dynamics
Vehicle Dynamics Blockset / Vehicle Body

## Description

The Vehicle Body 3DOF Longitudinal block implements a three degrees-of-freedom (3DOF) rigid vehicle body model with configurable axle stiffness to calculate longitudinal, vertical, and pitch motion. The block accounts for body mass, aerodynamic drag, road incline, and weight distribution between the axles due to acceleration and the road profile.

You can specify the type of axle attachment to the vehicle:

- Grade angle - Vertical axle displacement from road surface to axles remains constant. The block uses tabular stiffness and damping parameters to model the suspension forces acting between the vehicle body and axles.
- Axle displacement - Axles have input-provided vertical displacement and velocity with respect to the road grade. The block uses tabular stiffness and damping parameters to model the suspension forces acting between the vehicle body and axle.
- External suspension - Axles have externally applied forces for coupling the vehicle body to custom suspension models.

If the weight transfer from vertical and pitch motions are not negligible, consider using this block to represent vehicle motion in powertrain and fuel economy studies. For example, in studies with heavy breaking or acceleration or road profiles that contain larger vertical changes.

The block uses rigid-body vehicle motion, suspension system forces, and wind and drag forces to calculate the normal forces on the front and rear axles. The block resolves the force components and moments on the rigid vehicle body frame:

$$
\begin{aligned}
& F_{x}=F_{w F}+F_{w R}-F_{d, x}-F_{s x, F}-F_{s X, R}+F_{g, x} \\
& F_{z}=F_{d, z}-F_{s z, F}-F_{s z, R}+F_{g, z} \\
& M_{y}=a F_{s z, F}-b F_{s z, R}+h\left(F_{w F}+F_{w R}+F_{s x, F}+F_{s x, R}\right)-M_{d, y}
\end{aligned}
$$



## Rigid-Body Vehicle Motion

The vehicle axles are parallel and form a plane. The longitudinal direction lies in this plane and is perpendicular to the axles. If the vehicle is traveling on an inclined slope, the normal direction is not parallel to gravity but is always perpendicular to the axle-longitudinal plane.

The block uses the net effect of all the forces and torques acting on it to determine the vehicle motion. The longitudinal tire forces push the vehicle forward or backward. The weight of the vehicle acts through its center of gravity (CG). Depending on the inclined angle, the weight pulls the vehicle to the ground and either forward or backward. Whether the vehicle travels forward or backward, aerodynamic drag slows it down. For simplicity, the drag is assumed to act through the CG.

The Vehicle Body 3DOF Longitudinal implements these equations.

$$
\begin{aligned}
& \ddot{x}=\frac{F_{x}}{m}-q z \\
& \ddot{z}=\frac{F_{z}}{m}-q x \\
& \dot{q}=\frac{M_{y}}{I_{y y}} \\
& \dot{\theta}=q
\end{aligned}
$$

## Suspension System Forces

If you configure the block with the Ground interaction type parameter Grade angle or Axle displacement, velocity, the block uses nonlinear stiffness and damping parameters to model the suspension system.

The front and rear axle suspension forces are given by:

$$
\begin{aligned}
& F s_{F}=N_{F}\left[F k_{F}+F b_{F}\right] \\
& F s_{R}=N_{R}\left[F k_{R}+F b_{R}\right]
\end{aligned}
$$

The block uses lookup tables to implement the front and rear suspension stiffness. To account for kinematic and material nonlinearities, including collisions with end-stops, the tables are functions of the stroke.

$$
\begin{aligned}
& F k_{F}=f\left(d Z_{F}\right) \\
& F k_{R}=f\left(d Z_{R}\right)
\end{aligned}
$$

The block uses lookup tables to implement the front and rear suspension damping. To account for nonlinearities, compression, and rebound, the tables are functions of the stroke rate.

$$
\begin{aligned}
& F b_{F}=f\left(d \dot{Z}_{F}\right) \\
& F b_{R}=f\left(d \dot{Z}_{R}\right)
\end{aligned}
$$

The stroke is the difference in the vehicle vertical and axle positions. The stroke rate is the difference in the vertical and axle velocities.

$$
\begin{aligned}
& d Z_{F}=Z_{F}-\bar{Z}_{F} \\
& d Z_{R}=Z_{R}-\bar{Z}_{R} \\
& d \dot{Z}_{F}=\dot{Z}_{F}-\dot{\bar{Z}}_{F} \\
& d \dot{Z}_{R}=\dot{Z}_{R}-\dot{\bar{Z}}_{R}
\end{aligned}
$$

When the Ground interaction type parameter is Grade angle, the axle vertical positions $\left(\bar{Z}_{F}, \bar{Z}_{R}\right)$ and velocities $\left(\dot{\bar{Z}}_{F}, \dot{\bar{Z}}_{R}\right)$ are set to 0 .

## Wind and Drag Forces

The block subtracts the wind speeds from the vehicle velocity components to obtain a net relative airspeed. To calculate the drag force and moments acting on the vehicle, the block uses the net relative airspeed:

$$
\begin{aligned}
& F_{d, x}=\frac{1}{2 T R} C_{d} A_{f} P_{a b s}{ }^{\dot{x}} \\
& F_{d, z}=\frac{1}{2 T R} C_{l} A_{f} P_{a b s} 1^{\dot{x}} \\
& M_{d, y}=\left.\frac{1}{2 T R} C_{p m} A_{f} P_{a b s}\right|^{\dot{x}}(a+b)
\end{aligned}
$$

## Power Accounting

For the power accounting, the block implements these equations.

| Bus Signal |  |  | Description | Equations |
| :---: | :---: | :---: | :---: | :---: |
| PwrInf 0 | PwrTrnsfrd Power transferred between blocks <br> - Positive signals indicate flow into block <br> - Negative signals indicate flow out of block | PwrFxExt | Externally applied longitudinal force power | $P_{F x E x t}=F_{x E x t} \dot{\chi}$ |
|  |  | PwrFzExt | Externally applied longitudinal force power | $P_{F z E x t}=F_{z E x t} \dot{z}$ |
|  |  | PwrMyExt | Externally applied pitch moment power | $P_{M z E x t}=M_{z E x t} \dot{\theta}$ |
|  |  | PwrFwFx | Longitudinal force applied at the front axle | $P_{F w F x}=F_{w F} \dot{X}$ |
|  |  | PwrFwRx | Longitudinal force applied at the rear axle | $P_{F w R x}=F_{w R} \dot{X}$ |
|  | PwrNotTrnsfrd <br> - Power crossing the block boundary, but not transferred <br> - Positive signals indicate an input <br> - Negative signals indicate a loss | PwrFsF | Internal power transferred between suspension and vehicle body at the front axle | $\begin{aligned} & P_{F s, F}=-P_{F w F X}+P_{F s b F} \\ & +P_{F s k, F}+F_{X F} \dot{\mathrm{X}}_{F}+F_{z F} \dot{z}_{F} \end{aligned}$ |
|  |  | PwrFsR | Internal power transferred between suspension and vehicle body at the rear axle | $\begin{aligned} & P_{F s, R}=-P_{F w R x}+P_{F s b, R} \\ & +P_{F s k, R}+F_{x F} \dot{\chi}_{F}+F_{z F} \dot{z}_{F} \end{aligned}$ |
|  |  | PwrFxDrag | Longitudinal drag force power | $P_{d, x}=F_{d, x} \dot{\chi}$ |
|  |  | PwrFzDrag | Vertical drag force power | $P_{d, z}=F_{d, z} \dot{z}$ |
|  |  | PwrMyDrag | Drag pitch moment power | $P_{d, M y}=M_{d, y} \dot{\theta}$ |
|  |  | PwrFsb | Total suspension damping power | $P_{F s b}=\sum_{i=F, R} F_{s b, i} \dot{z}_{i}$ |
|  | PwrStored Stored energy rate of change <br> - Positive signals indicate an increase <br> - Negative signals indicate a decrease | PwrStoredGrvty | Rate change in gravitational potential energy | $P_{g}=-m g \dot{Z}$ |
|  |  | PwrStoredxdot | Rate of change of longitudinal kinetic energy | $P_{\dot{\chi}}=m \ddot{\chi} \dot{\chi}$ |
|  |  | PwrStoredzdot | Rate of change of longitudinal kinetic energy | $P_{\dot{z}}=m \ddot{z} \dot{z}$ |


| Bus Signal |  | Description | Equations |  |
| :--- | :--- | :--- | :--- | :--- |
|  | PwrStoredq | Rate of change of <br> rotational pitch <br> kinetic energy | $P_{\dot{\theta}}=I_{y y} \ddot{\theta} \dot{\theta}$ |  |
|  |  | PwrStoredFsFzSp <br> rng | Stored spring <br> energy from front <br> suspension | $P_{F s k F}=F_{s k, F} \dot{z}_{F}$ |
|  | Stored spring <br> energy from rear <br> suspension | $P_{F s k F}=F_{s k, R} \dot{z}_{R}$ |  |  |
|  |  |  |  |  |

The equations use these variables.
$F_{x} \quad$ Longitudinal force on vehicle
$F_{z} \quad$ Normal force on vehicle
$M_{y} \quad$ Torque on vehicle about the vehicle-fixed $y$-axis
$F_{w F}, F_{w R} \quad$ Longitudinal force on front and rear axles along vehicle-fixed $x$-axis
$F_{d, x}, F_{d, z} \quad$ Longitudinal and normal drag force on vehicle CG
$F_{s x, F,}, F_{s x, R} \quad$ Longitudinal suspension force on front and rear axles
$F_{s z, F}, F_{s z, R} \quad$ Normal suspension force on front and rear axles
$F_{g, x} F_{g, z} \quad$ Longitudinal and normal gravitational force on vehicle along the vehicle-fixed frame
$M_{d, y} \quad$ Torque due to drag on vehicle about the vehicle-fixed $y$-axis
$a, b$
h
$F s_{F}, F s_{R}$
$Z_{w F}, Z_{w R}$
$\Theta$
m
$N_{F}, N_{R}$
$I_{y y}$
$x, \dot{x}, \ddot{x} \quad$ Vehicle longitudinal position, velocity, and acceleration along the vehicle-fixed $x$ axis
$z, \dot{z}, \ddot{z} \quad$ Vehicle normal position, velocity, and acceleration along the vehicle-fixed $z$-axis
$F k_{F}, F k_{R} \quad$ Front and rear wheel suspension stiffness force along vehicle-fixed $z$-axis
$F b_{F}, F b_{R} \quad$ Front and rear wheel suspension damping force along vehicle-fixed $z$-axis
$Z_{F}, Z_{R}$
$\dot{Z}_{F}, \dot{Z}_{R}$
$\bar{Z}_{F}, \bar{Z}_{R}$
Front and rear vehicle vertical position along earth-fixed $Z$-axis
Front and rear vehicle vertical velocity along vehicle-fixed $z$-axis
Front and rear wheel axle vertical position along vehicle-fixed $z$-axis
$\dot{\bar{Z}}_{F}, \dot{\bar{Z}}_{R}$
Front and rear wheel axle vertical velocity along earth-fixed $z$-axis

| $d Z_{F}, d Z_{R}$ | Front and rear axle suspension deflection along vehicle-fixed $z$-axis |
| :--- | :--- |
| $d \dot{Z}_{F}, d \dot{Z}_{R}$ | Front and rear axle suspension deflection rate along vehicle-fixed $z$-axis |
| $C_{d}$ | Frontal air drag coefficient acting along the vehicle-fixed $x$-axis |
| $C_{l}$ | Lateral air drag coefficient acting along the vehicle-fixed $z$-axis |
| $C_{p m}$ | Air drag pitch moment acting about the vehicle-fixed $y$-axis |
| $A_{f}$ | Frontal area |
| $P_{a b s}$ | Environmental absolute pressure |
| $R$ | Atmospheric specific gas constant |
| $T$ | Environmental air temperature |
| $w_{\chi}$ | Wind speed along the vehicle-fixed $x$-axis |

## Ports

Input
FExt - External force on vehicle CG
array
External forces applied to vehicle CG, $F_{\text {xext }}, F_{\text {yext }}, F_{\text {zext }}$, in vehicle-fixed frame, in N. Signal vector dimensions are [1×3] or [3x1].
Dependencies
To enable this port, select External forces.
MExt - External moment about vehicle CG
array
External moment about vehicle CG, $M_{x}, M_{y}, M_{z}$, in the vehicle-fixed frame, in $N \cdot m$. Signal vector dimensions are [1x3] or [3x1].

## Dependencies

To enable this port, select External moments.
FwF - Total longitudinal force on the front axle scalar

Longitudinal force on the front axle, $F w_{F}$, along vehicle-fixed $x$-axis, in N .
FwR - Total longitudinal force on the rear axle
scalar
Longitudinal force on the rear axle, $F w_{R}$, along vehicle-fixed $x$-axis, in N .
Grade - Road grade angle scalar

Road grade angle, $\gamma$, in deg.
FsF - Suspension force on front axle per wheel vector

Suspension force on front axle, $F s_{F}$, along the vehicle-fixed $z$-axis, in $N$.

## Dependencies

To enable this port, for the Ground interaction type parameter, select External suspension.
FsR - Suspension force on rear axle per wheel
vector
Suspension force on rear axle, $F s_{R}$, along the vehicle-fixed $z$-axis, in N .

## Dependencies

To enable this port, for the Ground interaction type parameter, select External suspension.
WindXYZ - Wind speed
array
Wind speed, $W_{X}, W_{Y}, W_{Z}$ along earth-fixed $X$-, $Y$-, and $Z$-axes, in m/s. Signal vector dimensions are [1x3] or [3x1].

AirTemp - Ambient air temperature
scalar
Ambient air temperature, $T_{\text {air }}$, in K . Considering this option if you want to vary the temperature during run-time.

## Dependencies

To enable this port, select Air temperature.
$\mathbf{z F}, \mathbf{R}$ - Forward and rear axle positions
vector
Forward and rear axle positions along the vehicle-fixed $z$-axis, $\bar{Z}_{F}, \bar{Z}_{R}$, in m .

## Dependencies

To enable this port, for the Ground interaction type parameter, select Axle displacement, velocity.
zdotF,R - Forward and rear axle velocities
vector
Forward and rear axle velocities along the vehicle-fixed $z$-axis, $\dot{\bar{Z}}_{F}, \dot{\bar{Z}}_{R}$, in m/s.

## Dependencies

To enable this port, for the Ground interaction type parameter, select Axle displacement, velocity.

## Output

Info - Bus signal
bus
Bus signal containing these block values.

| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| InertFrm | Cg | Disp | X | Vehicle CG displacement along earth-fixed $X$-axis | Computed | m |
|  |  |  | Y | Vehicle CG displacement along earth-fixed $Y$-axis | 0 | m |
|  |  |  | Z | Vehicle CG displacement along earth-fixed $Z$-axis | Computed | m |
|  |  | Vel | Xdot | Vehicle CG velocity along earth-fixed $X$-axis | Computed | m/s |
|  |  |  | Ydot | Vehicle CG velocity along earth-fixed $Y$-axis | 0 | m/s |
|  |  |  | Zdot | Vehicle CG velocity along earth-fixed Z-axis | Computed | m/s |
|  |  | Ang | phi | Rotation of vehicle-fixed frame about the earth-fixed $X$-axis (roll) | 0 | rad |
|  |  |  | theta | Rotation of vehicle-fixed frame about the earth-fixed $Y$-axis (pitch) | Computed | rad |
|  |  |  | psi | Rotation of vehicle-fixed frame about the earth-fixed $Z$-axis (yaw) | 0 | rad |
|  | FrntAxl | Disp | X | Front axle displacement along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Y | Front axle displacement along the earth-fixed $Y$-axis | 0 | m |
|  |  |  | Z | Front axle displacement along the earth-fixed $Z$-axis | Computed | m |
|  |  | Vel | Xdot | Front axle velocity along the earth-fixed $X$-axis | Computed | $\mathrm{m} / \mathrm{s}$ |
|  |  |  | Ydot | Front axle velocity along the earth-fixed $Y$-axis | 0 | m/s |
|  |  |  | Zdot | Front axle velocity along the earth-fixed $Z$-axis | Computed | m/s |
|  | RearAxl | Disp | X | Rear axle displacement along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Y | Rear axle displacement along the earth-fixed $Y$-axis | 0 | m |
|  |  |  | Z | Rear axle displacement along the earth-fixed $Z$-axis | Computed | m |
|  |  | Vel | Xdot | Rear axle velocity along the earth-fixed $X$-axis | Computed | m/s |
|  |  |  | Ydot | Rear axle velocity along the earth-fixed $Y$-axis | 0 | m/s |


| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Zdot | Rear axle velocity along the earth-fixed Z-axis | Computed | m/s |
| BdyFrm | Cg | Disp | x | Vehicle CG displacement along the vehicle-fixed $x$ axis | Computed | m |
|  |  |  | y | Vehicle CG displacement along the vehicle-fixed $y$ axis | 0 | m |
|  |  |  | z | Vehicle CG displacement along the vehicle-fixed $z$ axis | Computed | m |
|  |  | Vel | xdot | Vehicle CG velocity along the vehicle-fixed $x$-axis | Computed | m/s |
|  |  |  | ydot | Vehicle CG velocity along the vehicle-fixed $y$-axis | 0 | m/s |
|  |  |  | zdot | Vehicle CG velocity along the vehicle-fixed $z$-axis | Computed | m/s |
|  |  | AngVel | p | Vehicle angular velocity about the vehicle-fixed $x$ axis (roll rate) | 0 | $\mathrm{rad} / \mathrm{s}$ |
|  |  |  | q | Vehicle angular velocity about the vehicle-fixed $y$ axis (pitch rate) | Computed | rad/s |
|  |  |  | r | Vehicle angular velocity about the vehicle-fixed $z$ axis (yaw rate) | 0 | rad/s |
|  |  | Accel | ax | Vehicle CG acceleration along the vehicle-fixed $x$ axis | Computed | gn |
|  |  |  | ay | Vehicle CG acceleration along the vehicle-fixed $y$ axis | 0 | gn |
|  |  |  | az | Vehicle CG acceleration along the vehicle-fixed $z$ axis | Computed | gn |
|  | Forces | Body | FX | Net force on vehicle CG along the vehicle-fixed $x$ axis | Computed | N |
|  |  |  | Fy | Net force on vehicle CG along the vehicle-fixed $y$ axis | 0 | N |
|  |  |  | Fz | Net force on vehicle CG along the vehicle-fixed $z$ axis | Computed | N |



| Signal |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Fy | Drag force on vehicle CG along the vehicle-fixed $y$ axis | Computed | N |
|  |  | Fz | Drag force on vehicle CG along the vehicle-fixed $z$ axis | Computed | N |
|  | Grvty | Fx | Gravity force on vehicle CG along the vehicle-fixed $x$ axis | Computed | N |
|  |  | Fy | Gravity force on vehicle CG along the vehicle-fixed $y$ axis | 0 | N |
|  |  | Fz | Gravity force on vehicle CG along the vehicle-fixed $z$ axis | Computed | N |
| Moments | Body | Mx | Body moment on vehicle CG about the vehicle-fixed $x$-axis | 0 | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | My | Body moment on vehicle CG about the vehicle-fixed $y$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | Mz | Body moment on vehicle CG about the vehicle-fixed $z$-axis | 0 | $\mathrm{N} \cdot \mathrm{m}$ |
|  | Drag | Mx | Drag moment on vehicle CG about the vehicle-fixed $x$-axis | 0 | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | My | Drag moment on vehicle CG about the vehicle-fixed $y$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | Mz | Drag moment on vehicle CG about the vehicle-fixed $z$-axis | 0 | $\mathrm{N} \cdot \mathrm{m}$ |
|  | Ext | Fx | External moment on vehicle CG about the vehicle-fixed x-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | Fy | External moment on vehicle CG about the vehicle-fixed $y$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | Fz | External moment on vehicle CG about the vehicle-fixed $z$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
| FrntAxl | Disp | x | Front axle displacement along the vehicle-fixed $x$ axis | Computed | m |



| Signal |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: |
|  | PwrFwFx | Longitudinal force applied at the front axle | Computed | W |
|  | PwrFwRx | Longitudinal force applied at the rear axle | Computed | W |
| PwrNotT rnsfrd | PwrFsF | Internal power transferred between suspension and vehicle body at the front axle | Computed | W |
|  | PwrFsR | Internal power transferred between suspension and vehicle body at the rear axle | Computed | W |
|  | PwrFxDrag | Longitudinal drag force power | Computed | W |
|  | PwrFzDrag | Vertical drag force power | Computed | W |
|  | PwrMyDrag | Drag pitch moment power | Computed | W |
|  | PwrFsb | Total suspension damping power | Computed | W |
| PwrStor ed | PwrStoredGrvty | Rate change in gravitational potential energy | Computed | W |
|  | PwrStoredxdot | Rate of change of longitudinal kinetic energy | Computed | W |
|  | PwrStoredzdot | Rate of change of longitudinal kinetic energy | Computed | W |
|  | PwrStoredq | Rate of change of rotational pitch kinetic energy | Computed | W |
|  | PwrStoredFsFzSprng | Stored spring energy from front suspension | Computed | W |
|  | PwrStoredFsRzSprng | Stored spring energy from rear suspension | Computed | W |

xdot - Vehicle longitudinal velocity
scalar
Vehicle CG velocity along the vehicle-fixed $x$-axis, in $m / s$.
FzF - Front axle normal force
scalar
Normal force on front axle, $F z_{F}$, along the vehicle-fixed $z$-axis, in N .
FzR - Rear axle normal force
scalar
Normal force on rear axle, $F z_{R}$, along the vehicle-fixed $z$-axis, in N .

## Parameters

## Options

External forces - FExt input port
off (default) | on
Specify to create input port FExt.
External moments - MExt input port
off (default) | on
Specify to create input port MExt.
Air temperature - AirTemp input port
off (default) | on
Specify to create input port AirTemp.

## Longitudinal

Number of wheels on front axle, NF - Front wheel count
2 (default) | scalar
Number of wheels on front axle, $N_{F}$. The value is dimensionless.
Number of wheels on rear axle, NR - Rear wheel count
2 (default) | scalar
Number of wheels on rear axle, $N_{R}$. The value is dimensionless.
Mass, $\mathbf{m}$ - Vehicle mass
1200 (default) | scalar
Vehicle mass, $m$, in kg.
Horizontal distance from CG to front axle, a - Front axle distance
1.4 (default) | scalar

Horizontal distance $a$ from the vehicle CG to the front wheel axle, in m.
Horizontal distance from CG to rear axle, b-Rear axle distance
1.8 (default) | scalar

Horizontal distance $b$ from the vehicle CG to the rear wheel axle, in m .
CG height above axles, $\mathbf{h}$ - Height
0.35 (default) | scalar

Height of vehicle CG above the axles, $h$, in m.

## Longitudinal drag coefficient, Cd - Drag

. 3 (default) | scalar
Air drag coefficient, $C_{d}$. The value is dimensionless.

## Frontal area, Af - Area

2 (default) | scalar
Effective vehicle cross-sectional area, $A_{f}$ to calculate the aerodynamic drag force on the vehicle, in $\mathrm{m}^{\wedge} 2$.

Initial position, x_0-Position
0 (default) | scalar
Vehicle body longitudinal initial position along earth-fixed $x$-axis, $\chi_{0}$, in m .
Initial velocity, xdot_o - Velocity
0 (default) | scalar
Vehicle body longitudinal initial velocity along earth-fixed $x$-axis, $\dot{x}_{0}$, in $\mathrm{m} / \mathrm{s}$.

## Vertical

Longitudinal lift coefficient, CI - Lift
. 1 (default) | scalar
Lift coefficient, $C_{l}$. The value is dimensionless.
Initial vertical position, z_o - Position
-. 35 (default) | scalar
Initial vertical CG position, $z_{0}$, along the vehicle-fixed $z$-axis, in m .
Initial vertical velocity, zdot_o - Velocity
0 (default) | scalar
Initial vertical CG velocity, $z d o t_{o}$, along the vehicle-fixed $z$-axis, in m .
Pitch
Inertia, lyy - About body y-axis
3500 (default) | scalar
Vehicle body moment of inertia about body $z$-axis.
Longitudinal drag pitch moment, Cpm - Drag coefficient
. 1 (default) | scalar
Pitch drag moment coefficient. The value is dimensionless.
Initial pitch angle, theta_o - Pitch
0 (default) | scalar
Initial pitch angle about body $z$-axis, in rad.
Initial angular velocity, q_o - Pitch velocity
0 (default) | scalar
Initial vehicle body angular velocity about body $z$-axis, in rad/s.

## Suspension

## Front axle stiffness force data, FskF - Force

$[-50,-1,0,2,3,52] . * 1.5 e 4$ (default) | vector
Front axle stiffness force data, $F k_{F}$, in N.

## Dependencies

To enable this parameter, for the Ground interaction type parameter, select Grade angle or Axle displacement, velocity.

Front axle displacement data, dzsF - Displacement
[-5e-3, -1e-4, 0, .2, .2001, .2051] (default) | vector
Front axle displacement data, in m .

## Dependencies

To enable this parameter, for the Ground interaction type parameter, select Grade angle or Axle displacement, velocity.

Front axle damping force data, FsbF - Damping force

```
[-10000 -100 -10 0 10 100 10000] (default)|vector
```

Front axle damping force, in N.

## Dependencies

To enable this parameter, for the Ground interaction type parameter, select Grade angle or Axle displacement, velocity.

Front axle velocity data, dzdotsF - Velocity

```
[-10 -1 -. 1 0 . 1 1 10] (default)|vector
```

Front axle velocity data, in m/s.

## Dependencies

To enable this parameter, for the Ground interaction type parameter, select Grade angle or Axle displacement, velocity.

Rear axle stiffness force data, FskR - Force
[-50, -1, 0, 2, 3, 52].*le4 (default)| vector
Rear axle stiffness force data, in N .

## Dependencies

To enable this parameter, for the Ground interaction type parameter, select Grade angle or Axle displacement, velocity.

Rear axle displacement data, dzsR - Displacement
[-5e-3, -1e-4, 0, .2, .2001, .2051] (default)|vector
Rear axle displacement data, in m .

## Dependencies

To enable this parameter, for the Ground interaction type parameter, select Grade angle or Axle displacement, velocity.

Rear axle damping force data, FsbR - Damping force
[-10000-100 -10 010100 10000] (default) |vector
Rear axle damping force, in N .

## Dependencies

To enable this parameter, for the Ground interaction type parameter, select Grade angle or Axle displacement, velocity.

Rear axle velocity data, dzdotsR - Velocity
[-10 -1 -. 1 0 . 11 10] (default)| vector
Rear axle velocity data, in m/s.

## Dependencies

To enable this parameter, for the Ground interaction type parameter, select Grade angle or Axle displacement, velocity.

## Environment

Absolute air pressure, Pabs - Pressure
101325 (default) | scalar
Environmental air absolute pressure, $P_{\text {abs }}$, in Pa.
Air temperature, Tair - Ambient air temperature
273 (default) | scalar
Ambient air temperature, $T_{\text {air }}$, in K.
Dependencies
To enable this parameter, clear Air temperature.
Gravitational acceleration, $\mathbf{g}$ - Gravity
9.81 (default)

Gravitational acceleration, $g$, in $\mathrm{m} / \mathrm{s}^{2}$.

## Version History

Introduced in R2017a

## References

[1] Gillespie, Thomas. Fundamentals of Vehicle Dynamics. Warrendale, PA: Society of Automotive Engineers, 1992.
[2] Vehicle Dynamics Standards Committee. Vehicle Dynamics Terminology. SAE J670. Warrendale, PA: Society of Automotive Engineers, 2008.
[3] Technical Committee. Road vehicles - Vehicle dynamics and road-holding ability - Vocabulary. ISO 8855:2011. Geneva, Switzerland: International Organization for Standardization, 2011.

## Extended Capabilities

C/C++ Code Generation
Generate C and C++ code using Simulink ${ }^{\circledR}$ Coder ${ }^{\mathrm{TM}}$.

## See Also

Vehicle Body 1DOF Longitudinal | Vehicle Body Total Road Load

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"

## Vehicle Body 3DOF

3DOF rigid vehicle body to calculate longitudinal, lateral, and yaw motion


## Libraries:

Vehicle Dynamics Blockset / Vehicle Body

## Description

The Vehicle Body 3DOF block implements a rigid two-axle vehicle body model to calculate longitudinal, lateral, and yaw motion. The block accounts for body mass and aerodynamic drag between the axles due to acceleration and steering.

Use this block in vehicle dynamics and automated driving studies to model nonholonomic vehicle motion when vehicle pitch, roll, and vertical motion are not significant.

In the Vehicle Dynamics Blockset library, there are two types of Vehicle Body 3DOF blocks that model longitudinal, lateral, and yaw motion.


Use the Axle forces parameter to specify the type of force.

| Axle Forces Setting | Implementation |
| :---: | :---: |
| External longitudinal velocity | - The block assumes that the external longitudinal velocity is in a quasi-steady state, so the longitudinal acceleration is approximately zero. <br> - Because the motion is quasi-steady, the block calculates lateral forces using the tire slip angles and linear cornering stiffness. <br> - Consider this setting when you want to: <br> - Generate virtual sensor signal data. <br> - Conduct high-level software studies that are not impacted by driveline or nonlinear tire responses. |
| External longitudinal forces | - The block uses the external longitudinal force to accelerate or brake the vehicle. <br> - The block calculates lateral forces using the tire slip angles and linear cornering stiffness. <br> - Consider this setting when you want to: <br> - Account for changes in the longitudinal velocity on the lateral and yaw motion. <br> - Specify the external longitudinal motion through a force instead of an external longitudinal velocity. <br> - Connect the block to tractive actuators, wheels, brakes, and hitches. |
| External forces | - The block uses the external lateral and longitudinal forces to steer, accelerate, or brake the vehicle. <br> - The block does not use the steering input to calculate vehicle motion. <br> - Consider this setting when you need tire models with more accurate nonlinear combined lateral and longitudinal slip. |

You can use these block parameters to create additional input ports. This table summarizes the settings.

| Input Signals Pane Parameter | Input Port | Description |
| :--- | :--- | :--- |
| Front wheel steering | WhlAngF | Front wheel angle, $\delta_{F}$ |
| External wind | WindXYZ | Wind speed, $W_{X}, W_{Y}, W_{Z}$, in the inertial <br> reference frame |
| External forces | FExt | External force on vehicle center of gravity (CG), <br> $F_{x}, F_{y}, F_{z}$, in the vehicle-fixed frame |
| Rear wheel steering | WhlAngR | Rear wheel angle, $\delta_{R}$ |
| External friction | Mu | Friction coefficient |
| External moments | MExt | External moment about vehicle CG, $M_{x}, M_{y}, M_{z}$ <br> in vehicle-fixed frame |


| Input Signals Pane Parameter | Input Port | Description |
| :---: | :---: | :---: |
| Hitch forces | Fh | Hitch force applied to the body at the hitch location, $F h_{x}, F h_{y}$, and $F h_{z}$, in the vehicle-fixed frame |
| Hitch moments | Mh | Hitch moment at the hitch location, $M h_{x}, M h_{y}$ and $M h_{z}$, about the vehicle-fixed frame |
| Initial longitudinal position | X_0 | Initial vehicle CG displacement along the earthfixed $X$-axis, in $m$ |
| Initial lateral position | Y_0 | Initial vehicle CG displacement along the earthfixed $Y$-axis, in $m$ |
| Initial longitudinal velocity | xdot_o | Initial vehicle CG velocity along the vehiclefixed $x$-axis, in $m / s$ |
| Initial lateral velocity | ydot_0 | Initial vehicle CG velocity along the vehiclefixed $y$-axis, in $\mathrm{m} / \mathrm{s}$ |
| Initial yaw angle | psi_o | Initial rotation of the vehicle-fixed frame about the earth-fixed $Z$-axis (yaw), in rad |
| Initial yaw rate | r_o | Initial vehicle angular velocity about the vehicle-fixed $z$-axis (yaw rate), in rad/s |
| Air temperature | AirTemp | Ambient air temperature. Considering this option if you want to vary the temperature during run-time. |

## Theory

The Vehicle Body 3DOF block implements a rigid two-axle vehicle body model to calculate longitudinal, lateral, and yaw motion. The block accounts for body mass, aerodynamic drag, and weight distribution between the axles due to acceleration and steering. To determine the vehicle motion, the block implements these equations for the single track, dual track, and drag calculations.

## Single Track

| Calculation | Description |
| :--- | :--- |
| Dynamics | The block uses these equations to calculate the rigid body planar dynamics.  <br>  $\ddot{y}=-\dot{x} r+\frac{F_{y f}+F_{y r}+F_{y e x t}}{m}$ <br> $\dot{r}=\frac{a F_{y f}-b F_{y r}+M_{z e x t}}{I_{z z}}$  <br> $r=\dot{\psi}$  |
|  | If you set Axle forces to either External longitudinal forces or <br> External forces, the block uses this equation for the longitudinal <br> acceleration. <br> $\ddot{x}=\dot{y} r+\frac{F_{\chi f}+F_{x r}+F_{\chi e x t}}{m}$ <br> If you set Axle forces to External longitudinal velocity, the block <br> assumes a quasi-steady state for the longitudinal acceleration. <br> $\ddot{x}=0$ |
|  |  |


| Calculation | Description |
| :---: | :---: |
| External forces | External forces include both drag and external force inputs. The forces act on the vehicle CG. $\begin{aligned} & F_{x, y, z e x t}=F_{d x, y, z}+F_{x, y, z \text { input }} \\ & M_{x, y, z e x t}=M_{d x, y, z}+M_{x, y, z \text { input }} \end{aligned}$ <br> If you set Axle forces to External longitudinal forces, the block uses these equations. $\begin{aligned} & F_{x f t}=F_{x f i n p u t} \\ & F_{y f t}=-C_{y f} \alpha_{f} \mu_{f} \frac{F_{z f}}{F_{z n o m}} \\ & F_{x r t}=F_{x r i n p u t} \\ & F_{y r t}=-C_{y r} \alpha_{r} \mu_{r} \frac{F_{z r}}{F_{z n o m}} \end{aligned}$ <br> If you set Axle forces to External longitudinal velocity, the block uses these equations. $\begin{aligned} & F_{x f t}=0 \\ & F_{y f t}=-C_{y f} \alpha_{f} \mu_{f} \frac{F_{z f}}{F_{z n o m}} \\ & F_{x r t}=0 \\ & F_{y r t}=-C_{y r} \alpha_{r} \mu_{r} \frac{F_{z r}}{F_{z n o m}} \end{aligned}$ <br> The block divides the normal forces by the nominal normal load to vary the effective friction parameters during weight and load transfer. The block uses these equations to maintain pitch and roll equilibrium. $\begin{aligned} & F_{z f}=\frac{b m g-(\ddot{x}-\dot{y} r) m h+h F_{\text {xext }}+b F_{z e x t}-M_{y e x t}}{a+b} \\ & F_{z r}=\frac{a m g+(\ddot{x}-\dot{y} r) m h-h F_{\text {xext }}+a F_{z e x t}+M_{\text {yext }}}{a+b} \end{aligned}$ |


| Calculation | Description |
| :--- | :--- |
| Tire forces | The block uses the ratio of the local and longitudinal and lateral velocities to <br> determine the slip angles. <br>  <br> $\alpha_{f}=\operatorname{atan}\left(\frac{\dot{y}+a r}{\dot{x}}\right)-\delta_{f}$ <br> $\alpha_{r}=\operatorname{atan}\left(\frac{\dot{y}-b r}{\dot{x}}\right)-\delta_{r}$ <br> To determine the tire forces, the block uses the slip angles. <br> $F_{x f}=F_{x f t} \cos \left(\delta_{f}\right)-F_{y f t} \sin \left(\delta_{f}\right)$ <br> $F_{y f}=-F_{x f t} \sin \left(\delta_{f}\right)+F_{y f t} \cos \left(\delta_{f}\right)$ <br> $F_{x r}=F_{x r t} \cos \left(\delta_{r}\right)-F_{y r t} \sin \left(\delta_{r}\right)$ <br> $F_{y r}=-F_{x r t} \sin \left(\delta_{r}\right)+F_{y r t} \cos \left(\delta_{r}\right)$ <br> If you set Axle forces to External forces, the block sets the tire forces <br> equal to the external input force. <br> $F_{x f}=F_{x f t}=F_{x f i n p u t}$ <br> $F_{y f}=F_{y f t}=F_{y f i n p u t}$ <br> $F_{x r}=F_{x r t}=F_{x r i n p u t}$ <br> $F_{y r}=F_{y r t}=F_{y r i n p u t}$ |
|  |  |

## Dual Track



| Calculation | Description |
| :--- | :--- |
| Dynamics | $\ddot{x}=\dot{y} r+\frac{F_{x f l}+F_{x f r}+F_{x r l}+F_{x r r}+F_{x e x t}}{m}$ <br> $\ddot{y}=-\dot{x} r+\frac{F_{y f l}+F_{y f r}+F_{y r l}+F_{y r r}+F_{y e x t}}{m}$ <br> $\dot{r}=\frac{a\left(F_{y f l}+F_{y f r}\right)-b\left(F_{y r l}+F_{y r r}\right)+\frac{w_{f}\left(F_{x f l}-F_{x f r}\right)}{2}+\frac{w_{r}\left(F_{x r l}-F_{x r r}\right)}{2}+M_{z e x t}}{I_{z z}}$ <br> $r=\dot{\psi}$ <br> If you set Axle forces to External longitudinal velocity, the block <br> assumes a quasi-steady state for the longitudinal acceleration. <br> $\ddot{x}=0$ |
|  |  |


| Calculation | Description |
| :---: | :---: |
| External forces | External forces include both drag and external force inputs. The forces act on the vehicle CG. $\begin{aligned} & F_{x, y, z e x t}=F_{d x, y, z}+F_{x, y, z \text { input }} \\ & M_{x, y, z e x t}=M_{d x, y, z}+M_{x, y, z \text { input }} \end{aligned}$ <br> If you set Axle forces to External longitudinal forces, the block uses these equations. $\begin{aligned} & F_{x f l t}=F_{x f l i n p u t} \\ & F_{y f l t}=-C_{y f l} \alpha_{f l} \mu_{f l} \frac{F_{z f l}}{2 F_{z n o m}} \\ & F_{x f r t}=F_{x l r i n p u t} \\ & F_{y f r t}=-C_{y f r} \alpha_{f r} \mu_{f r} \frac{F_{z f r}}{2 F_{z n o m}} \\ & F_{x r l t}=F_{x r l i n p u t} \\ & F_{y r l t}=-C_{y r l} \alpha_{r l} \mu_{r l} \frac{F_{z r l}}{2 F_{z n o m}} \\ & F_{x r r t}=F_{x r r i n p u t} \\ & F_{y r r t}=-C_{y r r} \alpha_{r r} \mu_{r r} \frac{F_{z r r}}{2 F_{z n o m}} \end{aligned}$ <br> If you set Axle forces to External longitudinal velocity, the block uses these equations. $\begin{aligned} & F_{x f l t}=0 \\ & F_{y f l t}=-C_{y f l} \alpha_{f l} \mu_{f l} \frac{F_{z f l}}{2 F_{z n o m}} \\ & F_{x f r t}=0 \\ & F_{y f r t}=-C_{y f r} \alpha_{f r} \mu_{f r} \frac{F_{z f r}}{2 F_{z n o m}} \\ & F_{x r l t}=0 \\ & F_{y r l t}=-C_{y r l} \alpha_{r l} \mu_{r l} \frac{F_{z r l}}{2 F_{z n o m}} \\ & F_{x r r t}=0 \\ & F_{y r r t}=-C_{y r r} \alpha_{r r} \mu_{r r} \frac{F_{z r r}}{2 F_{z n o m}} \end{aligned}$ <br> The block divides the normal forces by the nominal normal load to vary the effective friction parameters during weight and load transfer. The block uses these equations to maintain pitch and roll equilibrium. |


| Calculation | Description |
| :---: | :---: |
|  | $\begin{aligned} & F_{z f}=\frac{b m g-(\ddot{x}-\dot{y} r) m h+h F_{x e x t}+b F_{z e x t}-M_{y e x t}}{a+b} \\ & F_{z r}=\frac{a m g+(\ddot{x}-\dot{y} r) m h-h F_{x e x t}+a F_{z e x t}+M_{y e x t}}{(a+b)} \\ & F_{z f l}=F_{z f}+\left(m h(\ddot{y}+\dot{x} r)-h F_{y e x t}-M_{x e x t}\right) \frac{2}{w_{f}} \\ & F_{z f r}=F_{z f}+\left(-m h(\ddot{y}+\dot{x} r)+h F_{y e x t}+M_{x e x t}\right) \frac{2}{w_{f}} \\ & F_{z r l}=F_{z r}+\left(m h(\ddot{y}+\dot{x} r)-h F_{y e x t}-M_{x e x t}\right) \frac{2}{w_{r}} \\ & F_{z r r}=F_{z r}+\left(-m h(\ddot{y}+\dot{x} r)+h F_{y e x t}+M_{x e x t}\right) \frac{2}{w_{r}} \end{aligned}$ |
| Tire forces | The block uses the ratio of the local and longitudinal and lateral velocities to determine the slip angles. $\begin{aligned} & \alpha_{f l}=\operatorname{atan}\left(\frac{\dot{y}+a r}{\dot{x}+r \frac{w_{f}}{2}}\right)-\delta_{f l} \\ & \alpha_{f r}=\operatorname{atan}\left(\frac{\dot{y}+a r}{\dot{x}-r \frac{w_{f}}{2}}\right)-\delta_{f r} \\ & \alpha_{r l}=\operatorname{atan}\left(\frac{\dot{y}-a r}{\dot{x}+r \frac{w_{r}}{2}}\right)-\delta_{r l} \\ & \alpha_{r r}=\operatorname{atan}\left(\frac{\dot{y}-a r}{\dot{x}-r \frac{w_{r}}{2}}\right)-\delta_{r r} \end{aligned}$ <br> The block uses the steering angles to transform the tire forces to the vehiclefixed frame. $\begin{aligned} & F_{x f}=F_{x f t} \cos \left(\delta_{f}\right)-F_{y f t} \sin \left(\delta_{f}\right) \\ & F_{y f}=-F_{x f t} \sin \left(\delta_{f}\right)+F_{y f t} \cos \left(\delta_{f}\right) \\ & F_{x r}=F_{x r t} \cos \left(\delta_{r}\right)-F_{y r t} \sin \left(\delta_{r}\right) \\ & F_{y r}=-F_{x r t} \sin \left(\delta_{r}\right)+F_{y r t} \cos \left(\delta_{r}\right) \end{aligned}$ <br> If you set Axle forces to External forces, the block uses these equations. The blocks assumes that the externally provided forces are in the vehiclefixed frame at the axle-wheel location. $\begin{aligned} & F_{x f}=F_{x f t}=F_{x f \text { input }} \\ & F_{y f}=F_{y f t}=F_{y f i n p u t} \\ & F_{x r}=F_{x r t}=F_{x r i n p u t} \\ & F_{y r}=F_{y r t}=F_{y r i n p u t} \end{aligned}$ |

## Drag

| Calculation | Description |
| :---: | :---: |
| Coordinate transformation | The block transforms the wind speeds from the inertial frame to the vehiclefixed frame. $\begin{aligned} & w_{\chi}=W_{\chi} \cos (\psi)+W_{y} \sin (\psi) \\ & w_{y}=W_{y} \cos (\psi)-W_{\chi} \sin (\psi) \\ & w_{z}=W_{z} \end{aligned}$ |
| Drag forces | To determine a relative airspeed, the block subtracts the wind speed from the CG vehicle velocity. Using the relative airspeed, the block determines the drag forces. $\begin{aligned} & \bar{w}=\sqrt{\left(\dot{x}-w_{\chi}\right)^{2}+\left(\dot{x}-w_{\chi}\right)^{2}+\left(w_{z}\right)^{2}} \\ & F_{d x}=-\frac{1}{2 T R} C_{d} A_{f} P_{a b s}{ }^{(\bar{w}} \\ & F_{d y}=-\frac{1}{2 T R} C_{s} A_{f} P_{a b s}{ }^{(\bar{w}} \\ & F_{d z}=-\left.\frac{1}{2 T R} C_{l} A_{f} P_{a b s}\right\|^{\bar{w}} \end{aligned}$ |
| Drag moments | Using the relative airspeed, the block determines the drag moments. $\begin{aligned} & M_{d r}=-\frac{1}{2 T R} C_{r m} A_{f} P_{a b s}\left(^{(\bar{w}}(a+b)\right. \\ & M_{d p}=-\frac{1}{2 T R} C_{p m} A_{f} P_{a b s}{ }^{\left({ }^{\bar{w}}\right.}(a+b) \\ & M_{d y}=-\frac{1}{2 T R} C_{y m} A_{f} P_{a b s}{ }^{\bar{w}}(a+b) \end{aligned}$ |

## Lateral Corner Stiffness and Relaxation Dynamics

| Description | Implementation |
| :--- | :--- |
| Constant values. | The block uses constant stiffness values for $C y_{f}$ and $C y_{r}$. |
| Lookup tables as a | The block uses lookup tables that are functions of the corner stiffness data |
| function of corner |  |
| stiffness data and slip | and slip angles. |
| angles. | $C y_{f}=f\left(\alpha_{f}, C y_{f d a t a}\right)$ |
|  | $C y_{r}=f\left(\alpha_{r}, C y_{r d a t a}\right)$ |

Description
Lookup tables as a
function of corner
stiffness data and slip
angles.
Slip angles include the relaxation length dynamic settings.

## Implementation

The block uses lookup tables that are functions of the corner stiffness data and slip angles. The slip angles include the relaxation length dynamic settings. The relaxation length approximates an effective corner stiffness force that is a function of wheel travel.

$$
\begin{aligned}
& C y_{f}=f\left(\alpha_{f \sigma}, C y_{f d a t a}\right) \\
& C y_{r}=f\left(\alpha_{r \sigma}, C y_{r d a t a}\right) \\
& \alpha_{f \sigma}=\frac{1}{s}\left[\frac{\left(\alpha_{f}-\alpha_{f \sigma}\right) v_{w f}}{\alpha_{f}}\right] \\
& \alpha_{r \sigma}=\frac{1}{s}\left[\frac{\left(\alpha_{r}-\alpha_{r \sigma}\right) v_{w r}}{\alpha_{r}}\right]
\end{aligned}
$$

The equations use these variables.

| $x, \dot{x}, \ddot{x}$ | Vehicle CG displacement, velocity, and acceleration, along the vehicle-fixed x-axis |
| :---: | :---: |
| $y, \dot{y}, \ddot{y}$ | Vehicle CG displacement, velocity, and acceleration, along the vehicle-fixed $y$-axis |
| $\psi$ | Rotation of the vehicle-fixed frame about the earth-fixed Z-axis (yaw) |
| $r, \dot{\Psi}$ | Vehicle angular velocity, about the vehicle-fixed $z$-axis (yaw rate) |
| $F_{x f}, F_{x r}$ | Longitudinal forces applied to front and rear wheels, along the vehiclefixed $x$-axis |
| $F_{y f}, F_{y r}$ | Lateral forces applied to front and rear wheels, along vehicle-fixed $y$-axis |
| $F_{x e x t}, F_{y e x t}, F_{z e x t}$ | External forces applied to vehicle CG, along the vehicle-fixed $x-, y$-, and $z$ axes |
| $F_{d x}, F_{d y}, F_{d z}$ | Drag forces applied to vehicle CG, along the vehicle-fixed $x$-, $y$-, and $z$-axes |
| $F_{\text {xinput }}, F_{\text {yinput }}, F_{\text {zinput }}$ | Input forces applied to vehicle CG, along the vehicle-fixed $x$-, $y$-, and $z$-axes |
| $M_{\text {xext }}, M_{y e x t}, M_{z e x t}$ | External moment about vehicle CG, about the vehicle-fixed $x$-, $y$-, and $z$ axes |
| $M_{d x}, M_{d y}, M_{d z}$ | Drag moment about vehicle CG, about the vehicle-fixed $x$-, $y$-, and $z$-axes |
| $M_{\text {xinput }}, M_{\text {yinput }}, M_{\text {zinput }}$ | Input moment about vehicle CG, about the vehicle-fixed $x$-, $y$-, and $z$-axes |
| $I_{z z}$ | Vehicle body moment of inertia about the vehicle-fixed $z$-axis |
| $F_{x f t}, F_{x r t}$ | Longitudinal tire force applied to front and rear wheels, along the vehiclefixed $x$-axis |
| $F_{y f t}, F_{y f t}$ | Lateral tire force applied to front and rear wheels, along vehicle-fixed $y$ axis |
| $F_{x f l}, F_{x f r}$ | Longitudinal force applied to front left and front right wheels, along the vehicle-fixed $x$-axis |
| $F_{y f f}, F_{y f r}$ | Lateral force applied to front left and front right wheels, along the vehiclefixed $y$-axis |
| $F_{x r l}, F_{x r r}$ | Longitudinal force applied to rear left and rear right wheels, along the vehicle-fixed $x$-axis |


| $F_{y r l}, F_{y r r}$ | Lateral force applied to rear left and rear right wheels, along the vehiclefixed $y$-axis |
| :---: | :---: |
| $F_{x f l t}, F_{x f r t}$ | Longitudinal tire force applied to front left and front right wheels, along the vehicle-fixed $x$-axis |
| $F_{y f t}, F_{y f r t}$ | Lateral force tire applied to front left and front right wheels, along the vehicle-fixed $y$-axis |
| $F_{x r l t}, F_{x r r t}$ | Longitudinal tire force applied to rear left and rear right wheels, along the vehicle-fixed $x$-axis |
| $F_{y r l t}, F_{y r r t}$ | Lateral force applied to rear left and rear right wheels, along the vehiclefixed $y$-axis |
| $F_{z f}, F_{z r}$ | Normal force applied to front and rear wheels, along vehicle-fixed $z$-axis |
| $F_{\text {znom }}$ | Nominal normal force applied to axles, along the vehicle-fixed $z$-axis |
| $F_{z f l}, F_{z f r}$ | Normal force applied to front left and right wheels, along vehicle-fixed $z$ axis |
| $F_{z r l}, F_{z r r}$ | Normal force applied to rear left and right wheels, along vehicle-fixed $z$ axis |
| $m$ | Vehicle body mass |
| $a, b$ | Distance of front and rear wheels, respectively, from the normal projection point of vehicle CG onto the common axle plane |
| $h$ | Height of vehicle CG above the axle plane |
| $d$ | Lateral distance from the geometric centerline to the center of mass along the vehicle-fixed $y$-axis |
| hh | Height of the hitch above the axle plane along the vehicle-fixed $z$-axis |
| $d h$ | Longitudinal distance of the hitch from the normal projection point of tractor CG onto the common axle plane |
| hl | Lateral distance from center of mass to hitch along the vehicle-fixed y-axis. |
| $\alpha_{f}, \alpha_{r}$ | Front and rear wheel slip angles |
| $\alpha_{f l}, \alpha_{f r}$ | Front left and right wheel slip angles |
| $\alpha_{r l}, \alpha_{r r}$ | Rear left and right wheel slip angles |
| $\delta_{f}, \delta_{r}$ | Front and rear wheel steering angles |
| $\delta_{r l}, \delta_{r r}$ | Rear left and right wheel steering angles |
| $\delta_{f l}, \delta_{f r}$ | Front left and right wheel steering angles |
| $w_{f}, w_{r}$ | Front and rear track widths |
| $C y_{f}, C y_{r}$ | Front and rear wheel cornering stiffness |
| $C y_{\text {fdata }}, C y_{\text {rdata }}$ | Front and rear wheel cornering stiffness data |
| $\sigma_{f}, \sigma_{r}$ | Front and rear wheel relaxation length |
| $\alpha_{f \sigma}, \alpha_{r \sigma}$ | Front and rear wheel slip angles that include relaxation length |
| $v_{w f}, v_{w r}$ | Magnitude of front and rear wheel hardpoint velocity |
| $\mu_{f}, \mu_{r}$ | Front and rear wheel friction coefficient |
| $\mu_{f l}, \mu_{f r}$ | Front left and right wheel friction coefficient |
| $\mu_{r l}, \mu_{r r}$ | Rear left and right wheel friction coefficient |


| $C_{d}$ | Air drag coefficient acting along vehicle-fixed $x$-axis |
| :--- | :--- |
| $C_{s}$ | Air drag coefficient acting along vehicle-fixed $y$-axis |
| $C_{l}$ | Air drag coefficient acting along vehicle-fixed $z$-axis |
| $C_{r m}$ | Air drag roll moment acting about the vehicle-fixed $x$-axis |
| $C_{p m}$ | Air drag pitch moment acting about the vehicle-fixed $y$-axis |
| $C_{y m}$ | Air drag yaw moment acting about the vehicle-fixed $z$-axis |
| $A_{f}$ | Frontal area |
| $R$ | Atmospheric specific gas constant |
| $T$ | Environmental air temperature |
| $P_{a b s}$ | Environmental absolute pressure |
| $w_{x}, w_{y}, w_{z}$ | Wind speed, along the vehicle-fixed $x$-, $y$-, and $z$-axes |
| $W_{x}, W_{y}, W_{z}$ | Wind speed, along inertial $X$-, $Y$-, and $Z$-axes |

## Ports

Input
WhIAngF - Front wheel steering angles
scalar|array
Front wheel steering angles, $\delta_{F}$, in rad.

| Vehicle Track Setting | Variable | Signal Dimension |
| :--- | :--- | :--- |
| Single (bicycle) | $\delta_{F}$ | Scalar - 1 |
| Dual | $\delta_{F}=\left[\delta_{f l} \delta_{f r}\right]$ or $\left[\begin{array}{l}\delta_{f l} \\ \delta_{f r}\end{array}\right]$ | Array - [1x2] or [2x1] |

## Dependencies

To enable this port, on the Input signals pane, select Front wheel steering.
WhIAngR - Rear wheel steering angles
scalar|array
Rear wheel steering angles, $\delta_{R}$, in rad.

| Vehicle Track Setting | Variable | Signal Dimension |
| :--- | :--- | :--- |
| Single (bicycle) | $\delta_{R}$ | Scalar - 1 |
| Dual | $\delta_{R}=\left[\delta_{r l} \delta_{r r}\right]$ or $\left[\begin{array}{l}\delta_{r l} \\ \delta_{r r}\end{array}\right]$ | Array - [1x2] or [2×1] |

## Dependencies

To enable this port, on the Input signals pane, select Rear wheel steering.
xdotin - Longitudinal velocity
scalar

Vehicle CG velocity along the vehicle-fixed $x$-axis, in $\mathrm{m} / \mathrm{s}$.

## Dependencies

To enable this port, set Axle forces to External longitudinal velocity.
FwF - Total force on the front wheels
scalar|array
Force on the front wheels, $F w_{F}$, along the vehicle-fixed axis, in $N$.

| Vehicle <br> Track <br> Setting | Axle Forces Setting | Description | Variable | Signal Dimension |
| :---: | :---: | :---: | :---: | :---: |
| Single <br> (bicycle) | External longitudinal forces | Longitudinal force on the front wheel | $F w F=F x_{f}$ | Scalar - 1 |
|  | External forces | Longitudinal and lateral forces on the front wheel | $F w F=\left[\begin{array}{lll}F x_{f} & F y_{f}\end{array}\right]$ or $\left[\begin{array}{l}F x_{f} \\ F y_{f}\end{array}\right]$ | $\begin{array}{\|l\|} \hline \text { Array }-[1 \times 2] \text { or } \\ {[2 \times 1]} \end{array}$ |
| Dual | External longitudinal forces | Longitudinal force on the front wheels | $F w F=\left[\begin{array}{l} F_{x f l} \\ F_{x f r} \end{array}\right] \text { or }\left[\begin{array}{l} F_{x f l} \\ F_{x f r} \end{array}\right.$ | $\begin{aligned} & \text { Array - }[1 \times 2] \text { or } \\ & {[2 \times 1]} \end{aligned}$ |
|  | External forces | Longitudinal and lateral forces on the front wheels | $F w F=\left[\begin{array}{lll}F_{\chi f l} & F_{x f r} \\ F_{y f l} & F_{y f r}\end{array}\right]$ | Array - [2x2] |

## Dependencies

To enable this port, set Axle forces to one of these options:

- External longitudinal forces
- External forces

FwR - Total force on the rear wheels
scalar|array
Force on the rear wheels, $F w_{R}$, along the vehicle-fixed axis, in $N$.

| Vehicle <br> Track <br> Setting | Axle Forces <br> Setting | Description | Variable | Signal <br> Dimension |
| :--- | :--- | :--- | :--- | :--- |
| Single <br> (bicycle) | External <br> longitudinal <br> forces | Longitudinal <br> force on the rear <br> wheel | $F w R=F x_{r}$ | Scalar - 1 |
|  | External <br> forces | Longitudinal and <br> lateral forces on <br> the rear wheel | $F w R=\left[F x_{r} F y_{r}\right]$ or $\left[\begin{array}{ll}F x_{r} \\ F y_{r}\end{array}\right]$ | Array - [1x2] or <br> $[2 \times 1]$ |


| Vehicle <br> Track <br> Setting | Axle Forces Setting | Description | Variable | Signal Dimension |
| :---: | :---: | :---: | :---: | :---: |
| Dual | External longitudinal forces | Longitudinal force on the rear wheels | $F w R=\left[F_{x r l} F_{x r r}\right] \text { or }\left[\begin{array}{l} F_{x r l} \\ F_{x r r} \end{array}\right.$ | $\begin{aligned} & \text { Array - [1×2] or } \\ & {[2 \times 1]} \end{aligned}$ |
|  | External forces | Longitudinal and lateral forces on the rear wheels | $F w R=\left[\begin{array}{ll} F_{x r l} & F_{x r r} \\ F_{y r l} & F_{y r r} \end{array}\right]$ | Array - [2x2] |

## Dependencies

To enable this port, set Axle forces to one of these options:

- External longitudinal forces
- External forces

FExt - External force on vehicle CG
array
External forces applied to vehicle CG, $F_{\text {xext }}, F_{\text {yext }}, F_{\text {zext }}$, in vehicle-fixed frame, in N. Signal vector dimensions are [ $1 \times 3$ ] or [ $3 \times 1$ ].

## Dependencies

To enable this port, on the Input signals pane, select External forces.

## MExt - External moment about vehicle CG

array
External moment about vehicle CG, $M_{x}, M_{y}, M_{z}$, in the vehicle-fixed frame, in $N \cdot m$. Signal vector dimensions are [ $1 \times 3$ ] or [3x1].

## Dependencies

To enable this port, on the Input signals pane, select External moments.
Fh - Hitch force on the body
array
Hitch force applied to the body at the hitch location, $F h_{x}, F h_{y}, F h_{z}$, in the vehicle-fixed frame, in N, specified as a 1-by-3 or 3-by-1 array.

## Dependencies

To enable this port, under Input signals, select Hitch forces.
Mh - Hitch moment about body
array
Hitch moment at the hitch location, $M h_{x}, M h_{y}, M h_{z}$, about the vehicle-fixed frame, in $\mathrm{N} \cdot \mathrm{m}$, specified as a 1-by-3 or 3-by-1 array.

## Dependencies

To enable this port, under Input signals, select Hitch moments.
WindXYZ - Wind speed
array
Wind speed, $W_{x}, W_{y}, W_{z}$ along inertial $X$-, $Y$-, and $Z$-axes, in $\mathrm{m} / \mathrm{s}$. Signal vector dimensions are [1x3] or [3x1].

## Dependencies

To enable this port, on the Input signals pane, select External wind.
$\mathbf{M u}$ - Tire friction coefficient
scalar
Tire friction coefficient, $\mu$. The value is dimensionless.

| Vehicle Track Setting | Description | Variable | Signal Dimension |
| :--- | :--- | :--- | :--- |
| Single (bicycle) | Longitudinal force on <br> the front wheel | $M u=\left[\begin{array}{ll}\mu_{f} & \mu_{r}\end{array}\right]$ or $\left[\begin{array}{l}\mu_{f} \\ \mu_{r}\end{array}\right]$ | Array - [1x2] or [2x1] |
| Dual | Longitudinal force on <br> the front wheels | $M u=\left[\begin{array}{ll}\mu_{f l} & \mu_{f r} \\ \mu_{r l} & \mu_{r r}\end{array}\right]$ | Array - [2x2] |

## Dependencies

To enable this port, on the Input signals pane, select External friction.

## AirTemp - Ambient air temperature

## scalar

Ambient air temperature, in K.
Dependencies
To enable this port, on the Input signals pane, select Air temperature.
X_0 - Initial longitudinal position
scalar
Initial vehicle CG displacement along the earth-fixed $X$-axis, in m.

## Dependencies

To enable this port, on the Input signals pane, select Initial longitudinal position.
$\mathbf{Y} \mathbf{0}$ - Initial lateral position
scalar

Initial vehicle CG displacement along the earth-fixed $Y$-axis, in $m$.

## Dependencies

To enable this port, on the Input signals pane, select Initial lateral position.
xdot_o - Initial longitudinal position

## scalar

Initial vehicle CG velocity along the vehicle-fixed $x$-axis, in $m / s$.

## Dependencies

To enable this port:
1 Set Axle forces to one of these options:

- External longitudinal forces
- External forces

2 On the Input signals pane, select Initial longitudinal velocity
ydot_o - Initial lateral position
scalar
Initial vehicle CG velocity along the vehicle-fixed $y$-axis, in $\mathrm{m} / \mathrm{s}$.

## Dependencies

To enable this port, on the Input signals pane, select Initial lateral velocity.
psi_o - Initial yaw angle
scalar
Rotation of the vehicle-fixed frame about the earth-fixed $Z$-axis (yaw), in rad.

## Dependencies

To enable this port, on the Input signals pane, select Initial yaw angle.
r_o - Initial yaw rate
scalar
Vehicle angular velocity about the vehicle-fixed $z$-axis (yaw rate), in rad/s.

## Dependencies

To enable this port, on the Input signals pane, select Initial yaw rate.

## Output

Info - Bus signal
bus
Bus signal containing these block values.

| Signal |  |  | Description | Value | Units |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| InertFrm | Cg | Disp | X | Vehicle CG displacement <br> along the earth-fixed $X-$ <br> axis | Computed | m |



| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Signal |  |  | Y | Front right wheel displacement along the earth-fixed $Y$-axis | Computed | m |
|  |  |  | Z | Front right wheel displacement along the earth-fixed $Z$-axis | 0 | m |
|  |  | Vel | $\begin{aligned} & \text { Xdo } \\ & \mathrm{t} \end{aligned}$ | Front right wheel velocity along the earth-fixed $X$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{Ydo} \\ & \mathrm{t} \end{aligned}$ | Front right wheel velocity along the earth-fixed $Y$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{Zdo} \\ & \mathrm{t} \end{aligned}$ | Front right wheel velocity along the earth-fixed Zaxis | 0 | m/s |
| RearAxl | Lft | Disp | X | Rear left wheel displacement along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Y | Rear left wheel displacement along the earth-fixed $Y$-axis | Computed | m |
|  |  |  | Z | Rear left wheel displacement along the earth-fixed Z-axis | 0 | m |
|  |  | Vel | $\begin{aligned} & \mathrm{Xdo} \\ & \mathrm{t} \end{aligned}$ | Rear left wheel velocity along the earth-fixed $X$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{Ydo} \\ & \mathrm{t} \end{aligned}$ | Rear left wheel velocity along the earth-fixed $Y$ axis | Computed | m/s |
|  |  |  | $\underset{t}{Z d o}$ | Rear left wheel velocity along the earth-fixed Zaxis | 0 | m/s |
|  | Rght | Disp | X | Rear right wheel displacement along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Y | Rear right wheel displacement along the earth-fixed $Y$-axis | Computed | m |
|  |  |  | Z | Rear right wheel displacement along the earth-fixed $Z$-axis | 0 | m |
|  |  | Vel | $\begin{aligned} & \mathrm{Xdo} \\ & \mathrm{t} \end{aligned}$ | Rear right wheel velocity along the earth-fixed $X$ axis | Computed | m/s |


| Signal |  |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{aligned} & \mathrm{Ydo} \\ & \mathrm{t} \end{aligned}$ | Rear right wheel velocity along the earth-fixed $Y$ axis | Computed | $\mathrm{m} / \mathrm{s}$ |
|  |  |  |  | $\underset{+}{Z \mathrm{Zdo}}$ | Rear right wheel velocity along the earth-fixed Zaxis | 0 | m/s |
|  | Hitch | Disp | X |  | Hitch offset from axle plane along the earthfixed $X$-axis | Computed | m |
|  |  |  | Y |  | Hitch offset from center plane along the earthfixed $Y$-axis | Computed | m |
|  |  |  | Z |  | Hitch offset from axle plane along the earthfixed $Z$-axis | Computed | m |
|  |  | Vel | Xdot |  | Hitch offset velocity from axle plane along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Ydot |  | Hitch offset velocity from center plane along the earth-fixed $Y$-axis | Computed | m |
|  |  |  | Zdot |  | Hitch offset velocity from axle plane along the earth-fixed Z-axis | Computed | m |
|  | Geom | Disp | X |  | Vehicle chassis offset from axle plane along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Y |  | Vehicle chassis offset from center plane along the earth-fixed $Y$-axis | Computed | m |
|  |  |  | Z |  | Vehicle chassis offset from axle plane along the earth-fixed Z-axis | Computed | m |
|  |  | Vel | Xdot |  | Vehicle chassis offset velocity along the earthfixed $X$-axis | Computed | m/s |
|  |  |  | Ydot |  | Vehicle chassis offset velocity along the earthfixed $Y$-axis | Computed | $\mathrm{m} / \mathrm{s}$ |
|  |  |  | Zdot |  | Vehicle chassis offset velocity along the earthfixed $Z$-axis | Computed | m/s |
| BdyFrm | Cg | Vel | xdot |  | Vehicle CG velocity along the vehicle-fixed $x$-axis | Computed | m/s |



| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | DCM | Direction cosine matrix |  |  | Computed | rad |
| Forces | Body | Fx |  | Net force on vehicle CG along the vehicle-fixed $x$ axis | Computed | N |
|  |  | Fy |  | Net force on vehicle CG along the vehicle-fixed $y$ axis | Computed | N |
|  |  | Fz |  | Net force on vehicle CG along the vehicle-fixed $z$ axis | 0 | N |
|  | Ext | Fx |  | External force on vehicle CG along the vehicle-fixed $x$-axis | Computed | N |
|  |  | Fy |  | External force on vehicle CG along the vehicle-fixed $y$-axis | Computed | N |
|  |  | Fz |  | External force on vehicle CG along the vehicle-fixed $z$-axis | 0 | N |
|  | Hitch | FX |  | Hitch force applied to body at the hitch location along the vehicle-fixed $x$ axis | Input | N |
|  |  | Fy |  | Hitch force applied to body at the hitch location along the vehicle-fixed $y$ axis | Input | N |
|  |  | Fz |  | Hitch force applied to body at the hitch location along the vehicle-fixed $z$ axis | Input | N |
|  | FrntAxl | Lft | FX | Longitudinal force on left front wheel, along the vehicle-fixed $x$-axis | Computed | N |
|  |  |  | Fy | Lateral force on left front wheel along the vehiclefixed $y$-axis | Computed | N |
|  |  |  | Fz | Normal force on left front wheel, along the vehiclefixed $z$-axis | Computed | N |
|  |  | Rght | FX | Longitudinal force on right front wheel, along the vehicle-fixed $x$-axis | Computed | N |


| Signal |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Fy | Lateral force on right front wheel along the vehicle-fixed $y$-axis | Computed | N |
|  |  | Fz | Normal force on right front wheel, along the vehicle-fixed $z$-axis | Computed | N |
| RearAxl | Lft | Fx | Longitudinal force on left rear wheel, along the vehicle-fixed $x$-axis | Computed | N |
|  |  | Fy | Lateral force on left rear wheel along the vehiclefixed $y$-axis | Computed | N |
|  |  | Fz | Normal force on left rear wheel, along the vehiclefixed $z$-axis | Computed | N |
|  | Rght | Fx | Longitudinal force on right rear wheel, along the vehicle-fixed $x$-axis | Computed | N |
|  |  | Fy | Lateral force on right rear wheel along the vehiclefixed $y$-axis | Computed | N |
|  |  | Fz | Normal force on right rear wheel, along the vehiclefixed $z$-axis | Computed | N |
| Tires | FrntTir es |  | Front left tire force, along the vehicle-fixed $x$-axis | Computed | N |
|  |  | t $\begin{aligned} & \text { F } \\ & \text { y }\end{aligned}$ | Front left tire force, along the vehicle-fixed $y$-axis | Computed | N |
|  |  | F | Front left tire force, along the vehicle-fixed $z$-axis | Computed | N |
|  |  |  | Front right tire force, along the vehicle-fixed $x$ axis | Computed | N |
|  |  | t $\begin{aligned} & \text { F } \\ & \text { y }\end{aligned}$ | Front right tire force, along the vehicle-fixed $y$ axis | Computed | N |
|  |  | F | Front right tire force, along the vehicle-fixed $z$ axis | Computed | N |
|  | $\begin{aligned} & \text { RearTir } \\ & \text { es } \end{aligned}$ | L F <br> f X <br>   <br>   | Rear left tire force, along the vehicle-fixed $x$-axis | Computed | N |
|  |  | tF <br> y | Rear left tire force, along the vehicle-fixed $y$-axis | Computed | N |


| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{aligned} & \mathrm{F} \\ & \mathrm{z} \end{aligned}$ | Rear left tire force, along the vehicle-fixed $z$-axis | Computed | N |
|  |  |  | $R$ $F$ <br> g x <br> h  <br>   | Rear right tire force, along the vehicle-fixed $x$ axis | Computed | N |
|  |  |  | $\mathrm{t} \stackrel{\mathrm{~F}}{\mathrm{~F}} \mathrm{y}$ | Rear right tire force, along the vehicle-fixed $y$ axis | Computed | N |
|  |  |  | $\begin{aligned} & \mathrm{F} \\ & \mathrm{z} \end{aligned}$ | Rear right tire force, along the vehicle-fixed $z$ axis | Computed |  |
|  | Drag | FX |  | Drag force on vehicle CG along the vehicle-fixed $x$ axis | Computed | N |
|  |  | Fy |  | Drag force on vehicle CG along the vehicle-fixed $y$ axis | Computed | N |
|  |  | Fz |  | Drag force on vehicle CG along the vehicle-fixed $z$ axis | Computed | N |
|  | Grvty | FX |  | Gravity force on vehicle CG along the vehicle-fixed x-axis | Computed | N |
|  |  | Fy |  | Gravity force on vehicle CG along the vehicle-fixed $y$-axis | Computed | N |
|  |  | Fz |  | Gravity force on vehicle CG along the vehicle-fixed $z$-axis | Computed | N |
| Moments | Body | Mx |  | Body moment on vehicle CG about the vehicle-fixed $x$-axis | 0 | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | My |  | Body moment on vehicle CG about the vehicle-fixed $y$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | Mz |  | Body moment on vehicle CG about the vehicle-fixed $z$-axis | 0 | $\mathrm{N} \cdot \mathrm{m}$ |
|  | Drag | Mx |  | Drag moment on vehicle CG about the vehicle-fixed x-axis | 0 | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | My |  | Drag moment on vehicle CG about the vehicle-fixed $y$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |



|  |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Signal |  |  | z | Front right wheel displacement along the vehicle-fixed $z$-axis | Computed | m |
|  |  | Vel | $\begin{aligned} & \hline x d o \\ & t \end{aligned}$ | Front right wheel velocity along the vehicle-fixed $x$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \text { ydo } \\ & \text { t } \end{aligned}$ | Front right wheel velocity along the vehicle-fixed $y$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{zdo} \\ & \mathrm{t} \end{aligned}$ | Front right wheel velocity along the vehicle-fixed $z$ axis | 0 | m/s |
|  | Steer | WhlAngFL |  | Front left wheel steering angle | Computed | rad |
|  |  | WhlAngFR |  | Front right wheel steering angle | Computed | rad |
| RearAxl | Lft | Disp | x | Rear left wheel displacement along the vehicle-fixed $x$-axis | Computed | m |
|  |  |  | y | Rear left wheel displacement along the vehicle-fixed $y$-axis | Computed | m |
|  |  |  | z | Rear left wheel displacement along the vehicle-fixed $z$-axis | Computed | m |
|  |  | Vel | $\begin{aligned} & \mathrm{xdo} \\ & \mathrm{t} \end{aligned}$ | Rear left wheel velocity along the vehicle-fixed $x$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{ydo} \\ & \mathrm{t} \end{aligned}$ | Rear left wheel velocity along the vehicle-fixed $y$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{zdo} \\ & \mathrm{t} \end{aligned}$ | Rear left wheel velocity along the vehicle-fixed $z$ axis | 0 | m/s |
|  | Rght | Disp | x | Rear right wheel displacement along the vehicle-fixed $x$-axis | Computed | m |
|  |  |  | y | Rear right wheel displacement along the vehicle-fixed $y$-axis | Computed | m |
|  |  |  | z | Rear right wheel displacement along the vehicle-fixed $z$-axis | Computed | m |


|  |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Signal |  | Vel | $\begin{aligned} & \mathrm{xdo} \\ & \mathrm{t} \end{aligned}$ | Rear right wheel velocity along the vehicle-fixed $x$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{ydo} \\ & \mathrm{t} \end{aligned}$ | Rear right wheel velocity along the vehicle-fixed $y$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{zdo} \\ & \mathrm{t} \end{aligned}$ | Rear right wheel velocity along the vehicle-fixed $z$ axis | 0 | m/s |
|  | Steer | WhlangRL |  | Rear left wheel steering angle | Computed | rad |
|  |  | WhlangRR |  | Rear right wheel steering angle | Computed | rad |
| Hitch | Disp |  | X | Hitch offset from axle plane along the vehiclefixed $x$-axis | Input | m |
|  |  |  | y | Hitch offset from center plane along the vehiclefixed $y$-axis | Input | m |
|  |  |  | z | Hitch offset from axle plane along the earthfixed $z$-axis | Input | m |
|  | Vel |  | $\begin{aligned} & \mathrm{xdo} \\ & \mathrm{t} \end{aligned}$ | Hitch offset velocity along the vehicle-fixed $x$-axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{ydo} \\ & \mathrm{t} \end{aligned}$ | Hitch offset velocity along the vehicle-fixed $y$-axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{zdo} \\ & \mathrm{t} \end{aligned}$ | Hitch offset velocity along the vehicle-fixed $z$-axis | Computed | m/s |
| Pwr | Ext |  |  | Applied external power | Computed | W |
|  | Hitch |  |  | Power loss due to hitch | Computed | W |
|  | Drag |  |  | Power loss due to drag | Computed | W |
| Geom | Disp |  | x | Vehicle chassis offset from axle plane along the vehicle-fixed $x$-axis | Input | m |
|  |  |  | y | Vehicle chassis offset from center plane along the vehicle-fixed $y$-axis | Input | m |
|  |  |  | z | Vehicle chassis offset from axle plane along the earth-fixed $z$-axis | Input | m |
|  | Vel |  | $\begin{aligned} & \mathrm{xdo} \\ & \mathrm{t} \end{aligned}$ | Vehicle chassis offset velocity along the vehiclefixed $x$-axis | Computed | m/s |


| Signal |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \text { ydo } \\ & t \end{aligned}$ | Vehicle chassis offset velocity along the vehiclefixed $y$-axis | Computed | m/s |
|  |  | $\begin{aligned} & \text { zdo } \\ & t \end{aligned}$ | Vehicle chassis offset velocity along the vehiclefixed $z$-axis | 0 | m/s |
|  | Beta | Bet a | Body slip angle, $\beta$ $\beta=\frac{V_{y}}{V_{x}}$ | Computed | rad |


| Signal |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: |
| PwrInfo | PwrTrnsfrd | PwrFxExt | Externally applied longitudinal force power | Comp uted | W |
|  |  | PwrFyExt | Externally applied lateral force power | Comp uted | W |
|  |  | PwrMzExt | Externally applied roll moment power | Comp uted | W |
|  |  | PwrFwFLx | Longitudinal force applied at the front left axle power | Comp uted | W |
|  |  | PwrFwFLy | Lateral force applied at the front left axle power | Comp uted | W |
|  |  | PwrFwFRx | Longitudinal force applied at the front right axle power | Comp uted | W |
|  |  | PwrFwFRy | Lateral force applied at the front right axle power | Comp uted | W |
|  |  | PwrFwRLx | Longitudinal force applied at the rear left axle power | Comp uted | W |
|  |  | PwrFwRLy | Lateral force applied at the rear left axle power | Comp uted | W |
|  |  | PwrFwRRx | Longitudinal force applied at the rear right axle power | Comp uted | W |
|  |  | PwrFwRRy | Lateral force applied at the rear right axle power | Comp uted | W |
|  | PwrNotTrnsfr d | PwrFxDrag | Longitudinal drag force power | Comp uted | W |
|  |  | PwrFyDrag | Lateral drag force power | Comp uted | W |
|  |  | PwrMzDrag | Drag pitch moment power | Comp uted | W |
|  | PwrStored | PwrStoredGrvty | Rate change in gravitational potential energy | Comp uted | W |


| Signal |  | Description | Value | Units |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  |  | PwrStoredxdot | Rate of change of longitudinal <br> kinetic energy | Comp <br> uted | W |
|  |  | PwrStoredydot | Rate of change of lateral kinetic <br> energy | Comp <br> uted | W |
|  |  | PwrStoredr | Rate of change of rotational yaw <br> kinetic energy | Comp <br> uted | W |

xdot - Vehicle longitudinal velocity
scalar
Vehicle CG velocity along the vehicle-fixed $x$-axis, in $m / s$.
ydot - Vehicle lateral velocity
scalar
Vehicle CG velocity along the vehicle-fixed $y$-axis, in $\mathrm{m} / \mathrm{s}$.
psi - Yaw
scalar
Rotation of the vehicle-fixed frame about the earth-fixed $Z$-axis (yaw), in rad.
$\mathbf{r}$ - Yaw rate
scalar
Vehicle angular velocity, r , about the vehicle-fixed $z$-axis (yaw rate), in rad/s.
FzF - Normal force on front wheels
scalar|array
Normal force on front wheels, $F z_{F}$, along the vehicle-fixed $z$-axis, in N .

| Vehicle Track <br> Setting | Description | Variable | Signal Dimension |
| :--- | :--- | :--- | :--- |
| Single <br> (bicycle) | Normal force on front <br> axle | $F z F=F z_{f}$ | Scalar - 1 |
| Dual | Normal force on the <br> front wheels | $F z F=\left[F z_{f l} F z_{f r}\right]$ | Array - [1×2] |

FzR - Normal force on rear wheels
scalar|array
Normal force on rear wheels, $F z_{R}$, along the vehicle-fixed $z$-axis, in N .

| Vehicle Track <br> Setting | Description | Variable | Signal Dimension |
| :--- | :--- | :--- | :--- |
| Single (bicycle) | Normal force on rear <br> wheel | $F z R=F z_{r}$ | Scalar - 1 |


| Vehicle Track <br> Setting | Description | Variable | Signal Dimension |
| :--- | :--- | :---: | :--- |
| Dual | Normal force on the <br> rear wheels | $F z R=\left[F z_{r l} F z_{r r}\right]$ | Array - [1x2] |

## Parameters

## Options

Vehicle track - Number of wheels
Single (bicycle)|Dual
In the Vehicle Dynamics Blockset library, there are two types of Vehicle Body 3DOF blocks that model longitudinal, lateral, and yaw motion.

| Block | Vehicle Track <br> Setting | Implementation |
| :--- | :--- | :--- |
| Vehicle Body 3DOF Single Track | Single <br> (bicycle) | Forces act along the center line at the front <br> and rear axles. <br> No lateral load transfer. |
| Vehicle Body 3DOF Dual Track | Dual | Forces act at the four vehicle corners or hard <br> points. |
| Wwhing |  |  |

Axle forces - Type of axle force
External longitudinal velocity|External longitudinal forces|External forces
Use the Axle forces parameter to specify the type of force.

| Axle Forces Setting | Implementation |
| :---: | :---: |
| External longitudinal velocity | - The block assumes that the external longitudinal velocity is in a quasi-steady state, so the longitudinal acceleration is approximately zero. <br> - Because the motion is quasi-steady, the block calculates lateral forces using the tire slip angles and linear cornering stiffness. <br> - Consider this setting when you want to: <br> - Generate virtual sensor signal data. <br> - Conduct high-level software studies that are not impacted by driveline or nonlinear tire responses. |
| External longitudinal forces | - The block uses the external longitudinal force to accelerate or brake the vehicle. <br> - The block calculates lateral forces using the tire slip angles and linear cornering stiffness. <br> - Consider this setting when you want to: <br> - Account for changes in the longitudinal velocity on the lateral and yaw motion. <br> - Specify the external longitudinal motion through a force instead of an external longitudinal velocity. <br> - Connect the block to tractive actuators, wheels, brakes, and hitches. |
| External forces | - The block uses the external lateral and longitudinal forces to steer, accelerate, or brake the vehicle. <br> - The block does not use the steering input to calculate vehicle motion. <br> - Consider this setting when you need tire models with more accurate nonlinear combined lateral and longitudinal slip. |

Input Signals
Front wheel steering - WhlAngF input port
on (default) | off
Specify to create input port WhlAngF.
External wind - WindXYZ input port
off (default) | on
Specify to create input port WindXYZ.
External forces - FExt input port
off (default) | on
Specify to create input port FExt.
External moments - MExt input port
off (default) | on

Specify to create input port MExt.
Rear wheel steering - WhlAngR input port off (default) | on

Specify to create input port WhlAngR.
External friction - Mu input port
off (default) | on
Specify to create input port Mu.
Hitch forces - Fh input port
on (default) | off
Select to create input port Fh.
Hitch moments - Mh input port
on (default) | off
Specify to create input port Mh.
Initial longitudinal position - X_o input port
off (default) | on
Specify to create input port X_0.
Initial lateral position - Y _o input port
off (default) | on
Specify to create input port Y_o.
Initial longitudinal velocity — xdot_o input port
off (default) | on
Specify to create input port xdot_o.
Initial lateral velocity - ydot_o input port
off (default) | on
Specify to create input port ydot_o.
Initial yaw angle - psi_o input port
off (default)|on
Specify to create input port psi_o.
Initial yaw rate - r_o input port
off (default) |on
Specify to create input port r_o.
Air temperature - AirTemp input port
off (default) |on
Specify to create input port AirTemp.

## Longitudinal

Number of wheels on front axle, NF - Front wheel count
2 (default) | scalar
Number of wheels on front axle, $N_{F}$. The value is dimensionless.
Number of wheels on rear axle, NR - Rear wheel count
2 (default) | scalar
Number of wheels on rear axle, $N_{R}$. The value is dimensionless.
Vehicle mass, $\mathbf{m}$ - Vehicle mass
2000 (default) | scalar
Vehicle mass, $m$, in kg .
Longitudinal distance from center of mass to front axle, a - Front axle distance 1.4 (default) | scalar

Horizontal distance $a$ from the vehicle CG to the front wheel axle, in $m$.
Longitudinal distance from center of mass to rear axle, b - Rear axle distance 1.6 (default) | scalar

Horizontal distance $b$ from the vehicle CG to the rear wheel axle, in m .
Vertical distance from center of mass to axle plane, $\mathbf{h}$ - Height
0.35 (default) | scalar

Height of vehicle CG above the axles, $h$, in $m$.
Longitudinal distance from center of mass to hitch, $\mathbf{d h}$ - Distance from CM to hitch 1 (default) | scalar

Longitudinal distance from center of mass to hitch, $d h$, in m.

## Dependencies

To enable this parameter, on the Input signals pane, select Hitch forces or Hitch moments.
Vertical distance from hitch to axle plane, hh - Distance from hitch to axle plane 0.2 (default) | scalar

Vertical distance from hitch to axle plane, $h h$, in $m$.

## Dependencies

To enable this parameter, on the Input signals pane, select Hitch forces or Hitch moments.
Initial inertial frame longitudinal position, X_o - Position
0 (default) | scalar
Initial vehicle CG displacement along earth-fixed $X$-axis, in $m$.
Initial longitudinal velocity, xdot_o - Velocity
0 (default) | scalar

Initial vehicle CG velocity along vehicle-fixed $x$-axis, in $\mathrm{m} / \mathrm{s}$.

## Dependencies

For the Vehicle Body 3DOF Single Track or Vehicle Body 3DOF Dual Track blocks, to enable this parameter, set Axle forces to one of these options:

- External longitudinal forces
- External forces


## Lateral

Front tire corner stiffness, Cy_f - Stiffness
12e3 (default) | scalar
Front tire corner stiffness, $C y_{f}$, in $\mathrm{N} / \mathrm{rad}$.

## Dependencies

For the Vehicle Body 3DOF Single Track or Vehicle Body 3DOF Dual Track blocks, to enable this parameter:

1 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces

2 Clear Mapped corner stiffness.
Rear tire corner stiffness, Cy_r - Stiffness
11e3 (default) | scalar
Rear tire corner stiffness, $C y_{r}$, in N/rad.

## Dependencies

For the Vehicle Body 3DOF Single Track or Vehicle Body 3DOF Dual Track blocks, to enable this parameter:

1 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces


## 2 Clear Mapped corner stiffness.

Initial inertial frame lateral displacement, Y_o - Position
0 (default) | scalar
Initial vehicle CG displacement along earth-fixed $Y$-axis, in m.
Initial lateral velocity, ydot_o - Velocity
0 (default) | scalar
Initial vehicle CG velocity along vehicle-fixed $y$-axis, in $m / s$.
Mapped corner stiffness - Selection
off (default) | on

Enables mapped corner stiffness calculation.

## Dependencies

To enable this parameter, set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces

Include relaxation length dynamics - Enable relaxation length dynamics
on (default) | off
Enables relaxation length dynamics.

## Dependencies

To enable this parameter:
1 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces


## 2 Clear Mapped corner stiffness.

Lateral distance from geometric centerline to center of mass, d - Distance
0 (default) | scalar
Lateral distance from geometric centerline to center of mass, $d$, in $m$, along the vehicle-fixed $y$. Positive values indicate that the vehicle CM is to the right of the geometric centerline. Negative values indicate that the vehicle CM is to the left of the geometric centerline.

Lateral distance from geometric centerline to hitch, hl - Distance
0 (default) | scalar
Lateral distance from geometric centerline to the hitch, $h l$, in $m$, along the vehicle-fixed $y$. Positive values indicate that the hitch is to the right of the geometric centerline. Negative values indicate that the hitch is to the left of the geometric centerline.

## Dependencies

To enable this parameter, on the Input signals pane, select Hitch forces or Hitch moments.
Track width - Width
[1.4,1.4] (default)| 1-by-2 vector
Track width, $w$, in .

## Dependencies

To enable this parameter, set Vehicle track to Dual.
Front tire(s) relaxation length, sigma_f - Relaxation length
. 1 (default) | scalar
Front tire relaxation length, $\sigma_{f}$, in m .

## Dependencies

To enable this parameter:
1 Set Vehicle track to one of these options:

- Single 2-axle
- Dual 2-axle
- Single 3-axle
- Dual 3-axle

2 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces

3 Do either of these:

- Select Mapped corner stiffness.
- Clear Mapped corner stiffness and select Include relaxation length dynamics.

Rear tire(s) relaxation length, sigma_r - Relaxation length
. 1 (default) | scalar
Rear tire relaxation length, $\sigma_{r}$, in m .

## Dependencies

To enable this parameter:
1 Set Vehicle track to one of these options:

- Single 2-axle
- Dual 2-axle
- Single 3-axle
- Dual 3-axle

2 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces

3 Do either of these:

- Select Mapped corner stiffness.
- Clear Mapped corner stiffness and select Include relaxation length dynamics.


## Front axle slip angle breakpoints, alpha_f_brk - Breakpoints

[-. 1 .1] (default)|vector
Front axle slip angle breakpoints, $\alpha_{f b r k}$, in rad.

## Dependencies

To enable this parameter:

1 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces

2 Select Mapped corner stiffness.
Front axle corner data, Cy_f_data - Breakpoints
[-9e3 9e3] (default) |vector
Front axle corner data, $C y_{f d a t a}$, in $\mathrm{N} / \mathrm{rad}$.

## Dependencies

To enable this parameter:
1 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces

2 Select Mapped corner stiffness.
Rear axle slip angle breakpoints, alpha_r_brk - Breakpoints
[-. 1 .1] (default)|vector
Rear axle slip angle breakpoints, $\alpha_{r b r k}$, in rad.
Dependencies
To enable this parameter:
1 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces


## 2 Select Mapped corner stiffness.

Rear axle corner data, Cy_r_data - Data
[-9e3 9e3] (default) |vector
Rear axle corner data, $C y_{\text {rdata }}$, in $\mathrm{N} /$ rad.

## Dependencies

To enable this parameter:
1 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces

2 Select Mapped corner stiffness.
Yaw
Yaw polar inertia, Izz - Inertia
4000 (default) | scalar

Yaw polar inertia, in $\mathrm{kg}^{*} \mathrm{~m}^{\wedge} 2$.
Initial yaw angle, psi_o - Psi rotation
0 (default) | scalar
Rotation of the vehicle-fixed frame about earth-fixed Z-axis (yaw), in rad.
Initial yaw rate, r_o - Yaw rate
0 (default) | scalar
Vehicle angular velocity about the vehicle-fixed $z$-axis (yaw rate), in rad/s.

## Aerodynamic

Longitudinal drag area, Af - Effective vehicle cross-sectional area
2 (default) | scalar
Effective vehicle cross-sectional area, $A_{f}$, to calculate the aerodynamic drag force on the vehicle, in $\mathrm{m}^{2}$.

Longitudinal drag coefficient, Cd - Air drag coefficient
. 3 (default) | scalar
Air drag coefficient, $C_{d}$. The value is dimensionless.
Longitudinal lift coefficient, CI - Air lift coefficient
. 1 (default) | scalar
Air lift coefficient, $C_{l}$. The value is dimensionless.

## Longitudinal drag pitch moment, Cpm - Pitch drag

. 1 (default) | scalar
Longitudinal drag pitch moment coefficient, $C_{p m}$. The value is dimensionless.
Relative wind angle vector, beta_w - Wind angle
[0:0.01:0.3] (default) | vector
Relative wind angle vector, $\beta_{w}$, in rad.
Side force coefficient vector, Cs - Side force coefficient
[0:0.03:0.9] (default) | vector
Side force coefficient vector coefficient, $C_{s}$. The value is dimensionless.
Yaw moment coefficient vector, Cym - Yaw moment drag
[0:0.01:0.3] (default) | vector
Yaw moment coefficient vector coefficient, $C_{y m}$. The value is dimensionless.

## Environment

Absolute air pressure, Pabs - Pressure
101325 (default) | scalar | scalar
Environmental absolute pressure, $P_{a b s}$, in Pa.

Air temperature, Tair - Temperature
273 (default) | scalar
Environmental absolute temperature, $T$, in K .

## Dependencies

To enable this parameter, clear Air temperature.
Gravitational acceleration, g-Gravity
9.81 (default) | scalar

Gravitational acceleration, $g$, in $\mathrm{m} / \mathrm{s}^{\wedge} 2$.
Nominal friction scaling factor, mu - Friction scale factor
1 (default) | scalar
Nominal friction scale factor, $\mu$. The value is dimensionless.

## Dependencies

For the Vehicle Body 3DOF Single Track or Vehicle Body 3DOF Dual Track blocks, to enable this parameter:

1 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces


## 2 Clear External Friction.

## Simulation

## Longitudinal velocity tolerance, xdot_tol - Tolerance

## . 01 (default) | scalar

Longitudinal velocity tolerance, in $\mathrm{m} / \mathrm{s}$.
Nominal normal force, Fznom - Normal force
5000 (default) | scalar
Nominal normal force, in N .

## Dependencies

For the Vehicle Body 3DOF Single Track or Vehicle Body 3DOF Dual Track blocks, to enable this parameter, set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces

Geometric longitudinal offset from axle plane, longOff - Longitudinal offset 0 (default) | scalar

Vehicle chassis offset from axle plane along body-fixed $x$-axis, in $m$. When you use the 3D visualization engine, consider using the offset to locate the chassis independent of the vehicle CG.

Geometric lateral offset from center plane, latOff - Lateral offset
0 (default) | scalar
Vehicle chassis offset from center plane along body-fixed $y$-axis, in $m$. When you use the 3D visualization engine, consider using the offset to locate the chassis independent of the vehicle CG.

Geometric vertical offset from axle plane, vertOff - Vertical offset 0 (default) | scalar

Vehicle chassis offset from axle plane along body-fixed $z$-axis, in m . When you use the 3D visualization engine, consider using the offset to locate the chassis independent of the vehicle CG.

Wrap Euler angles, wrapAng - Selection
off (default) | on
Wrap the Euler angles to the interval [-pi, pi]. For vehicle maneuvers that might undergo vehicle yaw rotations that are outside of the interval, consider deselecting the parameter if you want to:

- Track the total vehicle yaw rotation.
- Avoid discontinuities in the vehicle state estimators.


## Version History <br> Introduced in R2018a

## References

[1] Gillespie, Thomas. Fundamentals of Vehicle Dynamics. Warrendale, PA: Society of Automotive Engineers (SAE), 1992.

## Extended Capabilities

## C/C++ Code Generation

Generate C and C++ code using Simulink ${ }^{\circledR}$ Coder ${ }^{\mathrm{TM}}$.

## See Also

Vehicle Body 3DOF Longitudinal | Vehicle Body 6DOF | Vector Concatenate, Matrix Concatenate
Topics
"Coordinate Systems in Vehicle Dynamics Blockset"

## Vehicle Body 6DOF

Two-axle vehicle body with translational and rotational motion


## Libraries:

Vehicle Dynamics Blockset / Vehicle Body

## Description

The Vehicle Body 6DOF block implements a six degrees-of-freedom (DOF) rigid two-axle vehicle body model to calculate longitudinal, lateral, vertical, pitch, roll, and yaw motion. The block accounts for body mass, inertia, aerodynamic drag, road incline, and weight distribution between the axles due to suspension and external forces and moments. Use the Inertial Loads parameters to analyze the vehicle dynamics under different loading conditions.

You can connect the block to virtual sensors, suspension system, or external systems like body control actuators. Use the Vehicle Body 6DOF block in ride and handling studies to model the effects of drag forces, passenger loading, and suspension hardpoint locations.

To create additional input ports, under Input signals, select these block parameters.

| Parameter | Input Port | Description |
| :--- | :--- | :--- |
| Front hitch forces | FhF | Hitch force applied to the body at the front hitch location, <br> $F h F_{x}, F h F_{y}$, and $F h F_{z}$, in the vehicle-fixed frame |
| Front hitch moments | MhF | Hitch moment at the front hitch location, $M h F_{x}, M h F_{y}$, and <br> $M h F_{z}$, about the vehicle-fixed frame |
| Rear hitch forces | FhR | Hitch force applied to the body at the rear hitch location, <br> $F h R_{x}, F h R_{y}$, and $F h R_{z}$, in the vehicle-fixed frame |
| Rear hitch moments | MhR | Hitch moment at the rear hitch location, $M h R_{x}, M h R_{y}$, and <br> $M h R_{z}$, about the vehicle-fixed frame |

## Inertial Loads

To analyze the vehicle dynamics under different loading conditions, use the Inertial Loads parameters. Specifically, you can specify these loads:

- Front powertrain
- Front and rear row passengers
- Overhead cargo
- Rear cargo

For each of the loads, you can specify the mass, location, and inertia.
The illustrations provide the load locations and vehicle parameter dimensions. The table provides the corresponding location parameter sign settings.


This table summarizes the parameter settings that specify the load locations indicated by the dots. For the location, the block uses this distance vector:

- Front suspension hardpoint to load, along the vehicle-fixed $x$-axis
- Vehicle centerline to load, along the vehicle-fixed $y$-axis
- Front suspension hardpoint to load, along the vehicle-fixed $z$-axis

| Load | Parameter | Example Location |
| :---: | :---: | :---: |
| Front | Distance vector from front axle, z1R | - $\operatorname{z1R}(1,1)<0-$ Forward of the front axle <br> - $\operatorname{z1R}(1,2)>0-$ Right of the vehicle centerline <br> - $\operatorname{z1R}(1,3)>0-$ Above the front axle suspension hardpoint |
| Overhead | Distance vector from front axle, z2R | - $\operatorname{z2R}(1,1)>0-$ Rear of the front axle <br> - $z 2 R(1,2)<0-$ Left of the vehicle centerline <br> - $\operatorname{z2R}(1,3)>0-$ Above the front axle suspension hardpoint |
| Row 1, left side | Distance vector from front axle, z3R | - $\operatorname{z3R}(1,1)>0-$ Rear of the front axle <br> - $z 3 R(1,2)<0-$ Left of the vehicle centerline <br> - $z 3 R(1,3)>0-$ Above the front axle suspension hardpoint |
| Row 1, right side | Distance vector from front axle, z4R | - $\quad \operatorname{z4R}(1,1)>0-$ Rear of the front axle <br> - $z 4 R(1,2)>0-$ Right of the vehicle centerline <br> - $z 4 R(1,3)>0-$ Above the front axle suspension hardpoint |
| Row 2, left side | Distance vector from front axle, z5R | - $\quad \operatorname{z5R}(1,1)>0-$ Rear of the front axle <br> - $z 5 R(1,2)<0-$ Left of the vehicle centerline <br> - $z 5 R(1,3)>0-$ Above the front axle suspension hardpoint |
| Row 2, right side | Distance vector from front axle, z6R | - $\operatorname{z6R}(1,1)>0-$ Rear of the front axle <br> - $z 6 R(1,2)>0-$ Right of the vehicle centerline <br> - $\quad \operatorname{z6R}(1,3)>0-$ Above the front axle suspension hardpoint |
| Rear | Distance vector from front axle, z7R | - $\quad \operatorname{z7R}(1,1)>0-$ Rear of the front axle <br> - $z 7 R(1,2)>0-$ Right of the vehicle centerline <br> - $\quad \operatorname{z7R}(1,3)>0-$ Above the front axle suspension hardpoint |

## Equations of Motion

To determine the vehicle motion, the block implements calculations for the rigid body vehicle dynamics, wind drag, inertial loads, and coordinate transformations. The body-fixed and the vehiclefixed are the same coordinate systems.

The Vehicle Body 6DOF block considers the rotation of a body-fixed coordinate frame about a flat earth-fixed inertial reference frame. The origin of the body-fixed coordinate frame is the vehicle center of gravity of the body.


The block uses this equation to calculate the translational motion of the body-fixed coordinate frame, where the applied forces $\left[F_{x} F_{y} F_{z}\right]^{\mathrm{T}}$ are in the body-fixed frame, and the mass of the body, $m$, is assumed constant.

$$
\begin{aligned}
& \bar{F}_{b}=\left[\begin{array}{l}
F_{x} \\
F_{y} \\
F_{z}
\end{array}\right]=m\left(\dot{\bar{V}}_{b}+\bar{\omega} \times \bar{V}_{b}\right) \\
& \bar{M}_{b}=\left[\begin{array}{l}
L \\
M \\
N
\end{array}\right]=I \dot{\bar{\omega}}+\bar{\omega} \times(I \bar{\omega}) \\
& I=\left[\begin{array}{ccc}
I_{x x} & -I_{x y} & -I_{x z} \\
-I_{y x} & I_{y y} & -I_{y z} \\
-I_{z x} & -I_{z y} & I_{z z}
\end{array}\right]
\end{aligned}
$$

To determine the relationship between the body-fixed angular velocity vector, $\left[\begin{array}{l}p q r\end{array}\right]^{\mathrm{T}}$, and the rate of change of the Euler angles, $\left[\begin{array}{lll}\dot{\phi} & \dot{\theta} & \dot{\psi}\end{array}\right]^{T}$, the block resolves the Euler rates into the body-fixed frame.

$$
\left[\begin{array}{l}
p \\
q \\
r
\end{array}\right]=\left[\begin{array}{l}
\dot{\phi} \\
0 \\
0
\end{array}\right]+\left[\begin{array}{ccc}
1 & 0 & 0 \\
0 & \cos \phi & \sin \phi \\
0 & -\sin \phi & \cos \phi
\end{array}\right]\left[\begin{array}{l}
0 \\
\dot{\theta} \\
0
\end{array}\right]+\left[\begin{array}{ccc}
1 & 0 & 0 \\
0 & \cos \phi & \sin \phi \\
0 & -\sin \phi & \cos \phi
\end{array}\right]\left[\begin{array}{ccc}
\cos \theta & 0 & -\sin \theta \\
0 & 1 & 0 \\
\sin \theta & 0 & \cos \theta
\end{array}\right]\left[\begin{array}{l}
0 \\
0 \\
\dot{\psi}
\end{array}\right] \equiv J^{-1}\left[\begin{array}{c}
\dot{\phi} \\
\dot{\theta} \\
\dot{\psi}
\end{array}\right]
$$

Inverting $J$ gives the required relationship to determine the Euler rate vector.

$$
\left[\begin{array}{c}
\dot{\phi} \\
\dot{\theta} \\
\dot{\psi}
\end{array}\right]=J\left[\begin{array}{l}
p \\
q \\
r
\end{array}\right]=\left[\begin{array}{ccc}
1 & (\sin \phi \tan \theta) & (\cos \phi \tan \theta) \\
0 & \cos \phi & -\sin \phi \\
0 & \frac{\sin \phi}{\cos \theta} & \frac{\cos \phi}{\cos \theta}
\end{array}\right]\left[\begin{array}{l}
p \\
q \\
r
\end{array}\right]
$$

The applied forces and moments are the sum of the drag, gravitational, external, and suspension forces.

$$
\left.\begin{array}{l}
\bar{F}_{b}=\left[\begin{array}{l}
F_{x} \\
F_{y} \\
F_{z}
\end{array}\right]=\left[\begin{array}{l}
F_{d_{x}} \\
F_{d_{y}} \\
F_{d_{z}}
\end{array}\right]+\left[\begin{array}{l}
F_{g_{x}} \\
F_{g_{y}} \\
F_{g_{z}}
\end{array}\right]+\left[\begin{array}{l}
F_{\text {ext }}^{x} \\
F_{\text {ext }}^{y}
\end{array}\right. \\
F_{\text {ext }}^{z}
\end{array}\right]+\left[\begin{array}{l}
F_{F L_{x}} \\
F_{F L_{y}} \\
F_{F L_{z}}
\end{array}\right]+\left[\begin{array}{l}
F_{F R_{x}} \\
F_{F R_{y}} \\
F_{F R_{z}}
\end{array}\right]+\left[\begin{array}{l}
F_{R L_{x}} \\
F_{R L_{y}} \\
F_{R L_{z}}
\end{array}\right]+\left[\begin{array}{l}
F_{R R_{x}} \\
F_{R R_{y}} \\
F_{R R_{z}}
\end{array}\right] \quad\left[\begin{array}{l}
M_{x} \\
M_{y} \\
\bar{M}_{b}
\end{array}\right]\left[\begin{array}{l}
M_{d_{x}} \\
M_{d_{y}} \\
M_{d_{z}}
\end{array}\right]+\left[\begin{array}{l}
M_{e x t_{x}} \\
M_{e x t_{y}} \\
M_{e x t_{z}}
\end{array}\right]+\left[\begin{array}{l}
M_{F L_{x}} \\
M_{F L_{y}} \\
M_{F L_{z}}
\end{array}\right]+\left[\begin{array}{l}
M_{F R_{x}} \\
M_{F R_{y}} \\
M_{F R_{z}}
\end{array}\right]+\left[\begin{array}{l}
M_{R L_{x}} \\
M_{R L_{y}} \\
M_{R L_{z}}
\end{array}\right]+\left[\begin{array}{l}
M_{R R_{x}} \\
M_{R R_{y}} \\
M_{R R_{z}}
\end{array}\right]+\bar{M}_{F} .
$$

| Calculation | Implementation <br> Load masses and <br> inertias |
| :--- | :--- |
| Gravitational forces, <br> $F_{g}$ | Block uses parallel axis theorem to resolve the individual load masses and <br> inertias with the vehicle mass and inertia. <br> $J_{i j}=I_{i j}+m\left(\|R\|^{2} \delta_{i j}-R_{i} R_{j}\right)$ |
| Drag forces, $F_{d}$, and <br> moments, $M_{d}$ <br> Block uses direction cosine matrix (DCM) to transform the gravitational <br> vector in the inertial-fixed frame to the body-fixed frame. |  |
| To determine a relative airspeed, the block subtracts the wind speed from <br> the vehicle center of mass (CM) velocity. Using the relative airspeed, the <br> block determines the drag forces. |  |
| $\bar{w}=\sqrt{\left(\dot{x}-w_{\chi}\right)^{2}+\left(\dot{x}-w_{x}\right)^{2}+\left(w_{z}\right)^{2}}$ <br> $F_{d x}=-\frac{1}{2 T R} C_{d} A_{f} P_{a b s}\left({ }^{\bar{w}}\right.$ |  |
| $F_{d y}=-\frac{1}{2 T R} C_{s} A_{f} P_{a b s}{ }^{(\bar{w}}$ |  |
| $F_{d z}=-\frac{1}{2 T R} C_{l} A_{f} P_{a b s}\left({ }^{\bar{w}}\right.$ |  |
| Using the relative airspeed, the block determines the drag moments. |  |
| $M_{d r}=-\frac{1}{2 T R} C_{r m} A_{f} P_{a b s}\left({ }^{\bar{w}}(a+b)\right.$ |  |
| $M_{d p}=-\frac{1}{2 T R} C_{p m} A_{f} P_{a b s}\left({ }^{\bar{w}}(a+b)\right.$ |  |
| $M_{d y}=-\frac{1}{2 T R} C_{y m} A_{f} P_{a b s}\left({ }^{\bar{w}}(a+b)\right.$ |  |


| Calculation | Implementation |
| :---: | :---: |
| Suspension forces and moments | Block assumes that the suspension forces and moments act on these hardpoint locations: <br> - $F_{F L}, M_{F L}$ - Front left <br> - $F_{F R}, M_{F R}$ - Front right <br> - $F_{R L}, M_{R L}$ - Rear left <br> - $F_{R R}, M_{R R}$ - Rear right |

The equations use these variables.

| $x, \dot{\chi}, \ddot{\chi}$ | Vehicle CM displacement, velocity, and acceleration along the vehicle-fixed $x$-axis |
| :---: | :---: |
| $y, \dot{y}, \ddot{y}$ | Vehicle CM displacement, velocity, and acceleration along the vehicle-fixed $y$-axis |
| $z, \dot{z}, \ddot{z}$ | Vehicle CM displacement, velocity, and acceleration along the vehicle-fixed $z$-axis |
| $\varphi$ | Rotation of the vehicle-fixed frame about the earth-fixed $X$-axis (roll) |
| $\theta$ | Rotation of the vehicle-fixed frame about the earth-fixed $Y$-axis (pitch) |
| $\psi$ | Rotation of the vehicle-fixed frame about the earth-fixed Z-axis (yaw) |
| $F_{F L x}, F_{F L y}, F_{F L z}$ | Suspension forces applied to front left hardpoint along the vehicle-fixed $x$-, $y$-, and $z$-axes |
| $F_{F R X}, F_{F R y}, F_{F R z}$ | Suspension forces applied to front right hardpoint along the vehicle-fixed $x$-, $y$-, and $z$-axes |
| $F_{R L x}, F_{R L y}, F_{R L z}$ | Suspension forces applied to rear left hardpoint along the vehicle-fixed $x$-, $y$-, and $z$-axes |
| $F_{R R x}, F_{R R y}, F_{R R z}$ | Suspension forces applied to rear right hardpoint along the vehicle-fixed $x$-, $y$-, and $z$-axes |
| $M_{F x}, F_{F y}, F_{F z}$ | Suspension moments applied to vehicle CM about the vehicle-fixed $x-, y$-, and $z$-axes |
| $F_{e x t x}, F_{e x t y}, F_{e x t z}$ | External forces applied to vehicle CM along the vehicle-fixed $x-, y$-, and $z$ axes |
| $F_{d x}, F_{d y}, F_{d z}$ | Drag forces applied to vehicle CM along the vehicle-fixed $x$-, $y$-, and $z$-axes |
| $M_{\text {extx }}, M_{\text {exty }}, M_{\text {extz }}$ | External moment about vehicle CM about the vehicle-fixed $x$-, $y$-, and $z$-axes |
| $M_{d x}, M_{d y}, M_{d z}$ | Drag moment about vehicle CM about the vehicle-fixed $x$-, $y$-, and $z$-axes |
| $I$ | Vehicle body moments of inertia |
| $a, b$ | Distance of front and rear wheels, respectively, from the normal projection point of vehicle CM onto the common axle plane |
| $d$ | Lateral distance from the geometric centerline to the center of mass along the vehicle-fixed $y$-axis |
| $h$ | Height of vehicle CM above the axle plane |
| hh | Height of the hitch above the axle plane along the vehicle-fixed $z$-axis |
| $d h$ | Longitudinal distance of the hitch from the normal projection point of tractor CG onto the common axle plane |


| $h l$ | Lateral distance from center of mass to hitch along the vehicle-fixed $y$-axis. |
| :--- | :--- |
| $w_{F}, w_{R}$ | Front and rear track widths |
| $C_{d}$ | Air drag coefficient acting along the vehicle-fixed $x$-axis |
| $C_{s}$ | Air drag coefficient acting along the vehicle-fixed $y$-axis |
| $C_{l}$ | Air drag coefficient acting along the vehicle-fixed $z$-axis |
| $C_{r m}$ | Air drag roll moment acting about vehicle-fixed $x$-axis |
| $C_{p m}$ | Air drag pitch moment acting about the vehicle-fixed $y$-axis |
| $C_{y m}$ | Air drag yaw moment acting about vehicle-fixed $z$-axis |
| $A_{f}$ | Frontal area |
| $R$ | Atmospheric specific gas constant |
| $T$ | Environmental air temperature |
| $P_{a b s}$ | Environmental absolute pressure |
| $w_{x}, w_{y}, w_{z}$ | Wind speed along the vehicle-fixed $x-, y$-, and $z$-axes |
| $W_{x}, W_{y}, W_{z}$ | Wind speed along inertial $X$-, $Y$-, and $Z$-axes |

## Ports

## Input

FSusp - Suspension forces on vehicle
array
Suspension longitudinal, lateral, and vertical suspension forces applied to the vehicle at the hardpoint location, in N. Signal dimensions are [3x4].

$$
F S u s p=\left[\begin{array}{llll}
F_{F L x} & F_{F R x} & F_{R L x} & F_{R R x} \\
F_{F L y} & F_{F R y} & F_{R L y} & F_{R R y} \\
F_{F L z} & F_{F R z} & F_{R L z} & F_{R R z}
\end{array}\right]
$$

| Array Element | Axle | Wheel | Force Axis |
| :---: | :---: | :---: | :---: |
| FSusp (1,1) | Front | Left | Vehicle-fixed $x$-axis (longitudinal) |
| FSusp (1,2) | Front | Right |  |
| FSusp (1,3) | Rear | Left |  |
| FSusp (1,4) | Rear | Right |  |
| FSusp (2,1) | Front | Left | Vehicle-fixed $y$-axis (lateral) |
| FSusp (2,2) | Front | Right |  |
| FSusp (2,3) | Rear | Left |  |
| FSusp (2,4) | Rear | Right |  |
| FSusp ( 3,1 ) | Front | Left | Vehicle-fixed $z$-axis (vertical) |
| FSusp (3,2) | Front | Right |  |
| FSusp ( 3,3 ) | Rear | Left |  |
| FSusp ( 3,4 ) | Rear | Right |  |

MSusp - Suspension moment on vehicle
array
Suspension longitudinal, lateral, and vertical suspension moments applied about the vehicle at the hardpoint location, in $N \cdot m$. Signal dimensions are [ $3 \times 4$ ].

$$
M S u s p=\left[\begin{array}{llll}
M_{F L x} & M_{F R x} & M_{R L x} & M_{R R x} \\
M_{F L y} & M_{F R y} & M_{R L y} & M_{R R y} \\
M_{F L z} & M_{F R z} & M_{R L z} & M_{R R z}
\end{array}\right]
$$

| Array Element | Axle | Wheel | Moment Axis |
| :---: | :---: | :---: | :---: |
| MSusp (1,1) | Front | Left | Vehicle-fixed $x$-axis (longitudinal) |
| MSusp (1,2) | Front | Right |  |
| MSusp (1,3) | Rear | Left |  |
| MSusp (1,4) | Rear | Right |  |
| MSusp (2,1) | Front | Left | Vehicle-fixed $y$-axis (lateral) |
| MSusp (2,2) | Front | Right |  |
| MSusp (2,3) | Rear | Left |  |
| MSusp ( 2,4 ) | Rear | Right |  |
| MSusp (3,1) | Front | Left | Vehicle-fixed $z$-axis (vertical) |
| MSusp (3,2) | Front | Right |  |
| MSusp (3,3) | Rear | Left |  |
| MSusp (3,4) | Rear | Right |  |

FExt - External forces acting on vehicle vector

External forces on the vehicle, in N, specified as a 1-by-3 or 3-by-1 vector.

$$
\text { FExt }=F_{\text {ext }}=\left[\begin{array}{llll}
F_{\text {ext }} & F_{\text {ext }}^{y} & F_{\text {ext }}
\end{array}\right] \text { or }\left[\begin{array}{l}
F_{\text {ext }}^{x} \\
F_{\text {ext }}^{y} \\
F_{\text {ext }}^{z}
\end{array}\right]
$$

| Array Element | Force Axis |
| :--- | :--- |
| FExt $(1,1)$ | Vehicle-fixed $x$-axis (longitudinal) |
| FExt $(1,2)$ or | Vehicle-fixed $y$-axis (lateral) |
| FExt $(2,1)$ |  |
| FExt $(1,3)$ or <br> FExt $(3,1)$ | Vehicle-fixed $z$-axis (vertical) |

MExt - External moments acting on vehicle
vector
External moments acting on the vehicle, in $\mathrm{N} \cdot \mathrm{m}$, specified as a 1-by-3 or 3-by-1 vector.

$$
\text { MExt }=M_{e x t}=\left[\begin{array}{lll}
M_{e x t_{x}} & M_{e x t_{y}} & M_{e x t_{z}}
\end{array}\right] o r\left[\begin{array}{l}
M_{e x t_{x}} \\
M_{\text {ext }}^{y}
\end{array}\right]\left[\begin{array}{l}
M_{\text {ext }}^{z}
\end{array}\right]
$$

| Array Element | Force Axis |
| :--- | :--- |
| MExt $(1,1)$ | Vehicle-fixed $x$-axis (longitudinal) |
| MExt $(1,2)$ or <br> MExt $(2,1)$ | Vehicle-fixed $y$-axis (lateral) |
| MExt $(1,3)$ or <br> MExt $(3,1)$ | Vehicle-fixed $z$-axis (vertical) |

Fh - Hitch force on the body
array
Hitch force applied to the body at the hitch location, $F h_{x}, F h_{y}, F h_{z}$, in the vehicle-fixed frame, in N, specified as a 1-by-3 or 3-by-1 array.

## Dependencies

To enable this port, under Input signals, select Hitch forces.
Mh - Hitch moment about body
array
Hitch moment at the hitch location, $M h_{x}, M h_{y}, M h_{z}$, about the vehicle-fixed frame, in $\mathrm{N} \cdot \mathrm{m}$, specified as a 1-by-3 or 3-by-1 array.

## Dependencies

To enable this port, under Input signals, select Hitch moments.

## WindXYZ - Wind speed

array
Wind speed, $W_{x}, W_{y}, W_{z}$ along inertial $X-, Y$-, and $Z$-axes, in m/s, specified as a 1-by-3 or 3-by-1 array.

AirTemp - Ambient air temperature
scalar
Ambient air temperature, $T_{\text {air }}$, in $K$, specified as a scalar.

## Dependencies

To enable this port, under Environment, select Air temperature.

## Output

Info - Bus signal
bus
Bus signal containing these block values.

| Signal |  |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| InertFrm | Cg | Disp | X |  | Vehicle CM displacement along the earth-fixed $X$ axis | Computed | m |
|  |  |  | Y |  | Vehicle CM displacement along the earth-fixed $Y$ axis | Computed | m |
|  |  |  | Z |  | Vehicle CM displacement along the earth-fixed $Z$ axis | Computed | m |
|  |  | Vel | Xdot |  | Vehicle CM velocity along the earth-fixed $X$-axis | Computed | m/s |
|  |  |  | Ydot |  | Vehicle CM velocity along the earth-fixed $Y$-axis | Computed | m/s |
|  |  |  | Zdot |  | Vehicle CM velocity along the earth-fixed $Z$-axis | Computed | m/s |
|  |  | Ang | phi |  | Rotation of the vehiclefixed frame about the earth-fixed $X$-axis (roll) | Computed | rad |
|  |  |  | theta |  | Rotation of the vehiclefixed frame about the earth-fixed $Y$-axis (pitch) | Computed | rad |
|  |  |  | psi |  | Rotation of the vehiclefixed frame about the earth-fixed $Z$-axis (yaw) | Computed | rad |
|  | FrntAxl | Lft | Disp | X | Front left axle displacement along the earth-fixed $X$-axis | Computed | m |
|  |  |  |  | Y | Front left axle displacement along the earth-fixed $Y$-axis | Computed | m |
|  |  |  |  | Z | Front left axle displacement along the earth-fixed Z-axis | Computed | m |
|  |  |  | Vel | $\begin{aligned} & \mathrm{Xdo} \\ & \mathrm{t} \end{aligned}$ | Front left axle velocity along the earth-fixed $X$ axis | Computed | m/s |
|  |  |  |  | $\begin{aligned} & \text { Ydo } \\ & \mathrm{t} \end{aligned}$ | Front left axle velocity along the earth-fixed $Y$ axis | Computed | m/s |
|  |  |  |  | $\begin{aligned} & \mathrm{Zdo} \\ & \dagger \end{aligned}$ | Front left axle velocity along the earth-fixed Zaxis | Computed | m/s |


| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Rght | Disp | X | Front right axle displacement along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Y | Front right axle displacement along the earth-fixed $Y$-axis | Computed | m |
|  |  |  | Z | Front right axle displacement along the earth-fixed $Z$-axis | Computed | m |
|  |  | Vel | $\begin{aligned} & \mathrm{Xdo} \\ & \mathrm{t} \end{aligned}$ | Front right axle velocity along the earth-fixed $X$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{Ydo} \\ & \mathrm{t} \end{aligned}$ | Front right axle velocity along the earth-fixed $Y$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{Zdo} \\ & \mathrm{t} \end{aligned}$ | Front right axle velocity along the earth-fixed $Z$ axis | Computed | m/s |
| RearAxl | Lft | Disp | X | Rear left axle displacement along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Y | Rear left axle displacement along the earth-fixed $Y$-axis | Computed | m |
|  |  |  | Z | Rear left axle displacement along the earth-fixed $Z$-axis | Computed | m |
|  |  | Vel | $\begin{aligned} & \mathrm{Xdo} \\ & \mathrm{t} \end{aligned}$ | Rear left axle velocity along the earth-fixed $X$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{Ydo} \\ & \mathrm{t} \end{aligned}$ | Rear left axle velocity along the earth-fixed $Y$ axis | Computed | $\mathrm{m} / \mathrm{s}$ |
|  |  |  | $\begin{aligned} & \text { Zdo } \\ & \dagger \end{aligned}$ | Rear left axle velocity along the earth-fixed Zaxis | Computed | m/s |
|  | Rght | Disp | X | Rear right axle displacement along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Y | Rear right axle displacement along the earth-fixed $Y$-axis | Computed | m |
|  |  |  | Z | Rear right axle displacement along the earth-fixed $Z$-axis | Computed | m |


| Signal |  |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Vel | $\begin{aligned} & \mathrm{Xdo} \\ & \mathrm{t} \end{aligned}$ | Rear right axle velocity along the earth-fixed $X$ axis | Computed | $\mathrm{m} / \mathrm{s}$ |
|  |  |  |  | $\begin{aligned} & \text { Ydo } \\ & \mathrm{t} \end{aligned}$ | Rear right axle velocity along the earth-fixed $Y$ axis | Computed | $\mathrm{m} / \mathrm{s}$ |
|  |  |  |  | $\begin{aligned} & \text { Zdo } \\ & \mathrm{t} \end{aligned}$ | Rear right axle velocity along the earth-fixed Zaxis | Computed | $\mathrm{m} / \mathrm{s}$ |
|  | Hitch | Disp | X |  | Hitch offset from axle plane along the earthfixed $X$-axis | Computed | m |
|  |  |  | Y |  | Hitch offset from axle plane along the earthfixed $Y$-axis | Computed | m |
|  |  |  | Z |  | Hitch offset from axle plane along the earthfixed $Z$-axis | Computed | m |
|  |  | Vel | Xdot |  | Hitch velocity along the earth-fixed $X$-axis | Computed | m/s |
|  |  |  | Ydot |  | Hitch velocity along the earth-fixed $Y$-axis | Computed | m/s |
|  |  |  | Zdot |  | Hitch velocity along the earth-fixed Z-axis | Computed | m/s |
|  | Geom | Disp | X |  | Vehicle chassis offset from axle plane along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Y |  | Vehicle chassis offset from center plane along the earth-fixed $Y$-axis | Computed | m |
|  |  |  | Z |  | Vehicle chassis offset from axle plane along the earth-fixed Z-axis | Computed | m |
|  |  | Vel | Xdot |  | Vehicle chassis offset velocity along the earthfixed $X$-axis | Computed | m/s |
|  |  |  | Ydot |  | Vehicle chassis offset velocity along the earthfixed $Y$-axis | Computed | $\mathrm{m} / \mathrm{s}$ |
|  |  |  | Zdot |  | Vehicle chassis offset velocity along the earthfixed $Z$-axis | Computed | $\mathrm{m} / \mathrm{s}$ |
| BdyFrm | Cg | Vel | xdot |  | Vehicle CM velocity along the vehicle-fixed $x$-axis | Computed | m/s |





| Signal |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Signal |  | Fy | Drag force on vehicle CM along the vehicle-fixed $y$ axis | Computed | N |
|  |  | Fz | Drag force on vehicle CM along the vehicle-fixed $z$ axis | Computed | N |
|  | Grvty | Fx | Gravity force on vehicle CM along the vehiclefixed $x$-axis | Computed | N |
|  |  | Fy | Gravity force on vehicle CM along the vehiclefixed $y$-axis | Computed | N |
|  |  | Fz | Gravity force on vehicle CM along the vehiclefixed $z$-axis | Computed | N |
| Moments | Body | Mx | Body moment on vehicle CM about the vehiclefixed $x$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | My | Body moment on vehicle CM about the vehiclefixed $y$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | Mz | Body moment on vehicle CM about the vehiclefixed $z$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  | Drag | Mx | Drag moment on vehicle CM about the vehiclefixed $x$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | My | Drag moment on vehicle CM about the vehiclefixed $y$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | Mz | Drag moment on vehicle CM about the vehiclefixed $z$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  | Ext | Mx | External moment on vehicle CG about the vehicle-fixed $x$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | My | External moment on vehicle CG about the vehicle-fixed $y$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | Mz | External moment on vehicle CG about the vehicle-fixed $z$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  | Hitch | Mx | Hitch moment at the hitch location about vehiclefixed $x$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |


| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | My |  | Hitch moment at the hitch location about vehiclefixed $y$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | Mz |  | Hitch moment at the hitch location about vehiclefixed $z$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
| FrntAxl | Lft | Disp | x | Front left axle displacement along the vehicle-fixed $x$-axis | Computed | m |
|  |  |  | y | Front left axle displacement along the vehicle-fixed $y$-axis | Computed | m |
|  |  |  | z | Front left axle displacement along the vehicle-fixed $z$-axis | Computed | m |
|  |  | Vel | $\begin{aligned} & \mathrm{xdo} \\ & \mathrm{t} \end{aligned}$ | Front left axle velocity along the vehicle-fixed $x$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{ydo} \\ & \mathrm{t} \end{aligned}$ | Front left axle velocity along the vehicle-fixed $y$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{zdo} \\ & \mathrm{t} \end{aligned}$ | Front left axle velocity along the vehicle-fixed $z$ axis | Computed | m/s |
|  | Rght | Disp | X | Front right axle displacement along the vehicle-fixed $x$-axis | Computed | m |
|  |  |  | y | Front right axle displacement along the vehicle-fixed $y$-axis | Computed | m |
|  |  |  | z | Front right axle displacement along the vehicle-fixed $z$-axis | Computed | m |
|  |  | Vel | $\begin{aligned} & \mathrm{xdo} \\ & \mathrm{t} \end{aligned}$ | Front right axle velocity along the vehicle-fixed $x$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{ydo} \\ & \mathrm{t} \end{aligned}$ | Front right axle velocity along the vehicle-fixed $y$ axis | Computed | m/s |
|  |  |  | $\underset{+}{\mathrm{zdo}}$ | Front right axle velocity along the vehicle-fixed $z$ axis | Computed | m/s |
| RearAxl | Lft | Disp | X | Rear left axle displacement along the vehicle-fixed $x$-axis | Computed | m |



| Signal |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \mathrm{ydo} \\ & \mathrm{t} \end{aligned}$ | Hitch offset velocity along the vehicle-fixed $y$-axis | Computed | m/s |
|  |  | $\begin{aligned} & \mathrm{zdo} \\ & \mathrm{t} \end{aligned}$ | Hitch offset velocity along the vehicle-fixed $z$-axis | Computed | m/s |
| Pwr | PwrExt |  | Applied external power | Computed | W |
|  | Drag |  | Power loss due to drag | Computed | W |
| Geom | Disp | x | Vehicle chassis offset from axle plane along the vehicle-fixed $x$-axis | Input | m |
|  |  | y | Vehicle chassis offset from center plane along the vehicle-fixed $y$-axis | Input | m |
|  |  | z | Vehicle chassis offset from axle plane along the vehicle-fixed $z$-axis | Input | m |
|  | Vel | $\begin{aligned} & \mathrm{xdo} \\ & \mathrm{t} \end{aligned}$ | Vehicle chassis offset velocity along the vehiclefixed $x$-axis | Computed | m/s |
|  |  | $\begin{aligned} & \mathrm{ydo} \\ & \mathrm{t} \end{aligned}$ | Vehicle chassis offset velocity along the vehiclefixed $y$-axis | Computed | m/s |
|  |  | $\begin{aligned} & \mathrm{zdo} \\ & \mathrm{t} \end{aligned}$ | Vehicle chassis offset velocity along the vehiclefixed $z$-axis | Computed | m/s |
|  | Ang | Bet a | Body slip angle, $\beta$ $\beta=\frac{V_{y}}{V_{x}}$ | Computed | rad |

## $\mathbf{V b}$ - Vehicle velocity along vehicle-fixed frame

## vector

Vehicle CM velocity along the vehicle-fixed $x$-, $y$-, $z$-axes, respectively, in $m / s$, returned as a vector.
$\mathbf{p q r}$ - Vehicle angular velocity about vehicle-fixed frame
vector
Vehicle CM angular velocity about the vehicle-fixed $x$-(roll rate), $y$-(pitch rate), $z$-axes (yaw rate), respectively, in rad/s, returned as a vector.

DCM - Direction cosine matrix
array
Direction cosine matrix, in rad, returned as an array.
Euler - Euler angles
array

Euler angles, $\varphi, \theta$, and $\psi$, respectively, in rad, returned as an array.
$\mathbf{X e}$ - Vehicle position in inertial reference frame vector

Vehicle CM position along inertial-fixed $X$-, $Y$-, $Z$-axes, respectively, in m, returned as a vector.
Ve - Vehicle velocity in inertial reference frame vector

Vehicle CM velocity along inertial-fixed $X$-, $Y$-, $Z$-axes, respectively, in $\mathrm{m} / \mathrm{s}$, returned as a vector.

## Parameters

## Block Options

Input Signals
Hitch forces - Create input port
off (default) | on
Select to create an input port, Fh, for the hitch forces.
Hitch moments - Create input port
off (default) |on
Select to create an input port, Mh, for the hitch moments.

## Chassis

Vehicle mass, $\mathbf{m}$ - Mass
2000 (default) | scalar
Vehicle mass, $m$, in kg.
Longitudinal distance from center of mass to front axle, a - Distance
1.4 (default) | scalar

Distance from vehicle CM to front axle, $a$, in m .


Longitudinal distance from center of mass to rear axle, b-Distance 1.6 (default) | scalar

Distance from vehicle CM to front axle, $b$, in $m$.


Lateral distance from geometric centerline to center of mass, $\mathbf{d}$ - Distance
0 (default) | scalar
Lateral distance from geometric centerline to center of mass, $d$, in $m$, along the vehicle-fixed $y$. Positive values indicate that the vehicle CM is to the right of the geometric centerline. Negative values indicate that the vehicle CM is to the left of the geometric centerline.


Vertical distance from center of mass to axle plane, $\mathbf{h}$ - Distance . 35 (default) | scalar

Vertical distance from vehicle CM to axle plane, $h$, in m .


Longitudinal distance from center of mass to hitch, $\mathbf{d h}$ - Longitudinal distance from CM to hitch 1 (default) | scalar

Longitudinal distance from center of mass to hitch, $d h$, in m.


## Dependencies

To enable this parameter, on the Input signals pane, select Hitch forces or Hitch moments.
Longitudinal distance from center of mass to hitch, hl - Lateral distance from CM to hitch
0 (default) | scalar
Lateral distance from center of mass to hitch, $h l$, in $m$.


## Dependencies

To enable this parameter, on the Input signals pane, select Hitch forces or Hitch moments.
Vertical distance from hitch to axle plane, $\mathbf{h h}$ - Distance from hitch to axle plane 0.1 (default) | scalar

Vertical distance from hitch to axle plane, $h h$, in m.


## Dependencies

To enable this parameter, on the Input signals pane, select Hitch forces or Hitch moments.
Initial position in the inertial frame [Xeo,Yeo,Zeo], Xe_o - Position
[0,0,0] (default) | vector
Initial position of vehicle in the inertial frame, $X e_{o}$, in $m$.
Initial velocity in body axes [xdot_0,ydot_o,zdot_o], xbdot_o - Velocity
[0,0,0] (default) | vector
Initial vehicle CM velocity along the vehicle-fixed $x, y$-, and $z$-axes, respectively, in $\mathrm{m} / \mathrm{s}$.
Initial Euler orientation [roll, pitch, yaw], eul_o - Rotation
[0,0,0] (default) | vector
Initial Euler rotation of the vehicle-fixed frame about the earth-fixed $X$ (roll)-, $Y$ (pitch)-, $Z$ (yaw)- axes, respectively, in rad.

Initial body rotation rates [p,q,r], p_o - Rotation rate
[0,0,0] (default) | vector
Initial vehicle CM angular velocity about the vehicle-fixed $x$ (roll rate)-, $y$ (pitch rate)-, $z$ (yaw rate)axes, respectively, in rad/s.

Chassis inertia tensor, Iveh - Inertia
[430 0 0; 0 1900 0; 002100 ] (default)|array
Vehicle inertia tensor, $I_{v e h}$, in $\mathrm{kg}^{*} \mathrm{~m} \wedge 2$. Dimensions are [3-by-3].
Track widths [front,rear], w - Widths
[1.9,1.9] (default)| vector
Front and rear track width, in $m$. Dimensions are [1-by-2].
Inertial Loads
Front
Mass, z1m - Mass
0 (default) | scalar
Mass, $z 1 m$, in kg.
Distance vector from front axle, z1R - Distance
[-. 25,. 125, .15] (default) | vector
Distance vector from front axle to load, $z 1 R$, in m. Dimensions are [1-by-3].

| Array Element | Description |
| :--- | :--- |
| $z 1 R(1,1)$ | Front suspension hardpoint to load, along the <br> vehicle-fixed $x$-axis |
| $z 1 R(1,2)$ | Vehicle centerline to load, along the vehicle-fixed $y$ - <br> axis |
| $z 1 R(1,3)$ | Front suspension hardpoint to load, along the <br> vehicle-fixed $z$-axis |



For example, this table summarizes the parameter settings that specify the load location indicated by the dots.

| Example Location | Sign |
| :--- | :--- |
| - Forward of the front axle | - $\operatorname{z1R}(1,1)<0$ |
| - Right of the vehicle centerline | - $z 1 R(1,2)>0$ |
| - Above the front axle suspension hardpoint | - $\operatorname{z1R}(1,3)>0$ |

## Inertia tensor, z1I - Inertia

[1.4,-.2,.1;-.2,1.4,.1;.1,.1,2.25].*0 (default)|array
Inertia tensor, $z 11$, in $\mathrm{kg} \cdot \mathrm{m} \wedge 2$. Dimensions are [3-by-3].

$$
z 1 I=\left[\begin{array}{lll}
I_{x x} & I_{x y} & I_{x z} \\
I_{y x} & I_{y y} & I_{y z} \\
I_{z x} & I_{z y} & I_{z z}
\end{array}\right]
$$

The tensor uses a coordinate system with an origin at the load CM.

- $x$-axis along the vehicle-fixed $x$-axis
- $y$-axis along the vehicle-fixed $y$-axis
- $z$-axis along the vehicle-fixed $z$-axis



## Overhead

Mass, z2m - Mass
0 (default) | scalar
Mass, $z 2 m$, in kg.
Distance vector from front axle, $\mathbf{z 2 R}$ - Distance
[1.4,0, .8] (default) |vector
Distance vector from front axle to load, $z 2 R$, in m. Dimensions are [1-by -3].

| Array Element | Description |
| :--- | :--- |
| z2R $(1,1)$ | Front suspension hardpoint to load, along the <br> vehicle-fixed $x$-axis |
| z2R $(1,2)$ | Vehicle centerline to load, along the vehicle-fixed $y$ - <br> axis |
| z2R $(1,3)$ | Front suspension hardpoint to load, along the <br> vehicle-fixed $z$-axis |



For example, this table summarizes the parameter settings that specify the load location indicated by the dot.

| Example Location | Sign |
| :--- | :--- |
| - | Rear of the front axle |
| - | Left of the vehicle centerline |
| - | Above the front axle suspension hardpoint |

## Inertia tensor, z2I - Inertia

[1.4,-.2,.1;-.2,1.4,.1;.1,.1,2.25].*0 (default)|array
Inertia tensor, $z 2 I$, in $\mathrm{kg} \cdot \mathrm{m} \wedge 2$. Dimensions are [3-by-3].

$$
z 2 I=\left[\begin{array}{lll}
I_{x x} & I_{x y} & I_{x z} \\
I_{y x} & I_{y y} & I_{y z} \\
I_{z x} & I_{z y} & I_{z z}
\end{array}\right]
$$

The tensor uses a coordinate system with an origin at the load CM.

- $x$-axis along the vehicle-fixed $x$-axis
- $y$-axis along the vehicle-fixed $y$-axis
- $z$-axis along the vehicle-fixed $z$-axis


5-112

Row 1, left side
Mass, $\mathbf{z 3 m}$ - Mass
0 (default) | scalar
Mass, $z 3 m$, in kg.
Distance vector from front axle, z3R - Distance
[.75, -. 5, . 4] (default) |vector
Distance vector from front axle to load, $z 3 R$, in m. Dimensions are [1-by-3].

| Array Element | Description |
| :--- | :--- |
| $z 3 R(1,1)$ | Front suspension hardpoint to load, along the <br> vehicle-fixed $x$-axis |
| $z 3 R(1,2)$ | Vehicle centerline to load, along the vehicle-fixed $y$ - <br> axis |
| $z 3 R(1,3)$ | Front suspension hardpoint to load, along the <br> vehicle-fixed $z$-axis |



For example, this table summarizes the parameter settings that specify the load location indicated by the dot.

| Example Location | Sign |
| :--- | :--- |
| - | Rear of the front axle |
| - | Left of the vehicle centerline |
| - | Above the front axle suspension hardpoint |

Inertia tensor, z3I - Inertia
[5,-.1,-2;-2,9,.1;-.1,.1,6].*0 (default)|array
Inertia tensor, $z 3 I$, in $\mathrm{kg} \cdot \mathrm{m}^{\wedge} 2$. Dimensions are [3-by-3].

$$
z 3 I=\left[\begin{array}{lll}
I_{x x} & I_{x y} & I_{x z} \\
I_{y x} & I_{y y} & I_{y z} \\
I_{z x} & I_{z y} & I_{z z}
\end{array}\right]
$$

The tensor uses a coordinate system with an origin at the load CM.

- $x$-axis along the vehicle-fixed $x$-axis
- $y$-axis along the vehicle-fixed $y$-axis
- $z$-axis along the vehicle-fixed $z$-axis



## Row 1, right side

Mass, $\mathbf{2 4 m}$ - Mass
0 (default) | scalar
Mass, $z 4 m$, in kg.
Distance vector from front axle, $\mathbf{z 4 R}$ - Distance
[.75, .5,.4] (default) | vector
Distance vector from front axle to load, $z 4 R$, in m. Dimensions are [1-by-3].

| Array Element | Description |
| :--- | :--- |
| z4R $(1,1)$ | Front suspension hardpoint to load, along the <br> vehicle-fixed $x$-axis |
| z4R $(1,2)$ | Vehicle centerline to load, along the vehicle-fixed $y$ - <br> axis |
| z4R $(1,3)$ | Front suspension hardpoint to load, along the <br> vehicle-fixed $z$-axis |



For example, this table summarizes the parameter settings that specify the load location indicated by the dot.

| Example Location | Sign |
| :--- | :--- |
| - Rear of the front axle | - $\mathrm{z4R}(1,1)>0$ |
| - Right of the vehicle centerline | - $\mathrm{z4R}(1,2)>0$ |
| - Above the front axle suspension hardpoint | - $\mathrm{z4R}(1,3)>0$ |

Inertia tensor, $\mathbf{z 4 I}$ - Inertia
[5,-.1,-2;-2,9,.1;-.1,.1,6].*0 (default)|array
Inertia tensor, $z 4 I$, in $\mathrm{kg} \cdot \mathrm{m} \wedge 2$. Dimensions are [3-by-3].

$$
z 4 I=\left[\begin{array}{lll}
I_{x x} & I_{x y} & I_{x z} \\
I_{y x} & I_{y y} & I_{y z} \\
I_{z x} & I_{z y} & I_{z z}
\end{array}\right]
$$

The tensor uses a coordinate system with an origin at the load CM.

- $x$-axis along the vehicle-fixed $x$-axis
- $y$-axis along the vehicle-fixed $y$-axis
- $z$-axis along the vehicle-fixed $z$-axis


Row 2, left side
Mass, z5m - Mass
0 (default) | scalar
Mass, z5m, in kg.
Distance vector from front axle, z5R - Distance
[1.25,-.5,.4] (default)| vector
Distance vector from front axle to load, $z 5 R$, in m. Dimensions are [1-by-3].

| Array Element | Description |
| :--- | :--- |
| $z 5 R(1,1)$ | Front suspension hardpoint to load, along the <br> vehicle-fixed $x$-axis |
| $z 5 R(1,2)$ | Vehicle centerline to load, along the vehicle-fixed $y$ - <br> axis |
| $z 5 R(1,3)$ | Front suspension hardpoint to load, along the <br> vehicle-fixed $z$-axis |



For example, this table summarizes the parameter settings that specify the load location indicated by the dot.

| Example Location | Sign |
| :--- | :--- |
| - | Rear of the front axle |
| - | Left of the vehicle centerline |
| - | Above the front axle suspension hardpoint |

Inertia tensor, $\mathbf{z 5 I}$ - Inertia
[5,-.1,-2;-2,9,.1;-.1,.1,6].*0 (default)|array
Inertia tensor, $z 5 I$, in $\mathrm{kg} \cdot \mathrm{m}^{\wedge} 2$. Dimensions are [3-by-3].

$$
z 5 I=\left[\begin{array}{lll}
I_{x x} & I_{x y} & I_{x z} \\
I_{y x} & I_{y y} & I_{y z} \\
I_{z x} & I_{z y} & I_{z z}
\end{array}\right]
$$

The tensor uses a coordinate system with an origin at the load CM.

- $x$-axis along the vehicle-fixed $x$-axis
- $y$-axis along the vehicle-fixed $y$-axis
- $z$-axis along the vehicle-fixed $z$-axis



## Row 2, right side

Mass, $\mathbf{2 6 m}$ - Mass
0 (default) | scalar
Mass, $z 6 \mathrm{~m}$, in kg.
Distance vector from front axle, $\mathbf{z 6 R}$ - Distance
[1.25,-.5,.4] (default)| vector
Distance vector from front axle to load, $z 6 R$, in m. Dimensions are [1-by -3].

| Array Element | Description |
| :--- | :--- |
| z6R $(1,1)$ | Front suspension hardpoint to load, along the <br> vehicle-fixed $x$-axis |
| z6R $(1,2)$ | Vehicle centerline to load, along the vehicle-fixed $y$ - <br> axis |
| z6R $(1,3)$ | Front suspension hardpoint to load, along the <br> vehicle-fixed $z$-axis |



For example, this table summarizes the parameter settings that specify the load location indicated by the dot.

| Example Location | Sign |
| :--- | :--- |
| - $\quad$ Rear of the front axle | - $\operatorname{z6R}(1,1)>0$ |
| - Right of the vehicle centerline | - $\operatorname{z6R}(1,2)>0$ |
| - Above the front axle suspension hardpoint | - $z 6 R(1,3)>0$ |

Inertia tensor, z6I - Inertia
[5,-.1,-2;-2, 9, .1;-.1, .1,6].*0 (default)|array
Inertia tensor, $z 6 I$, in $\mathrm{kg} \cdot \mathrm{m}^{\wedge} 2$. Dimensions are [3-by-3].

$$
z 6 I=\left[\begin{array}{lll}
I_{x x} & I_{x y} & I_{x z} \\
I_{y x} & I_{y y} & I_{y z} \\
I_{z x} & I_{z y} & I_{z z}
\end{array}\right]
$$

The tensor uses a coordinate system with an origin at the load CM.

- $x$-axis along the vehicle-fixed $x$-axis
- $y$-axis along the vehicle-fixed $y$-axis
- $z$-axis along the vehicle-fixed $z$-axis



## Rear

Mass, $\mathbf{z 7 m}$ - Mass
0 (default) | scalar
Mass, $z 7$, in kg.
Distance vector from front axle, z7R - Distance
[2,0, .25] (default) | vector
Distance vector from front axle to load, $z 7 R$, in m. Dimensions are [1-by-3].

| Array Element | Description |
| :--- | :--- |
| z7R $(1,1)$ | Front suspension hardpoint to load, along the <br> vehicle-fixed $x$-axis |
| z7R $(1,2)$ | Vehicle centerline to load, along the vehicle-fixed $y$ - <br> axis |
| z7R $(1,3)$ | Front suspension hardpoint to load, along the <br> vehicle-fixed $z$-axis |



For example, this table summarizes the parameter settings that specify the load location indicated by the dot.

| Example Location | Sign |
| :--- | :--- |
| - Rear of the front axle | - $\operatorname{z7R}(1,1)>0$ |
| - | Right of the vehicle centerline |
| - | Above the front axle suspension hardpoint | - $\quad z 7 R(1,3)>0$

Inertia tensor, z7I - Inertia
[1.4,-.2,.1;-.2,1.4,.1;.1,.1,2.25].*0 (default)|array
Inertia tensor, $z 7 \mathrm{I}$, in $\mathrm{kg} \cdot \mathrm{m} \wedge 2$. Dimensions are [3-by-3].

$$
z 7 I=\left[\begin{array}{lll}
I_{x x} & I_{x y} & I_{x z} \\
I_{y x} & I_{y y} & I_{y z} \\
I_{z x} & I_{z y} & I_{z z}
\end{array}\right]
$$

The tensor uses a coordinate system with an origin at the load CM.

- $x$-axis along the vehicle-fixed $x$-axis
- $y$-axis along the vehicle-fixed $y$-axis
- $z$-axis along the vehicle-fixed $z$-axis



## Aerodynamic

Longitudinal drag area, Af - Area
2 (default) | scalar
Effective vehicle cross-sectional area, $A_{f}$ to calculate the aerodynamic drag force on the vehicle, in $\mathrm{m}^{\wedge} 2$.

Longitudinal drag coefficient, Cd - Drag
. 3 (default) | scalar
Air drag coefficient, $C_{d}$, dimensionless.

## Longitudinal lift coefficient, CI - Lift

. 1 (default) | scalar
Air lift coefficient, $C_{l}$, dimensionless.
Longitudinal drag pitch moment, Cpm - Pitch drag
. 1 (default) | scalar
Longitudinal drag pitch moment coefficient, $C_{p m}$, dimensionless.
Relative wind angle vector, beta_w - Wind angle
[0:0.001:0.01] (default)| vector
Relative wind angle vector, $\beta_{w}$, in rad.
Side force coefficient vector, Cs - Side force drag
[0:0.01:0.1] (default)| vector
Side force coefficient vector coefficient, $C_{s}$, dimensionless.
Yaw moment coefficient vector, Cym - Yaw moment drag
[0:0.001:0.01] (default) | vector
Yaw moment coefficient vector coefficient, $C_{y m}$, dimensionless.

## Environment

Absolute air pressure, Pabs - Pressure
101325 (default) | scalar
Environmental air absolute pressure, $P_{\text {abs }}$ in Pa.
Air temperature, Tair - Ambient air temperature
273 (default) | scalar
Ambient air temperature, $T_{\text {air }}$ in K .

## Dependencies

To enable this parameter, clear Air temperature.
Gravitational acceleration, $\mathbf{g}$ - Gravity
9.81 (default) | scalar

Gravitational acceleration, $g$, in $\mathrm{m} / \mathrm{s}^{\wedge} 2$.

## Simulation

## Longitudinal velocity tolerance, xdot_tol - Tolerance <br> . 1 (default) | scalar

Longitudinal velocity tolerance, $x d o t_{t o l}$, in $\mathrm{m} / \mathrm{s}$.
The block uses this parameter to avoid a division by zero when it calculates the body slip angle, $\beta$.

## Geometric longitudinal offset from axle plane, longOff - Longitudinal offset

0 (default) | scalar
Vehicle chassis offset from axle plane along body-fixed $x$-axis, in $m$. When you use the 3D visualization engine, consider using the offset to locate the chassis independent of the vehicle CG.

Geometric lateral offset from center plane, latOff - Lateral offset
0 (default) | scalar
Vehicle chassis offset from center plane along body-fixed $y$-axis, in $m$. When you use the 3D visualization engine, consider using the offset to locate the chassis independent of the vehicle CG.

Geometric vertical offset from axle plane, vertOff - Vertical offset
0 (default) | scalar
Vehicle chassis offset from axle plane along body-fixed $z$-axis, in m . When you use the 3D visualization engine, consider using the offset to locate the chassis independent of the vehicle CG.

## Wrap Euler angles, wrapAng - Selection

on (default) | off
Wrap the Euler angles to the interval [-pi, pi]. For vehicle maneuvers that might undergo vehicle yaw rotations that are outside of the interval, consider deselecting the parameter if you want to:

- Track the total vehicle yaw rotation.
- Avoid discontinuities in the vehicle state estimators.


## Version History

Introduced in R2018a

## References

[1] Gillespie, Thomas. Fundamentals of Vehicle Dynamics. Warrendale, PA: Society of Automotive Engineers (SAE), 1992.

## Extended Capabilities

C/C++ Code Generation
Generate C and C++ code using Simulink ${ }^{\circledR}$ Coder $^{\mathrm{TM}}$.

## See Also

6DOF (Euler Angles) | Vehicle Body 3DOF | Vector Concatenate, Matrix Concatenate

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"

## Trailer Body 3DOF

Trailer body with longitudinal, lateral, and yaw motion


## Libraries:

Vehicle Dynamics Blockset / Vehicle Body

## Description

The Trailer Body 3DOF block implements a rigid one-axle, two-axle or three-axle trailer body model to calculate longitudinal, lateral, and yaw motion. Configure the block for a single or dual track. The block accounts for axle and hitch reaction forces due to the trailer acceleration, aerodynamic drag, and steering.

Use this block in vehicle dynamics and automated driving studies to model nonholonomic vehicle motion when vehicle pitch, roll, and vertical motion are not significant.

Use the Vehicle track parameter to specify the number of wheels.

| Vehicle Track Setting | Implementation |
| :--- | :--- |
| Single 1-axle | Trailer with a single track and one axle. <br> - <br> - Forces act along the center line of the axle. |
| Dual lateral load transfer. |  |

Use the Axle forces parameter to specify the type of force.

| Axle Forces Setting | Implementation |
| :---: | :---: |
| External longitudinal velocity | - The block assumes that the external longitudinal velocity is in a quasi-steady state, and the longitudinal acceleration is approximately zero. <br> - Because the motion is quasi-steady, the block calculates lateral forces using the tire slip angles and linear cornering stiffness. <br> - Consider this setting when you want to: <br> - Generate virtual sensor signal data. <br> - Conduct high-level software studies that are not impacted by driveline or nonlinear tire responses. |
| External longitudinal forces | - The block uses the external longitudinal force to accelerate or brake the vehicle. <br> - The block calculates lateral forces using the tire slip angles and linear cornering stiffness. <br> - Consider this setting when you want to: <br> - Account for changes in the longitudinal velocity on the lateral and yaw motion. <br> - Specify the external longitudinal motion through a force instead of an external longitudinal velocity. <br> - Connect the block to tractive actuators, wheels, brakes, and hitches. |
| External forces | - The block uses the external lateral and longitudinal forces to steer, accelerate, or brake the vehicle. <br> - The block does not use the steering input to calculate vehicle motion. <br> - Consider this setting when you need tire models with more accurate nonlinear combined lateral and longitudinal slip. |

To create additional input ports, under Input signals, select these block parameters.

| Input Signals Pane <br> Parameter | Input Port | Description |
| :--- | :--- | :--- |
| Front wheel steering | WhlAngF | Front wheel angle, $\delta_{F}$ |
| Middle wheel steering | WhlAngM | Middle wheel angle, $\delta_{M}$ |
| Rear wheel steering | WhlAngR | Rear wheel angle, $\delta_{R}$ |
| External wind | WindXYZ | Wind speed, $W_{X}, W_{Y}$, and $W_{Z}$, in an inertial reference frame |
| External friction | Mu | Friction coefficient |
| External forces | FExt | External force on the vehicle center of gravity (CG), $F_{x^{\prime}}, F_{y}$, <br> and $F_{z}$, in the vehicle-fixed frame |
| External moments | MExt | External moment about the vehicle CG, $M_{x}, M_{y}$, and $M_{z}$, in <br> the vehicle-fixed frame |
| Front hitch forces | FhF | Hitch force applied to the body at the front hitch location, <br> $F h F_{x}, F h F_{y}$, and $F h F_{z}$, in the vehicle-fixed frame |


| Input Signals Pane <br> Parameter | Input Port | Description |
| :--- | :--- | :--- |
| Front hitch moments | MhF | Hitch moment at the front hitch location, $M h F_{x}, M h F_{y}$, and <br> $M h F_{z}$, about the vehicle-fixed frame |
| Rear hitch forces | FhR | Hitch force applied to the body at the rear hitch location, <br> $F h R_{x}, F h R_{y}$, and $F h R_{z}$, in the vehicle-fixed frame |
| Rear hitch moments | MhR | Hitch moment at the rear hitch location, $M h R_{x}, M h R_{y}$, and <br> $M h R_{z}$, about the vehicle-fixed frame |
| Initial longitudinal <br> position | $\mathrm{X} \_0^{\text {Initial yaw angle }}$ | Initial vehicle CG displacement along the earth-fixed $X$-axis |
| Initial longitudinal <br> velocity | xsi_o | Initial rotation of the vehicle-fixed frame about the earth- <br> fixed Z-axis (yaw) |
| Initial yaw rate | Initial vehicle CG velocity along the vehicle-fixed $x$-axis |  |
| Initial lateral position | r_o | Initial vehicle angular velocity about the vehicle-fixed $z$ - <br> axis (yaw rate) |
| Air temperature | AirTemp | Initial vehicle CG displacement along the earth-fixed $Y$-axis <br> Ambient air temperature. Consider this option if you want <br> to vary the temperature during run time. |
| Initial lateral velocity | ydot_o | Initial vehicle CG velocity along the vehicle-fixed $y$-axis |

## Theory

To determine the vehicle motion, the block solves the rigid body planar dynamics equations of motion.

| Calculation | Description |
| :--- | :--- |
| Dynamics | The block solves the rigid-body planar dynamics equations to determine the <br> vehicle longitudinal motion. If you set Axle forces to External <br> longitudinal velocity, the block assumes a quasi-steady state for the <br> longitudinal acceleration. |
| External forces | External forces include both drag and external force inputs. The forces act <br> on the vehicle CG. <br> The block divides the normal forces by the nominal normal load to vary the <br> effective friction parameters during weight and load transfer. The block <br> maintains pitch and roll equilibrium. |
| Tire forces | The block uses the ratio of the local, longitudinal, and lateral velocities to <br> determine the slip angles. |
| The block uses the steering angles to transform the tire forces to the vehicle- <br> fixed frame. <br> If you set Axle forces to External forces, the block assumes that the <br> externally provided forces are in the vehicle-fixed frame at the axle-wheel <br> location. |  |

## Single Track - Three Axles



## Single Track - Two Axles



## Single Track - One Axle





Dual Track - One Axle


The illustrations use these variables.

| $a, b, c$ | Longitudinal distance of the front, middle, and rear axles, respectively, from the <br> normal projection point of the vehicle CG onto the common axle plane |
| :--- | :--- |
| $h$ | Height of the tractor CG above the axle plane along the vehicle-fixed $z$-axis |
| $d$ | Lateral distance from the geometric centerline to the center of mass along the <br> vehicle-fixed $y$-axis |
| $h h f, h h_{-} r$ | Height of the front and rear hitch, respectively, above the axle plane along the <br> vehicle-fixed $z$-axis |
| $d h f, d h_{-} r$ | Longitudinal distance of the front and rear hitch, respectively, from the normal <br> projection point of tractor CG onto the common axle plane |
| $w f, w m, w r$ | Front, middle, and rear track width, respectively |

This table summarizes the block implementation for the drag calculation.

| Calculation | Description |
| :--- | :--- |
| Coordinate <br> transformation | The block transforms the wind speeds from the inertial frame to the vehicle- <br> fixed frame. |
| Drag forces | To determine a relative airspeed, the block subtracts the wind speed from <br> the CG vehicle velocity. Using the relative airspeed, the block determines the <br> drag forces. |
| Drag moments | Using the relative airspeed, the block determines the drag moments. |

## Lateral Corner Stiffness and Relaxation Dynamics

To enable the mapped corner stiffness and relaxation length dynamic parameters, set Axle forces to External longitudinal forces or External longitudinal velocity.

| Parameter Settings | Description |  |
| :--- | :--- | :--- |
| Mapped Corner <br> Stiffness | Include Relaxation <br> Length Dynamics |  |
| Off (default) | On (default) | The block uses constant corner stiffness values. <br> The slip angles include the relaxation length dynamic <br> settings. The relaxation length approximates an <br> effective corner stiffness force that is a function of <br> wheel travel. |
| On | On (default) | The block uses lookup tables that are functions of the <br> corner stiffness data and slip angles. <br> The slip angles include the relaxation length dynamic <br> settings. The relaxation length approximates an <br> effective corner stiffness force that is a function of <br> wheel travel. |
| Off (default) | Off | The block uses constant corner stiffness values. |

## Ports

## Input

WhIAngF - Front wheel steering angles
scalar|array
Front wheel steering angles, $\delta_{F}$, in rad.

| Vehicle Track Setting | Variable | Signal Dimension |
| :--- | :--- | :--- |
| Single 1-axle <br> Single 2-axle <br> Single 3-axle | $\delta_{F}$ | Scalar-1 |
| Dual 1-axle |  |  |
| Dual 2-axle | $\delta_{F}=\left[\delta_{f l} \delta_{f r}\right]$ or $\left[\begin{array}{l}\delta_{f l} \\ \delta_{f r}\end{array}\right]$ | Array - [1x2] or [2x1] |
| Dual 3-axle |  |  |

## Dependencies

To enable this port, under Input signals, select Front wheel steering.
WhIAngM - Middle wheel steering angles
scalar | array
Middle wheel steering angles, $\delta_{M}$, in rad.

| Vehicle Track Setting | Variable | Signal Dimension |
| :--- | :--- | :--- |
| Single 3-axle | $\delta_{M}$ | Scalar - 1 |
| Dual 3-axle | $\delta_{M}=\left[\delta_{m l} \delta_{m r}\right]$ or $\left[\begin{array}{ll}\delta_{m l} \\ \delta_{m r}\end{array}\right]$ | Array - [1×2] or [2x1] |

## Dependencies

To enable this port:

- Set Vehicle track to Single 3-axle or Dual 3-axle.
- To enable this port, under Input signals, select Middle wheel steering.

WhIAngR - Rear wheel steering angles
scalar|array
Rear wheel steering angles, $\delta_{R}$, in rad.

| Vehicle Track Setting | Variable | Signal Dimension |
| :--- | :--- | :--- |
| Single 1-axle <br> Single 2-axle <br> Single 3-axle | $\delta_{R}$ | Scalar - 1 |
| Dual 1-axle |  |  |
| Dual 2-axle | $\delta_{R}=\left[\delta_{r l} \delta_{r r}\right]$ or $\left[\begin{array}{l}\delta_{r l} \\ \delta_{r r}\end{array}\right]$ | Array - [1x2] or [2×1] |
| Dual 3-axle |  |  |

## Dependencies

To enable this port, under Input signals, select Rear wheel steering.
xdotin - Longitudinal velocity
scalar
Vehicle CG velocity along the vehicle-fixed $x$-axis, in $m / s$.

## Dependencies

To enable this port, set Axle forces to External longitudinal velocity.
FwF - Total force on the front wheels

## scalar|array

Force on the front wheels, $F w_{F}$, along the vehicle-fixed axis, in $N$.

| Vehicle Track Setting | Axle Forces Setting | Description | Variable | Signal Dimension |
| :---: | :---: | :---: | :---: | :---: |
| Single 1axle | External <br> longitudinal <br> forces | Longitudinal force on the front wheel | $F w F=F x_{f}$ | Scalar - 1 |
| Single 2- <br> axle <br> Single 3 - <br> axle | External forces | Longitudinal and lateral forces on the front wheel | $F w F=\left[\begin{array}{lll} F x_{f} & F y_{f} \end{array}\right] \text { or }\left[\begin{array}{l} F x_{f} \\ F y_{f} \end{array}\right]$ | $\begin{aligned} & \text { Array - [1x2] or } \\ & {[2 \times 1]} \end{aligned}$ |
| Dual 1axle <br> Dual 2axle | External longitudinal forces | Longitudinal force on the front wheels | $F w F=\left[F_{x f l} F_{x f r}\right] \text { or }\left[\begin{array}{l} F_{x f l} \\ F_{x f r} \end{array}\right.$ | $\begin{aligned} & \text { Array - [1x2] or } \\ & {[2 \times 1]} \end{aligned}$ |
| Dual 3axle | External forces | Longitudinal and lateral forces on the front wheels | $F w F=\left[\begin{array}{ll}F_{\chi f l} & F_{\chi f r} \\ F_{y f l} & F_{y f r}\end{array}\right]$ | Array - [2x2] |

## Dependencies

To enable this port, set Axle forces to one of these options:

- External longitudinal forces
- External forces

FwM - Total force on the middle wheels
scalar|array
Force on the middle wheels, $F w_{M}$, along the vehicle-fixed axis, in N .

| Vehicle <br> Track <br> Setting | Axle Forces <br> Setting | Description | Variable | Signal <br> Dimension |
| :--- | :--- | :--- | :--- | :--- |
| Single 3- <br> axle | External <br> longitudinal <br> forces | Longitudinal <br> force on the <br> middle wheel | $F w M=F x_{r}$ | Scalar - 1 |
| External <br> forces | Longitudinal and <br> lateral forces on <br> the middle wheel | $F w M=\left[F x_{m} F y_{m}\right]$ or <br> $\left[\begin{array}{l}F x_{m} \\ F y_{m}\end{array}\right]$ | Array - [1x2] or <br> $[2 \times 1]$ |  |
| Dual 3- <br> axle | External <br> longitudinal <br> forces | Longitudinal <br> force on the <br> middle wheels | $F w M=\left[F_{x m l} F_{x m r}\right]$ or <br> $\left[\begin{array}{l}F_{x m l} \\ F_{x m r}\end{array}\right]$ | Array - [1x2] or <br> $[2 \times 1]$ |

## Dependencies

To enable this port, set:

- Vehicle track to Single 3-axle or Dual 3-axle.
- Axle forces to External longitudinal forces or External forces.

FwR - Total force on the rear wheels
scalar| array
Force on the rear wheels, $F w_{R}$, along the vehicle-fixed axis, in N.

| Vehicle <br> Track Setting | Axle Forces Setting | Description | Variable | Signal Dimension |
| :---: | :---: | :---: | :---: | :---: |
| Single 2axle <br> Single 3axle | External <br> longitudinal forces | Longitudinal force on the rear wheel | $F w R=F \chi_{r}$ | Scalar - 1 |
|  | External forces | Longitudinal and lateral forces on the rear wheel | $F w R=\left[\begin{array}{lll}F \chi_{r} & F y_{r}\end{array}\right]$ or $\left[\begin{array}{l}F \chi_{r} \\ F y_{r}\end{array}\right]$ | $\begin{aligned} & \text { Array - [1×2] or } \\ & {[2 \times 1]} \end{aligned}$ |


| Vehicle Track Setting | Axle Forces Setting | Description | Variable | Signal Dimension |
| :---: | :---: | :---: | :---: | :---: |
| Dual 2axle <br> Dual 3axle | External longitudinal forces | Longitudinal force on the rear wheels | $F w R=\left[F_{x r l} F_{x r r}\right] \text { or }\left[\begin{array}{l} F_{x r l} \\ F_{x r r} \end{array}\right.$ | $\begin{aligned} & \text { Array - [1×2] or } \\ & {[2 \times 1]} \end{aligned}$ |
|  | External forces | Longitudinal and lateral forces on the rear wheels | $F w R=\left[\begin{array}{lll}F_{x r l} & F_{x r r} \\ F_{y r l} & F_{y r r}\end{array}\right]$ | Array - [2x2] |

## Dependencies

To enable this port, set:

- Vehicle track to Single 3-axle, Single 2-axle, Dual 3-axle or Dual 2-axle.
- Axle forces to External longitudinal forces or External forces.

FExt - External force on the vehicle CG
array
External forces applied to the vehicle CG, $F_{\text {xext }}, F_{\text {yext }}, F_{z e x t}$, in vehicle-fixed frame, in $N$. The signal vector dimensions are [ $1 \times 3$ ] or [ $3 \times 1$ ].

## Dependencies

To enable this port, under Input signals, select External forces.

## MExt - External moment about vehicle CG

array
External moment about the vehicle CG, $M_{x}, M_{y}, M_{z}$, in the vehicle-fixed frame, in $\mathrm{N} \cdot \mathrm{m}$. The signal vector dimensions are [ $1 \times 3$ ] or [ $3 \times 1$ ].

## Dependencies

To enable this port, under Input signals, select External moments.
FhF - Front hitch force on the body array

Hitch force applied to the body at the front hitch location, $F h F_{x}, F h F_{y}, F h F_{z}$, in the vehicle-fixed frame, in N, specified as a 1-by-3 or 3-by-1 array.

## Dependencies

To enable this port, under Input signals, select Front hitch forces.
MhF - Front hitch moment about body
array
Hitch moment at the front hitch location, $M h F_{x}, M h F_{y}, M h F_{z}$, about the vehicle-fixed frame, in $\mathrm{N} \cdot \mathrm{m}$, specified as a 1-by-3 or 3-by-1 array.

## Dependencies

To enable this port, under Input signals, select Front hitch moments.
FhR - Rear hitch force on the body
array
Hitch force applied to the body at the rear hitch location, $F h R_{x}, F h R_{y}, F h R_{z}$, in the vehicle-fixed frame, in N , specified as a 1-by-3 or 3-by-1 array.

## Dependencies

To enable this port, under Input signals, select Rear hitch forces.
MhR - Rear hitch moment about body
array
Hitch moment at the rear hitch location, $M h R_{x}, M h R_{y}, M h R_{z}$, about the vehicle-fixed frame, in $N \cdot m$, specified as a 1-by-3 or 3-by-1 array.

## Dependencies

To enable this port, under Input signals, select Rear hitch moments.
WindXYZ - Wind speed
array
Wind speed, $W_{x}, W_{y}, W_{z}$, along the inertial $X$-, $Y$-, and $Z$-axes, in $\mathrm{m} / \mathrm{s}$. The signal vector dimensions are 1-by-3 or 3-by-1.

## Dependencies

To enable this port, under Input signals, select External wind.
$\mathbf{M u}$ - Tire friction coefficient
array
Tire friction coefficient, $\mu$. The value is dimensionless.

| Vehicle Track Setting | Description | Variable | Signal Dimension |
| :---: | :---: | :---: | :---: |
| Single 1-axle | Friction coefficient on the wheels | $M u=\mu_{f}$ | Array - [1x1] |
| Dual 1-axle | Friction coefficient on the wheels | $\begin{aligned} & M u=\left[\begin{array}{ll} \mu_{f l} & \left.\mu_{f r}\right] \text { or } \\ {\left[\begin{array}{l} \mu_{f l} \\ \mu_{f r} \end{array}\right]} \end{array} .\right. \end{aligned}$ | Array - [1x2] or [2x1] |
| Single 2-axle | Friction coefficient on the wheels | $M u=\left[\begin{array}{ll} \mu_{f} & \left.\mu_{r}\right] \text { or }\left[\begin{array}{l} \mu_{f} \\ \mu_{r} \end{array}\right] \end{array}\right.$ | Array - [1x2] or [2x1] |
| Dual 2-axle | Friction coefficient on the wheels | $M u=\left[\begin{array}{ll}\mu_{f l} & \mu_{f r} \\ \mu_{r l} & \mu_{r r}\end{array}\right]$ | Array - [2x2] |


| Vehicle Track Setting | Description | Variable | Signal Dimension |
| :---: | :---: | :---: | :---: |
| Single 3-axle | Friction coefficient on the wheels | $\begin{aligned} & M u=\left[\begin{array}{lll} \mu_{f} & \mu_{m} & \mu_{r} \end{array}\right] \text { or } \\ & {\left[\begin{array}{l} \mu_{f} \\ \mu_{m} \\ \mu_{r} \end{array}\right]} \end{aligned}$ | Array - [1x3] or [3x1] |
| Dual 3-axle | Friction coefficient on the wheels | $M u=\left[\begin{array}{ll}\mu_{f l} & \mu_{f r} \\ \mu_{m l} & \mu_{m r} \\ \mu_{r l} & \mu_{r r}\end{array}\right]$ | Array - [3x2] |

## Dependencies

To enable this port, under Input signals, select External friction.
AirTemp - Ambient air temperature
scalar
Ambient air temperature, in K.

## Dependencies

To enable this port, under Input signals, select Air temperature.
X_0 - Initial longitudinal position
scalar
Initial vehicle CG displacement along the earth-fixed $X$-axis, in m.

## Dependencies

To enable this port, under Input signals, select Initial longitudinal position.
Y_o - Initial lateral position
scalar
Initial vehicle CG displacement along the earth-fixed $Y$-axis, in $m$.

## Dependencies

To enable this port, under Input signals, select Initial lateral position.
xdot_o - Initial longitudinal position
scalar
Initial vehicle CG velocity along the vehicle-fixed $x$-axis, in m/s.

## Dependencies

To enable this port:
1 Set Axle forces to one of these options:

- External longitudinal forces
- External forces

2 Under Input signals, select Initial longitudinal velocity
ydot_o - Initial lateral position
scalar
Initial vehicle CG velocity along the vehicle-fixed $y$-axis, in $\mathrm{m} / \mathrm{s}$.

## Dependencies

To enable this port, under Input signals, select Initial lateral velocity.
psi_o - Initial yaw angle
scalar
Rotation of the vehicle-fixed frame about the earth-fixed $Z$-axis (yaw), in rad.

## Dependencies

To enable this port, under Input signals, select Initial yaw angle.
r_o - Initial yaw rate
scalar
Vehicle angular velocity about the vehicle-fixed $z$-axis (yaw rate), in rad/s.

## Dependencies

To enable this port, under Input signals, select Initial yaw rate.

## Output

Info - Trailer data
bus
Trailer data, returned as a bus signal containing these block values.

| Signal |  |  |  | Description | Value | Units |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| InertFrm | Cg | Disp | X | Vehicle CG displacement <br> along the earth-fixed $X$ - <br> axis | Computed | m |
|  |  |  | Y | Vehicle CG displacement <br> along the earth-fixed $Y$ - <br> axis | Computed | m |
|  |  |  | Vehicle CG displacement <br> along the earth-fixed $Z-$ <br> axis | 0 | m |  |
|  |  | Vel | Xdot | Vehicle CG velocity along <br> the earth-fixed $X$-axis | Computed | $\mathrm{m} / \mathrm{s}$ |
|  | Vehicle CG velocity along <br> the earth-fixed $Y$-axis | Computed | $\mathrm{m} / \mathrm{s}$ |  |  |  |


| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Signal |  | Zdot |  | Vehicle CG velocity along the earth-fixed $Z$-axis | 0 | m/s |
|  | Ang | phi |  | Rotation of the vehiclefixed frame about the earth-fixed $X$-axis (roll) | 0 | rad |
|  |  | theta |  | Rotation of the vehiclefixed frame about the earth-fixed $Y$-axis (pitch) | 0 | rad |
|  |  | psi |  | Rotation of the vehiclefixed frame about the earth-fixed $Z$-axis (yaw) | Computed | rad |
| FrntAxl | Lft | Disp | X | Front left wheel displacement along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Y | Front left wheel displacement along the earth-fixed $Y$-axis | Computed | m |
|  |  |  | Z | Front left wheel displacement along the earth-fixed Z-axis | 0 | m |
|  |  | Vel | $\begin{aligned} & \hline \text { Xdo } \\ & \mathrm{t} \end{aligned}$ | Front left wheel velocity along the earth-fixed $X$ axis | Computed | $\mathrm{m} / \mathrm{s}$ |
|  |  |  | $\begin{array}{\|l} \hline \text { Ydo } \\ \mathrm{t} \end{array}$ | Front left wheel velocity along the earth-fixed $Y$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{Zdo} \\ & \mathrm{t} \end{aligned}$ | Front left wheel velocity along the earth-fixed $Z$ axis | 0 | m/s |
|  | Rght | Disp | X | Front right wheel displacement along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Y | Front right wheel displacement along the earth-fixed $Y$-axis | Computed | m |
|  |  |  | Z | Front right wheel displacement along the earth-fixed Z-axis | 0 | m |
|  |  | Vel | $\begin{aligned} & \hline \text { Xdo } \\ & \mathrm{t} \end{aligned}$ | Front right wheel velocity along the earth-fixed $X$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{Ydo} \\ & \mathrm{t} \end{aligned}$ | Front right wheel velocity along the earth-fixed $Y$ axis | Computed | m/s |


| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{aligned} & \mathrm{Zdo} \\ & \mathrm{t} \end{aligned}$ | Front right wheel velocity along the earth-fixed Zaxis | 0 | m/s |
| Midlaxl | Lft | Disp | X | Middle left wheel displacement along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Y | Middle left wheel displacement along the earth-fixed $Y$-axis | Computed | m |
|  |  |  | Z | Middle left wheel displacement along the earth-fixed $Z$-axis | 0 | m |
|  |  | Vel | $\begin{aligned} & \mathrm{Xdo} \\ & \mathrm{t} \end{aligned}$ | Middle left wheel velocity along the earth-fixed $X$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{Ydo} \\ & \mathrm{t} \end{aligned}$ | Middle left wheel velocity along the earth-fixed $Y$ axis | Computed | $\mathrm{m} / \mathrm{s}$ |
|  |  |  | $\begin{aligned} & \text { Zdo } \\ & \dagger \end{aligned}$ | Middle left wheel velocity along the earth-fixed Zaxis | 0 | m/s |
|  | Rght | Disp | X | Middle right wheel displacement along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Y | Middle right wheel displacement along the earth-fixed $Y$-axis | Computed | m |
|  |  |  | Z | Middle right wheel displacement along the earth-fixed $Z$-axis | 0 | m |
|  |  | Vel | $\begin{aligned} & \mathrm{Xdo} \\ & \mathrm{t} \end{aligned}$ | Middle right wheel velocity along the earthfixed $X$-axis | Computed | $\mathrm{m} / \mathrm{s}$ |
|  |  |  | $\begin{aligned} & \mathrm{Ydo} \\ & \mathrm{t} \end{aligned}$ | Middle right wheel velocity along the earthfixed $Y$-axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{Zdo} \\ & \dagger \end{aligned}$ | Middle right wheel velocity along the earthfixed $Z$-axis | 0 | m/s |
| RearAxl | Lft | Disp | X | Rear left wheel displacement along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Y | Rear left wheel displacement along the earth-fixed $Y$-axis | Computed | m |


| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Z | Rear left wheel displacement along the earth-fixed Z-axis | 0 | m |
|  |  | Vel | $\begin{aligned} & \mathrm{Xdo} \\ & \mathrm{t} \end{aligned}$ | Rear left wheel velocity along the earth-fixed $X$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \text { Ydo } \\ & \mathrm{t} \end{aligned}$ | Rear left wheel velocity along the earth-fixed $Y$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \text { Zdo } \\ & \mathrm{t} \end{aligned}$ | Rear left wheel velocity along the earth-fixed Zaxis | 0 | m/s |
|  | Rght | Disp | X | Rear right wheel displacement along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Y | Rear right wheel displacement along the earth-fixed $Y$-axis | Computed | m |
|  |  |  | Z | Rear right wheel displacement along the earth-fixed Z-axis | 0 | m |
|  |  | Vel | $\begin{aligned} & \mathrm{Xdo} \\ & \mathrm{t} \end{aligned}$ | Rear right wheel velocity along the earth-fixed $X$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \text { Ydo } \\ & \mathrm{t} \end{aligned}$ | Rear right wheel velocity along the earth-fixed $Y$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{Zdo} \\ & \dagger \end{aligned}$ | Rear right wheel velocity along the earth-fixed Zaxis | 0 | m/s |
| Geom | Disp | X |  | Trailer body offset from the axle plane along the earth-fixed $X$-axis | Computed | m |
|  |  | Y |  | Trailer body offset from the center plane along the earth-fixed $Y$-axis | Computed | m |
|  |  | Z |  | Trailer body offset from the axle plane along the earth-fixed Z-axis | Computed | m |
|  | Vel | Xdot |  | Trailer body offset velocity along the earthfixed $X$-axis | Computed | m/s |
|  |  | Ydot |  | Trailer body offset velocity along the earthfixed $Y$-axis | Computed | m/s |


| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Zdot | Trailer body offset velocity along the earthfixed $Z$-axis | Computed | m/s |
|  | HitchF | Disp | X | Trailer front hitch offset from the axle plane along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Y | Trailer front hitch offset from the center plane along the earth-fixed $Y$ axis | Computed | m |
|  |  |  | Z | Trailer front hitch offset from the axle plane along the earth-fixed $Z$-axis | Computed | m |
|  |  | Vel | Xdot | Trailer front hitch offset velocity along the earthfixed $X$-axis | Computed | m/s |
|  |  |  | Ydot | Trailer front hitch offset velocity along the earthfixed $Y$-axis | Computed | m/s |
|  |  |  | Zdot | Trailer front hitch offset velocity along the earthfixed $Z$-axis | Computed | m/s |
|  | HitchR | Disp | X | Trailer rear hitch offset from the axle plane along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Y | Trailer rear hitch offset from the center plane along the earth-fixed $Y$ axis | Computed | m |
|  |  |  | Z | Trailer rear hitch offset from the axle plane along the earth-fixed $Z$-axis | Computed | m |
|  |  | Vel | Xdot | Trailer rear hitch offset velocity along the earthfixed $X$-axis | Computed | m/s |
|  |  |  | Ydot | Trailer rear hitch offset velocity along the earthfixed $Y$-axis | Computed | m/s |
|  |  |  | Zdot | Trailer rear hitch offset velocity along the earthfixed $Z$-axis | Computed | m/s |
| BdyFrm | Cg | Vel | xdot | Vehicle CG velocity along the vehicle-fixed $x$-axis | Computed | m/s |
|  |  |  | ydot | Vehicle CG velocity along the vehicle-fixed $y$-axis | Computed | m/s |


| Signal |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | zdot | Vehicle CG velocity along the vehicle-fixed $z$-axis | 0 | m/s |
|  | Ang | Beta | Body slip angle, $\beta$ $\beta=\frac{V_{y}}{V_{x}}$ | Computed | rad |
|  | AngVel | p | Vehicle angular velocity about the vehicle-fixed $x$ axis (roll rate) | 0 | rad/s |
|  |  | q | Vehicle angular velocity about the vehicle-fixed $y$ axis (pitch rate) | 0 | rad/s |
|  |  | r | Vehicle angular velocity about the vehicle-fixed $z$ axis (yaw rate) | Computed | rad/s |
|  | Acc | ax | Vehicle CG acceleration along the vehicle-fixed $x$ axis | Computed | gn |
|  |  | ay | Vehicle CG acceleration along the vehicle-fixed $y$ axis | Computed | gn |
|  |  | az | Vehicle CG acceleration along the vehicle-fixed $z$ axis | 0 | gn |
|  |  | xddot | Vehicle CG acceleration along the vehicle-fixed $x$ axis | Computed | $\mathrm{m} / \mathrm{s}^{\wedge} 2$ |
|  |  | yddot | Vehicle CG acceleration along the vehicle-fixed $y$ axis | Computed | $\mathrm{m} / \mathrm{s}^{\wedge} 2$ |
|  |  | zddot | Vehicle CG acceleration along the vehicle-fixed $z$ axis | 0 | $\mathrm{m} / \mathrm{s}^{\wedge} 2$ |
|  | AngAcc | pdot | Vehicle angular acceleration about the vehicle-fixed $x$-axis | 0 | rad/s |
|  |  | qdot | Vehicle angular acceleration about the vehicle-fixed $y$-axis | 0 | rad/s |
|  |  | rdot | Vehicle angular acceleration about the vehicle-fixed $z$-axis | Computed | rad/s |
| Forces | Body | FX | Net force on the vehicle CG along the vehicle-fixed x-axis | Computed | N |





| Signal |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Fy | Gravity force on the vehicle CG along the vehicle-fixed $y$-axis | Computed | N |
|  |  | Fz | Gravity force on the vehicle CG along the vehicle-fixed $z$-axis | Computed | N |
| Moments | Body | Mx | Body moment on the vehicle CG about the vehicle-fixed $x$-axis | 0 | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | My | Body moment on the vehicle CG about the vehicle-fixed $y$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | Mz | Body moment on the vehicle CG about the vehicle-fixed $z$-axis | 0 | $\mathrm{N} \cdot \mathrm{m}$ |
|  | Drag | Mx | Drag moment on the vehicle CG about the vehicle-fixed $x$-axis | 0 | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | My | Drag moment on the vehicle CG about the vehicle-fixed $y$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | Mz | Drag moment on the vehicle CG about the vehicle-fixed $z$-axis | 0 | $\mathrm{N} \cdot \mathrm{m}$ |
|  | Ext | Mx | External moment on the vehicle CG about the vehicle-fixed $x$-axis | 0 | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | My | External moment on the vehicle CG about the vehicle-fixed $y$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | Mz | External moment on the vehicle CG about the vehicle-fixed $z$-axis | 0 | $\mathrm{N} \cdot \mathrm{m}$ |
|  | HitchF | Mx | Hitch moment at the front hitch location about vehicle-fixed $x$-axis | 0 | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | My | Hitch moment at the front hitch location about vehicle-fixed $y$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | Mz | Hitch moment at the front hitch location about vehicle-fixed $z$-axis | 0 | $\mathrm{N} \cdot \mathrm{m}$ |
|  | HitchR | Mx | Hitch moment at the rear hitch location about vehicle-fixed $x$-axis | 0 | $\mathrm{N} \cdot \mathrm{m}$ |



| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | WhlAngFR |  | Front right wheel steering angle | Computed | rad |
| MidlAxl | Lft | Disp | x | Middle left wheel displacement along the vehicle-fixed $x$-axis | Computed | m |
|  |  |  | y | Middle left wheel displacement along the vehicle-fixed $y$-axis | Computed | m |
|  |  |  | z | Middle left wheel displacement along the vehicle-fixed $z$-axis | Computed | m |
|  |  | Vel | $\begin{array}{\|l\|} \hline \text { xdo } \\ \mathrm{t} \end{array}$ | Middle left wheel velocity along the vehicle-fixed $x$ axis | Computed | m/s |
|  |  |  | $\begin{array}{\|l\|} \hline \text { ydo } \\ \mathrm{t} \end{array}$ | Middle left wheel velocity along the vehicle-fixed $y$ axis | Computed | m/s |
|  |  |  | $\begin{array}{\|l\|} \hline \text { zdo } \\ \mathrm{t} \end{array}$ | Middle left wheel velocity along the vehicle-fixed $z$ axis | 0 | m/s |
|  | Rght | Disp | x | Middle right wheel displacement along the vehicle-fixed $x$-axis | Computed | m |
|  |  |  | y | Middle right wheel displacement along the vehicle-fixed $y$-axis | Computed | m |
|  |  |  | z | Middle right wheel displacement along the vehicle-fixed $z$-axis | Computed | m |
|  |  | Vel | $\begin{aligned} & \hline \text { xdo } \\ & \mathrm{t} \end{aligned}$ | Middle right wheel velocity along the vehiclefixed $x$-axis | Computed | m/s |
|  |  |  | $\begin{array}{\|l\|} \hline \text { ydo } \\ \mathrm{t} \end{array}$ | Middle right wheel velocity along the vehiclefixed $y$-axis | Computed | m/s |
|  |  |  | $\begin{array}{\|l\|} \hline \text { zdo } \\ \mathrm{t} \end{array}$ | Middle right wheel velocity along the vehiclefixed $z$-axis | 0 | m/s |
|  | Steer | WhlangRL |  | Middle left wheel steering angle | Computed | rad |
|  |  | WhlAngRR |  | Middle right wheel steering angle | Computed | rad |



|  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Signal |  | y | Front hitch offset from center plane along the vehicle-fixed $y$-axis | Input | m |
|  |  | z | Front hitch offset from axle plane along the earth-fixed $z$-axis | Input | m |
|  | Vel | $\begin{aligned} & \mathrm{xdo} \\ & \mathrm{t} \end{aligned}$ | Front hitch offset velocity along the vehicle-fixed $x$ axis | Computed | m/s |
|  |  | $\begin{aligned} & \mathrm{ydo} \\ & \mathrm{t} \end{aligned}$ | Front hitch offset velocity along the vehicle-fixed $y$ axis | Computed | m/s |
|  |  | $\begin{aligned} & \mathrm{zdo} \\ & \dagger \end{aligned}$ | Front hitch offset velocity along the vehicle-fixed $z$ axis | 0 | m/s |
| HitchR | Disp | x | Rear hitch offset from axle plane along the vehiclefixed $x$-axis | Input | m |
|  |  | y | Rear hitch offset from center plane along the vehicle-fixed $y$-axis | Input | m |
|  |  | z | Rear hitch offset from axle plane along the earthfixed $z$-axis | Input | m |
|  | Vel | $\begin{aligned} & \mathrm{xdo} \\ & \mathrm{t} \end{aligned}$ | Rear hitch offset velocity along the vehicle-fixed $x$ axis | Computed | m/s |
|  |  | $\begin{aligned} & \mathrm{ydo} \\ & \mathrm{t} \end{aligned}$ | Rear hitch offset velocity along the vehicle-fixed $y$ axis | Computed | $\mathrm{m} / \mathrm{s}$ |
|  |  | $\begin{aligned} & \mathrm{zdo} \\ & \mathrm{t} \end{aligned}$ | Rear hitch offset velocity along the vehicle-fixed $z$ axis | 0 | $\mathrm{m} / \mathrm{s}$ |
| Pwr | Ext |  | Applied external power | Computed | W |
|  | HitchF |  | Front hitch power | Computed | W |
|  | HitchR |  | Rear hitch power | Computed | W |
|  | Drag |  | Power loss due to drag | Computed | W |
| Geom | Disp | x | Trailer offset from axle plane along the vehiclefixed $x$-axis | Input | m |
|  |  | y | Trailer offset from center plane along the vehiclefixed $y$-axis | Input | m |


| Signal |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | z | Trailer offset from axle plane along the vehiclefixed $z$-axis | Input | m |
|  | Vel | $\begin{aligned} & \text { xdo } \\ & t \end{aligned}$ | Trailer offset velocity along the vehicle-fixed $x$ axis | Computed | m/s |
|  |  | $\begin{aligned} & \text { ydo } \\ & t \end{aligned}$ | Trailer offset velocity along the vehicle-fixed $y$ axis | Computed | m/s |
|  |  | $\begin{aligned} & \text { zdo } \\ & t \end{aligned}$ | Trailer offset velocity along the vehicle-fixed $z$ axis | 0 | $\mathrm{m} / \mathrm{s}$ |
|  | Ang | Bet <br> a | Body slip angle, $\beta$ $\beta=\frac{V_{y}}{V_{x}}$ | Computed | rad |


| Signal |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: |
| PwrInfo | PwrTrnsfrd | PwrFxExt | Externally applied longitudinal force power | Comp uted | W |
|  |  | PwrFyExt | Externally applied lateral force power | Comp uted | W |
|  |  | PwrMzExt | Externally applied yaw moment power | Comp uted | W |
|  |  | PwrFwFLx | Longitudinal force applied at the front left axle power | Comp uted | W |
|  |  | PwrFwFLy | Lateral force applied at the front left axle power | Comp uted | W |
|  |  | PwrFwFRx | Longitudinal force applied at the front right axle power | Comp uted | W |
|  |  | PwrFwFRy | Lateral force applied at the front right axle power | Comp uted | W |
|  |  | PwrFwMLx | Longitudinal force applied at the middle left axle power | Comp uted | W |
|  |  | PwrFwMLy | Lateral force applied at the middle left axle power | Comp uted | W |
|  |  | PwrFwMRx | Longitudinal force applied at the middle right axle power | Comp uted | W |
|  |  | PwrFwMRy | Lateral force applied at the middle right axle power | Comp uted | W |
|  |  | PwrFwRLx | Longitudinal force applied at the rear left axle power | Comp uted | W |


xdot - Trailer longitudinal velocity
scalar
Trailer CG velocity along the vehicle-fixed $x$-axis, in $\mathrm{m} / \mathrm{s}$.
ydot - Trailer lateral velocity
scalar
Trailer CG velocity along the vehicle-fixed $y$-axis, in $\mathrm{m} / \mathrm{s}$.
psi - Yaw
scalar
Rotation of the vehicle-fixed frame about the earth-fixed Z-axis (yaw), in rad.
r-Yaw rate
scalar
Vehicle angular velocity, $r$, about the vehicle-fixed $z$-axis (yaw rate), in rad/s.
FzF - Normal force on the front wheels
scalar|array
Normal force on the front wheels, $F z_{F}$, along the vehicle-fixed $z$-axis, in N .

| Vehicle Track <br> Setting | Description | Variable | Signal Dimension |
| :--- | :--- | :---: | :--- |
| Single 2-axle <br> Single 3-axle | Normal force on the <br> front axle | $F z F=F z_{f}$ | Scalar - 1 |
| Dual 2-axle <br> Dual 3-axle | Normal force on the <br> front wheels | $F z F=\left[F z_{f l} F z_{f r}\right]$ | Array - [1x2] |

FzM - Normal force on the middle wheels
scalar| array
Normal force on the middle wheels, $F z_{M}$, along the vehicle-fixed $z$-axis, in N .

| Vehicle Track <br> Setting | Description | Variable | Signal Dimension |
| :--- | :--- | :---: | :--- |
| Single 3-axle | Normal force on the <br> middle axle | $F z M=F z_{m}$ | Scalar - 1 |
| Dual 3-axle | Normal force on the <br> right and left middle <br> wheels | $F z M=\left[F z_{m l} F z_{r l}\right]$ | Array - [1x2] |

## Dependencies

To enable this port, set Vehicle track to Single 3-axle or Dual 3-axle.
FzR - Normal force on the rear wheels
scalar array
scalar|array
Normal force on the rear wheels, $F z_{R}$, along the vehicle-fixed $z$-axis, in N .

| Vehicle Track <br> Setting | Description | Variable | Signal Dimension |
| :--- | :--- | :--- | :--- |
| Single 2-axle <br> Single 3-axle | Normal force on the <br> rear wheel | $F z R=F z_{r}$ | Scalar - 1 |
| Dual 2-axle <br> Dual 3-axle | Normal force on the <br> rear wheels | $F z R=\left[F z_{r l} F z_{r r}\right]$ | Array - [1x2] |

Fhz - Normal component of hitch force on the body
scalar
Normal hitch force applied to the body at the hitch location, $F h_{z}$, in the vehicle-fixed frame $z$-axis, in N .

If you enable the Hitch forces parameter, the block offsets the normal hitch force, $F h_{z}$, with the value of the Fh input port component along the vehicle-fixed $z$-axis.

## Parameters

## Options

Vehicle track - Type of vehicle track
Dual 2-axle (default)|Single 1-axle|Dual 1-axle|Single 2-axle|Dual 3-axle
Use the Vehicle track parameter to specify the number of wheels.

| Vehicle Track Setting | Implementation |
| :--- | :--- |
| Single 1-axle | Trailer with a single track and one axle. <br> - <br> - Forces act along the center line of the axle. |
| Do lateral load transfer. |  |

Axle forces - Type of axle force
External forces (default)|External longitudinal velocity|External longitudinal forces

Use the Axle forces parameter to specify the type of force.

| Axle Forces Setting | Implementation |
| :---: | :---: |
| External longitudinal velocity | - The block assumes that the external longitudinal velocity is in a quasi-steady state, and the longitudinal acceleration is approximately zero. <br> - Because the motion is quasi-steady, the block calculates lateral forces using the tire slip angles and linear cornering stiffness. <br> - Consider this setting when you want to: <br> - Generate virtual sensor signal data. <br> - Conduct high-level software studies that are not impacted by driveline or nonlinear tire responses. |


| Axle Forces Setting | Implementation |
| :---: | :---: |
| External longitudinal forces | - The block uses the external longitudinal force to accelerate or brake the vehicle. <br> - The block calculates lateral forces using the tire slip angles and linear cornering stiffness. <br> - Consider this setting when you want to: <br> - Account for changes in the longitudinal velocity on the lateral and yaw motion. <br> - Specify the external longitudinal motion through a force instead of an external longitudinal velocity. <br> - Connect the block to tractive actuators, wheels, brakes, and hitches. |
| External forces | - The block uses the external lateral and longitudinal forces to steer, accelerate, or brake the vehicle. <br> - The block does not use the steering input to calculate vehicle motion. <br> - Consider this setting when you need tire models with more accurate nonlinear combined lateral and longitudinal slip. |

## Input Signals

Front wheel steering - WhlAngF input port
off (default) | on
Select to create input port WhlAngF.
Middle wheel steering - WhlAngM input port
off (default) | on
Select to create input port WhlAngM.

## Dependencies

To enable this parameter, set Vehicle track to Single 3-axle or Dual 3-axle.
Rear wheel steering - WhlAngR input port
off (default) | on
Select to create input port WhlAngR.

## Dependencies

To enable this parameter, set Vehicle track to Single 2-axle, Dual 2-axle, Single 3-axle, or Dual 3-axle.

External wind - WindXYZ input port
off (default) | on
Select to create input port WindXYZ.
External friction - Mu input port
off (default) | on

Select to create input port Mu.

## Dependencies

To enable this parameter, set Axle forces to one of these options:

- External longitudinal forces
- External forces

External forces - FExt input port
off (default) | on
Select to create input port FExt.
External moments - MExt input port
off (default) | on
Select to create input port MExt.
Front hitch forces - FhF input port
on (default) | off
Select to create input port Fh.
Front hitch moments - MhF input port
on (default) | off
Select to create input port Mh.
Rear hitch forces - FhR input port
off (default) | on
Select to create input port Fh.
Rear hitch moments - MhR input port
off (default) | on
Select to create input port Mh.
Initial longitudinal position - X_o input port
off (default) | on
Select to create input port X_o.
Initial yaw angle - psi_o input port
off (default) | on
Select to create input port psi_o.
Initial longitudinal velocity - xdot_o input port
off (default) | on
Select to create input port xdot o.

## Dependencies

To enable this parameter, set Axle forces to External longitudinal forces or External forces.

Initial yaw rate - r_o input port
off (default) | on
Select to create input port r_o.
Initial lateral position - Y_o input port
off (default) | on
Select to create input port Y_o.
Air temperature - AirTemp input port
off (default) | on
Select to create input port AirTemp.
Initial lateral velocity - ydot_o input port
off (default) | on
Select to create input port ydot_o.

## Longitudinal

Number of wheels on front axle, NF - Front wheel count
2 (default) | scalar
Number of wheels on the front axle, $N_{F}$. The value is dimensionless.
Number of wheels on middle axle, NM - Middle wheel count
2 (default) | scalar
Number of wheels on the middle axle, $N_{M}$. The value is dimensionless.

## Dependencies

To enable this parameter, set Vehicle track to Single 3-axle or Dual 3-axle.
Number of wheels on rear axle, NR - Rear wheel count
2 (default) | scalar
Number of wheels on the rear axle, $N_{R}$. The value is dimensionless.
To enable this parameter, set Vehicle track to Single 2-axle, Single 3-axle, Dual 2-axle, or Dual 3-axle.

Vehicle mass, $\mathbf{m}$ - Vehicle mass
26000 (default) | scalar
Vehicle mass, $m$, in kg.
Longitudinal distance from center of mass to front axle, a - Distance from CM to front axle 4 (default) | scalar

Distance from the vehicle CM to the front axle, $a$, in $m$.


Longitudinal distance from center of mass to middle axle, b-Distance from CM to middle axle 4.5 (default) | scalar

Distance from vehicle CM to middle axle, $b$, in $m$.


Dependencies
To enable this parameter, set Vehicle track to Single 3-axle or Dual 3-axle.
Longitudinal distance from center of mass to rear axle, c-Distance from CM to rear axle 5 (default) | scalar

Distance from vehicle CM to the front axle, $c$, in m .


## Dependencies

To enable this parameter, set Vehicle track to Single 2-axle, Single 3-axle, Single 3-axle, or Dual 3-axle.

Vertical distance from center of mass to axle plane, $\mathbf{h}$ - Distance from CM to axle plane 2 (default) | scalar

Vertical distance from vehicle CM to the axle plane, $h$, in $m$.


Longitudinal distance from center of mass to front hitch, $\mathbf{d h} \mathbf{f}$ - Distance to front hitch
7.5 (default) | scalar

Longitudinal distance from the center of mass to the front hitch, $d h f$, in m .


## Dependencies

To enable this parameter, on the Input signals pane, select Front hitch forces or Front hitch moments.

Vertical distance from front hitch to axle plane, $\mathbf{h h} \mathbf{f}$ - Distance from front hitch to axle plane 0.6 (default) | scalar

Vertical distance from the front hitch to the axle plane, $h h f$, in $m$.


## Dependencies

To enable this parameter, on the Input signals pane, select Front hitch forces or Front hitch moments.

Longitudinal distance from center of mass to rear hitch, $\mathbf{d h} \mathbf{r}$ - Distance to front hitch 7.5 (default) | scalar

Longitudinal distance from the center of mass to the rear hitch, $d h_{-} r$, in $m$.


## Dependencies

To enable this parameter, on the Input signals pane, select Rear hitch forces or Rear hitch moments.

Vertical distance from front hitch to axle plane, hh_r - Distance from rear hitch to axle plane 0.6 (default) | scalar

Vertical distance from the rear hitch to the axle plane, $h h_{-} r$, in $m$.


## Dependencies

To enable this parameter, on the Input signals pane, select Rear hitch forces or Rear hitch moments.

Initial inertial frame longitudinal position, X_o - Initial inertial X location
0 (default) | scalar
Initial vehicle CG displacement along the earth-fixed $X$-axis, in m .
Initial longitudinal velocity, xdot_o - Initial velocity
0 (default) | scalar
Initial vehicle CG velocity along the vehicle-fixed $x$-axis, in $\mathrm{m} / \mathrm{s}$.

## Dependencies

To enable this parameter, set Axle forces to one of these options:

- External longitudinal forces
- External forces

Lateral
Mapped corner stiffness - Selection
off (default) | on

Enables mapped corner stiffness calculation.

## Dependencies

To enable this parameter, set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces

Include relaxation length dynamics - Enable relaxation length dynamics
on (default) | off
Enables relaxation length dynamics.
Dependencies
To enable this parameter:
1 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces


## 2 Clear Mapped corner stiffness.

Lateral distance from geometric centerline to center of mass, $\mathbf{d}$ - Distance from centerline to CM

```
0 (default) | scalar
```

Lateral distance from the geometric centerline to the center of mass, $d$, in $m$, along the vehicle-fixed $y$. Positive values indicate that the trailer CM is to the right of the geometric centerline. Negative values indicate that the trailer CM is to the left of the geometric centerline.


Lateral distance from geometric centerline to front hitch, hl_f - Distance from centerline to front hitch
0 (default) | scalar
Lateral distance from the geometric centerline to the front hitch, hl $f$, in m , along the vehicle-fixed $y$. Positive values indicate that the trailer hitch is to the right of the geometric centerline. Negative values indicate that the trailer hitch is to the left of the geometric centerline.


## Dependencies

To enable this parameter, on the Input signals pane, select Front hitch forces or Front hitch moments.

Lateral distance from geometric centerline to rear hitch, hl_r - Distance from centerline to rear hitch
0 (default) | scalar
Lateral distance from the geometric centerline to the rear hitch, $h l r$, in $m$, along the vehicle-fixed $y$. Positive values indicate that the trailer hitch is to the right of the geometric centerline. Negative values indicate that the trailer hitch is to the left of the geometric centerline.


## Dependencies

To enable this parameter, on the Input signals pane, select Rear hitch forces or Rear hitch moments.

Front track width, w_f - Front track width
1.82 (default) | scalar

Front track width, $w f$, in m.


Dependencies
To enable this parameter, set Vehicle track to Dual 2-axle, Dual 2-axle, or Dual 3-axle.
Middle track width, w_m - Middle track width
1.82 (default) | scalar

Middle track width, wm, in m.


## Dependencies

To enable this parameter, set Vehicle track to Dual 3-axle.
Rear track width, w_r - Rear track width
1.82 (default) | scalar

Rear track width, $w r$, in $m$.


## Dependencies

To enable this parameter, set Vehicle track to Dual 2-axle or Dual 3-axle.
Front axle tire corner stiffness, Cy_f - Front axle tire stiffness
12.3 (default) | scalar

Front tire corner stiffness, $C y_{f}$, in $\mathrm{N} / \mathrm{rad}$.

## Dependencies

To enable this parameter:
1 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces

2 Clear Mapped corner stiffness.
Middle axle tire corner stiffness, Cy_m - Middle axle tire stiffness
11.3 (default) | scalar

Middle tire corner stiffness, $C y_{m}$, in N/rad.

## Dependencies

To enable this parameter:
1 Set Vehicle track to one of these options:

- Single 3-axle
- Dual 3-axle

2 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces

3 Clear Mapped corner stiffness.

Rear axle tire corner stiffness, Cy_r - Rear axle tire stiffness
11.3 (default) | scalar

Rear tire corner stiffness, $C y_{r}$, in $\mathrm{N} / \mathrm{rad}$.

## Dependencies

To enable this parameter:
1 Set Vehicle track to one of these options:

- Single 2-axle
- Dual 2-axle
- Single 3-axle
- Dual 3-axle

2 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces

3 Clear Mapped corner stiffness.
Front tire(s) relaxation length, sigma_f - Relaxation length
. 1 (default) | scalar
Front tire relaxation length, $\sigma_{f}$, in m .

## Dependencies

To enable this parameter:
1 Set Vehicle track to one of these options:

- Single 2-axle
- Dual 2-axle
- Single 3-axle
- Dual 3-axle

2 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces

3 Do either of these:

- Select Mapped corner stiffness.
- Clear Mapped corner stiffness and select Include relaxation length dynamics.

Middle tire(s) relaxation length, sigma_m - Relaxation length
. 1 (default) | scalar
Middle tire relaxation length, $\sigma_{m}$, in m .

## Dependencies

To enable this parameter:

1 Set Vehicle track to one of these options:

- Single 3-axle
- Dual 3-axle

2 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces

3 Do either of these:

- Select Mapped corner stiffness.
- Clear Mapped corner stiffness and select Include relaxation length dynamics.

Rear tire(s) relaxation length, sigma_r - Relaxation length
. 1 (default) | scalar
Rear tire relaxation length, $\sigma_{r}$, in m .

## Dependencies

To enable this parameter:
1 Set Vehicle track to one of these options:

- Single 2-axle
- Dual 2-axle
- Single 3-axle
- Dual 3-axle

2 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces

3 Do either of these:

- Select Mapped corner stiffness.
- Clear Mapped corner stiffness and select Include relaxation length dynamics.


## Front axle slip angle breakpoints, alpha_f_brk - Breakpoints

[-. 1 .1] (default)|vector
Front axle slip angle breakpoints, $\alpha_{f b r k}$, in rad.

## Dependencies

To enable this parameter:
1 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces

2 Select Mapped corner stiffness.

## Front axle corner data, Cy_f_data - Breakpoints

## [-9e3 9e3] (default)|vector

Front axle corner data, $C y_{f f a t a}$, in N/rad.

## Dependencies

To enable this parameter:
1 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces

2 Select Mapped corner stiffness.
Middle axle slip angle breakpoints, alpha_m_brk - Breakpoints
[-. 1 .1] (default) |vector
Middle axle slip angle breakpoints, $\alpha_{m b r k}$, in rad.

## Dependencies

To enable this parameter:
1 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces


## 2 Select Mapped corner stiffness.

Middle axle corner data, Cy_m_data - Breakpoints
[-9e3 9e3] (default)|vector
Middle axle corner data, $C y_{\text {mdata }}$, in $\mathrm{N} / \mathrm{rad}$.

## Dependencies

To enable this parameter:
1 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces

2 Select Mapped corner stiffness.
Rear axle slip angle breakpoints, alpha_r_brk - Breakpoints
[-. 1 .1] (default)|vector
Rear axle slip angle breakpoints, $\alpha_{r b r k}$, in rad.
Dependencies
To enable this parameter:
1 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces

2 Select Mapped corner stiffness.
Rear axle corner data, Cy_r_data - Data
[-9e3 9e3] (default) | vector
Rear axle corner data, $C y_{\text {rdata }}$, in $\mathrm{N} / \mathrm{rad}$.

## Dependencies

To enable this parameter:
1 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces


## 2 Select Mapped corner stiffness.

Initial inertial frame lateral displacement, Y_o - Position
0 (default) | scalar
Initial vehicle CG displacement along the earth-fixed $Y$-axis, in $m$.
Initial lateral velocity, ydot_o - Velocity
0 (default) | scalar
Initial vehicle CG velocity along the vehicle-fixed $y$-axis, in $\mathrm{m} / \mathrm{s}$.

## Yaw

Yaw polar inertia, Izz - Inertia
4000 (default) | scalar
Yaw polar inertia, in $\mathrm{kg}^{*} \mathrm{~m}^{\wedge} 2$.
Initial yaw angle, psi_o - Psi rotation
0 (default) | scalar
Rotation of the vehicle-fixed frame about earth-fixed $Z$-axis (yaw), in rad.
Initial yaw rate, r_o - Yaw rate
0 (default) | scalar
Vehicle angular velocity about the vehicle-fixed $z$-axis (yaw rate), in rad/s.

## Aerodynamic

Longitudinal drag area, Af - Effective vehicle cross-sectional area
2 (default) | scalar
Effective vehicle cross-sectional area, $A_{f}$, to calculate the aerodynamic drag force on the vehicle, in $\mathrm{m}^{2}$.

Longitudinal drag coefficient, Cd - Air drag coefficient
. 3 (default) | scalar

Air drag coefficient, $C_{d}$. The value is dimensionless.
Longitudinal lift coefficient, CI - Air lift coefficient
. 1 (default) | scalar
Air lift coefficient, $C_{l}$. The value is dimensionless.
Longitudinal drag pitch moment, Cpm - Pitch drag
. 1 (default) | scalar
Longitudinal drag pitch moment coefficient, $C_{p m}$. The value is dimensionless.
Relative wind angle vector, beta_w - Wind angle
[0:0.01:0.3] (default) | vector
Relative wind angle vector, $\beta_{w}$, in rad.
Side force coefficient vector, Cs - Side force coefficient
[0:0.03:0.9] (default)| vector
Side force coefficient vector coefficient, $C_{s}$. The value is dimensionless.
Yaw moment coefficient vector, Cym - Yaw moment drag
[0:0.01:0.3] (default) | vector
Yaw moment coefficient vector coefficient, $C_{y m}$. The value is dimensionless.

## Environment

## Absolute air pressure, Pabs - Pressure

101325 (default) | scalar
Environmental absolute pressure, $P_{a b s}$, in Pa.
Air temperature, Tair - Temperature
273 (default) | scalar
Environmental absolute temperature, $T$, in K.

## Dependencies

To enable this parameter, clear Air temperature.
Gravitational acceleration, $\mathbf{g}$ - Gravity
9.81 (default) | scalar

Gravitational acceleration, $g$, in $m / \mathrm{s}^{\wedge} 2$.
Nominal friction scaling factor, mu - Friction scale factor
1 (default) | scalar
Nominal friction scale factor, $\mu$. The value is dimensionless.

## Dependencies

To enable this parameter:

1 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces


## 2 Clear External Friction.

## Simulation

Longitudinal velocity tolerance, xdot_tol - Tolerance
. 01 (default) | scalar
Longitudinal velocity tolerance, in $\mathrm{m} / \mathrm{s}$.
Nominal normal force, Fznom - Normal force
5000 (default) | scalar
Nominal normal force, in N .

## Dependencies

To enable this parameter, set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces

Geometric longitudinal offset from axle plane, longOff - Longitudinal offset 0 (default) | scalar

Vehicle chassis offset from the axle plane along the vehicle-fixed $x$-axis, in $m$. When you use the 3D visualization engine, consider using the offset to locate the chassis independently of the vehicle CG.

## Geometric lateral offset from center plane, latOff - Lateral offset

0 (default) | scalar
Vehicle chassis offset from the center plane along the vehicle-fixed $y$-axis, in $m$. When you use the 3D visualization engine, consider using the offset to locate the chassis independently of the vehicle CG.

Geometric vertical offset from axle plane, vertOff - Vertical offset
0 (default) | scalar
Vehicle chassis offset from the axle plane along the vehicle-fixed $z$-axis, in m . When you use the 3D visualization engine, consider using the offset to locate the chassis independently of the vehicle CG.

Wrap Euler angles, wrapAng - Wrap the Euler angles to the interval [-pi, pi]
off (default) | on
Wrap the Euler angles to the interval [-pi, pi]. For vehicle maneuvers that might undergo vehicle yaw rotations that are outside of this interval, consider clearing the parameter if you want to:

- Track the total vehicle yaw rotation.
- Avoid discontinuities in the vehicle state estimators.


## Version History

## Introduced in R2020a

## References

[1] Gillespie, Thomas. Fundamentals of Vehicle Dynamics. Warrendale, PA: Society of Automotive Engineers (SAE), 1992.

## Extended Capabilities

C/C++ Code Generation
Generate C and $\mathrm{C}++$ code using Simulink $®$ Coder $^{\mathrm{TM}}$.

## See Also

Vehicle Body 3DOF Three Axles | Vehicle Body 3DOF | Trailer Body 6DOF
Topics
"Coordinate Systems in Vehicle Dynamics Blockset"

## Trailer Body 6DOF

Trailer body with translational and rotational motion


## Libraries:

Vehicle Dynamics Blockset / Vehicle Body

## Description

The Trailer Body 6DOF block implements a rigid one-axle, two-axle or three-axle trailer body model that calculates longitudinal, lateral, vertical, pitch, roll, and yaw motion. The block accounts for body mass, inertia, aerodynamic drag, road incline, and weight distribution between the axle hard-point locations due to suspension and external forces and moments.

Use the Inertial Loads parameters to analyze the trailer dynamics under different loading conditions. To specify the number of trailer axles, use the Number of axles parameter.

To create additional input ports, under Input signals, select these block parameters.

| Parameter | Input Port | Description |
| :--- | :--- | :--- |
| Front hitch forces | FhF | Hitch force applied to the body at the front hitch location, <br> $F h F_{x}, F h F_{y}$, and $F h F_{z}$, in the vehicle-fixed frame |
| Front hitch moments | MhF | Hitch moment at the front hitch location, $M h F_{x}, M h F_{y}$, and <br> $M h F_{z}$, about the vehicle-fixed frame |
| Rear hitch forces | FhR | Hitch force applied to the body at the rear hitch location, <br> $F h R_{x}, F h R_{y}$, and $F h R_{z}$, in the vehicle-fixed frame |
| Rear hitch moments | MhR | Hitch moment at the rear hitch location, $M h R_{x}, M h R_{y}$, and <br> $M h R_{z}$, about the vehicle-fixed frame |

## Inertial Loads

To analyze the vehicle dynamics under different loading conditions, use the Inertial Loads parameters. You can specify these loads:

- Front end
- Overhead
- Front left and front right
- Rear left and rear right
- Rear end

For each of the loads, you can specify the mass, location, and inertia.
The illustrations provide the load locations and vehicle parameter dimensions. The table provides the corresponding location parameter sign settings.


This table summarizes the parameter settings that specify the load locations indicated by the dots. For the location, the block uses this distance vector:

- Front axle to load, along the vehicle-fixed $x$-axis
- Vehicle centerline to load, along the vehicle-fixed $y$-axis
- Front axle to load, along the vehicle-fixed $z$-axis

| Load | Parameter | Example Location |
| :---: | :---: | :---: |
| Front end | Distance vector from front axle, z1R | - $\operatorname{z1R}(1,1)<0-$ Forward of the front axle <br> - $\operatorname{z1R}(1,2)>0-$ Right of the vehicle centerline <br> - $\quad \operatorname{z1R}(1,3)>0-$ Above the front axle suspension hardpoint |
| Overhead | Distance vector from front axle, z2R | - $\operatorname{z2R}(1,1)>0-$ Rear of the front axle <br> - $\operatorname{z2R}(1,2)<0-$ Left of the vehicle centerline <br> - $z 2 R(1,3)>0-$ Above the front axle suspension hardpoint |
| Front left | Distance vector from front axle, z3R | - $\operatorname{z3R}(1,1)>0-$ Rear of the front axle <br> - $z 3 R(1,2)<0-$ Left of the vehicle centerline <br> - $z 3 R(1,3)>0-$ Above the front axle suspension hardpoint |


| Load | Parameter | Example Location |
| :---: | :---: | :---: |
| Front right | Distance vector from front axle, z4R | - $\quad z 4 R(1,1)>0-$ Rear of the front axle <br> - $z 4 R(1,2)>0-$ Right of the vehicle centerline <br> - $z 4 R(1,3)>0-$ Above the front axle suspension hardpoint |
| Rear left | Distance vector from front axle, z5R | - $\quad 25 R(1,1)>0-$ Rear of the front axle <br> - $z 5 R(1,2)<0-$ Left of the vehicle centerline <br> - $\quad \operatorname{z5R}(1,3)>0-$ Above the front axle suspension hardpoint |
| Rear right | Distance vector from front axle, z6R | - $\operatorname{z6R}(1,1)>0-$ Rear of the front axle <br> - $\quad 26 R(1,2)>0-$ Right of the vehicle centerline <br> - $\quad \operatorname{z6R}(1,3)>0-$ Above the front axle suspension hardpoint |
| Rear end | Distance vector from front axle, z7R | - $\operatorname{z7R}(1,1)>0-$ Rear of the front axle <br> - $\quad$ 77R $(1,2)>0-$ Right of the vehicle centerline <br> - $z 7 R(1,3)>0-$ Above the front axle suspension hardpoint |

## Equations of Motion

To determine the vehicle motion, the block implements calculations for the rigid body vehicle dynamics, wind drag, inertial loads, and coordinate transformations. The body-fixed and vehicle-fixed coordinate systems are the same.

The block considers the rotation of a body-fixed coordinate frame about a flat earth-fixed inertial reference frame. The origin of the body-fixed coordinate frame is the vehicle center of gravity of the body.

The block uses this equation to calculate the translational motion of the body-fixed coordinate frame, where the applied forces $\left[F_{x} F_{y} F_{z}\right]^{\mathrm{T}}$ are in the body-fixed frame, and the mass of the body, $m$, is assumed to be constant.

$$
\begin{aligned}
& \bar{F}_{b}=\left[\begin{array}{l}
F_{x} \\
F_{y} \\
F_{z}
\end{array}\right]=m\left(\dot{\bar{V}}_{b}+\bar{\omega} \times \bar{V}_{b}\right) \\
& \bar{M}_{b}=\left[\begin{array}{l}
L \\
M \\
N
\end{array}\right]=I \dot{\bar{\omega}}+\bar{\omega} \times(I \bar{\omega}) \\
& I=\left[\begin{array}{ccc}
I_{x x} & -I_{x y} & -I_{x z} \\
-I_{y x} & I_{y y} & -I_{y z} \\
-I_{z x} & -I_{z y} & I_{z z}
\end{array}\right]
\end{aligned}
$$

To determine the relationship between the body-fixed angular velocity vector, $[p q r]^{\mathrm{T}}$, and the rate of change of the Euler angles, $\left[\begin{array}{lll}\dot{\phi} & \dot{\theta} & \dot{\psi}\end{array}\right]^{T}$, the block resolves the Euler rates into the body-fixed frame.

$$
\left[\begin{array}{l}
p \\
q \\
r
\end{array}\right]=\left[\begin{array}{l}
\dot{\phi} \\
0 \\
0
\end{array}\right]+\left[\begin{array}{ccc}
1 & 0 & 0 \\
0 & \cos \phi & \sin \phi \\
0 & -\sin \phi & \cos \phi
\end{array}\right]\left[\begin{array}{l}
0 \\
\dot{\theta} \\
0
\end{array}\right]+\left[\begin{array}{ccc}
1 & 0 & 0 \\
0 & \cos \phi & \sin \phi \\
0 & -\sin \phi & \cos \phi
\end{array}\right]\left[\begin{array}{ccc}
\cos \theta & 0 & -\sin \theta \\
0 & 1 & 0 \\
\sin \theta & 0 & \cos \theta
\end{array}\right]\left[\begin{array}{l}
0 \\
0 \\
\dot{\psi}
\end{array}\right] \equiv J^{-1}\left[\begin{array}{c}
\dot{\phi} \\
\dot{\theta} \\
\dot{\psi}
\end{array}\right]
$$

Inverting $J$ gives the required relationship to determine the Euler rate vector.

$$
\left[\begin{array}{c}
\dot{\phi} \\
\dot{\theta} \\
\dot{\psi}
\end{array}\right]=J\left[\begin{array}{l}
p \\
q \\
r
\end{array}\right]=\left[\begin{array}{ccc}
1 & (\sin \phi \tan \theta) & (\cos \phi \tan \theta) \\
0 & \cos \phi & -\sin \phi \\
0 & \frac{\sin \phi}{\cos \theta} & \frac{\cos \phi}{\cos \theta}
\end{array}\right]\left[\begin{array}{l}
p \\
q \\
r
\end{array}\right]
$$

The applied forces and moments are the sum of the drag, gravitational, external, and suspension forces.

$$
\begin{aligned}
& \bar{F}_{b}=\left[\begin{array}{l}
F_{x} \\
F_{y} \\
F_{z}
\end{array}\right]=\left[\begin{array}{l}
F_{d_{x}} \\
F_{d_{y}} \\
F_{d_{z}}
\end{array}\right]+\left[\begin{array}{l}
F_{g_{x}} \\
F_{g_{y}} \\
F_{g_{z}}
\end{array}\right]+\left[\begin{array}{l}
F_{\text {ext }} \\
F_{e x t_{y}} \\
F_{\text {ext }}
\end{array}\right]+\left[\begin{array}{l}
F_{F L_{x}} \\
F_{F L_{y}} \\
F_{F L_{z}}
\end{array}\right]+\left[\begin{array}{l}
F_{F R_{x}} \\
F_{F R_{y}} \\
F_{F R_{z}}
\end{array}\right]+\left[\begin{array}{l}
F_{M L_{x}} \\
F_{M L_{y}} \\
F_{M L_{z}}
\end{array}\right]+\left[\begin{array}{l}
F_{M R_{x}} \\
F_{M R_{y}} \\
F_{M R_{z}}
\end{array}\right]+\left[\begin{array}{l}
F_{R L_{x}} \\
F_{R L_{y}} \\
F_{R L_{z}}
\end{array}\right]+\left[\begin{array}{l}
F_{R R_{x}} \\
F_{R R_{y}} \\
F_{R R_{z}}
\end{array}\right]=\left[\begin{array}{l}
M_{d_{x}} \\
M_{d_{y}} \\
M_{d_{z}}
\end{array}\right]+\left[\begin{array}{l}
M_{\text {extx }} \\
M_{\text {exty }} \\
M_{\text {ext }}
\end{array}\right]+\left[\begin{array}{l}
M_{F L_{x}} \\
M_{F L_{y}} \\
M_{F L_{z}}
\end{array}\right]+\left[\begin{array}{l}
M_{F R_{x}} \\
M_{F R_{y}} \\
M_{F R_{z}}
\end{array}\right]+\left[\begin{array}{l}
M_{M L_{x}} \\
M_{M L_{y}} \\
M_{M L_{z}}
\end{array}\right]+\left[\begin{array}{l}
M_{M R_{x}} \\
M_{M R_{y}} \\
M_{M R_{z}}
\end{array}\right]+\left[\begin{array}{l}
M_{R L_{x}} \\
M_{R L_{y}} \\
M_{R L_{z}}
\end{array}\right]+\left[\begin{array}{l}
M_{R R_{x}} \\
M_{R R_{y}} \\
M_{R R_{z}}
\end{array}\right]+\bar{M}_{F}
\end{aligned}
$$

| Calculation | Implementation |
| :--- | :--- |
| Load masses and <br> inertias | The block uses the parallel axis theorem to resolve the individual load <br> masses and inertias with the vehicle mass and inertia. <br> $\quad J_{i j}=I_{i j}+m\left(\|R\|^{2} \delta_{i j}-R_{i} R_{j}\right)$ |
| Gravitational forces, <br> $F_{g}$ | The block uses the direction cosine matrix (DCM) to transform the <br> gravitational vector in the inertial-fixed frame to the body-fixed frame. |


| Calculation | Implementation |
| :---: | :---: |
| Drag forces, $F_{d}$, and moments, $M_{d}$ | To determine a relative airspeed, the block subtracts the wind speed from the vehicle center of mass (CM) velocity. Using the relative airspeed, the block determines the drag forces. $\begin{aligned} & \bar{w}=\sqrt{\left(\dot{x}-w_{\chi}\right)^{2}+\left(\dot{x}-w_{\chi}\right)^{2}+\left(w_{z}\right)^{2}} \\ & F_{d x}=-\frac{1}{2 T R} C_{d} A_{f} P_{a b s}\left({ }^{\bar{w}}\right. \\ & F_{d y}=-\frac{1}{2 T R} C_{s} A_{f} P_{a b s}\left({ }^{\bar{w}}\right. \\ & F_{d z}=-\frac{1}{2 T R} C_{l} A_{f} P_{a b s} s^{\bar{w}} \end{aligned}$ <br> Using the relative airspeed, the block determines the drag moments. $\begin{aligned} & M_{d r}=-\frac{1}{2 T R} C_{r m} A_{f} P_{a b s}\left({ }^{\bar{w}}(a+c)\right. \\ & M_{d p}=-\frac{1}{2 T R} C_{p m} A_{f} P_{a b s}{ }^{\bar{w}}(a+c) \\ & M_{d y}=-\frac{1}{2 T R} C_{y m} A_{f} P_{a b s}{ }^{\bar{w}}(a+c) \end{aligned}$ |
| External forces, $F_{i n}$, and moments, $M_{i n}$ | The external forces and moments are input via ports FExt and MExt. |
| Suspension forces and moments | The block assumes that the suspension forces and moments act on these hardpoint locations: <br> - $F_{F L}, M_{F L}-$ Front left <br> - $F_{F R}, M_{F R}-$ Front right <br> - $F_{M L}, M_{M L}$ - Middle left <br> - $F_{M R}, M_{M R}$ - Middle right <br> - $F_{R L}, M_{R L}-$ Rear left <br> - $F_{R R}, M_{R R}-$ Rear right |

The equations use these variables.

| $x, \dot{x}, \ddot{x}$ | Vehicle CM displacement, velocity, and acceleration along the vehicle-fixed |
| :--- | :--- |
| $y, \dot{y}, \ddot{y}$ | -axis |
| $z, \dot{z}, \ddot{z}$ | Vehicle CM displacement, velocity, and acceleration along the vehicle-fixed <br>  <br> $\varphi$ |
| -axis |  |
| $\theta$ | Vehicle CM displacement, velocity, and acceleration along the vehicle-fixed |
| $\psi$ | Rotation of the vehicle-fixed frame about the earth-fixed $X$-axis (roll) |
| Rotation of the vehicle-fixed frame about the earth-fixed $Y$-axis (pitch) |  |
|  | Rotation of the vehicle-fixed frame about the earth-fixed $Z$-axis (yaw) |


| $F_{F L X}, F_{F L y}, F_{F L z}$ | Suspension forces applied to the front left hardpoint along the vehicle-fixed $x$-, $y$-, and $z$-axes |
| :---: | :---: |
| $F_{F R X}, F_{F R y}, F_{F R z}$ | Suspension forces applied to the front right hardpoint along the vehiclefixed $x$-, $y$-, and $z$-axes |
| $F_{M L \chi}, F_{M L y}, F_{M L z}$ | Suspension forces applied to the middle left hardpoint along the vehiclefixed $x$-, $y$-, and $z$-axes |
| $F_{M R X}, F_{M R y}, F_{M R z}$ | Suspension forces applied to the middle right hardpoint along the vehiclefixed $x$-, $y$-, and $z$-axes |
| $F_{R L \chi}, F_{R L y^{\prime}} F_{R L z}$ | Suspension forces applied to the rear left hardpoint along the vehicle-fixed $x$-, $y$-, and $z$-axes |
| $F_{R R x}, F_{R R y}, F_{R R z}$ | Suspension forces applied to the rear right hardpoint along the vehicle-fixed $x$-, $y$-, and $z$-axes |
| $M_{F L \chi}, M_{F L L}, M_{F L z}$ | Suspension moment applied to the front left hardpoint about the vehiclefixed $x$-, $y$-, and $z$-axes |
| $M_{F R X}, M_{F R y}, M_{\text {FRz }}$ | Suspension moment applied to the front right hardpoint about the vehiclefixed $x$-, $y$-, and $z$-axes |
| $M_{M L \chi}, M_{M L y}, M_{M L z}$ | Suspension moment applied to the middle left hardpoint about the vehiclefixed $x$-, $y$-, and $z$-axes |
| $M_{M R x}, M_{M R y}, M_{M R z}$ | Suspension moment applied to the middle right hardpoint about the vehiclefixed $x$-, $y$-, and $z$-axes |
| $M_{R L \chi}, M_{\text {RLL }}, M_{R L z}$ | Suspension moment applied to the rear left hardpoint about the vehiclefixed $x$-, $y$-, and $z$-axes |
| $M_{R R x}, M_{R R y}, M_{R R z}$ | Suspension moment applied to the rear right hardpoint about the vehiclefixed $x$-, $y$-, and $z$-axes |
| $F_{\text {extx }}, F_{\text {exty }}, F_{\text {extz }}$ | External forces applied to the vehicle CM along the vehicle-fixed $x$-, $y$-, and $z$-axes |
| $F_{d x}, F_{d y}, F_{d z}$ | Drag forces applied to the vehicle CM along the vehicle-fixed $x-, y$-, and $z$ axes |
| $M_{\text {extx }}, M_{\text {exty }}, M_{\text {extz }}$ | External moment about the vehicle CM about the vehicle-fixed $x$-, $y$-, and $z$ axes |
| $M_{d x}, M_{d y}, M_{d z}$ | Drag moment about the vehicle CM about the vehicle-fixed $x$-, $y$-, and $z$-axes |
| $I$ | Vehicle body moments of inertia |
| $a, b, c$ | Distance of the front, middle, and rear axles, respectively, from the normal projection point of the vehicle CM onto the common axle plane |
| $h$ | Height of the vehicle CM above the axle plane |
| $d$ | Lateral distance from the geometric centerline to the center of mass along the vehicle-fixed $y$-axis |
| $h h f, h h_{-} r$ | Height of the front and rear hitches, respectively, above the axle plane along the vehicle-fixed $z$-axis |
| $d h f, d h \quad r$ | Longitudinal distance of the front and rear hitches, respectively, from the normal projection point of the vehicle CM onto the common axle plane |
| $h l f, h l \_r$ | Lateral distance from center of mass to the front and rear hitches, respectively, along the vehicle-fixed $y$-axis |
| $w_{F}, w_{M}, w_{R}$ | Front, middle, and rear track widths, respectively |


| $C_{d}$ | Air drag coefficient acting along the vehicle-fixed $x$-axis |
| :--- | :--- |
| $C_{s}$ | Air drag coefficient acting along the vehicle-fixed $y$-axis |
| $C_{l}$ | Air drag coefficient acting along the vehicle-fixed $z$-axis |
| $C_{r m}$ | Air drag roll moment acting about the vehicle-fixed $x$-axis |
| $C_{p m}$ | Air drag pitch moment acting about the vehicle-fixed $y$-axis |
| $C_{y m}$ | Air drag yaw moment acting about the vehicle-fixed $z$-axis |
| $A_{f}$ | Frontal area |
| $R$ | Atmospheric specific gas constant |
| $T$ | Environmental air temperature |
| $P_{a b s}$ | Environmental absolute pressure |
| $w_{x}, w_{y}, w_{z}$ | Wind speed along the vehicle-fixed $x$-, $y$-, and $z$-axes |
| $W_{x}, W_{y}, W_{z}$ | Wind speed along inertial $X$-, $Y$-, and $Z$-axes |

## Ports

## Input

FSusp - Suspension forces on trailer
3-by - 4 array (default) | 3-by-2 array | 3 -by - 6 array
Suspension longitudinal, lateral, and vertical suspension forces, FSusp, applied to the trailer at the hardpoint location, in N, specified as a 3-by-2, 3-by-4, or 3-by-6 array, depending on the Number of axles parameter.

| Number of axles Setting | Variable | Signal Dimension |
| :---: | :---: | :---: |
| 1 | $F S u s p=\left[\begin{array}{lll}F_{F L X} & F_{F R x} \\ F_{F L y} & F_{F R y} \\ F_{F L z} & F_{F R z}\end{array}\right]$ | Array - 3-by-2 |
| 2 | $F S u s p=\left[\begin{array}{llll}F_{F L x} & F_{F R x} & F_{R L x} & F_{R R x} \\ F_{F L y} & F_{F R y} & F_{R L y} & F_{R R y} \\ F_{F L z} & F_{F R z} & F_{R L z} & F_{R R z}\end{array}\right]$ | Array - 3-by-4 |
| 3 | $F$ Susp $=$ $\left.\left[\begin{array}{lllll} F_{F L x} & F_{F R x} & F_{M L x} & F_{M R x} & F_{R L x} \end{array} F_{R R x}\right] \text { } \begin{array}{llll} F_{F L y} & F_{F R y} & F_{M L y} & F_{M R y} \\ F_{R L y} & F_{R R y} \\ F_{F L z} & F_{F R z} & F_{M L z} & F_{M R z} \\ F_{R L z} & F_{R R z} \end{array}\right]$ | Array - 3-by-6 |

The arrays use these variables.
$F_{F L x}, F_{F L y}, F_{F L z} \quad$ Suspension forces applied to front left hardpoint along the vehicle-fixed $x$-, $y$-, and $z$-axes

| $F_{F R x}, F_{F R y}, F_{F R z}$ | Suspension forces applied to front right hardpoint along the vehicle-fixed $x$-, <br> $y$-, and $z$-axes |
| :--- | :--- |
| $F_{M L x}, F_{M L y}, F_{M L z}$ | Suspension forces applied to middle left hardpoint along the vehicle-fixed $x$-, <br> $y-$, and $z$-axes |
| $F_{M R x}, F_{M R y}, F_{M R z}$ | Suspension forces applied to middle right hardpoint along the vehicle-fixed <br> $x$-, $y$-, and $z$-axes |
| $F_{R L x}, F_{R L y}, F_{R L z}$ | Suspension forces applied to rear left hardpoint along the vehicle-fixed $x$-, <br> $y-$ - and $z$-axes |
| $F_{R R x}, F_{R R y}, F_{R R z}$ | Suspension forces applied to rear right hardpoint along the vehicle-fixed $x-$, <br> $y-$, and $z$-axes |

MSusp - Suspension moments on trailer
3-by-4 array (default)|3-by-2 array|3-by-6 array
Suspension longitudinal, lateral, and vertical suspension moments, MSusp, applied about the vehicle at the hardpoint location, in $\mathrm{N} \cdot \mathrm{m}$, specified as a $3-$ by -2 , 3-by-4, or 3-by-6 array, depending on the Number of axles parameter.

| Number of axles Setting | Variable | Signal Dimension |
| :---: | :---: | :---: |
| 1 | MSusp $=\left[\begin{array}{lll}M_{F L X} & M_{F R X} \\ M_{F L y} & M_{F R y} \\ M_{F L z} & M_{F R z}\end{array}\right]$ | Array - 3-by-2 |
| 2 | $\text { MSusp }=\left[\begin{array}{llll} M_{F L x} & M_{F R x} & M_{R L x} & M_{R R x} \\ M_{F L y} & M_{F R y} & M_{R L y} & M_{R R y} \\ M_{F L z} & M_{F R z} & M_{R L z} & M_{R R z} \end{array}\right]$ | Array - 3-by-4 |
| 3 | MSusp $=$ | Array - 3-by-6 |

The arrays use these variables.

| $M_{F L x}, M_{F L y}, M_{F L z}$ | Suspension moment applied to front left hardpoint about the vehicle-fixed <br> $x$-, $y$-, and $z$-axes |
| :--- | :--- |
| $M_{F R x}, M_{F R y}, M_{F R z}$ | Suspension moment applied to front right hardpoint about the vehicle-fixed <br> $x$-, $y$-, and $z$-axes |
| $M_{M L x}, M_{M L y}, M_{M L z}$ | Suspension moment applied to middle left hardpoint about the vehicle-fixed <br> $x-, y$-, and $z$-axes |
| $M_{M R x}, M_{M R y}, M_{M R z}$ | Suspension moment applied to middle right hardpoint about the vehicle- <br> fixed $x-, y-$, and $z$-axes |


| $M_{R L x}, M_{R L y}, M_{R L z}$ | Suspension moment applied to rear left hardpoint about the vehicle-fixed x-, |
| :--- | :--- |
|  | $y$-, and $z$-axes |
| $M_{R R x}, M_{R R y}, M_{R R z}$ | Suspension moment applied to rear right hardpoint about the vehicle-fixed <br> $x-, y$-, and $z$-axes |

FExt - External forces acting on vehicle vector

External forces on the vehicle, in $N$, specified as a 1-by-3 or 3-by-1 vector.

$$
\mathrm{FExt}=F_{\text {ext }}=\left[\begin{array}{llll}
F_{\text {ext }} & F_{\text {ext }} & F_{\text {ext }}
\end{array}\right] \text { or }\left[\begin{array}{l}
F_{\text {ext }}^{x} \\
F_{\text {ext }}^{y} \\
F_{\text {ext }}^{z}
\end{array}\right]
$$

| Array Element | Force Axis |
| :--- | :--- |
| FExt $(1,1)$ | Vehicle-fixed $x$-axis (longitudinal) |
| FExt $(1,2)$ or <br> FExt $(2,1)$ | Vehicle-fixed $y$-axis (lateral) |
| FExt $(1,3)$ or <br> FExt $(3,1)$ | Vehicle-fixed $z$-axis (vertical) |

MExt - External moments acting on vehicle

## vector

External moments acting on the vehicle, in $N \cdot m$, specified as a 1-by-3 or 3-by-1 vector.

$$
\mathrm{MExt}=M_{e x t}=\left[\begin{array}{lll}
M_{e x t_{\chi}} & M_{e x t_{y}} & M_{e x t_{z}}
\end{array}\right] \text { or }\left[\begin{array}{l}
M_{e x t_{\chi}} \\
M_{e x t_{y}} \\
M_{e x t_{z}}
\end{array}\right]
$$

| Array Element | Force Axis |
| :--- | :--- |
| MExt $(1,1)$ | Vehicle-fixed $x$-axis (longitudinal) |
| MExt $(1,2)$ or <br> MExt $(2,1)$ | Vehicle-fixed $y$-axis (lateral) |
| MExt $(1,3)$ or <br> MExt $(3,1)$ | Vehicle-fixed $z$-axis (vertical) |

FhF - Front hitch force on the body array

Hitch force applied to the body at the front hitch location, $F h F_{x}, F h F_{y}, F h F_{z}$, in the vehicle-fixed frame, in N , specified as a 1-by-3 or 3-by-1 array.

## Dependencies

To enable this port, under Input signals, select Front hitch forces.
MhF - Front hitch moment about body
array

Hitch moment at the front hitch location, $M h F_{x}, M h F_{y}, M h F_{z}$, about the vehicle-fixed frame, in $\mathrm{N} \cdot \mathrm{m}$, specified as a 1-by-3 or 3-by-1 array.

## Dependencies

To enable this port, under Input signals, select Front hitch moments.
FhR - Rear hitch force on the body
array
Hitch force applied to the body at the rear hitch location, $F h R_{x}, F h R_{y}, F h R_{z}$, in the vehicle-fixed frame, in N , specified as a 1-by-3 or 3-by-1 array.

## Dependencies

To enable this port, under Input signals, select Rear hitch forces.
MhR - Rear hitch moment about body array

Hitch moment at the rear hitch location, $M h R_{x}, M h R_{y}, M h R_{z}$, about the vehicle-fixed frame, in $\mathrm{N} \cdot \mathrm{m}$, specified as a 1-by-3 or 3-by-1 array.

## Dependencies

To enable this port, under Input signals, select Rear hitch moments.
WindXYZ - Wind speed
array
Wind speed, $W_{x}, W_{y}, W_{z}$ along inertial $X$-, $Y$-, and $Z$-axes, in m/s, specified as a 1-by-3 or 3-by-1 array.

AirTemp - Ambient air temperature
scalar
Ambient air temperature, $T_{\text {air }}$, in K , specified as a scalar.

## Dependencies

To enable this port, under Environment, select Air temperature.

## Output

Info - Trailer body information
bus
Trailer body information, returned as a bug signal containing the following values.

| Signal |  |  | Description | Value | Units |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| InertFrm | Cg | Disp | X | Vehicle CM displacement <br> along the earth-fixed $X-$ <br> axis | Computed | m |


|  |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Signal |  | Y |  | Vehicle CM displacement along the earth-fixed $Y$ axis | Computed | m |
|  |  | Z |  | Vehicle CM displacement along the earth-fixed Zaxis | Computed | m |
|  | Vel | Xdot |  | Vehicle CM velocity along the earth-fixed $X$-axis | Computed | m/s |
|  |  | Ydot |  | Vehicle CM velocity along the earth-fixed $Y$-axis | Computed | m/s |
|  |  | Zdot |  | Vehicle CM velocity along the earth-fixed $Z$-axis | Computed | m/s |
|  | Ang | phi |  | Rotation of the vehiclefixed frame about the earth-fixed $X$-axis (roll) | Computed | rad |
|  |  | theta |  | Rotation of the vehiclefixed frame about the earth-fixed $Y$-axis (pitch) | Computed | rad |
|  |  | psi |  | Rotation of the vehiclefixed frame about the earth-fixed $Z$-axis (yaw) | Computed | rad |
| FrntAxl | Lft | Disp | X | Front left axle displacement along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Y | Front left axle displacement along the earth-fixed $Y$-axis | Computed | m |
|  |  |  | Z | Front left axle displacement along the earth-fixed Z-axis | Computed | m |
|  |  | Vel | $\begin{aligned} & \mathrm{Xdo} \\ & \mathrm{t} \end{aligned}$ | Front left axle velocity along the earth-fixed $X$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \text { Ydo } \\ & \dagger \end{aligned}$ | Front left axle velocity along the earth-fixed $Y$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{Zdo} \\ & \mathrm{t} \end{aligned}$ | Front left axle velocity along the earth-fixed Zaxis | Computed | m/s |
|  | Rght | Disp | X | Front right axle displacement along the earth-fixed $X$-axis | Computed | m |


|  |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Signal |  |  | Y | Front right axle displacement along the earth-fixed $Y$-axis | Computed | m |
|  |  |  | Z | Front right axle displacement along the earth-fixed Z-axis | Computed | m |
|  |  | Vel | $\begin{aligned} & \text { Xdo } \\ & \mathrm{t} \end{aligned}$ | Front right axle velocity along the earth-fixed $X$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{Ydo} \\ & \mathrm{t} \end{aligned}$ | Front right axle velocity along the earth-fixed $Y$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{Zdo} \\ & \mathrm{t} \end{aligned}$ | Front right axle velocity along the earth-fixed Zaxis | Computed | m/s |
| Midlaxl | Lft | Disp | X | Middle left axle displacement along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Y | Middle left axle displacement along the earth-fixed $Y$-axis | Computed | m |
|  |  |  | Z | Middle left axle displacement along the earth-fixed Z-axis | Computed | m |
|  |  | Vel | $\begin{aligned} & \mathrm{Xdo} \\ & \mathrm{t} \end{aligned}$ | Middle left axle velocity along the earth-fixed $X$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{Ydo} \\ & \mathrm{t} \end{aligned}$ | Middle left axle velocity along the earth-fixed $Y$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{Zdo} \\ & \mathrm{t} \end{aligned}$ | Middle left axle velocity along the earth-fixed $Z$ axis | Computed | m/s |
|  | Rght | Disp | X | Middle right axle displacement along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Y | Middle right axle displacement along the earth-fixed $Y$-axis | Computed | m |
|  |  |  | Z | Middle right axle displacement along the earth-fixed $Z$-axis | Computed | m |
|  |  | Vel | $\begin{aligned} & \mathrm{Xdo} \\ & \mathrm{t} \end{aligned}$ | Middle right axle velocity along the earth-fixed $X$ axis | Computed | m/s |


| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{aligned} & \text { Ydo } \\ & \mathrm{t} \end{aligned}$ | Middle right axle velocity along the earth-fixed $Y$ axis | Computed | $\mathrm{m} / \mathrm{s}$ |
|  |  |  | $\begin{aligned} & \text { Zdo } \\ & \dagger \end{aligned}$ | Middle right axle velocity along the earth-fixed Zaxis | Computed | m/s |
| RearAxl | Lft | Disp | X | Rear left axle displacement along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Y | Rear left axle displacement along the earth-fixed $Y$-axis | Computed | m |
|  |  |  | Z | Rear left axle displacement along the earth-fixed Z-axis | Computed | m |
|  |  | Vel | $\begin{aligned} & \mathrm{Xdo} \\ & \mathrm{t} \end{aligned}$ | Rear left axle velocity along the earth-fixed $X$ axis | Computed | $\mathrm{m} / \mathrm{s}$ |
|  |  |  | $\begin{aligned} & \mathrm{Ydo} \\ & \mathrm{t} \end{aligned}$ | Rear left axle velocity along the earth-fixed $Y$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \hline \text { Zdo } \\ & \mathrm{t} \end{aligned}$ | Rear left axle velocity along the earth-fixed $Z$ axis | Computed | m/s |
|  | Rght | Disp | X | Rear right axle displacement along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Y | Rear right axle displacement along the earth-fixed $Y$-axis | Computed | m |
|  |  |  | Z | Rear right axle displacement along the earth-fixed $Z$-axis | Computed | m |
|  |  | Vel | $\begin{aligned} & \mathrm{Xdo} \\ & \mathrm{t} \end{aligned}$ | Rear right axle velocity along the earth-fixed $X$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{Ydo} \\ & \mathrm{t} \end{aligned}$ | Rear right axle velocity along the earth-fixed $Y$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{Zdo} \\ & \mathrm{t} \end{aligned}$ | Rear right axle velocity along the earth-fixed Zaxis | Computed | m/s |
| HitchF | Disp | X |  | Trailer front hitch offset from the axle plane along the earth-fixed $X$-axis | Computed | m |


|  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Signal |  | Y | Trailer front hitch offset from the center plane along the earth-fixed $Y$ axis | Computed | m |
|  |  | Z | Trailer front hitch offset from the axle plane along the earth-fixed $Z$-axis | Computed | m |
|  | Vel | Xdot | Trailer front hitch offset velocity along the earthfixed $X$-axis | Computed | m/s |
|  |  | Ydot | Trailer front hitch offset velocity along the earthfixed $Y$-axis | Computed | m/s |
|  |  | Zdot | Trailer front hitch offset velocity along the earthfixed $Z$-axis | Computed | m/s |
| HitchR | Disp | X | Trailer rear hitch offset from the axle plane along the earth-fixed $X$-axis | Computed | m |
|  |  | Y | Trailer rear hitch offset from the center plane along the earth-fixed $Y$ axis | Computed | m |
|  |  | Z | Trailer rear hitch offset from the axle plane along the earth-fixed $Z$-axis | Computed | m |
|  | Vel | Xdot | Hitch velocity along the earth-fixed $X$-axis | Computed | m/s |
|  |  | Ydot | Hitch velocity along the earth-fixed $Y$-axis | Computed | m/s |
|  |  | Zdot | Hitch velocity along the earth-fixed Z-axis | Computed | $\mathrm{m} / \mathrm{s}$ |
| Geom | Disp | X | Trailer offset from the axle plane along the earth-fixed $X$-axis | Computed | m |
|  |  | Y | Trailer offset from the center plane along the earth-fixed $Y$-axis | Computed | m |
|  |  | Z | Trailer offset from the axle plane along the earth-fixed Z-axis | Computed | m |
|  | Vel | Xdot | Trailer offset velocity along the earth-fixed $X$ axis | Computed | m/s |


| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Ydot | Trailer offset velocity along the earth-fixed $Y$ axis | Computed | $\mathrm{m} / \mathrm{s}$ |
|  |  |  | Zdot | Trailer offset velocity along the earth-fixed Zaxis | Computed | $\mathrm{m} / \mathrm{s}$ |
| BdyFrm | Cg | Vel | xdot | Vehicle CM velocity along the vehicle-fixed $x$-axis | Computed | $\mathrm{m} / \mathrm{s}$ |
|  |  |  | ydot | Vehicle CM velocity along the vehicle-fixed $y$-axis | Computed | $\mathrm{m} / \mathrm{s}$ |
|  |  |  | zdot | Vehicle CM velocity along the vehicle-fixed $z$-axis | Computed | $\mathrm{m} / \mathrm{s}$ |
|  |  | AngVel | p | Vehicle angular velocity about the vehicle-fixed $x$ axis (roll rate) | Computed | rad/s |
|  |  |  | q | Vehicle angular velocity about the vehicle-fixed $y$ axis (pitch rate) | Computed | rad/s |
|  |  |  | r | Vehicle angular velocity about the vehicle-fixed $z$ axis (yaw rate) | Computed | rad/s |
|  |  | Acc | ax | Vehicle CM acceleration along the vehicle-fixed $x$ axis | Computed | gn |
|  |  |  | ay | Vehicle CM acceleration along the vehicle-fixed $y$ axis | Computed | gn |
|  |  |  | az | Vehicle CM acceleration along the vehicle-fixed $z$ axis | Computed | gn |
|  |  |  | xddot | Vehicle CM acceleration along the vehicle-fixed $x$ axis | Computed | $\mathrm{m} / \mathrm{s}^{\wedge} 2$ |
|  |  |  | yddot | Vehicle CM acceleration along the vehicle-fixed $y$ axis | Computed | $\mathrm{m} / \mathrm{s}^{\wedge} 2$ |
|  |  |  | zddot | Vehicle CM acceleration along the vehicle-fixed $z$ axis | Computed | $\mathrm{m} / \mathrm{s}^{\wedge} 2$ |
|  |  | DCM | Direction cosine matrix |  | Computed | rad |
|  | Forces | Body | Fx | Net force on the vehicle CM along the vehiclefixed $x$-axis | Computed | N |





| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | R F <br> g x <br> h  <br>   <br>   <br>   | Middle right tire force along the vehicle-fixed $x$ axis | Computed | N |
|  |  |  | $\mathrm{t} \left\lvert\, \begin{aligned} & \mathrm{F} \\ & \mathrm{y} \end{aligned}\right.$ | Middle right tire force along the vehicle-fixed $y$ axis | Computed | N |
|  |  |  | F | Middle right tire force along the vehicle-fixed $z$ axis | Computed | N |
|  |  | $\begin{aligned} & \text { RearTir } \\ & \text { es } \end{aligned}$ |  | Rear left tire force along the vehicle-fixed $x$-axis | Computed | N |
|  |  |  | $\begin{aligned} & \mathrm{t} \\ & \hline \mathrm{~F} \\ & \mathrm{y} \end{aligned}$ | Rear left tire force along the vehicle-fixed $y$-axis | Computed | N |
|  |  |  |  | Rear left tire force along the vehicle-fixed $z$-axis | Computed | N |
|  |  |  |  | Rear right tire force along the vehicle-fixed $x$-axis | Computed | N |
|  |  |  |  | Rear right tire force along the vehicle-fixed $y$-axis | Computed | N |
|  |  |  | $\begin{aligned} & \mathrm{F} \\ & \mathrm{z} \end{aligned}$ | Rear right tire force along the vehicle-fixed $z$-axis | Computed | N |
|  | Drag | FX |  | Drag force on the vehicle CM along the vehiclefixed $x$-axis | Computed | N |
|  |  | Fy |  | Drag force on the vehicle CM along the vehiclefixed $y$-axis | Computed | N |
|  |  | Fz |  | Drag force on the vehicle CM along the vehiclefixed $z$-axis | Computed | N |
|  | Grvty | FX |  | Gravity force on the vehicle CM along the vehicle-fixed $x$-axis | Computed | N |
|  |  | Fy |  | Gravity force on the vehicle CM along the vehicle-fixed $y$-axis | Computed | N |
|  |  | Fz |  | Gravity force on the vehicle CM along the vehicle-fixed $z$-axis | Computed | N |
| Moments | Body | Mx |  | Body moment on the vehicle CM about the vehicle-fixed $x$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |


| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | My |  | Body moment on the vehicle CM about the vehicle-fixed $y$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | Mz |  | Body moment on the vehicle CM about the vehicle-fixed $z$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  | Drag | Mx |  | Drag moment on the vehicle CM about the vehicle-fixed $x$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | My |  | Drag moment on the vehicle CM about the vehicle-fixed $y$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | Mz |  | Drag moment on the vehicle CM about the vehicle-fixed $z$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  | Ext | Mx |  | External moment on the vehicle CG about the vehicle-fixed $x$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | My |  | External moment on the vehicle CG about the vehicle-fixed $y$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | Mz |  | External moment on the vehicle CG about the vehicle-fixed $z$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  | HitchF | Mx |  | Hitch moment at the front hitch location about vehicle-fixed $x$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | My |  | Hitch moment at the front hitch location about vehicle-fixed $y$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | Mz |  | Hitch moment at the front hitch location about vehicle-fixed $z$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  | HitchR | Mx |  | Hitch moment at the rear hitch location about vehicle-fixed $x$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | My |  | Hitch moment at the rear hitch location about vehicle-fixed $y$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | Mz |  | Hitch moment at the rear hitch location about vehicle-fixed $z$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
| FrntAxl | Lft | Disp | x | Front left axle displacement along the vehicle-fixed $x$-axis | Computed | m |


| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | y | Front left axle displacement along the vehicle-fixed $y$-axis | Computed | m |
|  |  |  | z | Front left axle displacement along the vehicle-fixed $z$-axis | Computed | m |
|  |  | Vel | $\begin{aligned} & \mathrm{xdo} \\ & \mathrm{t} \end{aligned}$ | Front left axle velocity along the vehicle-fixed $x$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{ydo} \\ & \mathrm{t} \end{aligned}$ | Front left axle velocity along the vehicle-fixed $y$ axis | Computed | $\mathrm{m} / \mathrm{s}$ |
|  |  |  | $\begin{aligned} & \mathrm{zdo} \\ & \mathrm{t} \end{aligned}$ | Front left axle velocity along the vehicle-fixed $z$ axis | Computed | m/s |
|  | Rght | Disp | x | Front right axle displacement along the vehicle-fixed $x$-axis | Computed | m |
|  |  |  | y | Front right axle displacement along the vehicle-fixed $y$-axis | Computed | m |
|  |  |  | z | Front right axle displacement along the vehicle-fixed $z$-axis | Computed | m |
|  |  | Vel | $\begin{aligned} & \mathrm{xdo} \\ & \mathrm{t} \end{aligned}$ | Front right axle velocity along the vehicle-fixed $x$ axis | Computed | $\mathrm{m} / \mathrm{s}$ |
|  |  |  | $\begin{aligned} & \mathrm{ydo} \\ & \mathrm{t} \end{aligned}$ | Front right axle velocity along the vehicle-fixed $y$ axis | Computed | $\mathrm{m} / \mathrm{s}$ |
|  |  |  | $\begin{aligned} & \mathrm{zdo} \\ & \mathrm{t} \end{aligned}$ | Front right axle velocity along the vehicle-fixed $z$ axis | Computed | $\mathrm{m} / \mathrm{s}$ |
| Midlaxl | Lft | Disp | x | Middle left axle displacement along the vehicle-fixed $x$-axis | Computed | m |
|  |  |  | y | Middle left axle displacement along the vehicle-fixed $y$-axis | Computed | m |
|  |  |  | z | Middle left axle displacement along the vehicle-fixed $z$-axis | Computed | m |
|  |  | Vel | $\begin{aligned} & \mathrm{xdo} \\ & \mathrm{t} \end{aligned}$ | Middle left axle velocity along the vehicle-fixed $x$ axis | Computed | m/s |


|  |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Signal |  |  | $\begin{aligned} & \mathrm{ydo} \\ & \mathrm{t} \end{aligned}$ | Middle left axle velocity along the vehicle-fixed $y$ axis | Computed | $\mathrm{m} / \mathrm{s}$ |
|  |  |  | $\begin{aligned} & \mathrm{zdo} \\ & \mathrm{t} \end{aligned}$ | Middle left axle velocity along the vehicle-fixed $z$ axis | Computed | m/s |
|  | Rght | Disp | x | Middle right axle displacement along the vehicle-fixed $x$-axis | Computed | m |
|  |  |  | y | Middle right axle displacement along the vehicle-fixed $y$-axis | Computed | m |
|  |  |  | z | Middle right axle displacement along the vehicle-fixed $z$-axis | Computed | m |
|  |  | Vel | $\begin{aligned} & \mathrm{xdo} \\ & \mathrm{t} \end{aligned}$ | Middle right axle velocity along the vehicle-fixed $x$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{ydo} \\ & \mathrm{t} \end{aligned}$ | Middle right axle velocity along the vehicle-fixed $y$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{zdo} \\ & \mathrm{t} \end{aligned}$ | Middle right axle velocity along the vehicle-fixed $z$ axis | Computed | m/s |
| RearAxl | Lft | Disp | x | Rear left axle displacement along the vehicle-fixed $x$-axis | Computed | m |
|  |  |  | y | Rear left axle displacement along the vehicle-fixed $y$-axis | Computed | m |
|  |  |  | z | Rear left axle displacement along the vehicle-fixed $z$-axis | Computed | m |
|  |  | Vel | $\begin{aligned} & \mathrm{xdo} \\ & \mathrm{t} \end{aligned}$ | Rear left axle velocity along the vehicle-fixed $x$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{ydo} \\ & \mathrm{t} \end{aligned}$ | Rear left axle velocity along the vehicle-fixed $y$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{zdo} \\ & \mathrm{t} \end{aligned}$ | Rear left axle velocity along the vehicle-fixed $z$ axis | Computed | m/s |
|  | Rght | Disp | X | Rear right axle displacement along the vehicle-fixed $x$-axis | Computed | m |



$\mathbf{V b}$ - Vehicle velocity along vehicle-fixed frame

## vector

Vehicle CM velocity along the vehicle-fixed $x$-, $y$-, $z$-axes, respectively, in $m / s$, returned as a vector.
pqr - Vehicle angular velocity about vehicle-fixed frame
vector
Vehicle CM angular velocity about the vehicle-fixed $x$-(roll rate), $y$-(pitch rate), $z$-axes (yaw rate), respectively, in rad/s, returned as a vector.

DCM - Direction cosine matrix
array
Direction cosine matrix, in rad, returned as an array.

## Euler - Euler angles

array
Euler angles, $\varphi, \theta$, and $\psi$, respectively, in rad, returned as an array.
$\mathbf{X e}$ - Vehicle position in inertial reference frame vector

Vehicle CM position along inertial-fixed $X-, Y-, Z$-axes, respectively, in m, returned as a vector.
Ve - Vehicle velocity in inertial reference frame vector

Vehicle CM velocity along inertial-fixed $X$-, $Y$-, $Z$-axes, respectively, in $\mathrm{m} / \mathrm{s}$, returned as a vector.

## Parameters

## Block Options

Number of axles - Create hitch force input port
2 (default) | 1 | 3
Specify the number of axles on the trailer.
Input Signals
Front hitch forces - FhF input port
on (default) | off
Select to create input port Fh.
Front hitch moments - MhF input port
on (default) | off
Select to create input port Mh.
Rear hitch forces - FhR input port
off (default) | on
Select to create input port Fh.
Rear hitch moments - MhR input port
off (default) | on
Select to create input port Mh.

## Chassis

Vehicle mass, m - Mass
2000 (default) | scalar
Vehicle mass, $m$, in kg.
Longitudinal distance from center of mass to front axle, a - Distance from center of mass to front axle
1.4 (default) | scalar

Distance from the vehicle CM to the front axle, $a$, in $m$.


Longitudinal distance from center of mass to middle axle, b-Distance from center of mass to middle axle
1.6 (default) | scalar

Distance from the vehicle CM to the middle axle, $b$, in $m$.


Dependencies
To enable this parameter, set Number of axles to 3.
Longitudinal distance from center of mass to rear axle, c-Distance from center of mass to rear axle
1.9 (default) | scalar

Distance from the vehicle CM to the rear axle, $c$, in $m$.


## Dependencies

To enable this parameter, set Number of axles to 2 or 3.
Lateral distance from geometric centerline to center of mass, $\mathbf{d}$ - Distance from geometric centerline to center of mass
0 (default) | scalar
Lateral distance from the geometric centerline to the CM, $d$, in $m$, along the vehicle-fixed $y$-axis. Positive values indicate that the vehicle CM is to the right of the geometric centerline. Negative values indicate that the vehicle CM is to the left of the geometric centerline.


Vertical distance from center of mass to axle plane, $\mathbf{h}$ - Distance from center of mass to axle plane
. 35 (default) | scalar
Vertical distance from the vehicle CM to the axle plane, $h$, in $m$.


Longitudinal distance from center of mass to front hitch, $\mathbf{d h} \mathbf{f}$ - Longitudinal distance from CM to hitch
1 (default) | scalar

Longitudinal distance from center of mass to front hitch, $d h f$, in $m$.


## Dependencies

To enable this parameter, on the Input signals pane, select Front hitch forces or Front hitch moments.

Lateral distance from geometric centerline to front hitch, hl_f - Distance from centerline to front hitch
0 (default) | scalar
Lateral distance from the geometric centerline to the front hitch, hlf, in $m$, along the vehicle-fixed $y$. Positive values indicate that the trailer hitch is to the right of the geometric centerline. Negative values indicate that the trailer hitch is to the left of the geometric centerline.


## Dependencies

To enable this parameter, on the Input signals pane, select Front hitch forces or Front hitch moments.

Vertical distance from front hitch to axle plane, $\mathbf{h h}_{\mathbf{f}} \mathbf{f}$ - Distance from front hitch to axle plane 0.1 (default) | scalar

Vertical distance from front hitch to axle plane, $h h f$, in $m$.


## Dependencies

To enable this parameter, on the Input signals pane, select Front hitch forces or Front hitch moments.

Longitudinal distance from center of mass to rear hitch, $\mathbf{d h} \mathbf{r}$ - Distance to front hitch 1 (default) | scalar

Longitudinal distance from the center of mass to the rear hitch, $d h_{-} r$, in $m$.


## Dependencies

To enable this parameter, on the Input signals pane, select Rear hitch forces or Rear hitch moments.

Lateral distance from geometric centerline to rear hitch, hl_r - Distance from centerline to rear hitch
0 (default) | scalar
Lateral distance from the geometric centerline to the rear hitch, $h l_{-} r$, in $m$, along the vehicle-fixed $y$. Positive values indicate that the trailer hitch is to the right of the geometric centerline. Negative values indicate that the trailer hitch is to the left of the geometric centerline.


## Dependencies

To enable this parameter, on the Input signals pane, select Rear hitch forces or Rear hitch moments.

Vertical distance from rear hitch to axle plane, $\mathbf{h h} \mathbf{r} \mathbf{r}$ - Distance from rear hitch to axle plane 0.1 (default) | scalar

Vertical distance from the rear hitch to the axle plane, $h h_{-} r$, in $m$.


## Dependencies

To enable this parameter, on the Input signals pane, select Rear hitch forces or Rear hitch moments.

Initial position in the inertial frame [Xeo,Yeo,Zeo], Xe_o - Initial position
[0,0,0] (default) | vector
Initial position of the vehicle in the inertial frame, $X e_{0}$, in $m$.
Initial velocity in body axes [xdot_o,ydot_o,zdot_o], xbdot_o - Initial velocity [0,0,0] (default) | vector

Initial vehicle CM velocity along the vehicle-fixed $x, y$-, and $z$-axes, respectively, in $\mathrm{m} / \mathrm{s}$.
Initial Euler orientation [roll, pitch, yaw], eul_o - Rotation
[0,0,0] (default) | vector
Initial Euler rotation of the vehicle-fixed frame about the earth-fixed $X$ - (roll), $Y$ - (pitch), $Z$-axes (yaw), respectively, in rad.

Initial body rotation rates [p,q,r], p_o - Initial rotation rate
[0,0,0] (default) | vector
Initial vehicle CM angular velocity about the vehicle-fixed $x$ - (roll rate), $y$ - (pitch rate), $z$-axes (yaw rate), respectively, in rad/s.

## Chassis inertia tensor, Iveh - Inertia

[430 0 0; 0 1900 0; 00 2100] (default)|array
Vehicle inertia tensor, $I_{\text {veh }}$, in $\mathrm{kg}^{*} \mathrm{~m}^{\wedge} 2$. Dimensions are [3-by-3].
Front track width, w_f - Front track width
1.9 (default) | scalar

Front track width, in m.


Middle track width, w_m - Middle track width
1.9 (default) | scalar

Middle track width, in m.


## Dependencies

To enable this parameter, set Number of axles to 3 .
Rear track width, w_r - Rear track width
1.9 (default) | scalar

Rear track width, in m.


## Dependencies

To enable this parameter, set Number of axles to 2 or 3.

## Inertial Loads

## Front End

Mass, z1m - Mass
0 (default) | scalar
Mass, $z 1 \mathrm{~m}$, in kg.

Distance vector from front axle, z1R - Distance
[-.25,.125,.15] (default)| vector
Distance vector from front axle to load, $z 1 R$, in $m$. Dimensions are 1-by-3.

| Array Element | Description |
| :--- | :--- |
| $z 1 R(1,1)$ | Front suspension hardpoint to load, along vehicle- <br> fixed $x$-axis |
| $z 1 R(1,2)$ | Vehicle centerline to load, along vehicle-fixed $y$-axis |
| $z 1 R(1,3)$ | Front suspension hardpoint to load, along vehicle- <br> fixed $z$-axis |

For example, this table summarizes the parameter settings that specify the load location.

| Example Location | Sign |
| :--- | :--- |
| - | Forward of the front axle |
| - | Right of the vehicle centerline |
| - | Above the front axle suspension hardpoint |

## Inertia tensor, z1I - Inertia

[1.4,-.2,.1;-.2,1.4,.1;.1,.1,2.25].*0 (default)|array
Inertia tensor, $z 1 I$, in $\mathrm{kg} \cdot \mathrm{m} \wedge 2$. Dimensions are [3-by-3].

$$
z 1 I=\left[\begin{array}{lll}
I_{x x} & I_{x y} & I_{x z} \\
I_{y x} & I_{y y} & I_{y z} \\
I_{z x} & I_{z y} & I_{z z}
\end{array}\right]
$$

The tensor uses a coordinate system with an origin at the load CM.

- $x$-axis along the vehicle-fixed $x$-axis
- $y$-axis along the vehicle-fixed $y$-axis
- $z$-axis along the vehicle-fixed $z$-axis


## Overhead

Mass, z2m - Mass
0 (default) | scalar
Mass, $z 2 \mathrm{~m}$, in kg.
Distance vector from front axle, z2R - Distance
[1.4,0, .8] (default) | vector
Distance vector from front axle to load, $z 2 R$, in m. Dimensions are 1-by-3.

| Array Element | Description |
| :--- | :--- |
| $z 2 R(1,1)$ | Front suspension hardpoint to load, along vehicle- <br> fixed $x$-axis |


| Array Element | Description |
| :--- | :--- |
| $z 2 R(1,2)$ | Vehicle centerline to load, along vehicle-fixed $y$-axis |
| $z 2 R(1,3)$ | Front suspension hardpoint to load, along vehicle- <br> fixed $z$-axis |

For example, this table summarizes the parameter settings that specify the load location.

| Example Location | Sign |
| :--- | :--- |
| - Rear of the front axle | - z2R $(1,1)>0$ |
| - Left of the vehicle centerline | - z2R $(1,2)<0$ |
| - Above the front axle suspension hardpoint | - z2R $(1,3)>0$ |

Inertia tensor, z21 - Inertia
[1.4,-.2,.1;-.2,1.4,.1;.1,.1,2.25].*0 (default)|array
Inertia tensor, $z 2 I$, in $\mathrm{kg} \cdot \mathrm{m}^{\wedge} 2$. Dimensions are [3-by-3].

$$
z 2 I=\left[\begin{array}{lll}
I_{x x} & I_{x y} & I_{x z} \\
I_{y x} & I_{y y} & I_{y z} \\
I_{z x} & I_{z y} & I_{z z}
\end{array}\right]
$$

The tensor uses a coordinate system with an origin at the load CM.

- $x$-axis along the vehicle-fixed $x$-axis
- $y$-axis along the vehicle-fixed $y$-axis
- $z$-axis along the vehicle-fixed $z$-axis


## Front Left

Mass, z3m - Mass
0 (default) | scalar
Mass, $z 3 m$, in kg.
Distance vector from front axle, z3R - Distance
[.75,-.5,.4] (default)| vector
Distance vector from front axle to load, $z 3 R$, in m. Dimensions are 1-by-3.

| Array Element | Description |
| :--- | :--- |
| $\operatorname{z3R}(1,1)$ | Front suspension hardpoint to load, along vehicle- <br> fixed $x$-axis |
| $\operatorname{z3R}(1,2)$ | Vehicle centerline to load, along vehicle-fixed $y$-axis |
| $\operatorname{z3R}(1,3)$ | Front suspension hardpoint to load, along vehicle- <br> fixed $z$-axis |

For example, this table summarizes the parameter settings that specify the load location.

| Example Location | Sign |
| :--- | :--- |
| - Rear of the front axle | - $z 3 R(1,1)>0$ |
| - Left of the vehicle centerline | - $z 3 R(1,2)<0$ |
| - Above the front axle suspension hardpoint | - $z 3 R(1,3)>0$ |

Inertia tensor, z3I - Inertia
[5,-.1,-2;-2,9,.1;-.1,.1,6].*0 (default)|array
Inertia tensor, $z 3 I$, in $\mathrm{kg} \cdot \mathrm{m} \wedge 2$. Dimensions are [3-by-3].

$$
z 3 I=\left[\begin{array}{lll}
I_{x x} & I_{x y} & I_{x z} \\
I_{y x} & I_{y y} & I_{y z} \\
I_{z x} & I_{z y} & I_{z z}
\end{array}\right]
$$

The tensor uses a coordinate system with an origin at the load CM.

- $x$-axis along the vehicle-fixed $x$-axis
- $y$-axis along the vehicle-fixed $y$-axis
- $z$-axis along the vehicle-fixed $z$-axis


## Front Right

Mass, $\mathbf{z 4 m}$ - Mass
0 (default) | scalar
Mass, $z 4 m$, in kg.
Distance vector from front axle, $\mathbf{z 4 R}$ - Distance
[.75, .5,.4] (default) | vector
Distance vector from front axle to load, $z 4 R$, in m. Dimensions are 1-by-3.

| Array Element | Description |
| :--- | :--- |
| z4R $(1,1)$ | Front suspension hardpoint to load, along vehicle- <br> fixed $x$-axis |
| z4R $(1,2)$ | Vehicle centerline to load, along vehicle-fixed $y$-axis |
| Z4R $(1,3)$ | Front suspension hardpoint to load, along vehicle- <br> fixed $z$-axis |

For example, this table summarizes the parameter settings that specify the load location.

| Example Location | Sign |
| :--- | :--- |
| - $\quad$ Rear of the front axle | - $z 4 R(1,1)>0$ |
| - Right of the vehicle centerline | - $z 4 R(1,2)>0$ |
| - Above the front axle suspension hardpoint | - $\quad \mathrm{z4R}(1,3)>0$ |

Inertia tensor, $\mathbf{z 4 I}$ - Inertia
[5,-.1,-2;-2, 9,.1;-.1,.1,6].*0 (default)| array
Inertia tensor, $z 4 I$, in $\mathrm{kg} \cdot \mathrm{m}^{\wedge} 2$. Dimensions are [3-by-3].

$$
z 4 I=\left[\begin{array}{lll}
I_{x x} & I_{x y} & I_{x z} \\
I_{y x} & I_{y y} & I_{y z} \\
I_{z x} & I_{z y} & I_{z z}
\end{array}\right]
$$

The tensor uses a coordinate system with an origin at the load CM.

- $x$-axis along the vehicle-fixed $x$-axis
- $y$-axis along the vehicle-fixed $y$-axis
- $z$-axis along the vehicle-fixed $z$-axis


## Rear Left

Mass, z5m - Mass
0 (default) | scalar
Mass, z5m, in kg.
Distance vector from front axle, z5R - Distance
[1.25, -. 5, .4] (default) | vector
Distance vector from front axle to load, $z 5 R$, in m. Dimensions are 1-by-3.

| Array Element | Description |
| :--- | :--- |
| z5R $(1,1)$ | Front suspension hardpoint to load, along vehicle- <br> fixed $x$-axis |
| z5R $(1,2)$ | Vehicle centerline to load, along vehicle-fixed $y$-axis |
| z5R $(1,3)$ | Front suspension hardpoint to load, along vehicle- <br> fixed $z$-axis |

For example, this table summarizes the parameter settings that specify the load location.

| Example Location | Sign |
| :---: | :---: |
| - Rear of the front axle | - $\mathrm{z5R}(1,1)>0$ |
| - Left of the vehicle centerline | - $\mathrm{z5R}(1,2)<0$ |
| - Above the front axle suspension hardpoint | - $\mathrm{z} 5 \mathrm{R}(1,3)>0$ |

Inertia tensor, $\mathbf{z 5 I}$ - Inertia
[5,-.1,-2;-2, 9,.1;-.1,.1,6].*0 (default)|array
Inertia tensor, $z 5 I$, in $\mathrm{kg} \cdot \mathrm{m}^{\wedge} 2$. Dimensions are [3-by-3].

$$
z 5 I=\left[\begin{array}{lll}
I_{x x} & I_{x y} & I_{x z} \\
I_{y x} & I_{y y} & I_{y z} \\
I_{z x} & I_{z y} & I_{z z}
\end{array}\right]
$$

The tensor uses a coordinate system with an origin at the load CM.

- $x$-axis along the vehicle-fixed $x$-axis
- $y$-axis along the vehicle-fixed $y$-axis
- $z$-axis along the vehicle-fixed $z$-axis


## Rear Right

Mass, $\mathbf{2 6 m}$ - Mass
0 (default) | scalar
Mass, $z 6 \mathrm{~m}$, in kg.
Distance vector from front axle, z6R - Distance
[1.25,-.5,.4] (default) | vector
Distance vector from front axle to load, $z 6 R$, in m. Dimensions are 1-by-3.

| Array Element | Description |
| :--- | :--- |
| $z 6 R(1,1)$ | Front suspension hardpoint to load, along vehicle- <br> fixed $x$-axis |
| $z 6 R(1,2)$ | Vehicle centerline to load, along vehicle-fixed $y$-axis |
| $z 6 R(1,3)$ | Front suspension hardpoint to load, along vehicle- <br> fixed $z$-axis |

For example, this table summarizes the parameter settings that specify the load location.

| Example Location | Sign |
| :--- | :--- |
| - $\quad$ Rear of the front axle | - $\mathrm{z} 6 \mathrm{R}(1,1)>0$ |
| - | Right of the vehicle centerline |
| - | Above the front axle suspension hardpoint |

Inertia tensor, z6I - Inertia
[5,-.1,-2;-2,9,.1;-.1,.1,6].*0 (default)|array
Inertia tensor, $z 6 I$, in $\mathrm{kg} \cdot \mathrm{m}^{\wedge} 2$. Dimensions are [3-by-3].

$$
z 6 I=\left[\begin{array}{lll}
I_{x x} & I_{x y} & I_{x z} \\
I_{y x} & I_{y y} & I_{y z} \\
I_{z x} & I_{z y} & I_{z z}
\end{array}\right]
$$

The tensor uses a coordinate system with an origin at the load CM.

- $x$-axis along the vehicle-fixed $x$-axis
- $y$-axis along the vehicle-fixed $y$-axis
- $z$-axis along the vehicle-fixed $z$-axis


## Rear End

Mass, $\mathbf{z 7 m}$ - Mass
0 (default) | scalar
Mass, $z 7 \mathrm{~m}$, in kg.
Distance vector from front axle, z7R - Distance
[2,0,.25] (default) | vector

Distance vector from front axle to load, $z 7 R$, in m. Dimensions are 1-by-3.

| Array Element | Description |
| :--- | :--- |
| z7R $(1,1)$ | Front suspension hardpoint to load, along vehicle- <br> fixed $x$-axis |
| z7R $(1,2)$ | Vehicle centerline to load, along vehicle-fixed $y$-axis |
| z7R $(1,3)$ | Front suspension hardpoint to load, along vehicle- <br> fixed $z$-axis |

For example, this table summarizes the parameter settings that specify the load location.

| Example Location | Sign |
| :--- | :--- |
| • Rear of the front axle | • $\quad$ 77R $(1,1)>0$ |
| - Right of the vehicle centerline | • z7R $(1,2)>0$ |
| - Above the front axle suspension hardpoint | • $\quad \mathrm{z7R}(1,3)>0$ |

## Inertia tensor, z71 - Inertia

[1.4,-.2,.1;-.2,1.4,.1;.1,.1,2.25].*0 (default)|array
Inertia tensor, $z 7 \mathrm{I}$, in $\mathrm{kg} \cdot \mathrm{m} \wedge$ 2. Dimensions are [3-by-3].

$$
z 7 I=\left[\begin{array}{lll}
I_{x x} & I_{x y} & I_{x z} \\
I_{y x} & I_{y y} & I_{y z} \\
I_{z x} & I_{z y} & I_{z z}
\end{array}\right]
$$

The tensor uses a coordinate system with an origin at the load CM.

- $x$-axis along the vehicle-fixed $x$-axis
- $y$-axis along the vehicle-fixed $y$-axis
- $z$-axis along the vehicle-fixed $z$-axis


## Aerodynamic

Longitudinal drag area, Af - Drag area
2 (default) | scalar
Effective vehicle cross-sectional area, $A_{f}$ to calculate the aerodynamic drag force on the vehicle, in $\mathrm{m}^{\wedge} 2$.

Longitudinal drag coefficient, Cd - Drag coefficient
. 3 (default) | scalar
Air drag coefficient, $C_{d}$, dimensionless.
Longitudinal lift coefficient, CI - Lift
. 1 (default) | scalar
Air lift coefficient, $C_{l}$, dimensionless.
Longitudinal drag pitch moment, Cpm - Pitch drag
. 1 (default) | scalar

Longitudinal drag pitch moment coefficient, $C_{p m}$, dimensionless.
Relative wind angle vector, beta_w - Wind angle
[0:0.001:0.01] (default) | vector
Relative wind angle vector, $\beta_{w}$, in rad.
Side force coefficient vector, Cs - Side force drag
[0:0.01:0.1] (default) |vector
Side force coefficient vector coefficient, $C_{s}$, dimensionless.
Yaw moment coefficient vector, Cym - Yaw moment drag
[0:0.001:0.01] (default) | vector
Yaw moment coefficient vector coefficient, $C_{y m}$, dimensionless.

## Environment

Absolute air pressure, Pabs - Pressure
101325 (default) | scalar
Environmental air absolute pressure, $P_{a b s}$, in Pa .
Air temperature, Tair - Ambient air temperature
273 (default) | scalar
Ambient air temperature, $T_{\text {air }}$, in K .

## Dependencies

To enable this parameter, clear Air temperature.
Gravitational acceleration, g-Gravity
9.81 (default) | scalar

Gravitational acceleration, $g$, in $\mathrm{m} / \mathrm{s}^{\wedge} 2$.

## Simulation

## Longitudinal velocity tolerance, xdot_tol - Tolerance

. 1 (default) | scalar
Longitudinal velocity tolerance, $x d o t_{\text {tol }}$, in $\mathrm{m} / \mathrm{s}$.
The block uses this parameter to avoid a division by zero when it calculates the body slip angle, $\beta$.
Geometric longitudinal offset from axle plane, longOff - Longitudinal offset
0 (default) | scalar
Trailer offset from axle plane along body-fixed $x$-axis, in $m$. When you use the 3D visualization engine, consider using the offset to locate the chassis independently of the vehicle CG.

Geometric lateral offset from center plane, latOff - Lateral offset
0 (default) | scalar

Trailer offset from center plane along body-fixed $y$-axis, in $m$. When you use the 3D visualization engine, consider using the offset to locate the chassis independently of the vehicle CG.

Geometric vertical offset from axle plane, vertOff - Vertical offset
0 (default) | scalar
Trailer offset from axle plane along body-fixed $z$-axis, in $m$. When you use the 3D visualization engine, consider using the offset to locate the chassis independently of the vehicle CG.

Wrap Euler angles, wrapAng - Selection
on (default) | off
Wrap the Euler angles to the interval [-pi, pi]. For vehicle maneuvers that might undergo vehicle yaw rotations that are outside of the interval, consider clearing the parameter if you want to:

- Track the total vehicle yaw rotation.
- Avoid discontinuities in the vehicle state estimators.


## Version History

Introduced in R2020b

## References

[1] Gillespie, Thomas. Fundamentals of Vehicle Dynamics. Warrendale, PA: Society of Automotive Engineers (SAE), 1992.

## Extended Capabilities

$\mathbf{C} / \mathbf{C + +}$ Code Generation
Generate C and $\mathrm{C}++$ code using Simulink ${ }^{\circledR}$ Coder $^{\mathrm{TM}}$.

## See Also

Vehicle Body 3DOF Longitudinal | Vehicle Body 6DOF | Trailer Body 3DOF

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"

## Vehicle Body 3DOF Three Axles

Three-axle vehicle body with longitudinal, lateral, and yaw motion


## Libraries:

Vehicle Dynamics Blockset / Vehicle Body

## Description

The Vehicle Body 3DOF Three Axles block implements a rigid, three-axle vehicle body model to calculate longitudinal, lateral, and yaw motion. The block accounts for the axle and hitch reaction forces due to the vehicle body mass acceleration, aerodynamic drag, and steering.

Use this block in vehicle dynamics and automated driving studies to model nonholonomic vehicle motion when vehicle pitch, roll, and vertical motion are not significant.

Use the Vehicle track parameter to specify the number of wheels.

| Vehicle Track Setting | Implementation |
| :--- | :--- |
| Single (bicycle) | - Forces act along the center line of the axles. <br>  <br>  <br> - No lateral load transfer. |
| Dual | Forces act at the axle hard-point locations. |

Use the Axle forces parameter to specify the type of force.

| Axle Forces Setting | Implementation |
| :---: | :---: |
| External longitudinal velocity | - The block assumes that the external longitudinal velocity is in a quasi-steady state, so the longitudinal acceleration is approximately zero. <br> - Because the motion is quasi-steady, the block calculates lateral forces using the tire slip angles and linear cornering stiffness. <br> - Consider this setting when you want to: <br> - Generate virtual sensor signal data. <br> - Conduct high-level software studies that are not impacted by driveline or nonlinear tire responses. |


| Axle Forces Setting | Implementation |
| :---: | :---: |
| External longitudinal forces | - The block uses the external longitudinal force to accelerate or brake the vehicle. <br> - The block calculates lateral forces using the tire slip angles and linear cornering stiffness. <br> - Consider this setting when you want to: <br> - Account for changes in the longitudinal velocity on the lateral and yaw motion. <br> - Specify the external longitudinal motion through a force instead of an external longitudinal velocity. <br> - Connect the block to tractive actuators, wheels, brakes, and hitches. |
| External forces | - The block uses the external lateral and longitudinal forces to steer, accelerate, or brake the vehicle. <br> - The block does not use the steering input to calculate vehicle motion. <br> - Consider this setting when you need tire models with more accurate nonlinear combined lateral and longitudinal slip. |

To create additional input ports, under Input signals, select these block parameters.

| Input Signals Pane <br> Parameter | Input Port | Description |
| :--- | :--- | :--- |
| Front wheel steering | WhlAngF | Front wheel angle, $\delta_{F}$ |
| Middle wheel steering | WhlAngM | Middle wheel angle, $\delta_{M}$ |
| Rear wheel steering | WhlAngR | Rear wheel angle, $\delta_{R}$ |
| External wind | WindXYZ | Wind speed, $W_{X}, W_{Y}$, and $W_{Z}$, in an inertial reference frame |
| External friction | Mu | Friction coefficient |
| External forces | FExt | External force on the vehicle center of gravity (CG), $F_{x}, F_{y}$, <br> and $F_{z}$, in the vehicle-fixed frame |
| External moments | MExt | External moment about the vehicle CG, $M_{x}, M_{y}$, and $M_{z}$, in <br> the vehicle-fixed frame |
| Front hitch forces | FhF | Hitch force applied to the body at the front hitch location, <br> $F h F_{x}, F h F_{y}$, and $F h F_{z}$, in the vehicle-fixed frame |
| Front hitch moments | MhF | Hitch moment at the front hitch location, MhF $F_{x}, M h F_{y}$, and <br> $M h F_{z}$, about the vehicle-fixed frame |
| Rear hitch forces | FhR | Hitch force applied to the body at the rear hitch location, <br> $F h R_{x}, F h R_{y}$, and $F h R_{z}$, in the vehicle-fixed frame |
| Rear hitch moments | MhR | Hitch moment at the rear hitch location, $M h R_{x}, M h R_{y}$, and <br> $M h R_{z}$, about the vehicle-fixed frame |
| Initial longitudinal <br> position | X_o | Initial vehicle CG displacement along the earth-fixed $X$-axis |


| Input Signals Pane <br> Parameter | Input Port | Description |
| :--- | :--- | :--- |
| Initial yaw angle | psi_o | Initial rotation of the vehicle-fixed frame about the earth- <br> fixed $Z$-axis (yaw) |
| Initial longitudinal <br> velocity | xdot_o | Initial vehicle CG velocity along the vehicle-fixed $x$-axis |
| Initial yaw rate | r_o | Initial vehicle angular velocity about the vehicle-fixed $z$ - <br> axis (yaw rate) |
| Initial lateral position | Y_o | Initial vehicle CG displacement along the earth-fixed $Y$-axis |
| Air temperature | AirTemp | Ambient air temperature. Consider this option if you want <br> to vary the temperature during run time. |
| Initial lateral velocity | ydot_o | Initial vehicle CG velocity along the vehicle-fixed $y$-axis |

## Theory

To determine the vehicle motion, the block solves the rigid body planar dynamics equations of motion.

| Calculation | Description |
| :--- | :--- |
| Dynamics | The block solves the rigid-body planar dynamics equations to determine the <br> vehicle longitudinal motion. If you set Axle forces to External <br> longitudinal velocity, the block assumes a quasi-steady state for the <br> longitudinal acceleration. |
| External forces | External forces include both drag and external force inputs. The forces act <br> on the vehicle CG. <br> The block divides the normal forces by the nominal normal load to vary the <br> effective friction parameters during weight and load transfer. The block <br> maintains pitch and roll equilibrium. |
| Tire forces | The block uses the ratio of the local, longitudinal, and lateral velocities to <br> determine the slip angles. |
| The block uses the steering angles to transform the tire forces to the vehicle- <br> fixed frame. <br> If you set Axle forces to External forces, the block assumes that the <br> externally provided forces are in the vehicle-fixed frame at the axle-wheel <br> location. |  |

## Single Track



## Dual Track



The illustrations use these variables.

| $a, b, c$ | Longitudinal distance of the front, middle, and rear axles, respectively, from the <br> normal projection point of the vehicle CG onto the common axle plane |
| :--- | :--- |
| $h$ | Height of vehicle CG above the axle plane along the vehicle-fixed $z$-axis |
| $d$ | Lateral distance from geometric centerline to center of mass along the vehicle- <br> fixed $y$-axis |
| $h h$ | Height of the hitch above the axle plane along the vehicle-fixed $z$-axis |
| $d h$ | Longitudinal distance of the hitch from normal projection point of the vehicle CG <br> onto the common axle plane |
| $h l$ | Lateral distance from center of mass to hitch along the vehicle-fixed $y$-axis. |
| $w f, w m, w r$ | Front, middle, and rear track width, respectively |

## Drag

This table summarizes the block implementation for the drag calculation.

| Calculation | Description |
| :--- | :--- |
| Coordinate <br> transformation | The block transforms the wind speeds from the inertial frame to the vehicle- <br> fixed frame. |


| Calculation | Description |
| :--- | :--- |
| Drag forces | To determine a relative airspeed, the block subtracts the wind speed from <br> the CG vehicle velocity. Using the relative airspeed, the block determines the <br> drag forces. |
| Drag moments | Using the relative airspeed, the block determines the drag moments. |

## Lateral Corner Stiffness and Relaxation Dynamics

To enable the mapped corner stiffness and relaxation length dynamic parameters, set Axle forces to External longitudinal force or External longitudinal velocity.

| Parameter Settings | Description |  |
| :--- | :--- | :--- |
| Mapped Corner <br> Stiffness | Include Relaxation <br> Length Dynamics |  |
| Off (default) | On (default) | The block uses constant corner stiffness values. <br> The slip angles include the relaxation length dynamic <br> settings. The relaxation length approximates an <br> effective corner stiffness force that is a function of <br> wheel travel. |
| On | On (default) | The block uses lookup tables that are functions of the <br> corner stiffness data and slip angles. <br> The slip angles include the relaxation length dynamic |
| settings. The relaxation length approximates an |  |  |
| effective corner stiffness force that is a function of |  |  |
| wheel travel. |  |  |

## Ports

## Input

WhIAngF - Front wheel steering angles
scalar|array
Front wheel steering angles, $\delta_{F}$, in rad.

| Vehicle Track Setting | Variable | Signal Dimension |
| :--- | :--- | :--- |
| Single (bicycle) | $\delta_{F}$ | Scalar - 1 |
| Dual | $\delta_{F}=\left[\delta_{f l} \delta_{f r}\right]$ or $\left[\begin{array}{l}\delta_{f l} \\ \delta_{f r}\end{array}\right]$ | Array - [1x2] or [2x1] |

## Dependencies

To enable this port, on the Input signals pane, select Front wheel steering.
WhIAngM - Middle wheel steering angles
scalar|array

Middle wheel steering angles, $\delta_{M}$, in rad.

| Vehicle Track Setting | Variable | Signal Dimension |
| :--- | :--- | :--- |
| Single (bicycle) | $\delta_{M}$ | Scalar - 1 |
| Dual | $\delta_{M}=\left[\delta_{m l} \delta_{m r}\right]$ or $\left[\begin{array}{l}\delta_{m l} \\ \delta_{m r}\end{array}\right]$ | Array - [1×2] or [2×1] |

## Dependencies

To enable this port, on the Input signals pane, select Middle wheel steering.
WhIAngR - Rear wheel steering angles
scalar|array
Rear wheel steering angles, $\delta_{R}$, in rad.

| Vehicle Track Setting | Variable | Signal Dimension |
| :--- | :--- | :--- |
| Single (bicycle) | $\delta_{R}$ | Scalar - 1 |
| Dual | $\delta_{R}=\left[\delta_{r l} \delta_{r r}\right]$ or $\left[\begin{array}{l}\delta_{r l} \\ \delta_{r r}\end{array}\right]$ | Array - [1×2] or [2x1] |

## Dependencies

To enable this port, on the Input signals pane, select Rear wheel steering.
xdotin - Longitudinal velocity
scalar
Vehicle CG velocity along the vehicle-fixed $x$-axis, in $m / s$.

## Dependencies

To enable this port, set Axle forces to External longitudinal velocity.
FwF - Total force on the front wheels
scalar|array
Force on the front wheels, $F w_{F}$, along the vehicle-fixed axis, in N .

| Vehicle <br> Track <br> Setting | Axle Forces <br> Setting | Description | Variable | Signal <br> Dimension |
| :--- | :--- | :--- | :--- | :--- |
| Single <br> (bicycle) | External <br> longitudinal <br> forces | Longitudinal <br> force on the <br> front wheel | $F w F=F x_{f}$ | Scalar -1 |
|  | External <br> forces | Longitudinal and <br> lateral forces on <br> the front wheel | $F w F=\left[F x_{f} F y_{f}\right]$ or $\left[\begin{array}{ll}F x_{f} \\ F y_{f}\end{array}\right]$ | Array - [1x2] or <br> $[2 \times 1]$ |


| Vehicle Track Setting | Axle Forces Setting | Description | Variable | Signal Dimension |
| :---: | :---: | :---: | :---: | :---: |
| Dual | External longitudinal forces | Longitudinal force on the front wheels | $F w F=\left[\begin{array}{l} F_{x f l} \\ F_{x f r} \end{array}\right] \text { or }\left[\begin{array}{l} F_{x f l} \\ F_{x f r} \end{array}\right.$ | $\begin{aligned} & \text { Array }-[1 \times 2] \text { or } \\ & {[2 \times 1]} \end{aligned}$ |
|  | External forces | Longitudinal and lateral forces on the front wheels | $F w F=\left[\begin{array}{lll}F_{x f l} & F_{x f r} \\ F_{y f l} & F_{y f r}\end{array}\right]$ | Array - [2x2] |

## Dependencies

To enable this port, set Axle forces to one of these options:

- External longitudinal forces
- External forces

FwM - Total force on the middle wheels
scalar|array
Force on the middle wheels, $F w_{M}$, along the vehicle-fixed axis, in N.

| Vehicle <br> Track <br> Setting | Axle Forces Setting | Description | Variable | Signal Dimension |
| :---: | :---: | :---: | :---: | :---: |
| Single (bicycle) | External longitudinal forces | Longitudinal force on the middle wheel | $F w M=F \chi_{r}$ | Scalar - 1 |
|  | External forces | Longitudinal and lateral forces on the middle wheel | $F w M=\left[\begin{array}{lll}F x_{m} & F y_{m}\end{array}\right]$ or $\left[\begin{array}{l} F x_{m} \\ F y_{m} \end{array}\right]$ | $\begin{aligned} & \text { Array - [1×2] or } \\ & {[2 \times 1]} \end{aligned}$ |
| Dual | External longitudinal forces | Longitudinal force on the middle wheels | $\begin{aligned} & F w M=\left[\begin{array}{l} F_{x m l} \\ F_{x m r} \end{array}\right] \text { or } \\ & {\left[\begin{array}{l} F_{x m l} \\ F_{x m r} \end{array}\right]} \end{aligned}$ | $\begin{aligned} & \text { Array - [1x2] or } \\ & {[2 \times 1]} \end{aligned}$ |
|  | External forces | Longitudinal and lateral forces on the middle wheels | $F w M=\left[\begin{array}{ll} F_{x m l} & F_{x m r} \\ F_{y m l} & F_{y m r} \end{array}\right]$ | Array - [2x2] |

## Dependencies

To enable this port, set Axle forces to one of these options:

- External longitudinal forces
- External forces

FwR - Total force on the rear wheels
scalar|array
Force on the rear wheels, $F w_{R}$, along the vehicle-fixed axis, in N.

| Vehicle <br> Track <br> Setting | Axle Forces Setting | Description | Variable | Signal Dimension |
| :---: | :---: | :---: | :---: | :---: |
| Single (bicycle) | External longitudinal forces | Longitudinal force on the rear wheel | $F w R=F \chi_{r}$ | Scalar - 1 |
|  | External forces | Longitudinal and lateral forces on the rear wheel | $F w R=\left[\begin{array}{lll}F x_{r} & F y_{r}\end{array}\right]$ or $\left[\begin{array}{l}F x_{r} \\ F y_{r}\end{array}\right]$ | $\begin{aligned} & \text { Array - [1x2] or } \\ & {[2 \times 1]} \end{aligned}$ |
| Dual | External longitudinal forces | Longitudinal force on the rear wheels | $\begin{aligned} & F w R=\left[F_{x r l} F_{x r r}\right] \text { or }\left[\begin{array}{l} F_{x r l} \\ F_{x r r} \end{array}\right. \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { Array - [1×2] or } \\ & {[2 \times 1]} \end{aligned}$ |
|  | External forces | Longitudinal and lateral forces on the rear wheels | $F w R=\left[\begin{array}{ll}F_{x r l} & F_{x r r} \\ F_{y r l} & F_{y r r}\end{array}\right]$ | Array - [2x2] |

## Dependencies

To enable this port, set Axle forces to one of these options:

- External longitudinal forces
- External forces

FExt - External force on vehicle CG
array
External forces applied to the vehicle CG, $F_{x e x t}, F_{y e x t}, F_{z e x t}$, in vehicle-fixed frame, in N. The signal array dimensions are [ $1 \times 3$ ] or [ $3 \times 1$ ].

## Dependencies

To enable this port, on the Input signals pane, select External forces.
MExt - External moment about vehicle CG
array
External moment about the vehicle CG, $M_{x}, M_{y}, M_{z}$, in the vehicle-fixed frame, in N•m. The signal array dimensions are [ $1 \times 3$ ] or [3x1].

## Dependencies

To enable this port, on the Input signals pane, select External moments.
Fh - Hitch force on the body
array

Hitch force applied to the body at the hitch location, $F h_{x}, F h_{y}, F h_{z}$, in the vehicle-fixed frame, in N, specified as a 1-by-3 or 3-by-1 array.

## Dependencies

To enable this port, under Input signals, select Hitch forces.
Mh - Hitch moment about body array

Hitch moment at the hitch location, $M h_{x}, M h_{y}, M h_{z}$, about the vehicle-fixed frame, in $\mathrm{N} \cdot \mathrm{m}$, specified as a 1-by-3 or 3-by-1 array.

## Dependencies

To enable this port, under Input signals, select Hitch moments.
WindXYZ - Wind speed
array
Wind speed, $W_{x}, W_{y}, W_{z}$ along the inertial $X$-, $Y$-, and $Z$-axes, in $\mathrm{m} / \mathrm{s}$. The signal array dimensions are [1x3] or [3x1].

Dependencies
To enable this port, on the Input signals pane, select External wind.
$\mathbf{M u}$ - Tire friction coefficient
array
Tire friction coefficient, $\mu$, dimensionless.

| Vehicle Track Setting | Variable | Signal Dimension |
| :--- | :--- | :--- |
| Single (bicycle) | $M u=\left[\begin{array}{lll}\mu_{f} & \mu_{m} & \mu_{r}\end{array}\right]$ or $\left[\begin{array}{c}\mu_{f} \\ \mu_{m} \\ \mu_{r}\end{array}\right]$ | Array - [1×3] or [3x1] |
| Dual | $M u=\left[\begin{array}{ll}\mu_{f l} & \mu_{f r} \\ \mu_{m l} & \mu_{m r} \\ \mu_{r l} & \mu_{r r}\end{array}\right]$ | Array - [3x2] |

## Dependencies

To enable this port, on the Input signals pane, select External friction.

## AirTemp - Ambient air temperature

## scalar

Ambient air temperature, in K.

## Dependencies

To enable this port, on the Input signals pane, select Air temperature.
X_o - Initial longitudinal position
scalar

Initial vehicle CG displacement along the earth-fixed $X$-axis, in m .

## Dependencies

To enable this port, on the Input signals pane, select Initial longitudinal position.
Y_o - Initial lateral position
scalar
Initial vehicle CG displacement along the earth-fixed $Y$-axis, in m .

## Dependencies

To enable this port, on the Input signals pane, select Initial lateral position.
xdot_o - Initial longitudinal position
scalar
Initial vehicle CG velocity along the vehicle-fixed $x$-axis, in $\mathrm{m} / \mathrm{s}$.

## Dependencies

To enable this port:
1 Set Axle forces to one of these options:

- External longitudinal forces
- External forces

2 On the Input signals pane, select Initial longitudinal velocity
ydot_o - Initial lateral position
scalar
Initial vehicle CG velocity along the vehicle-fixed $y$-axis, in $\mathrm{m} / \mathrm{s}$.

## Dependencies

To enable this port, on the Input signals pane, select Initial lateral velocity.
psi_o - Initial yaw angle
scalar
Rotation of the vehicle-fixed frame about the earth-fixed $Z$-axis (yaw), in rad.

## Dependencies

To enable this port, on the Input signals pane, select Initial yaw angle.
r_o - Initial yaw rate
scalar
Vehicle angular velocity about the vehicle-fixed $z$-axis (yaw rate), in rad/s.

## Dependencies

To enable this port, on the Input signals pane, select Initial yaw rate.

## Output

Info - Vehicle data
bus
Vehicle data, returned as a bus signal containing these block values.

| Signal |  |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| InertFrm | Cg | Disp | X |  | Vehicle CG displacement along the earth-fixed $X$ axis | Computed | m |
|  |  |  | Y |  | Vehicle CG displacement along the earth-fixed $Y$ axis | Computed | m |
|  |  |  | Z |  | Vehicle CG displacement along the earth-fixed $Z$ axis | 0 | m |
|  |  | Vel | Xdot |  | Vehicle CG velocity along the earth-fixed $X$-axis | Computed | m/s |
|  |  |  | Ydot |  | Vehicle CG velocity along the earth-fixed $Y$-axis | Computed | $\mathrm{m} / \mathrm{s}$ |
|  |  |  | Zdot |  | Vehicle CG velocity along the earth-fixed $Z$-axis | 0 | m/s |
|  |  | Ang | phi |  | Rotation of the vehiclefixed frame about the earth-fixed $X$-axis (roll) | 0 | rad |
|  |  |  | theta |  | Rotation of the vehiclefixed frame about the earth-fixed $Y$-axis (pitch) | 0 | rad |
|  |  |  | psi |  | Rotation of the vehiclefixed frame about the earth-fixed $Z$-axis (yaw) | Computed | rad |
|  | FrntAxl | Lft | Disp | X | Front left wheel displacement along the earth-fixed $X$-axis | Computed | m |
|  |  |  |  | Y | Front left wheel displacement along the earth-fixed $Y$-axis | Computed | m |
|  |  |  |  | Z | Front left wheel displacement along the earth-fixed Z-axis | 0 | m |
|  |  |  | Vel | $\begin{aligned} & \text { Xdo } \\ & \mathrm{t} \end{aligned}$ | Front left wheel velocity along the earth-fixed $X$ axis | Computed | m/s |
|  |  |  |  | $\begin{array}{\|l} \hline \text { Ydo } \\ \mathrm{t} \end{array}$ | Front left wheel velocity along the earth-fixed $Y$ axis | Computed | m/s |


| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{aligned} & \mathrm{Zdo} \\ & \mathrm{t} \end{aligned}$ | Front left wheel velocity along the earth-fixed Zaxis | 0 | m/s |
|  | Rght | Disp | X | Front right wheel displacement along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Y | Front right wheel displacement along the earth-fixed $Y$-axis | Computed | m |
|  |  |  | Z | Front right wheel displacement along the earth-fixed Z-axis | 0 | m |
|  |  | Vel | $\begin{aligned} & \mathrm{Xdo} \\ & \mathrm{t} \end{aligned}$ | Front right wheel velocity along the earth-fixed $X$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{Ydo} \\ & \mathrm{t} \end{aligned}$ | Front right wheel velocity along the earth-fixed $Y$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \text { Zdo } \\ & \dagger \end{aligned}$ | Front right wheel velocity along the earth-fixed $Z$ axis | 0 | m/s |
| MidlAxl | Lft | Disp | X | Middle left wheel displacement along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Y | Middle left wheel displacement along the earth-fixed $Y$-axis | Computed | m |
|  |  |  | Z | Middle left wheel displacement along the earth-fixed $Z$-axis | 0 | m |
|  |  | Vel | $\begin{aligned} & \mathrm{Xdo} \\ & \mathrm{t} \end{aligned}$ | Middle left wheel velocity along the earth-fixed $X$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{Ydo} \\ & \mathrm{t} \end{aligned}$ | Middle left wheel velocity along the earth-fixed $Y$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{Zdo} \\ & \dagger \end{aligned}$ | Middle left wheel velocity along the earth-fixed Zaxis | 0 | m/s |
|  | Rght | Disp | X | Middle right wheel displacement along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Y | Middle right wheel displacement along the earth-fixed $Y$-axis | Computed | m |


| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Signal |  |  | Z | Middle right wheel displacement along the earth-fixed $Z$-axis | 0 | m |
|  |  | Vel | $\begin{aligned} & \mathrm{Xdo} \\ & \mathrm{t} \end{aligned}$ | Middle right wheel velocity along the earthfixed $X$-axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \text { Ydo } \\ & \mathrm{t} \end{aligned}$ | Middle right wheel velocity along the earthfixed $Y$-axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{Zdo} \\ & \mathrm{t} \end{aligned}$ | Middle right wheel velocity along the earthfixed $Z$-axis | 0 | m/s |
| RearAxl | Lft | Disp | X | Rear left wheel displacement along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Y | Rear left wheel displacement along the earth-fixed $Y$-axis | Computed | m |
|  |  |  | Z | Rear left wheel displacement along the earth-fixed Z-axis | 0 | m |
|  |  | Vel | $\begin{aligned} & \mathrm{Xdo} \\ & \mathrm{t} \end{aligned}$ | Rear left wheel velocity along the earth-fixed $X$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \text { Ydo } \\ & \mathrm{t} \end{aligned}$ | Rear left wheel velocity along the earth-fixed $Y$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{Zdo} \\ & \mathrm{t} \end{aligned}$ | Rear left wheel velocity along the earth-fixed Zaxis | 0 | m/s |
|  | Rght | Disp | X | Rear right wheel displacement along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Y | Rear right wheel displacement along the earth-fixed $Y$-axis | Computed | m |
|  |  |  | Z | Rear right wheel displacement along the earth-fixed Z-axis | 0 | m |
|  |  | Vel | $\begin{aligned} & \mathrm{Xdo} \\ & \mathrm{t} \end{aligned}$ | Rear right wheel velocity along the earth-fixed $X$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{Ydo} \\ & \mathrm{t} \end{aligned}$ | Rear right wheel velocity along the earth-fixed $Y$ axis | Computed | m/s |



| Signal |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | zdot | Vehicle CG velocity along the vehicle-fixed $z$-axis | 0 | m/s |
|  | Ang | Beta | Body slip angle, $\beta$ $\beta=\frac{V_{y}}{V_{x}}$ | Computed | rad |
|  | AngVel | p | Vehicle angular velocity about the vehicle-fixed $x$ axis (roll rate) | 0 | rad/s |
|  |  | q | Vehicle angular velocity about the vehicle-fixed $y$ axis (pitch rate) | 0 | rad/s |
|  |  | r | Vehicle angular velocity about the vehicle-fixed $z$ axis (yaw rate) | Computed | rad/s |
|  | Acc | ax | Vehicle CG acceleration along the vehicle-fixed $x$ axis | Computed | gn |
|  |  | ay | Vehicle CG acceleration along the vehicle-fixed $y$ axis | Computed | gn |
|  |  | az | Vehicle CG acceleration along the vehicle-fixed $z$ axis | 0 | gn |
|  |  | xddot | Vehicle CG acceleration along the vehicle-fixed $x$ axis | Computed | $\mathrm{m} / \mathrm{s}^{\wedge} 2$ |
|  |  | yddot | Vehicle CG acceleration along the vehicle-fixed $y$ axis | Computed | $\mathrm{m} / \mathrm{s}^{\wedge} 2$ |
|  |  | zddot | Vehicle CG acceleration along the vehicle-fixed $z$ axis | 0 | $\mathrm{m} / \mathrm{s}^{\wedge} 2$ |
|  | AngAcc | pdot | Vehicle angular acceleration about the vehicle-fixed $x$-axis | 0 | rad/s |
|  |  | qdot | Vehicle angular acceleration about the vehicle-fixed $y$-axis | 0 | rad/s |
|  |  | rdot | Vehicle angular acceleration about the vehicle-fixed $z$-axis | Computed | rad/s |
| Forces | Body | Fx | Net force on vehicle CG along the vehicle-fixed $x$ axis | Computed | N |


|  |  |  | Signal ${ }^{\text {a }}$ ( Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Fy |  | Net force on vehicle CG along the vehicle-fixed $y$ axis | Computed | N |
|  | Fz |  | Net force on vehicle CG along the vehicle-fixed $z$ axis | 0 | N |
| Ext | Fx |  | External force on vehicle CG along the vehicle-fixed $x$-axis | Computed | N |
|  | Fy |  | External force on vehicle CG along the vehicle-fixed $y$-axis | Computed | N |
|  | Fz |  | External force on vehicle CG along the vehicle-fixed $z$-axis | 0 | N |
| Hitch | Fx |  | Hitch force applied to body at the hitch location along the vehicle-fixed $x$ axis | Computed | N |
|  | Fy |  | Hitch force applied to body at the hitch location along the vehicle-fixed $y$ axis | Computed | N |
|  | Fz |  | Hitch force applied to body at the hitch location along the vehicle-fixed $z$ axis | Computed | N |
| FrntAxl | Lft | Fx | Longitudinal force on left front wheel along the vehicle-fixed $x$-axis | Computed | N |
|  |  | Fy | Lateral force on left front wheel along the vehiclefixed $y$-axis | Computed | N |
|  |  | Fz | Normal force on left front wheel along the vehiclefixed $z$-axis | Computed | N |
|  | Rght | Fx | Longitudinal force on right front wheel along the vehicle-fixed $x$-axis | Computed | N |
|  |  | Fy | Lateral force on right front wheel along the vehicle-fixed $y$-axis | Computed | N |
|  |  | Fz | Normal force on right front wheel along the vehicle-fixed $z$-axis | Computed | N |


| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | MidlAxl | Lft | Fx | Longitudinal force on left middle wheel along the vehicle-fixed $x$-axis | Computed | N |
|  |  |  | Fy | Lateral force on left middle wheel along the vehicle-fixed $y$-axis | Computed | N |
|  |  |  | Fz | Normal force on left middle wheel along the vehicle-fixed $z$-axis | Computed | N |
|  |  | Rght | Fx | Longitudinal force on right middle wheel along the vehicle-fixed $x$-axis | Computed | N |
|  |  |  | Fy | Lateral force on right middle wheel along the vehicle-fixed $y$-axis | Computed | N |
|  |  |  | Fz | Normal force on right middle wheel along the vehicle-fixed $z$-axis | Computed | N |
|  | RearAxl | Lft | Fx | Longitudinal force on left rear wheel along the vehicle-fixed $x$-axis | Computed | N |
|  |  |  | Fy | Lateral force on left rear wheel along the vehiclefixed $y$-axis | Computed | N |
|  |  |  | Fz | Normal force on left rear wheel along the vehiclefixed $z$-axis | Computed | N |
|  |  | Rght | Fx | Longitudinal force on right rear wheel along the vehicle-fixed $x$-axis | Computed | N |
|  |  |  | Fy | Lateral force on right rear wheel along the vehiclefixed $y$-axis | Computed | N |
|  |  |  | Fz | Normal force on right rear wheel along the vehiclefixed $z$-axis | Computed | N |
|  | Tires | FrntTir es |  | Front left tire force along the vehicle-fixed $x$-axis | Computed | N |
|  |  |  | t¢ <br> F <br> y | Front left tire force along the vehicle-fixed $y$-axis | Computed | N |
|  |  |  | z | Front left tire force along the vehicle-fixed $z$-axis | Computed | N |


| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | R F <br> g x <br> h  <br>   <br>   <br>   | Front right tire force along the vehicle-fixed $x$ axis | Computed | N |
|  |  |  | $\mathrm{t} \left\lvert\, \begin{aligned} & \mathrm{F} \\ & \mathrm{y} \end{aligned}\right.$ | Front right tire force along the vehicle-fixed $y$ axis | Computed | N |
|  |  |  | F | Front right tire force along the vehicle-fixed $z$ axis | Computed | N |
|  |  | $\begin{aligned} & \text { RearTir } \\ & \text { es } \end{aligned}$ |  | Rear left tire force along the vehicle-fixed $x$-axis | Computed | N |
|  |  |  | $\mathrm{t} \begin{aligned} & \mathrm{F} \\ & \mathrm{y} \end{aligned}$ | Rear left tire force along the vehicle-fixed $y$-axis | Computed | N |
|  |  |  |  | Rear left tire force along the vehicle-fixed $z$-axis | Computed | N |
|  |  |  |  | Rear right tire force along the vehicle-fixed $x$-axis | Computed | N |
|  |  |  |  | Rear right tire force along the vehicle-fixed $y$-axis | Computed | N |
|  |  |  | $\begin{aligned} & \mathrm{F} \\ & \mathrm{z} \end{aligned}$ | Rear right tire force along the vehicle-fixed $z$-axis | Computed |  |
|  | Drag | FX |  | Drag force on vehicle CG along the vehicle-fixed $x$ axis | Computed | N |
|  |  | Fy |  | Drag force on vehicle CG along the vehicle-fixed $y$ axis | Computed | N |
|  |  | Fz |  | Drag force on vehicle CG along the vehicle-fixed $z$ axis | Computed | N |
|  | Grvty | Fx |  | Gravity force on vehicle CG along the vehicle-fixed $x$-axis | Computed | N |
|  |  | Fy |  | Gravity force on vehicle CG along the vehicle-fixed $y$-axis | Computed | N |
|  |  | Fz |  | Gravity force on vehicle CG along the vehicle-fixed $z$-axis | Computed | N |
| Moments | Body | Mx |  | Body moment on vehicle CG about the vehicle-fixed x-axis | 0 | $\mathrm{N} \cdot \mathrm{m}$ |




| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Signal |  |  | $\begin{aligned} & \mathrm{zdo} \\ & \mathrm{t} \end{aligned}$ | Middle left wheel velocity along the vehicle-fixed $z$ axis | 0 | m/s |
|  | Rght | Disp | x | Middle right wheel displacement along the vehicle-fixed $x$-axis | Computed | m |
|  |  |  | y | Middle right wheel displacement along the vehicle-fixed $y$-axis | Computed | m |
|  |  |  | z | Middle right wheel displacement along the vehicle-fixed $z$-axis | Computed | m |
|  |  | Vel | $\begin{aligned} & \mathrm{xdo} \\ & \mathrm{t} \end{aligned}$ | Middle right wheel velocity along the vehiclefixed $x$-axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{ydo} \\ & \mathrm{t} \end{aligned}$ | Middle right wheel velocity along the vehiclefixed $y$-axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{zdo} \\ & \mathrm{t} \end{aligned}$ | Middle right wheel velocity along the vehiclefixed $z$-axis | 0 | m/s |
|  | Steer | WhlAngRL |  | Middle left wheel steering angle | Computed | rad |
|  |  | WhlangRR |  | Middle right wheel steering angle | Computed | rad |
| RearAxl | Lft | Disp | x | Rear left wheel displacement along the vehicle-fixed $x$-axis | Computed | m |
|  |  |  | y | Rear left wheel displacement along the vehicle-fixed $y$-axis | Computed | m |
|  |  |  | z | Rear left wheel displacement along the vehicle-fixed $z$-axis | Computed | m |
|  |  | Vel | $\begin{aligned} & \mathrm{xdo} \\ & \mathrm{t} \end{aligned}$ | Rear left wheel velocity along the vehicle-fixed $x$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{ydo} \\ & \mathrm{t} \end{aligned}$ | Rear left wheel velocity along the vehicle-fixed $y$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \text { zdo } \\ & \mathrm{t} \end{aligned}$ | Rear left wheel velocity along the vehicle-fixed $z$ axis | 0 | m/s |


| Signal |  |  | Rght | Disp | x | Rear right wheel <br> displacement along the <br> vehicle-fixed $x$-axis | Computed |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  |  |  |  | y | m |  |  |


| Signal |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | y | Vehicle chassis offset from center plane along the vehicle-fixed $y$-axis | Input | m |
|  |  | z | Vehicle chassis offset from axle plane along the earth-fixed $z$-axis | Input | m |
|  | Vel | $\begin{aligned} & \mathrm{xdo} \\ & \mathrm{t} \end{aligned}$ | Vehicle chassis offset velocity along the vehiclefixed $x$-axis | Computed | m/s |
|  |  | $\begin{aligned} & \mathrm{ydo} \\ & \mathrm{t} \end{aligned}$ | Vehicle chassis offset velocity along the vehiclefixed $y$-axis | Computed | m/s |
|  |  | $\begin{aligned} & \mathrm{zdo} \\ & \mathrm{t} \end{aligned}$ | Vehicle chassis offset velocity along the vehiclefixed $z$-axis | 0 | m/s |
|  | Ang | $\begin{aligned} & \text { Bet } \\ & \text { a } \end{aligned}$ | Body slip angle, $\beta$ $\beta=\frac{V_{y}}{V_{x}}$ | Computed | rad |


| Signal |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: |
| PwrInfo | PwrTrnsfrd | PwrFxExt | Externally applied longitudinal force power | Comp uted | W |
|  |  | PwrFyExt | Externally applied lateral force power | Comp uted | W |
|  |  | PwrMzExt | Externally applied yaw moment power | Comp uted | W |
|  |  | PwrFwFLx | Longitudinal force applied at the front left axle power | Comp uted | W |
|  |  | PwrFwFLy | Lateral force applied at the front left axle power | Comp uted | W |
|  |  | PwrFwFRx | Longitudinal force applied at the front right axle power | Comp uted | W |
|  |  | PwrFwFRy | Lateral force applied at the front right axle power | Comp uted | W |
|  |  | PwrFwMLx | Longitudinal force applied at the middle left axle power | Comp uted | W |
|  |  | PwrFwMLy | Lateral force applied at the middle left axle power | Comp uted | W |
|  |  | PwrFwMRx | Longitudinal force applied at the middle right axle power | Comp uted | W |
|  |  | PwrFwMRy | Lateral force applied at the middle right axle power | Comp uted | W |


| Signal |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | PwrFwRLx | Longitudinal force applied at the rear left axle power | Comp uted | W |
|  |  | PwrFwRLy | Lateral force applied at the rear left axle power | Comp uted | W |
|  |  | PwrFwRRx | Longitudinal force applied at the rear right axle power | Comp uted | W |
|  |  | PwrFwRRy | Lateral force applied at the rear right axle power | Comp uted | W |
|  | PwrNotTrnsfr d | PwrFxDrag | Longitudinal drag force power | Comp uted | W |
|  |  | PwrFyDrag | Lateral drag force power | Comp uted | W |
|  |  | PwrMzDrag | Drag pitch moment power | Comp uted | W |
|  | PwrStored | PwrStoredGrvty | Rate change in gravitational potential energy | Comp uted | W |
|  |  | PwrStoredxdot | Rate of change of longitudinal kinetic energy | Comp uted | W |
|  |  | PwrStoredydot | Rate of change of lateral kinetic energy | Comp uted | W |
|  |  | PwrStoredr | Rate of change of rotational yaw kinetic energy | Comp uted | W |

xdot - Vehicle longitudinal velocity
scalar
Vehicle CG velocity along the vehicle-fixed $x$-axis, in $\mathrm{m} / \mathrm{s}$.

```
ydot - Vehicle lateral velocity
```

scalar
Vehicle CG velocity along the vehicle-fixed $y$-axis, in $\mathrm{m} / \mathrm{s}$.

```
psi - Yaw
```

scalar
Rotation of the vehicle-fixed frame about the earth-fixed Z-axis (yaw), in rad.
r-Yaw rate
scalar
Vehicle angular velocity, r , about the vehicle-fixed $z$-axis (yaw rate), in rad/s.
FzF - Normal force on front wheels
scalar|array
Normal force on the front wheels, $F z_{F}$, along the vehicle-fixed $z$-axis, in N .

| Vehicle Track <br> Setting | Description | Variable | Signal Dimension |
| :--- | :--- | :--- | :--- |
| Single <br> (bicycle) | Normal force on front <br> axle | $F z F=F z_{f}$ | Scalar - 1 |
| Dual | Normal force on the <br> right and left front <br> wheels | $F z F=\left[F z_{f l} F z_{f r}\right]$ | Array - [1×2] |

FzM - Normal force on middle wheels
scalar|array
Normal force on the middle wheels, $F z_{M}$, along the vehicle-fixed $z$-axis, in N .

| Vehicle Track <br> Setting | Description | Variable | Signal Dimension |
| :--- | :--- | :---: | :--- |
| Single <br> (bicycle) | Normal force on <br> middle axle | $F z M=F z_{m}$ | Scalar - 1 |
| Dual | Normal force on the <br> right and left middle <br> wheels | $F z M=\left[F z_{m l} F z_{r l}\right]$ | Array - [1×2] |

FzR - Normal force on rear wheels
scalar|array
Normal force on the rear wheels, $F z_{R}$, along the vehicle-fixed $z$-axis, in N .

| Vehicle Track <br> Setting | Description | Variable | Signal Dimension |
| :--- | :--- | :--- | :--- |
| Single (bicycle) | Normal force on rear <br> wheel | $F z R=F z_{r}$ | Scalar - 1 |
| Dual | Normal force on the <br> right and left rear <br> wheels | $F z R=\left[F z_{r l} F z_{r r}\right]$ | Array - [1×2] |

## Parameters

## Options

Vehicle track - Number of vehicle wheels
Dual (default)|Single (bicycle)
Use the Vehicle track parameter to specify the number of wheels.

| Vehicle Track Setting | Implementation |
| :--- | :--- |
| Single (bicycle) | - Forces act along the center line of the axles. <br>  <br> - No lateral load transfer. |
| Dual | Forces act at the axle hard-point locations. |

Axle forces - Type of axle force
External longitudinal velocity (default)|External longitudinal forces|External forces

Use the Axle forces parameter to specify the type of force.

| Axle Forces Setting | Implementation |
| :---: | :---: |
| External longitudinal velocity | - The block assumes that the external longitudinal velocity is in a quasi-steady state, so the longitudinal acceleration is approximately zero. <br> - Because the motion is quasi-steady, the block calculates lateral forces using the tire slip angles and linear cornering stiffness. <br> - Consider this setting when you want to: <br> - Generate virtual sensor signal data. <br> - Conduct high-level software studies that are not impacted by driveline or nonlinear tire responses. |
| External longitudinal forces | - The block uses the external longitudinal force to accelerate or brake the vehicle. <br> - The block calculates lateral forces using the tire slip angles and linear cornering stiffness. <br> - Consider this setting when you want to: <br> - Account for changes in the longitudinal velocity on the lateral and yaw motion. <br> - Specify the external longitudinal motion through a force instead of an external longitudinal velocity. <br> - Connect the block to tractive actuators, wheels, brakes, and hitches. |
| External forces | - The block uses the external lateral and longitudinal forces to steer, accelerate, or brake the vehicle. <br> - The block does not use the steering input to calculate vehicle motion. <br> - Consider this setting when you need tire models with more accurate nonlinear combined lateral and longitudinal slip. |

## Input Signals

## Front wheel steering - WhlAngF input port

on (default) | off
Select to create input port WhlAngF.
Middle wheel steering - WhlAngM input port
off (default) | on
Select to create input port WhlAngM.
Rear wheel steering - WhlAngR input port
off (default) | on

Select to create input port WhlAngR.
External wind - WindXYZ input port
off (default) |on
Select to create input port WindXYZ.
External friction - Mu input port
off (default) | on
Select to create input port Mu.

## Dependencies

To enable this parameter, set Axle forces to External longitudinal forces or External forces.

External forces - FExt input port
off (default) | on
Select to create input port FExt.
External moments - MExt input port
off (default) | on
Select to create input port MExt.
Hitch forces - Fh input port
on (default) | off
Select to create input port Fh.
Hitch moments - Mh input port
on (default) | off
Specify to create input port Mh.
Initial longitudinal position - X_o input port
off (default) | on
Specify to create input port X_o.
Initial yaw angle - psi_o input port
off (default) | on
Specify to create input port psi_o.
Initial longitudinal velocity - xdot_o input port
off (default) | on
Specify to create input port xdot_o.
Dependencies
To enable this parameter, set Axle forces to External longitudinal forces or External forces.

Initial yaw rate - r_o input port
off (default) | on
Specify to create input port r_o.
Initial lateral position - Y_o input port off (default) | on

Specify to create input port Y_o.
Air temperature - AirTemp input port off (default) | on

Specify to create input port AirTemp.
Initial lateral velocity - ydot_o input port
off (default) | on
Specify to create input port ydot_o.

## Longitudinal

Number of wheels on front axle, NF - Front wheel count
2 (default) | scalar
Number of wheels on the front axle, $N_{F}$, dimensionless.
Number of wheels on middle axle, NM - Middle wheel count
2 (default) | scalar
Number of wheels on the middle axle, $N_{M}$, dimensionless.
Number of wheels on rear axle, NR - Rear wheel count
2 (default) | scalar
Number of wheels on the rear axle, $N_{R}$, dimensionless.
Vehicle mass, m - Vehicle mass
47000 (default) | scalar
Vehicle mass, $m$, in kg .
Longitudinal distance from center of mass to front axle, a - Distance from CM to front axle 0.5 (default) | scalar

Distance from vehicle CM to front axle, $a$, in m .


Longitudinal distance from center of mass to middle axle, $\mathbf{b}$ - Distance from CM to middle axle 4.5 (default) | scalar

Distance from vehicle CM to middle axle, $b$, in $m$.


Longitudinal distance from center of mass to rear axle, c-Distance from CM to rear axle
5.7 (default) | scalar

Distance from vehicle CM to rear axle, $c$, in $m$.


Vertical distance from center of mass to axle plane, $\mathbf{h}$ - Distance from CM to axle plane 0.3 (default) | scalar

Vertical distance from vehicle CM to axle plane, $h$, in $m$.


Vertical distance from hitch to axle plane, $\mathbf{h h}$ - Distance from hitch to axle plane
0.5 (default) | scalar

Vertical distance from hitch to axle plane, $h h$, in m.


## Dependencies

To enable this parameter, on the Input signals pane, select Hitch forces or Hitch moments.
Longitudinal distance from center of mass to hitch, $\mathbf{d h}$ - Distance from CM to hitch 5 (default) | scalar

Longitudinal distance from center of mass to hitch, $d h$, in $m$.


## Dependencies

To enable this parameter, on the Input signals pane, select Hitch forces or Hitch moments.
Initial inertial frame longitudinal position, X_o - Initial longitudinal displacement
0 (default) | scalar
Initial vehicle CG displacement along the earth-fixed $X$-axis, in m .
Initial longitudinal velocity, xdot_o - Initial longitudinal velocity
0 (default) | scalar
Initial vehicle CG velocity along the vehicle-fixed $x$-axis, in $\mathrm{m} / \mathrm{s}$.

## Dependencies

To enable this parameter, set Axle forces to one of these options:

- External longitudinal forces
- External forces


## Lateral

Mapped corner stiffness - Enable mapped corner stiffness
off (default) | on
Enables mapped corner stiffness calculation.

## Dependencies

To enable this parameter, set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces

Include relaxation length dynamics - Enable relaxation length dynamics
on (default) | off
Enables relaxation length dynamics.

## Dependencies

To enable this parameter:
1 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces


## 2 Clear Mapped corner stiffness.

Lateral distance from geometric centerline to center of mass, d - Distance from centerline to CM
0 (default) | scalar
Lateral distance from the geometric centerline to the center of mass, $d$, in $m$, along the vehicle-fixed $y$-axis. Positive values indicate that the vehicle CM is to the right of the geometric centerline.
Negative values indicate that the vehicle CM is to the left of the geometric centerline.


Track width, w - Front, middle, and rear track widths
[1.82,1.82,1.82] (default) | vector
Front, middle, and rear track widths, $w f$, $w m$, and, $w r$, respectively, in m. Dimensions are 1-by-3.


## Dependencies

To enable this parameter, set Vehicle track to Dual.
Front axle tire corner stiffness, Cy_f - Front tire corner stiffness
12e3 | scalar
Front tire corner stiffness, $C y_{f}$, in $\mathrm{N} / \mathrm{rad}$.

## Dependencies

To enable this parameter:
1 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces

2 Clear Mapped corner stiffness.
Middle axle tire corner stiffness, Cy_m - Middle tire corner stiffness
11e3 | scalar
Middle axle tire corner stiffness, $C y_{m}$, in N/rad.

## Dependencies

To enable this parameter:

1 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces

2 Clear Mapped corner stiffness.
Rear axle tire corner stiffness, Cy_r - Rear tire corner stiffness 11e3|scalar

Rear axle tire corner stiffness, $C y_{r}$, in $\mathrm{N} / \mathrm{rad}$.

## Dependencies

To enable this parameter:
1 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces


## 2 Clear Mapped corner stiffness.

Front tire(s) relaxation length, sigma_f - Front tire relaxation length
. 1 (default) | scalar
Front tire relaxation length, $\sigma_{f}$, in m .

## Dependencies

To enable this parameter:
1 Set Vehicle track to one of these options:

- Single 2-axle
- Dual 2-axle
- Single 3-axle
- Dual 3-axle

2 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces

3 Do either of these:

- Select Mapped corner stiffness.
- Clear Mapped corner stiffness and select Include relaxation length dynamics.


## Middle tire(s) relaxation length, sigma_m - Middle tire relaxation length

. 1 (default) | scalar
Middle tire relaxation length, $\sigma_{m}$, in m .

## Dependencies

To enable this parameter:

1 Set Vehicle track to one of these options:

- Single 2-axle
- Dual 2-axle
- Single 3-axle
- Dual 3-axle

2 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces

3 Do either of these:

- Select Mapped corner stiffness.
- Clear Mapped corner stiffness and select Include relaxation length dynamics.

Rear tire(s) relaxation length, sigma_r - Rear tire relaxation length

## . 1 (default) scalar

Rear tire relaxation length, $\sigma_{r}$, in m.

## Dependencies

To enable this parameter:
1 Set Vehicle track to one of these options:

- Single 2-axle
- Dual 2-axle
- Single 3-axle
- Dual 3-axle

2 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces

3 Do either of these:

- Select Mapped corner stiffness.
- Clear Mapped corner stiffness and select Include relaxation length dynamics.

Front axle slip angle breakpoints, alpha_f_brk - Breakpoints
[-. 1 .1] (default)|vector
Front axle slip angle breakpoints, $\alpha_{f b r k}$, in rad.

## Dependencies

To enable this parameter:
1 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces

2 Select Mapped corner stiffness.
Front axle tire corner data, Cy_f_data - Front axle tire corner data
[-9e3 9e3] (default)|vector
Front axle tire corner data, $C y_{f d a t a}$, in $\mathrm{N} / \mathrm{rad}$.

## Dependencies

To enable this parameter:
1 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces

2 Select Mapped corner stiffness.
Middle axle slip angle breakpoints, alpha_m_brk - Breakpoints
[-. 1 .1] (default) |vector
Middle axle slip angle breakpoints, $\alpha_{m b r k}$, in rad.

## Dependencies

To enable this parameter:
1 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces

2 Select Mapped corner stiffness.
Middle axle tire corner data, Cy_m_data - Middle axle tire corner data [-9e3 9e3] (default) |vector

Middle axle tire corner data, $C y_{\text {mdata }}$, in $\mathrm{N} / \mathrm{rad}$.

## Dependencies

To enable this parameter:
1 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces

2 Select Mapped corner stiffness.
Rear axle slip angle breakpoints, alpha_r_brk - Breakpoints
[-. 1 .1] (default) |vector
Rear axle slip angle breakpoints, $\alpha_{r b r k}$ in rad.

## Dependencies

To enable this parameter:

1 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces

2 Select Mapped corner stiffness.
Rear axle tire corner data, Cy_r_data - Rear axle tire corner data
[-9e3 9e3] (default)|vector
Rear axle tire corner data, $C y_{\text {rdata, }}$, in N/rad.

## Dependencies

To enable this parameter:
1 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces


## 2 Select Mapped corner stiffness.

Initial inertial frame lateral displacement, Y_o - Initial lateral displacement
0 (default) | scalar
Initial vehicle CG displacement along the earth-fixed $Y$-axis, in $m$.
Initial lateral velocity, ydot_o - Initial lateral velocity
0 (default) | scalar
Initial vehicle CG velocity along the vehicle-fixed $y$-axis, in $\mathrm{m} / \mathrm{s}$.

## Yaw

Yaw polar inertia, Izz - Inertia
4000 (default) | scalar
Yaw polar inertia, in $\mathrm{kg}^{*} \mathrm{~m}^{\wedge} 2$.
Initial yaw angle, psi_o - Psi rotation
0 (default) | scalar
Rotation of the vehicle-fixed frame about earth-fixed Z-axis (yaw), in rad.
Initial yaw rate, r_o - Yaw rate
0 (default) | scalar
Vehicle angular velocity about the vehicle-fixed $z$-axis (yaw rate), in rad/s.

## Aerodynamic

Longitudinal drag area, Af - Effective vehicle cross-sectional area
2 (default) | scalar
Effective vehicle cross-sectional area, $A_{f}$, to calculate the aerodynamic drag force on the vehicle, in $\mathrm{m}^{2}$.

## Longitudinal drag coefficient, Cd - Air drag coefficient

## . 3 (default) | scalar

Air drag coefficient, $C_{d}$. The value is dimensionless.
Longitudinal lift coefficient, CI - Air lift coefficient
. 1 (default) | scalar
Air lift coefficient, $C_{l}$. The value is dimensionless.

## Longitudinal drag pitch moment, Cpm - Pitch drag

. 1 (default) | scalar
Longitudinal drag pitch moment coefficient, $C_{p m}$. The value is dimensionless.
Relative wind angle vector, beta_w - Wind angle
[0:0.01:0.3] (default) | vector
Relative wind angle vector, $\beta_{w}$, in rad.
Side force coefficient vector, Cs - Side force coefficient
[0:0.03:0.9] (default)| vector
Side force coefficient vector coefficient, $C_{s}$. The value is dimensionless.
Yaw moment coefficient vector, Cym - Yaw moment drag
[0:0.01:0.3] (default) | vector
Yaw moment coefficient vector coefficient, $C_{y m}$. The value is dimensionless.

## Environment

Absolute air pressure, Pabs - Pressure
101325 (default) | scalar
Environmental absolute pressure, $P_{a b s}$, in Pa.
Air temperature, Tair - Temperature
273 (default) | scalar
Environmental absolute temperature, $T$, in K .

## Dependencies

To enable this parameter, clear Air temperature.
Gravitational acceleration, g-Gravity
9.81 (default) | scalar

Gravitational acceleration, $g$, in $\mathrm{m} / \mathrm{s}^{\wedge} 2$.
Nominal friction scaling factor, mu - Friction scale factor
1 (default) | scalar
Nominal friction scale factor, $\mu$. The value is dimensionless.

## Dependencies

To enable this parameter:
1 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces


## 2 Clear External Friction.

## Simulation

## Longitudinal velocity tolerance, xdot_tol - Tolerance

. 01 (default) | scalar
Longitudinal velocity tolerance, in m/s.
Nominal normal force, Fznom - Normal force
5000 (default) | scalar
Nominal normal force, in N .

## Dependencies

To enable this parameter, set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces

Geometric longitudinal offset from axle plane, longOff - Longitudinal offset
0 (default) | scalar
Vehicle chassis offset from the axle plane along the vehicle-fixed $x$-axis, in $m$. When you use the 3D visualization engine, consider using the offset to locate the chassis independently of the vehicle CG.

## Geometric lateral offset from center plane, latOff - Lateral offset

0 (default) | scalar
Vehicle chassis offset from the center plane along the vehicle-fixed $y$-axis, in $m$. When you use the 3D visualization engine, consider using the offset to locate the chassis independently of the vehicle CG.

Geometric vertical offset from axle plane, vertOff - Vertical offset
0 (default) | scalar
Vehicle chassis offset from the axle plane along the vehicle-fixed $z$-axis, in m . When you use the 3D visualization engine, consider using the offset to locate the chassis independently of the vehicle CG.

Wrap Euler angles, wrapAng - Wrap the Euler angles to the interval [-pi, pi]
off (default) |on
Wrap the Euler angles to the interval [-pi, pi]. For vehicle maneuvers that might undergo vehicle yaw rotations that are outside of this interval, consider clearing the parameter if you want to:

- Track the total vehicle yaw rotation.
- Avoid discontinuities in the vehicle state estimators.


## Version History

Introduced in R2020a

## References

[1] Gillespie, Thomas. Fundamentals of Vehicle Dynamics. Warrendale, PA: Society of Automotive Engineers (SAE), 1992.

## Extended Capabilities

C/C++ Code Generation
Generate C and C++ code using Simulink ${ }^{\circledR}$ Coder ${ }^{\mathrm{TM}}$.

## See Also

Trailer Body 3DOF

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"

## Vehicle Body 6DOF Three Axles

Three-axle vehicle tractor body with translational and rotational motion


## Libraries:

Vehicle Dynamics Blockset / Vehicle Body

## Description

The Vehicle Body 6DOF Three Axles block implements a six degrees-of-freedom (DOF) rigid three-axle vehicle body model that calculates longitudinal, lateral, vertical, pitch, roll, and yaw motion. Use the block to model three-axle vehicles like a tractor. The block accounts for body mass, inertia, aerodynamic drag, road incline, and weight distribution between the axle hard-point locations due to suspension and external forces and moments. Use the Inertial Loads parameters to analyze the vehicle dynamics under different loading conditions.

Connect the block to virtual sensors, suspension systems, or external systems like body control actuators. Use the Vehicle Body 6DOF Three Axles block in ride and handling studies to model the effects of drag forces, passenger loading, and suspension hardpoint locations.

To create additional input ports, under Input signals, select these block parameters.

| Parameter | Input Port | Description |
| :--- | :--- | :--- |
| Front hitch forces | FhF | Hitch force applied to the body at the front hitch location, <br> $F h F_{x}, F h F_{y}$, and $F h F_{z}$, in the vehicle-fixed frame |
| Front hitch moments | MhF | Hitch moment at the front hitch location, $M h F_{x}, M h F_{y}$, and <br> $M h F_{z}$, about the vehicle-fixed frame |
| Rear hitch forces | FhR | Hitch force applied to the body at the rear hitch location, <br> $F h R_{x}, F h R_{y}$, and $F h R_{z}$, in the vehicle-fixed frame |
| Rear hitch moments | MhR | Hitch moment at the rear hitch location, $M h R_{x}, M h R_{y}$, and <br> $M h R_{z}$, about the vehicle-fixed frame |

## Inertial Loads

To analyze the vehicle dynamics under different loading conditions, use the Inertial Loads parameters. You can specify these loads:

- Tractor front
- Cab overhead
- Tractor frame left and frame right
- Cab left and cab right
- Tractor rear

For each of the loads, you can specify the mass, location, and inertia.

The illustrations provide the load locations and vehicle parameter dimensions. The table provides the corresponding location parameter sign settings.


This table summarizes the parameter settings that specify the load locations indicated by the dots. For the location, the block uses this distance vector:

- Front axle to load, along the vehicle-fixed $x$-axis
- Vehicle centerline to load, along the vehicle-fixed $y$-axis
- Front axle to load, along the vehicle-fixed $z$-axis

| Load | Parameter | Example Location |
| :---: | :---: | :---: |
| Tractor front | Distance vector from front axle, z1R | - $\operatorname{z1R}(1,1)<0-$ Forward of the front axle <br> - $\operatorname{z1R}(1,2)>0-$ Right of the vehicle centerline <br> - $\operatorname{z1R}(1,3)>0-$ Above the front axle suspension hardpoint |
| Cab overhead | Distance vector from front axle, z2R | - $\quad \operatorname{z2R}(1,1)>0-$ Rear of the front axle <br> - $z 2 R(1,2)<0-$ Left of the vehicle centerline <br> - $\quad z 2 R(1,3)>0-$ Above the front axle suspension hardpoint |
| Tractor frame left | Distance vector from front axle, z3R | - $\quad \operatorname{z3R}(1,1)>0-$ Rear of the front axle <br> - $z 3 R(1,2)<0-$ Left of the vehicle centerline <br> - $\operatorname{z3R}(1,3)>0-$ Above the front axle suspension hardpoint |
| Tractor frame right | Distance vector from front axle, z4R | - $\quad \operatorname{z4R}(1,1)>0-$ Rear of the front axle <br> - $z 4 R(1,2)>0-$ Right of the vehicle centerline <br> - $z 4 R(1,3)>0-$ Above the front axle suspension hardpoint |
| Cab left | Distance vector from front axle, z5R | - $\quad z 5 R(1,1)>0-$ Rear of the front axle <br> - $z 5 R(1,2)<0-$ Left of the vehicle centerline <br> - $z 5 R(1,3)>0-$ Above the front axle suspension hardpoint |
| Cab right | Distance vector from front axle, z6R | - $\operatorname{z6R}(1,1)>0-$ Rear of the front axle <br>  <br> - $z 6 R(1,3)>0-$ Above the front axle suspension hardpoint |
| Tractor rear | Distance vector from front axle, z7R | - $\quad \operatorname{z7R}(1,1)>0-$ Rear of the front axle <br> - $z 7 R(1,2)>0-$ Right of the vehicle centerline <br> - $\quad \operatorname{z7R}(1,3)>0-$ Above the front axle suspension hardpoint |

## Equations of Motion

To determine the vehicle motion, the block implements calculations for the rigid body vehicle dynamics, wind drag, inertial loads, and coordinate transformations. The body-fixed and vehicle-fixed coordinate systems are the same.

The block considers the rotation of a body-fixed coordinate frame about a flat earth-fixed inertial reference frame. The origin of the body-fixed coordinate frame is the vehicle center of gravity of the body.

The block uses this equation to calculate the translational motion of the body-fixed coordinate frame, where the applied forces $\left[F_{x} F_{y} F_{z}\right]^{\mathrm{T}}$ are in the body-fixed frame, and the mass of the body, $m$, is assumed to be constant.

$$
\begin{aligned}
& \bar{F}_{b}=\left[\begin{array}{l}
F_{x} \\
F_{y} \\
F_{z}
\end{array}\right]=m\left(\dot{\bar{V}}_{b}+\bar{\omega} \times \bar{V}_{b}\right) \\
& \bar{M}_{b}=\left[\begin{array}{l}
L \\
M \\
N
\end{array}\right]=I \dot{\bar{\omega}}+\bar{\omega} \times(I \bar{\omega}) \\
& I=\left[\begin{array}{ccc}
I_{x x} & -I_{x y} & -I_{x z} \\
-I_{y x} & I_{y y} & -I_{y z} \\
-I_{z x} & -I_{z y} & I_{z z}
\end{array}\right]
\end{aligned}
$$

To determine the relationship between the body-fixed angular velocity vector, $[p q r]^{\mathrm{T}}$, and the rate of change of the Euler angles, $\left[\begin{array}{lll}\dot{\phi} & \dot{\theta} & \dot{\psi}\end{array}\right]^{T}$, the block resolves the Euler rates into the body-fixed frame.

$$
\left[\begin{array}{l}
p \\
q \\
r
\end{array}\right]=\left[\begin{array}{l}
\dot{\phi} \\
0 \\
0
\end{array}\right]+\left[\begin{array}{ccc}
1 & 0 & 0 \\
0 & \cos \phi & \sin \phi \\
0 & -\sin \phi & \cos \phi
\end{array}\right]\left[\begin{array}{l}
0 \\
\dot{\theta} \\
0
\end{array}\right]+\left[\begin{array}{ccc}
1 & 0 & 0 \\
0 & \cos \phi & \sin \phi \\
0 & -\sin \phi & \cos \phi
\end{array}\right]\left[\begin{array}{ccc}
\cos \theta & 0 & -\sin \theta \\
0 & 1 & 0 \\
\sin \theta & 0 & \cos \theta
\end{array}\right]\left[\begin{array}{l}
0 \\
0 \\
\dot{\psi}
\end{array}\right] \equiv J^{-1}\left[\begin{array}{c}
\dot{\phi} \\
\dot{\theta} \\
\dot{\psi}
\end{array}\right]
$$

Inverting $J$ gives the required relationship to determine the Euler rate vector.

$$
\left[\begin{array}{c}
\dot{\phi} \\
\dot{\theta} \\
\dot{\psi}
\end{array}\right]=J\left[\begin{array}{l}
p \\
q \\
r
\end{array}\right]=\left[\begin{array}{ccc}
1 & (\sin \phi \tan \theta) & (\cos \phi \tan \theta) \\
0 & \cos \phi & -\sin \phi \\
0 & \frac{\sin \phi}{\cos \theta} & \frac{\cos \phi}{\cos \theta}
\end{array}\right]\left[\begin{array}{l}
p \\
q \\
r
\end{array}\right]
$$

The applied forces and moments are the sum of the drag, gravitational, external, and suspension forces.

$$
\begin{aligned}
& \bar{F}_{b}=\left[\begin{array}{c}
F_{x} \\
F_{y} \\
F_{z}
\end{array}\right]=\left[\begin{array}{c}
F_{d_{x}} \\
F_{d_{y}} \\
F_{d_{z}}
\end{array}\right]+\left[\begin{array}{c}
F_{g_{x}} \\
F_{g_{y}} \\
F_{g_{z}}
\end{array}\right]+\left[\begin{array}{c}
F_{\text {ext }} \\
F_{\text {ext }} \\
F_{\text {ext }}
\end{array}\right]+\left[\begin{array}{c}
F_{F L_{x}} \\
F_{F L_{y}} \\
F_{F L_{z}}
\end{array}\right]+\left[\begin{array}{c}
F_{F R_{x}} \\
F_{F R_{y}} \\
F_{F R_{z}}
\end{array}\right]+\left[\begin{array}{c}
F_{M L_{x}} \\
F_{M L_{y}} \\
F_{M L_{z}}
\end{array}\right]+\left[\begin{array}{c}
F_{M R_{x}} \\
F_{M R_{y}} \\
F_{M R_{z}}
\end{array}\right]+\left[\begin{array}{c}
F_{R L_{x}} \\
F_{R L_{y}} \\
F_{R L_{z}}
\end{array}\right]+\left[\begin{array}{c}
F_{R R_{x}} \\
F_{R R_{y}} \\
F_{R R_{z}}
\end{array}\right] \\
& \bar{M}_{b}=\left[\begin{array}{l}
M_{x} \\
M_{y} \\
M_{z}
\end{array}\right]=\left[\begin{array}{l}
M_{d_{x}} \\
M_{d_{y}} \\
M_{d_{z}}
\end{array}\right]+\left[\begin{array}{l}
M_{e x t_{x}} \\
M_{e x t_{y}} \\
M_{e x t_{z}}
\end{array}\right]+\left[\begin{array}{l}
M_{F L_{x}} \\
M_{F L_{y}} \\
M_{F L_{z}}
\end{array}\right]+\left[\begin{array}{l}
M_{F R_{x}} \\
M_{F R_{y}} \\
M_{F R_{z}}
\end{array}\right]+\left[\begin{array}{l}
M_{M L_{x}} \\
M_{M L_{y}} \\
M_{M L_{z}}
\end{array}\right]+\left[\begin{array}{l}
M_{M R_{x}} \\
M_{M R_{y}} \\
M_{M R_{z}}
\end{array}\right]+\left[\begin{array}{l}
M_{R L_{x}} \\
M_{R L_{y}} \\
M_{R L_{z}}
\end{array}\right]+\left[\begin{array}{l}
M_{R R_{x}} \\
M_{R R_{y}} \\
M_{R R_{z}}
\end{array}\right]+\bar{M}_{F}
\end{aligned}
$$

| Calculation | Implementation |
| :---: | :---: |
| Load masses and inertias | The block uses the parallel axis theorem to resolve the individual load masses and inertias with the vehicle mass and inertia. $J_{i j}=I_{i j}+m\left(\|R\|^{2} \delta_{i j}-R_{i} R_{j}\right)$ |
| Gravitational forces, $F_{g}$ | The block uses the direction cosine matrix (DCM) to transform the gravitational vector in the inertial-fixed frame to the body-fixed frame. |
| Drag forces, $F_{d}$, and moments, $M_{d}$ | To determine a relative airspeed, the block subtracts the wind speed from the vehicle center of mass (CM) velocity. Using the relative airspeed, the block determines the drag forces. $\begin{aligned} & \bar{w}=\sqrt{\left(\dot{x}-w_{\chi}\right)^{2}+\left(\dot{x}-w_{\chi}\right)^{2}+\left(w_{z}\right)^{2}} \\ & F_{d x}=-\frac{1}{2 T R} C_{d} A_{f} P_{a b s}{ }^{(\bar{w}} \\ & F_{d y}=-\frac{1}{2 T R} C_{s} A_{f} P_{a b s}{ }^{\bar{w}} \\ & F_{d z}=-\left.\frac{1}{2 T R} C_{l} A_{f} P_{a b s}\right\|^{\bar{w}} \end{aligned}$ <br> Using the relative airspeed, the block determines the drag moments. $\begin{aligned} & M_{d r}=-\frac{1}{2 T R} C_{r m} A_{f} P_{a b s}\left({ }^{\bar{w}}(a+c)\right. \\ & M_{d p}=-\frac{1}{2 T R} C_{p m} A_{f} P_{a b s}{ }^{\bar{w}}(a+c) \\ & M_{d y}=-\frac{1}{2 T R} C_{y m} A_{f} P_{a b s}{ }^{(\bar{w}}(a+c) \end{aligned}$ |
| External forces, $F_{i n}$, and moments, $M_{\text {in }}$ | The external forces and moments are input via ports FExt and MExt. |
| Suspension forces and moments | The block assumes that the suspension forces and moments act on these hardpoint locations: <br> - $F_{F L}, M_{F L}$ - Front left <br> - $F_{F R}, M_{F R}$ - Front right <br> - $F_{M L}, M_{M L}$ - Middle left <br> - $F_{M R}, M_{M R}-$ Middle right <br> - $F_{R L}, M_{R L}$ - Rear left <br> - $F_{R R}, M_{R R}-$ Rear right |

The equations use these variables.
$x, \dot{x}, \ddot{x}$
$y, \dot{y}, \ddot{y}$

Vehicle CM displacement, velocity, and acceleration along the vehicle-fixed x-axis
Vehicle CM displacement, velocity, and acceleration along the vehicle-fixed $y$-axis

| $z, \dot{z}, \ddot{z}$ | Vehicle CM displacement, velocity, and acceleration along the vehicle-fixed $z$-axis |
| :---: | :---: |
| $\varphi$ | Rotation of the vehicle-fixed frame about the earth-fixed $X$-axis (roll) |
| $\theta$ | Rotation of the vehicle-fixed frame about the earth-fixed $Y$-axis (pitch) |
| $\psi$ | Rotation of the vehicle-fixed frame about the earth-fixed $Z$-axis (yaw) |
| $F_{F L x}, F_{F L y}, F_{F L z}$ | Suspension forces applied to the front left hardpoint along the vehicle-fixed $x$-, $y$-, and $z$-axes |
| $F_{F R x}, F_{F R y}, F_{F R z}$ | Suspension forces applied to the front right hardpoint along the vehiclefixed $x$-, $y$-, and $z$-axes |
| $F_{M L x}, F_{M L y}, F_{M L z}$ | Suspension forces applied to the middle left hardpoint along the vehiclefixed $x$-, $y$-, and $z$-axes |
| $F_{M R X}, F_{M R y}, F_{M R z}$ | Suspension forces applied to the middle right hardpoint along the vehiclefixed $x$-, $y$-, and $z$-axes |
| $F_{R L x}, F_{R L y}, F_{R L z}$ | Suspension forces applied to the rear left hardpoint along the vehicle-fixed $x$-, $y$-, and $z$-axes |
| $F_{R R x}, F_{R R y}, F_{R R z}$ | Suspension forces applied to the rear right hardpoint along the vehicle-fixed $x$-, $y$-, and $z$-axes |
| $M_{F L \chi}, M_{F L y}, M_{F L z}$ | Suspension moment applied to the front left hardpoint about the vehiclefixed $x$-, $y$-, and $z$-axes |
| $M_{F R x}, M_{F R y}, M_{F R z}$ | Suspension moment applied to the front right hardpoint about the vehiclefixed $x$-, $y$-, and $z$-axes |
| $M_{M L \chi}, M_{M L y}, M_{M L z}$ | Suspension moment applied to the middle left hardpoint about the vehiclefixed $x$-, $y$-, and $z$-axes |
| $M_{M R x}, M_{M R y}, M_{M R z}$ | Suspension moment applied to the middle right hardpoint about the vehiclefixed $x$-, $y$-, and $z$-axes |
| $M_{R L \chi}, M_{R L y}, M_{R L z}$ | Suspension moment applied to the rear left hardpoint about the vehiclefixed $x$-, $y$-, and $z$-axes |
| $M_{R R x}, M_{R R y}, M_{R R z}$ | Suspension moment applied to the rear right hardpoint about the vehiclefixed $x$-, $y$-, and $z$-axes |
| $F_{\text {extx }}, F_{\text {exty }}, F_{\text {extz }}$ | External forces applied to the vehicle CM along the vehicle-fixed $x$-, $y$-, and $z$-axes |
| $F_{d x}, F_{d y}, F_{d z}$ | Drag forces applied to the vehicle CM along the vehicle-fixed $x-, y$-, and $z$ axes |
| $M_{\text {extx }}, M_{\text {exty }}, M_{\text {extz }}$ | External moment about the vehicle CM about the vehicle-fixed $x-y$-, and $z$ axes |
| $M_{d x}, M_{d y}, M_{d z}$ | Drag moment about the vehicle CM about the vehicle-fixed $x$-, $y$-, and $z$-axes |
| $I$ | Vehicle body moments of inertia |
| $a, b, c$ | Distance of the front, middle, and rear axles, respectively, from the normal projection point of the vehicle CM onto the common axle plane |
| $h$ | Height of the vehicle CM above the axle plane |
| $d$ | Lateral distance from the geometric centerline to the center of mass along the vehicle-fixed $y$-axis |


| $h h f, h h_{-} r$ | Height of the front and rear hitches, respectively, above the axle plane along <br> the vehicle-fixed $z$-axis |
| :--- | :--- |
| $d h f, d L_{-} r$ | Longitudinal distance of the front and rear hitches, respectively, from the <br> normal projection point of the vehicle CM onto the common axle plane |
| $h l f, h l_{-} r$ | Lateral distance from center of mass to the front and rear hitches, <br> respectively, along the vehicle-fixed $y$-axis |
| $w_{F}, w_{M}, w_{R}$ | Front, middle, and rear track widths, respectively |
| $C_{d}$ | Air drag coefficient acting along the vehicle-fixed $x$-axis |
| $C_{s}$ | Air drag coefficient acting along the vehicle-fixed $y$-axis |
| $C_{l}$ | Air drag coefficient acting along the vehicle-fixed $z$-axis |
| $C_{r m}$ | Air drag roll moment acting about the vehicle-fixed $x$-axis |
| $C_{p m}$ | Air drag pitch moment acting about the vehicle-fixed $y$-axis |
| $C_{y m}$ | Air drag yaw moment acting about the vehicle-fixed $z$-axis |
| $A_{f}$ | Frontal area |
| $R$ | Atmospheric specific gas constant |
| $T$ | Environmental air temperature |
| $P_{a b s}$ | Environmental absolute pressure |
| $w_{x}, w_{y}, w_{z}$ | Wind speed along the vehicle-fixed $x-, y$-, and $z$-axes |
| $W_{x}, W_{y}, W_{z}$ | Wind speed along inertial $X$-, $Y$-, and $Z$-axes |

## Ports

## Input

## FSusp - Suspension forces on vehicle

3-by-6 array
Suspension longitudinal, lateral, and vertical suspension forces applied to the vehicle at the hardpoint location, in N , specified as a 3-by-6 array.

$$
F S u s p=\left[\begin{array}{llllll}
F_{F L x} & F_{F R x} & F_{M L x} & F_{M R x} & F_{R L x} & F_{R R x} \\
F_{F L y} & F_{F R y} & F_{M L y} & F_{M R y} & F_{R L y} & F_{R R y} \\
F_{F L z} & F_{F R z} & F_{M L z} & F_{M R z} & F_{R L z} & F_{R R z}
\end{array}\right]
$$

| Array Element | Axle | Track | Force Axis |
| :---: | :---: | :---: | :---: |
| FSusp (1,1) | Front | Left | Vehicle-fixed $x$-axis (longitudinal) |
| FSusp (1,2) | Front | Right |  |
| FSusp (1,3) | Middle | Left |  |
| FSusp (1,4) | Middle | Right |  |
| FSusp (1,5) | Rear | Left |  |
| FSusp (1,6) | Rear | Right |  |
| FSusp (2,1) | Front | Left | Vehicle-fixed $y$-axis (lateral) |


| Array Element | Axle | Track | Force Axis |
| :---: | :---: | :---: | :---: |
| FSusp (2,2) | Front | Right |  |
| FSusp (2,3) | Middle | Left |  |
| FSusp (2,4) | Middle | Right |  |
| FSusp (2,5) | Rear | Left |  |
| FSusp (2,6) | Rear | Right |  |
| FSusp (3,1) | Front | Left | Vehicle-fixed $z$-axis (vertical) |
| FSusp (3,2) | Front | Right |  |
| FSusp (3,3) | Middle | Left |  |
| FSusp ( 3,4 ) | Middle | Right |  |
| FSusp ( 3,5 ) | Rear | Left |  |
| FSusp (3,6) | Rear | Right |  |

MSusp - Suspension moment on vehicle
3-by-6 array
Suspension longitudinal, lateral, and vertical suspension moments applied about the vehicle at the hardpoint location, in N , specified as a 3-by-6 array.

$$
\text { MSusp }=\left[\begin{array}{llllll}
M_{F L x} & M_{F R x} & M_{M L x} & M_{M R x} & M_{R L x} & M_{R R x} \\
M_{F L y} & M_{F R z} & M_{M L y} & M_{M R y} & M_{R L y} & M_{R R y} \\
M_{F L z} & M_{F R z} & M_{M L z} & M_{M R z} & M_{R L z} & M_{R R z}
\end{array}\right]
$$

| Array Element | Axle | Track | Moment Axis |
| :---: | :---: | :---: | :---: |
| $\operatorname{MSusp}(1,1)$ | Front | Left | Vehicle-fixed $x$-axis (longitudinal) |
| MSusp (1,2) | Front | Right |  |
| MSusp (1,3) | Middle | Left |  |
| MSusp (1,4) | Middle | Right |  |
| MSusp (1,5) | Rear | Left |  |
| MSusp (1,6) | Rear | Right |  |
| MSusp (2,1) | Front | Left | Vehicle-fixed $y$-axis (lateral) |
| MSusp (2,2) | Front | Right |  |
| MSusp $(2,3)$ | Middle | Left |  |
| MSusp $(2,4)$ | Middle | Right |  |
| MSusp $(2,5)$ | Rear | Left |  |
| MSusp (2,6) | Rear | Right |  |
| MSusp (3,1) | Front | Left | Vehicle-fixed $z$-axis (vertical) |
| MSusp (3,2) | Front | Right |  |
| MSusp (3,3) | Middle | Left |  |
| MSusp (3,4) | Middle | Right |  |


| Array Element | Axle | Track | Moment Axis |
| :--- | :--- | :--- | :--- |
| MSusp $(3,5)$ | Rear | Left |  |
| MSusp $(3,6)$ | Rear | Right |  |
|  |  |  |  |

FExt - External forces acting on vehicle vector

External forces on the vehicle, in N, specified as a 1-by-3 or 3-by-1 vector.

| Array Element | Force Axis |
| :--- | :--- |
| FExt $(1,1)$ | Vehicle-fixed $x$-axis (longitudinal) |
| FExt $(1,2)$ or | Vehicle-fixed $y$-axis (lateral) |
| FExt $(2,1)$ |  |
| FExt $(1,3)$ or | Vehicle-fixed $z$-axis (vertical) |
| FExt $(3,1)$ |  |

MExt - External moments acting on vehicle
vector
External moments acting on the vehicle, in $\mathrm{N} \cdot \mathrm{m}$, specified as a 1-by-3 or 3-by-1 vector.

$$
\text { MExt }=M_{e x t}=\left[\begin{array}{lll}
M_{e x t_{x}} & M_{e x t_{y}} & M_{e x t_{z}}
\end{array}\right] o r\left[\begin{array}{l}
M_{\text {ext }} \\
M_{\text {ext }} \\
\\
M_{\text {ext }}
\end{array}\right]
$$

| Array Element | Force Axis |
| :--- | :--- |
| MExt $(1,1)$ | Vehicle-fixed $x$-axis (longitudinal) |
| MExt $(1,2)$ or <br> MExt $(2,1)$ | Vehicle-fixed $y$-axis (lateral) |
| MExt $(1,3)$ or <br> MExt $(3,1)$ | Vehicle-fixed $z$-axis (vertical) |

Fh - Hitch force on the body
array
Hitch force applied to the body at the hitch location, $F h_{x}, F h_{y}, F h_{z}$, in the vehicle-fixed frame, in N, specified as a 1-by-3 or 3-by-1 array.

## Dependencies

To enable this port, under Input signals, select Hitch forces.
Mh - Hitch moment about body array

Hitch moment at the hitch location, $M h_{x}, M h_{y}, M h_{z}$, about the vehicle-fixed frame, in $\mathrm{N} \cdot \mathrm{m}$, specified as a 1-by-3 or 3-by-1 array.

## Dependencies

To enable this port, under Input signals, select Hitch moments.
WindXYZ - Wind speed
array
Wind speed, $W_{x}, W_{y}, W_{z}$ along inertial $X-, Y$-, and $Z$-axes, in m/s, specified as a 1-by-3 or 3-by-1 array.

AirTemp - Ambient air temperature

## scalar

Ambient air temperature, $T_{\text {air }}$, in $K$, specified as a scalar.

## Dependencies

To enable this port, under Environment, select Air temperature.

## Output

Info - Vehicle body information
bus
Vehicle body information, returned as a bug signal containing the following values.

| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| InertFrm | Cg | Disp | X | Vehicle CM displacement along the earth-fixed $X$ axis | Computed | m |
|  |  |  | Y | Vehicle CM displacement along the earth-fixed $Y$ axis | Computed | m |
|  |  |  | Z | Vehicle CM displacement along the earth-fixed $Z$ axis | Computed | m |
|  |  | Vel | Xdot | Vehicle CM velocity along the earth-fixed $X$-axis | Computed | m/s |
|  |  |  | Ydot | Vehicle CM velocity along the earth-fixed $Y$-axis | Computed | m/s |
|  |  |  | Zdot | Vehicle CM velocity along the earth-fixed $Z$-axis | Computed | m/s |
|  |  | Ang | phi | Rotation of the vehiclefixed frame about the earth-fixed $X$-axis (roll) | Computed | rad |
|  |  |  | theta | Rotation of the vehiclefixed frame about the earth-fixed $Y$-axis (pitch) | Computed | rad |


| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | psi |  | Rotation of the vehiclefixed frame about the earth-fixed $Z$-axis (yaw) | Computed | rad |
| FrntAxl | Lft | Disp | X | Front left axle displacement along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Y | Front left axle displacement along the earth-fixed $Y$-axis | Computed | m |
|  |  |  | Z | Front left axle displacement along the earth-fixed Z-axis | Computed | m |
|  |  | Vel | $\begin{aligned} & \mathrm{Xdo} \\ & \mathrm{t} \end{aligned}$ | Front left axle velocity along the earth-fixed $X$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \text { Ydo } \\ & \mathrm{t} \end{aligned}$ | Front left axle velocity along the earth-fixed $Y$ axis | Computed | $\mathrm{m} / \mathrm{s}$ |
|  |  |  | $\begin{aligned} & \mathrm{Zdo} \\ & \mathrm{t} \end{aligned}$ | Front left axle velocity along the earth-fixed $Z$ axis | Computed | m/s |
|  | Rght | Disp | X | Front right axle displacement along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Y | Front right axle displacement along the earth-fixed $Y$-axis | Computed | m |
|  |  |  | Z | Front right axle displacement along the earth-fixed Z-axis | Computed | m |
|  |  | Vel | $\begin{aligned} & \text { Xdo } \\ & \mathrm{t} \end{aligned}$ | Front right axle velocity along the earth-fixed $X$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{Ydo} \\ & \mathrm{t} \end{aligned}$ | Front right axle velocity along the earth-fixed $Y$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{Zdo} \\ & \dagger \end{aligned}$ | Front right axle velocity along the earth-fixed $Z$ axis | Computed | m/s |
| Midlaxl | Lft | Disp | X | Middle left axle displacement along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Y | Middle left axle displacement along the earth-fixed $Y$-axis | Computed | m |


| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Z | Middle left axle displacement along the earth-fixed $Z$-axis | Computed | m |
|  |  | Vel | $\begin{aligned} & \mathrm{Xdo} \\ & \mathrm{t} \end{aligned}$ | Middle left axle velocity along the earth-fixed $X$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \text { Ydo } \\ & \mathrm{t} \end{aligned}$ | Middle left axle velocity along the earth-fixed $Y$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{Zdo} \\ & \mathrm{t} \end{aligned}$ | Middle left axle velocity along the earth-fixed Zaxis | Computed | m/s |
|  | Rght | Disp | X | Middle right axle displacement along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Y | Middle right axle displacement along the earth-fixed $Y$-axis | Computed | m |
|  |  |  | Z | Middle right axle displacement along the earth-fixed $Z$-axis | Computed | m |
|  |  | Vel | $\begin{aligned} & \mathrm{Xdo} \\ & \mathrm{t} \end{aligned}$ | Middle right axle velocity along the earth-fixed $X$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \text { Ydo } \\ & \mathrm{t} \end{aligned}$ | Middle right axle velocity along the earth-fixed $Y$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{Zdo} \\ & \mathrm{t} \end{aligned}$ | Middle right axle velocity along the earth-fixed Zaxis | Computed | m/s |
| RearAxl | Lft | Disp | X | Rear left axle displacement along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Y | Rear left axle displacement along the earth-fixed $Y$-axis | Computed | m |
|  |  |  | Z | Rear left axle displacement along the earth-fixed Z-axis | Computed | m |
|  |  | Vel | $\begin{aligned} & \mathrm{Xdo} \\ & \mathrm{t} \end{aligned}$ | Rear left axle velocity along the earth-fixed $X$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \text { Ydo } \\ & \mathrm{t} \end{aligned}$ | Rear left axle velocity along the earth-fixed $Y$ axis | Computed | m/s |


| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{aligned} & \mathrm{Zdo} \\ & \mathrm{t} \end{aligned}$ | Rear left axle velocity along the earth-fixed $Z$ axis | Computed | m/s |
|  | Rght | Disp | X | Rear right axle displacement along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Y | Rear right axle displacement along the earth-fixed $Y$-axis | Computed | m |
|  |  |  | Z | Rear right axle displacement along the earth-fixed Z-axis | Computed | m |
|  |  | Vel | $\begin{aligned} & \mathrm{Xdo} \\ & \mathrm{t} \end{aligned}$ | Rear right axle velocity along the earth-fixed $X$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \text { Ydo } \\ & \mathrm{t} \end{aligned}$ | Rear right axle velocity along the earth-fixed $Y$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{Zdo} \\ & \mathrm{t} \end{aligned}$ | Rear right axle velocity along the earth-fixed Zaxis | Computed | m/s |
| Hitch | Disp | X |  | Hitch offset from the axle plane along the earthfixed $X$-axis | Computed | m |
|  |  | Y |  | Hitch offset from the axle plane along the earthfixed $Y$-axis | Computed | m |
|  |  | Z |  | Hitch offset from the axle plane along the earthfixed $Z$-axis | Computed | m |
|  | Vel | Xdot |  | Hitch velocity along the earth-fixed $X$-axis | Computed | m/s |
|  |  | Ydot |  | Hitch velocity along the earth-fixed $Y$-axis | Computed | m/s |
|  |  | Zdot |  | Hitch velocity along the earth-fixed $Z$-axis | Computed | m/s |
| Geom | Disp | X |  | Vehicle chassis offset from the axle plane along the earth-fixed $X$-axis | Computed | m |
|  |  | Y |  | Vehicle chassis offset from center plane along the earth-fixed $Y$-axis | Computed | m |


| Signal |  |  |  | Description | Value | Units |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  |  |  |  |  | Vehicle chassis offset from <br> the axle plane along the <br> earth-fixed Z-axis | Computed |


| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | zddot |  | Vehicle CM acceleration along the vehicle-fixed $z$ axis | Computed | $\mathrm{m} / \mathrm{s}^{\wedge} 2$ |
|  | DCM | Direction cosine matrix |  |  | Computed | rad |
| Forces | Body | Fx |  | Net force on the vehicle CM along the vehiclefixed $x$-axis | Computed | N |
|  |  | Fy |  | Net force on the vehicle CM along the vehiclefixed $y$-axis | Computed | N |
|  |  | Fz |  | Net force on the vehicle CM along the vehiclefixed $z$-axis | Computed | N |
|  | Ext | Fx |  | External force on the vehicle CM along the vehicle-fixed $x$-axis | Input | N |
|  |  | Fy |  | External force on the vehicle CM along the vehicle-fixed $x$-axis | Input | N |
|  |  | Fz |  | External force on the vehicle CM along the vehicle-fixed $x$-axis | Input | N |
|  | FrntAxl | Lft | Fx | Front left axle velocity along the earth-fixed $Y$ axis | Computed | N |
|  |  |  | Fy | Lateral force on the left side of the front axle left along the vehicle-fixed $y$ axis | Computed | N |
|  |  |  | Fz | Normal force on the left side of the front axle along the vehicle-fixed $z$ axis | Computed | N |
|  |  | Rght | Fx | Longitudinal force on the right side of the front axle along the vehicle-fixed $x$ axis | Computed | N |
|  |  |  | Fy | Lateral force on the right side of the front axle left along the vehicle-fixed $y$ axis | Computed | N |
|  |  |  | Fz | Normal force on the right side of the front axle along the vehicle-fixed $z$ axis | Computed | N |



| Signal |  |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Hitch | Fx |  |  | Hitch force applied to the body at the hitch location along the vehicle-fixed $x$ axis | Computed | N |
|  |  | Fy |  |  | Hitch force applied to the body at the hitch location along the vehicle-fixed $y$ axis | Computed | N |
|  |  | Fz |  |  | Hitch force applied to the body at the hitch location along the vehicle-fixed $z$ axis | Computed | N |
|  | Tires | FrntTir es | $\begin{array}{l\|l} \hline \mathrm{L} & \prime \\ \mathrm{f} \\ \mathrm{t} \end{array},$ |  | Front left tire force along the vehicle-fixed $x$-axis | Computed | N |
|  |  |  |  | F | Front left tire force along the vehicle-fixed $y$-axis | Computed | N |
|  |  |  |  | $z$ | Front left tire force along the vehicle-fixed $z$-axis | Computed | N |
|  |  |  |  |  | Front right tire force along the vehicle-fixed $x$ axis | Computed | N |
|  |  |  |  |  | Front right tire force along the vehicle-fixed $y$ axis | Computed | N |
|  |  |  |  |  | Front right tire force along the vehicle-fixed $z$ axis | Computed | N |
|  |  | MidlTir es | $\begin{array}{l\|} \hline \mathrm{L} \\ \mathrm{f} \\ \mathrm{t} \end{array}$ | F | Middle left tire force along the vehicle-fixed $x$ axis | Computed | N |
|  |  |  |  | F | Middle left tire force along the vehicle-fixed $y$ axis | Computed | N |
|  |  |  |  | F | Middle left tire force along the vehicle-fixed $z$ axis | Computed | N |
|  |  |  | $R$ $F$ <br> g $\times$ <br> h  <br>   <br>   | F | Middle right tire force along the vehicle-fixed $x$ axis | Computed | N |
|  |  |  |  | F | Middle right tire force along the vehicle-fixed $y$ axis | Computed | N |
|  |  |  |  | F | Middle right tire force along the vehicle-fixed $z$ axis | Computed | N |


| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Signal |  | $\begin{aligned} & \text { RearTir } \\ & \text { es } \end{aligned}$ | L $F$ <br> f  <br> x  | Rear left tire force along the vehicle-fixed $x$-axis | Computed | N |
|  |  | $\begin{aligned} & \mathrm{t} \\ & \hline \mathrm{~F} \\ & \mathrm{y} \end{aligned}$ | Rear left tire force along the vehicle-fixed $y$-axis | Computed | N |
|  |  | F | Rear left tire force along the vehicle-fixed $z$-axis | Computed | N |
|  |  |  | Rear right tire force along the vehicle-fixed $x$-axis | Computed | N |
|  |  |  | Rear right tire force along the vehicle-fixed $y$-axis | Computed | N |
|  |  | $\begin{aligned} & \mathrm{F} \\ & \mathrm{z} \end{aligned}$ | Rear right tire force along the vehicle-fixed $z$-axis | Computed | N |
|  | Drag |  | Fx |  | Drag force on the vehicle CM along the vehiclefixed $x$-axis | Computed | N |
|  |  |  | Fy |  | Drag force on the vehicle CM along the vehiclefixed $y$-axis | Computed | N |
|  |  |  | Fz |  | Drag force on the vehicle CM along the vehiclefixed $z$-axis | Computed | N |
|  | Grvty |  | FX |  | Gravity force on the vehicle CM along the vehicle-fixed $x$-axis | Computed | N |
|  |  |  | Fy |  | Gravity force on the vehicle CM along the vehicle-fixed $y$-axis | Computed | N |
|  |  | Fz |  | Gravity force on the vehicle CM along the vehicle-fixed $z$-axis | Computed | N |
| Moments | Body | Mx |  | Body moment on the vehicle CM about the vehicle-fixed $x$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | My |  | Body moment on the vehicle CM about the vehicle-fixed $y$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | Mz |  | Body moment on the vehicle CM about the vehicle-fixed $z$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  | Drag | Mx |  | Drag moment on the vehicle CM about the vehicle-fixed $x$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |


| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Signal |  | My |  | Drag moment on the vehicle CM about the vehicle-fixed $y$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | Mz |  | Drag moment on the vehicle CM about the vehicle-fixed $z$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  | Ext | Mx |  | External moment on the vehicle CG about the vehicle-fixed $x$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | My |  | External moment on the vehicle CG about the vehicle-fixed $y$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | Mz |  | External moment on the vehicle CG about the vehicle-fixed $z$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  | Hitch | Mx |  | Hitch moment at the hitch location about vehiclefixed $x$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | My |  | Hitch moment at the hitch location about vehiclefixed $y$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | Mz |  | Hitch moment at the hitch location about vehiclefixed $z$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
| FrntAxl | Lft | Disp | x | Front left axle displacement along the vehicle-fixed $x$-axis | Computed | m |
|  |  |  | y | Front left axle displacement along the vehicle-fixed $y$-axis | Computed | m |
|  |  |  | z | Front left axle displacement along the vehicle-fixed $z$-axis | Computed | m |
|  |  | Vel | $\begin{aligned} & \mathrm{xdo} \\ & \mathrm{t} \end{aligned}$ | Front left axle velocity along the vehicle-fixed $x$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{ydo} \\ & \mathrm{t} \end{aligned}$ | Front left axle velocity along the vehicle-fixed $y$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{zdo} \\ & \mathrm{t} \end{aligned}$ | Front left axle velocity along the vehicle-fixed $z$ axis | Computed | m/s |
|  | Rght | Disp | X | Front right axle displacement along the vehicle-fixed $x$-axis | Computed | m |


| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Signal |  |  | y | Front right axle displacement along the vehicle-fixed $y$-axis | Computed | m |
|  |  |  | z | Front right axle displacement along the vehicle-fixed $z$-axis | Computed | m |
|  |  | Vel | $\begin{aligned} & \mathrm{xdo} \\ & \mathrm{t} \end{aligned}$ | Front right axle velocity along the vehicle-fixed $x$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{ydo} \\ & \mathrm{t} \end{aligned}$ | Front right axle velocity along the vehicle-fixed $y$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{zdo} \\ & \mathrm{t} \end{aligned}$ | Front right axle velocity along the vehicle-fixed $z$ axis | Computed | m/s |
| Midlaxl | Lft | Disp | x | Middle left axle displacement along the vehicle-fixed $x$-axis | Computed | m |
|  |  |  | y | Middle left axle displacement along the vehicle-fixed $y$-axis | Computed | m |
|  |  |  | z | Middle left axle displacement along the vehicle-fixed $z$-axis | Computed | m |
|  |  | Vel | $\begin{aligned} & \mathrm{xdo} \\ & \mathrm{t} \end{aligned}$ | Middle left axle velocity along the vehicle-fixed $x$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \text { ydo } \\ & t \end{aligned}$ | Middle left axle velocity along the vehicle-fixed $y$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{zdo} \\ & \mathrm{t} \end{aligned}$ | Middle left axle velocity along the vehicle-fixed $z$ axis | Computed | $\mathrm{m} / \mathrm{s}$ |
|  | Rght | Disp | X | Middle right axle displacement along the vehicle-fixed $x$-axis | Computed | m |
|  |  |  | y | Middle right axle displacement along the vehicle-fixed $y$-axis | Computed | m |
|  |  |  | z | Middle right axle displacement along the vehicle-fixed $z$-axis | Computed | m |
|  |  | Vel | $\begin{aligned} & \mathrm{xdo} \\ & \mathrm{t} \end{aligned}$ | Middle right axle velocity along the vehicle-fixed $x$ axis | Computed | m/s |


| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{aligned} & \mathrm{ydo} \\ & \mathrm{t} \end{aligned}$ | Middle right axle velocity along the vehicle-fixed $y$ axis | Computed | $\mathrm{m} / \mathrm{s}$ |
|  |  |  | $\begin{aligned} & \mathrm{zdo} \\ & \mathrm{t} \end{aligned}$ | Middle right axle velocity along the vehicle-fixed $z$ axis | Computed | m/s |
| RearAxl | Lft | Disp | x | Rear left axle displacement along the vehicle-fixed $x$-axis | Computed | m |
|  |  |  | y | Rear left axle displacement along the vehicle-fixed $y$-axis | Computed | m |
|  |  |  | z | Rear left axle displacement along the vehicle-fixed $z$-axis | Computed | m |
|  |  | Vel | $\begin{aligned} & \text { xdo } \\ & t \end{aligned}$ | Rear left axle velocity along the vehicle-fixed $x$ axis | Computed | $\mathrm{m} / \mathrm{s}$ |
|  |  |  | $\begin{aligned} & \mathrm{ydo} \\ & \mathrm{t} \end{aligned}$ | Rear left axle velocity along the vehicle-fixed $y$ axis | Computed | m/s |
|  |  |  | $\begin{aligned} & \mathrm{zdo} \\ & \mathrm{t} \end{aligned}$ | Rear left axle velocity along the vehicle-fixed $z$ axis | Computed | m/s |
|  | Rght | Disp | x | Rear right axle displacement along the vehicle-fixed $x$-axis | Computed | m |
|  |  |  | y | Rear right axle displacement along the vehicle-fixed $y$-axis | Computed | m |
|  |  |  | z | Rear right axle displacement along the vehicle-fixed $z$-axis | Computed | m |
|  |  | Vel | $\begin{aligned} & \mathrm{xdo} \\ & \mathrm{t} \end{aligned}$ | Rear right axle velocity along the vehicle-fixed $x$ axis | Computed | $\mathrm{m} / \mathrm{s}$ |
|  |  |  | $\begin{aligned} & \mathrm{ydo} \\ & \mathrm{t} \end{aligned}$ | Rear right axle velocity along the vehicle-fixed $y$ axis | Computed | $\mathrm{m} / \mathrm{s}$ |
|  |  |  | $\begin{aligned} & \mathrm{zdo} \\ & \mathrm{t} \end{aligned}$ | Rear right axle velocity along the vehicle-fixed $z$ axis | Computed | m/s |
| Hitch | Disp |  | x | Hitch offset from the axle plane along the vehiclefixed $x$-axis | Input | m |


| Signal |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | y | Hitch offset from center plane along the vehiclefixed $y$-axis | Input | m |
|  |  | z | Hitch offset from the axle plane along the vehiclefixed $z$-axis | Input | m |
|  | Vel | $\begin{aligned} & \mathrm{xdo} \\ & \mathrm{t} \end{aligned}$ | Hitch offset velocity along the vehicle-fixed $x$-axis | Computed | m/s |
|  |  | $\begin{aligned} & \mathrm{ydo} \\ & \mathrm{t} \end{aligned}$ | Hitch offset velocity along the vehicle-fixed $y$-axis | Computed | m/s |
|  |  | $\begin{aligned} & \mathrm{zdo} \\ & \mathrm{t} \end{aligned}$ | Hitch offset velocity along the vehicle-fixed $z$-axis | Computed | m/s |
| Pwr | PwrExt |  | Applied external power | Computed | W |
|  | Drag |  | Power loss due to drag | Computed | W |
| Geom | Disp | X | Vehicle chassis offset from the axle plane along the vehicle-fixed $x$-axis | Input | m |
|  |  | y | Vehicle chassis offset from center plane along the vehicle-fixed $y$-axis | Input | m |
|  |  | z | Vehicle chassis offset from the axle plane along the vehicle-fixed $z$-axis | Input | m |
|  | Vel | $\begin{aligned} & \mathrm{xdo} \\ & \mathrm{t} \end{aligned}$ | Vehicle chassis offset velocity along the vehiclefixed $x$-axis | Computed | m/s |
|  |  | $\begin{aligned} & \mathrm{ydo} \\ & \mathrm{t} \end{aligned}$ | Vehicle chassis offset velocity along the vehiclefixed $y$-axis | Computed | m/s |
|  |  | $\begin{aligned} & \mathrm{zdo} \\ & \mathrm{t} \end{aligned}$ | Vehicle chassis offset velocity along the vehiclefixed $z$-axis | Computed | m/s |
|  | Ang | $\begin{aligned} & \text { Bet } \\ & \mathrm{a} \end{aligned}$ | Body slip angle, $\beta$ $\beta=\frac{V_{y}}{V_{x}}$ | Computed | rad |

$\mathbf{V b}$ - Vehicle velocity along vehicle-fixed frame

## vector

Vehicle CM velocity along the vehicle-fixed $x$-, $y$-, $z$-axes, respectively, in $m / s$, returned as a vector.

## pqr - Vehicle angular velocity about vehicle-fixed frame

vector

Vehicle CM angular velocity about the vehicle-fixed $x$ - (roll rate), $y$ - (pitch rate), $z$-axes (yaw rate), respectively, in rad/s, returned as a vector.

DCM - Direction cosine matrix
array
Direction cosine matrix, in rad, returned as an array.
Euler - Euler angles
array
Euler angles, $\varphi, \theta$, and $\psi$, respectively, in rad, returned as an array.
Xe - Vehicle position in inertial reference frame vector

Vehicle CM position along inertial-fixed $X$-, $Y$-, $Z$-axes, respectively, in m, returned as a vector.
Ve - Vehicle velocity in inertial reference frame vector

Vehicle CM velocity along inertial-fixed $X$-, $Y$-, $Z$-axes, respectively, in $\mathrm{m} / \mathrm{s}$, returned as a vector.

## Parameters

## Block Options

Input Signals
Hitch forces - Create hitch force input port
off (default) | on
Select to create an input port, Fh, for the hitch forces.
Hitch moments - Create hitch moment input port
off (default) |on
Select to create an input port, Mh , for the hitch moments.

## Chassis

Vehicle mass, m - Mass
2000 (default) | scalar
Vehicle mass, $m$, in kg.
Longitudinal distance from center of mass to front axle, a - Distance from center of mass to front axle
1.4 (default) | scalar

Distance from the vehicle CM to the front axle, $a$, in m .


Longitudinal distance from center of mass to middle axle, b - Distance from center of mass to middle axle
1.6 (default) | scalar

Distance from the vehicle CM to the middle axle, $b$, in $m$.


Longitudinal distance from center of mass to rear axle, c - Distance from center of mass to rear axle
1.8 (default) | scalar

Distance from the vehicle CM to the rear axle, $c$, in m .


Lateral distance from geometric centerline to center of mass, $\mathbf{d}$ - Distance from geometric centerline to center of mass
0 (default) | scalar
Lateral distance from the geometric centerline to the CM, $d$, in m , along the vehicle-fixed $y$. Positive values indicate that the vehicle CM is to the right of the geometric centerline. Negative values indicate that the vehicle CM is to the left of the geometric centerline.

Vertical distance from center of mass to axle plane, $\mathbf{h}$ - Distance
. 35 (default) | scalar
Vertical distance from the vehicle CM to the axle plane, $h$, in $m$.


Longitudinal distance from center of mass to hitch, $\mathbf{d h}$ - Longitudinal distance from CM to hitch 1 (default) | scalar

Longitudinal distance from the CM to the hitch, $d h$, in m .


## Dependencies

To enable this parameter, on the Input signals pane, select Hitch forces or Hitch moments.
Longitudinal distance from center of mass to hitch, hl - Lateral distance from CM to hitch 0 (default) | scalar

Lateral distance from the CM to the hitch, $h l$, in $m$.


## Dependencies

To enable this parameter, on the Input signals pane, select Hitch forces or Hitch moments.
Vertical distance from hitch to axle plane, $\mathbf{h h}$ - Distance from hitch to axle plane 0.1 (default) | scalar

Vertical distance from the hitch to the axle plane, $h h$, in $m$.


## Dependencies

To enable this parameter, on the Input signals pane, select Hitch forces or Hitch moments.
Initial position in the inertial frame [Xeo, Yeo,ZZe], Xe_o - Initial position
[0,0,0] (default) | vector
Initial position of the vehicle in the inertial frame, $\mathrm{Xe}_{0}$, in m .
Initial velocity in body axes [xdot_o,ydot_o,zdot_o], xbdot_o - Initial velocity
[0,0,0] (default) | vector
Initial vehicle CM velocity along the vehicle-fixed $x, y$-, and $z$-axes, respectively, in $\mathrm{m} / \mathrm{s}$.
Initial Euler orientation [roll, pitch, yaw], eul_o - Initial Euler rotation
[0,0,0] (default) | vector
Initial Euler rotation of the vehicle-fixed frame about the earth-fixed $X$ - (roll), $Y$ - (pitch), $Z$-axes (yaw), respectively, in rad.

Initial body rotation rates [p,q,r], p_o - Initial rotation rate [0,0,0] (default) | vector

Initial vehicle CM angular velocity about the vehicle-fixed $x$ - (roll rate), $y$ - (pitch rate), $z$-axes (yaw rate), respectively, in rad/s.

Chassis inertia tensor, Iveh - Inertia
[430 0 0; 0 1900 0; 002100 ] (default)|array
Vehicle inertia tensor, $I_{\text {veh, }}$, in $\mathrm{kg}^{*} \mathrm{~m}^{\wedge} 2$. Dimensions are 3-by-3.
Track widths [front,rear], w - Widths
[1.9,1.9,1.9] (default) | vector
Front, middle, and rear track widths, $w f$, $w m$, and, $w r$, respectively, in m. Dimensions are 1-by-3.


## Inertial Loads

## Tractor Front

Mass, z1m - Tractor front mass
0 (default) | scalar
Mass, $z 1 \mathrm{~m}$, in kg.
Distance vector from front axle, z1R - Tractor front distance from front axle
[-.25,.125,.15] (default)|vector
Distance vector from front axle to load, $z 1 R$, in m. Dimensions are 1-by-3.

| Array Element | Description |
| :--- | :--- |
| z1R $(1,1)$ | Front suspension hardpoint to load, along the <br> vehicle-fixed $x$-axis |
| z1R $(1,2)$ | Vehicle centerline to load, along the vehicle-fixed $y$ - <br> axis |
| z1R $(1,3)$ | Front suspension hardpoint to load, along the <br> vehicle-fixed $z$-axis |

For example, this table summarizes the parameter settings that specify the load location.

| Example Location | Sign |
| :---: | :---: |
| - Forward of the front axle | - z1R $(1,1)<0$ |
| - Right of the vehicle centerline | - $\operatorname{ziR}(1,2)>0$ |
| - Above the front axle suspension hardpoint | - $\operatorname{z1R}(1,3)>0$ |

## Inertia tensor, z1I - Tractor front inertia

[1.4,-.2,.1;-.2,1.4,.1;.1,.1,2.25].*0 (default)|array
Inertia tensor, $z 11$, in $\mathrm{kg} \cdot \mathrm{m}^{\wedge} 2$. Dimensions are 3-by-3.

$$
z 1 I=\left[\begin{array}{lll}
I_{x x} & I_{x y} & I_{x z} \\
I_{y x} & I_{y y} & I_{y z} \\
I_{z x} & I_{z y} & I_{z z}
\end{array}\right]
$$

The tensor uses a coordinate system with an origin at the load CM.

- $x$-axis along the vehicle-fixed $x$-axis
- $y$-axis along the vehicle-fixed $y$-axis
- $z$-axis along the vehicle-fixed $z$-axis


## Cab Overhead

Mass, 22m - Cab overhead mass
0 (default) | scalar
Mass, $z 2 m$, in kg.
Distance vector from front axle, $\mathbf{z 2 R}$ - Cab overhead distance from front axle
[1.4,0, .8] (default) |vector
Distance vector from front axle to load, $z 2 R$, in $m$. Dimensions are 1-by- 3 .

| Array Element | Description |
| :--- | :--- |
| z2R $(1,1)$ | Front suspension hardpoint to load, along the <br> vehicle-fixed $x$-axis |
| z2R(1,2) | Vehicle centerline to load, along the vehicle-fixed $y-$ <br> axis |

Array Element
z2R(1,3)

## Description

Front suspension hardpoint to load, along the vehicle-fixed $z$-axis

For example, this table summarizes the parameter settings that specify the load location.

| Example Location | Sign |
| :--- | :--- |
| - | Rear of the front axle |
| - | Left of the vehicle centerline |
| - | Above the front axle suspension hardpoint |

Inertia tensor, z2I - Cab overhead inertia
[1.4,-.2,.1;-.2,1.4,.1;.1,.1,2.25].*0 (default)|array
Inertia tensor, $z 2 I$, in $\mathrm{kg} \cdot \mathrm{m}^{\wedge} 2$. Dimensions are 3-by-3.

$$
z 2 I=\left[\begin{array}{lll}
I_{x x} & I_{x y} & I_{x z} \\
I_{y x} & I_{y y} & I_{y z} \\
I_{z x} & I_{z y} & I_{z z}
\end{array}\right]
$$

The tensor uses a coordinate system with an origin at the load CM.

- $x$-axis along the vehicle-fixed $x$-axis
- $y$-axis along the vehicle-fixed $y$-axis
- $z$-axis along the vehicle-fixed $z$-axis


## Tractor Frame Left

Mass, z3m - Tractor frame left mass
0 (default) | scalar
Mass, $z 3 \mathrm{~m}$, in kg.
Distance vector from front axle, z3R - Tractor frame left distance from front axle
[. 75, -. 5, . 4] (default) | vector
Distance vector from front axle to load, $z 3 R$, in $m$. Dimensions are 1-by- 3 .

| Array Element | Description |
| :--- | :--- |
| z3R $(1,1)$ | Front suspension hardpoint to load, along the <br> vehicle-fixed $x$-axis |
| z3R $(1,2)$ | Vehicle centerline to load, along the vehicle-fixed $y$ - <br> axis |
| z3R $(1,3)$ | Front suspension hardpoint to load, along the <br> vehicle-fixed $z$-axis |

For example, this table summarizes the parameter settings that specify the load location.

| Example Location | Sign |
| :--- | :--- |
| - $\quad$ Rear of the front axle | - $\quad z 3 R(1,1)>0$ |
| - Left of the vehicle centerline | - $z 3 R(1,2)<0$ |
| - Above the front axle suspension hardpoint | - $\quad z 3 R(1,3)>0$ |

Inertia tensor, z3I - Tractor frame left inertia
[5,-.1,-2;-2,9,.1;-.1,.1,6].*0 (default)|array
Inertia tensor, $z 3 I$, in $\mathrm{kg} \cdot \mathrm{m}^{\wedge} 2$. Dimensions are 3-by-3.

$$
z 3 I=\left[\begin{array}{lll}
I_{x x} & I_{x y} & I_{x z} \\
I_{y x} & I_{y y} & I_{y z} \\
I_{z x} & I_{z y} & I_{z z}
\end{array}\right]
$$

The tensor uses a coordinate system with an origin at the load CM.

- $x$-axis along the vehicle-fixed $x$-axis
- $y$-axis along the vehicle-fixed $y$-axis
- $z$-axis along the vehicle-fixed $z$-axis


## Tractor Frame Right

Mass, z4m - Tractor frame right mass
0 (default) | scalar
Mass, $z 4 \mathrm{~m}$, in kg.
Distance vector from front axle, $\mathbf{z 4 R}$ - Tractor frame right distance from front axle [.75, .5, .4] (default)|vector

Distance vector from front axle to load, $z 4 R$, in m. Dimensions are 1-by-3.

| Array Element | Description |
| :--- | :--- |
| z4R $(1,1)$ | Front suspension hardpoint to load, along the <br> vehicle-fixed $x$-axis |
| z4R $(1,2)$ | Vehicle centerline to load, along the vehicle-fixed $y$ - <br> axis |
| Z4R $(1,3)$ | Front suspension hardpoint to load, along the <br> vehicle-fixed $z$-axis |

For example, this table summarizes the parameter settings that specify the load location.

| Example Location | Sign |
| :--- | :--- |
| - | Rear of the front axle |
| - | Right of the vehicle centerline |
| - | Above the front axle suspension hardpoint |

## Inertia tensor, $\mathbf{z 4 I}$ - Tractor frame right inertia

[5,-.1,-2;-2,9,.1;-.1,.1,6].*0 (default)|array

Inertia tensor, $z 4 I$, in $\mathrm{kg} \cdot \mathrm{m}^{\wedge} 2$. Dimensions are 3 -by-3.

$$
z 4 I=\left[\begin{array}{lll}
I_{x x} & I_{x y} & I_{x z} \\
I_{y x} & I_{y y} & I_{y z} \\
I_{z x} & I_{z y} & I_{z z}
\end{array}\right]
$$

The tensor uses a coordinate system with an origin at the load CM.

- $x$-axis along the vehicle-fixed $x$-axis
- $y$-axis along the vehicle-fixed $y$-axis
- $z$-axis along the vehicle-fixed $z$-axis


## Cab Left

Mass, z5m - Cab left mass
0 (default) | scalar
Mass, z5m, in kg.
Distance vector from front axle, $\mathbf{z 5 R}$ - Cab left distance from front axle [1.25,-. 5, .4] (default) | vector

Distance vector from front axle to load, $z 5 R$, in m. Dimensions are 1-by-3.

| Array Element | Description |
| :--- | :--- |
| $z 5 R(1,1)$ | Front suspension hardpoint to load, along the <br> vehicle-fixed $x$-axis |
| $z 5 R(1,2)$ | Vehicle centerline to load, along the vehicle-fixed $y$ - <br> axis |
| $z 5 R(1,3)$ | Front suspension hardpoint to load, along the <br> vehicle-fixed $z$-axis |

For example, this table summarizes the parameter settings that specify the load location.

| Example Location | Sign |
| :--- | :--- |
| - Rear of the front axle | - $\quad \mathrm{z5R}(1,1)>0$ |
| - Left of the vehicle centerline | - $\mathrm{z5R}(1,2)<0$ |
| - Above the front axle suspension hardpoint | • $\mathrm{z5R}(1,3)>0$ |

## Inertia tensor, z5I - Cab left inertia

[5,-.1,-2;-2,9,.1;-.1,.1,6].*0 (default)|array
Inertia tensor, $z 5 I$, in $\mathrm{kg} \cdot \mathrm{m}^{\wedge} 2$. Dimensions are 3-by-3.

$$
z 5 I=\left[\begin{array}{lll}
I_{x x} & I_{x y} & I_{x z} \\
I_{y x} & I_{y y} & I_{y z} \\
I_{z x} & I_{z y} & I_{z z}
\end{array}\right]
$$

The tensor uses a coordinate system with an origin at the load CM.

- $x$-axis along the vehicle-fixed $x$-axis
- $y$-axis along the vehicle-fixed $y$-axis
- $z$-axis along the vehicle-fixed $z$-axis


## Cab Right

Mass, z6m - Cab right mass
0 (default) | scalar
Mass, $z 6 \mathrm{~m}$, in kg.
Distance vector from front axle, z6R - Cab right distance from front axle
[1.25, -. 5, .4] (default)|vector
Distance vector from front axle to load, $z 6 R$, in m. Dimensions are 1-by-3.

| Array Element | Description |
| :--- | :--- |
| $z 6 R(1,1)$ | Front suspension hardpoint to load, along the <br> vehicle-fixed $x$-axis |
| $z 6 R(1,2)$ | Vehicle centerline to load, along the vehicle-fixed $y$ - <br> axis |
| $z 6 R(1,3)$ | Front suspension hardpoint to load, along the <br> vehicle-fixed $z$-axis |

For example, this table summarizes the parameter settings that specify the load location.

| Example Location | Sign |
| :--- | :--- |
| - Rear of the front axle | • $\quad \mathrm{z6R}(1,1)>0$ |
| - Right of the vehicle centerline | - $\quad \mathrm{z6R}(1,2)>0$ |
| - Above the front axle suspension hardpoint | - $\quad \mathrm{z6R}(1,3)>0$ |

Inertia tensor, $\mathbf{z 6 I}$ - Cab right inertia
[5,-.1,-2;-2,9,.1;-.1,.1,6].*0 (default)|array
Inertia tensor, $z 6 I$, in $\mathrm{kg} \cdot \mathrm{m}^{\wedge} 2$. Dimensions are 3-by-3.

$$
z 6 I=\left[\begin{array}{lll}
I_{x x} & I_{x y} & I_{x z} \\
I_{y x} & I_{y y} & I_{y z} \\
I_{z x} & I_{z y} & I_{z z}
\end{array}\right]
$$

The tensor uses a coordinate system with an origin at the load CM.

- $x$-axis along the vehicle-fixed $x$-axis
- $y$-axis along the vehicle-fixed $y$-axis
- $z$-axis along the vehicle-fixed $z$-axis


## Tractor Rear

Mass, $\mathbf{z 7 m}$ - Tractor rear mass
0 (default) | scalar

Mass, $z 7$, in kg.
Distance vector from front axle, $\mathbf{z 7 R}$ - Tractor rear mass distance from front axle [2,0, .25] (default) | vector

Distance vector from front axle to load, $z 7 R$, in m. Dimensions are 1-by-3.

| Array Element | Description |
| :--- | :--- |
| z7R $(1,1)$ | Front suspension hardpoint to load, along the <br> vehicle-fixed $x$-axis |
| z7R $(1,2)$ | Vehicle centerline to load, along the vehicle-fixed $y$ - <br> axis |
| z7R $(1,3)$ | Front suspension hardpoint to load, along the <br> vehicle-fixed $z$-axis |

For example, this table summarizes the parameter settings that specify the load location.

| Example Location | Sign |
| :--- | :--- |
| - | Rear of the front axle |
| - | Right of the vehicle centerline |
| - | Above the front axle suspension hardpoint |

Inertia tensor, z71 - Tractor rear inertia
[1.4,-.2,.1;-.2,1.4,.1;.1,.1,2.25].*0 (default)|array
Inertia tensor, $z 71$, in $\mathrm{kg} \cdot \mathrm{m}^{\wedge} 2$. Dimensions are 3-by-3.

$$
z 7 I=\left[\begin{array}{lll}
I_{x x} & I_{x y} & I_{x z} \\
I_{y x} & I_{y y} & I_{y z} \\
I_{z x} & I_{z y} & I_{z z}
\end{array}\right]
$$

The tensor uses a coordinate system with an origin at the load CM.

- $x$-axis along the vehicle-fixed $x$-axis
- $y$-axis along the vehicle-fixed $y$-axis
- $z$-axis along the vehicle-fixed $z$-axis


## Aerodynamic

Longitudinal drag area, Af - Vehicle cross-sectional area
2 (default) | scalar
Effective vehicle cross-sectional area, $A_{f}$ to calculate the aerodynamic drag force on the vehicle, in $\mathrm{m}^{\wedge} 2$.

Longitudinal drag coefficient, Cd - Air drag coefficient
. 3 (default) | scalar
Air drag coefficient, $C_{d}$, dimensionless.

## Longitudinal lift coefficient, CI - Air lift coefficient

. 1 (default) | scalar
Air lift coefficient, $C_{l}$, dimensionless.

## Longitudinal drag pitch moment, Cpm - Pitch drag

. 1 (default) | scalar
Longitudinal drag pitch moment coefficient, $C_{p m}$, dimensionless.
Relative wind angle vector, beta_w - Wind angle
[0:0.001:0.01] (default) | vector
Relative wind angle vector, $\beta_{w}$, in rad.
Side force coefficient vector, Cs - Side force drag
[0:0.01:0.1] (default) | vector
Side force coefficient vector coefficient, $C_{s}$, dimensionless.
Yaw moment coefficient vector, Cym - Yaw moment drag
[0:0.001:0.01] (default)| vector
Yaw moment coefficient vector coefficient, $C_{y m}$, dimensionless.

## Environment

## Absolute air pressure, Pabs - Pressure

101325 (default) | scalar
Environmental air absolute pressure, $P_{a b s}$, in Pa.
Air temperature, Tair - Ambient air temperature
273 (default) | scalar
Ambient air temperature, $T_{\text {air }}$ in K .
Dependencies
To enable this parameter, clear Air temperature.
Gravitational acceleration, $\mathbf{g}$ - Gravity
9.81 (default) | scalar

Gravitational acceleration, $g$, in $\mathrm{m} / \mathrm{s}^{\wedge} 2$.

## Simulation

Longitudinal velocity tolerance, xdot_tol - Tolerance
. 1 (default) | scalar
Longitudinal velocity tolerance, $x d o t_{\text {tol }}$, in $\mathrm{m} / \mathrm{s}$.
The block uses this parameter to avoid a division by zero when it calculates the body slip angle, $\beta$.
Geometric longitudinal offset from axle plane, longOff - Longitudinal offset
0 (default) | scalar

Vehicle chassis offset from the axle plane along the body-fixed $x$-axis, in $m$. When you use the 3D visualization engine, consider using the offset to locate the chassis independently of the vehicle CG.

## Geometric lateral offset from center plane, latOff - Lateral offset <br> 0 (default) | scalar

Vehicle chassis offset from center plane along the body-fixed $y$-axis, in $m$. When you use the 3D visualization engine, consider using the offset to locate the chassis independently of the vehicle CG.

Geometric vertical offset from axle plane, vertOff - Vertical offset
0 (default) | scalar
Vehicle chassis offset from the axle plane along the body-fixed $z$-axis, in m . When you use the 3D visualization engine, consider using the offset to locate the chassis independently of the vehicle CG.

Wrap Euler angles, wrapAng - Selection
on (default) | off
Wrap the Euler angles to the interval [-pi, pi]. For vehicle maneuvers that might undergo vehicle yaw rotations that are outside of the interval, consider clearing the parameter if you want to:

- Track the total vehicle yaw rotation.
- Avoid discontinuities in the vehicle state estimators.


## Version History

Introduced in R2020b

## References

[1] Gillespie, Thomas. Fundamentals of Vehicle Dynamics. Warrendale, PA: Society of Automotive Engineers (SAE), 1992.

## Extended Capabilities

C/C++ Code Generation
Generate C and C++ code using Simulink ${ }^{\circledR}$ Coder ${ }^{\mathrm{TM}}$.

## See Also

Vehicle Body 3DOF Longitudinal | Vehicle Body 6DOF | Vector Concatenate, Matrix Concatenate

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"

## Three-axis Inertial Measurement Unit

Implement three-axis inertial measurement unit (IMU)


## Libraries:

Vehicle Dynamics Blockset / Sensors

## Description

The Three-Axis Inertial Measurement Unit block implements an inertial measurement unit (IMU) containing a three-axis accelerometer and a three-axis gyroscope.

For a description of the equations and application of errors, see Three-axis Accelerometer (Aerospace Blockset) and Three-axis Gyroscope (Aerospace Blockset).

## Limitations

- Vibropendulous error, hysteresis affects, anisoelastic bias and anisoinertial bias are not accounted for in this block.
- This block is not intended to model the internal dynamics of different forms of the instrument.


## Ports

Input

## A_b - Actual accelerations

three-element vector
Actual accelerations in body-fixed axes, specified as a three-element vector, in selected units.
Data Types: double
$\mathbf{w}$ - Angular rates
three-element vector
Angular rates in body-fixed axes, specified as a three-element vector, in radians per second.
Data Types: double
w_dot - Angular accelerations
three-element vector
Angular accelerations in body-fixed axes, specified as a three-element vector, in radians per second squared.

Data Types: double
CG - Location of center of gravity
three-element vector

Location of the center of gravity, specified as a three-element vector, in selected units.
Data Types: double
g - Gravity
three-element vector
Gravity in body axis, specified as a three-element vector, in selected units.
Data Types: double

## Output

A_meas - Measured accelerations
three-element vector
Measured accelerations from the accelerometer, specified as a three-element vector, in selected units.
Data Types: double
w_meas - Measured angular rates
three-element vector
Measured angular rates from the gyroscope, specified as a three-element vector, in radians per second.

Data Types: double

## Parameters

## Main

Units - Units
Metric (MKS) (default)|English
Input and output units, specified as:

| Units | Acceleration | Length |
| :--- | :--- | :--- |
| Metric (MKS ) | Meters per second squared | Meters |
| English (British Imperial) | Feet per second squared | Feet |

## Programmatic Use

Block Parameter: units
Type: character vector
Values: 'Metric (MKS)'|'English'
Default: 'Metric (MKS)'
IMU location - IMU location
$\left[\begin{array}{lll}0 & 0 & 0\end{array}\right]$ (default) | three-element vector
The location of the IMU, which is also the accelerometer group location, from the vehicle center of gravity, along the vehicle-fixed axis. This measurement reference is the same for the center of gravity input. The units are in selected length units.

Programmatic Use
Block Parameter: imu
Type: character vector
Values: three-element vector
Default: '[0 0 0]'
Update rate - Update rate
0 (default) | real, double scalar
Update rate of the accelerometer and gyroscope, specified as a real, double scalar, in seconds. An update rate of 0 creates a continuous accelerometer and continuous gyroscope. If you select the Noise on parameter and the update rate is 0 , the block updates the noise at a rate of 0.1.

Tip If you:

- Update this parameter value to 0 (continuous)
- Configure a fixed-step solver for the model
you must also select the Automatically handle rate transition for data transfer check box in the Solver pane. This check box enables the software to handle rate transitions correctly.

```
Programmatic Use
Block Parameter: a_Ts
Type: character vector
Values: real, double scalar
Default: '0'
Accelerometer
Second order dynamics for accelerometer - Second-order dynamics
on (default) | off
```

To apply second-order dynamics to acceleration readings, select this check box.

```
Programmatic Use
Block Parameter: dtype_a
Type: character vector
Values:'on'|'off'
Default: 'on'
Accelerometer natural frequency (rad/sec) - Accelerometer natural frequency
190 (default) | real, double scalar
```

Natural frequency of the accelerometer, specified as a real, double scalar, in radians per second.

## Programmatic Use

Block Parameter: w_a
Type: character vector
Values: real, double scalar
Default: ' 190 '
Dependencies
To enable this parameter, select Second order dynamics for accelerometer.

Accelerometer damping ratio - Accelerometer damping ratio
0.707 (default) | real, double scalar

Damping ratio of the accelerometer, specified as a real, double scalar, with no dimensions.
Programmatic Use
Block Parameter: z_a
Type: character vector
Values: real, double scalar
Default: ' 0.707 '
Dependencies
To enable this parameter, select Second order dynamics for accelerometer.
Accelerometer scale factor and cross-coupling - Scale factor and cross coupling
[1 0 0; 0 1 0; 0 0 1] (default) | 3-by-3 matrix
Scale factor and cross-coupling, specified as a 3-by-3 matrix, to skew the accelerometer from body axes and to scale accelerations along body axes.

Programmatic Use
Block Parameter: a_sf_cc
Type: character vector
Values: 3-by-3 matrix
Default: '[1 0 0; 0 1 0; 00 1]'
Accelerometer measurement bias - Accelerometer measurement bias
[0 0 0] (default)|three-element vector
Long-term biases along the accelerometer axes, specified as a three-element vector, in selected acceleration units.

Programmatic Use
Block Parameter: a_bias
Type: character vector
Values: three-element vector
Default: '[0 0 0]'
Accelerometer upper and lower limits - Minimum and maximum values of acceleration
[-inf -inf -inf inf inf inf] (default)| six-element vector
Three minimum values and three maximum values of acceleration in each of accelerometer axes, specified as a six-element vector, in selected acceleration units.

Programmatic Use
Block Parameter: a_sat
Type: character vector
Values: six-element vector
Default: '[-inf -inf -inf inf inf inf]'
Gyroscope
Second-order dynamics for gyro - Gyroscope second-order dynamics
on (default) | off
To apply second-order dynamics to gyroscope readings, select this check box.

```
Programmatic Use
Block Parameter: dtype_g
Type: character vector
Values: 'on'|'off'
Default: 'on'
Gyro natural frequency (rad/sec) - Gyroscope natural frequency
190 (default) | real, double scalar
```

Natural frequency of the gyroscope, specified as a real, double scalar, in radians per second.

## Programmatic Use <br> Block Parameter: w_g

Type: character vector
Values: real, double scalar
Default: ' 190 '

## Dependencies

To enable this parameter, select Second-order dynamics for gyro.

## Gyro damping ratio - Gyroscope damping ratio

0.707 (default) | real, double scalar

Damping ratio of the gyroscope, specified as a real, double scalar, with no dimensions.

## Programmatic Use

Block Parameter: z_g
Type: character vector
Values: real, double scalar
Default: '0.707'

## Dependencies

To enable this parameter, select Second-order dynamics for gyro.
Gyro scale factors and cross-coupling - Gyroscope scale factors and cross-coupling
[1 0 0; 0 1 0; 0 0 1] (default)| 3-by-3 matrix
Gyroscope scale factors and cross-coupling, specified as a 3-by-3 matrix, to skew the gyroscope from body axes and to scale angular rates along body axes.

## Programmatic Use

Block Parameter: g_sf_cc
Type: character vector
Values: 3-by-3 matrix
Default: '[1 0 0; 0 1 0; 00 1]'
Gyro measurement bias - Gyroscope measurement bias
[0 0 0] (default)| three-element vector
Long-term biases along the gyroscope axes, specified as three-element vector, in radians per second.

[^4]Values: three-element vector
Default: '[0 0 0]'
G-sensitive bias - Maximum change in rates
[0 0 0] (default) | three-element vector
Maximum change in rates due to linear acceleration, specified as a three-element vector, in radians per second per g-unit.

Programmatic Use
Block Parameter: g_sens
Type: character vector
Values: three-element vector
Default: '[0 0 0]'
Gyro upper and lower limits - Minimum and maximum values of angular rates [-inf -inf -inf inf inf inf] (default)|six-element vector

Three minimum values and three maximum values of angular rates in each of the gyroscope axes, specified as a six-element vector, in radians per second.

## Programmatic Use

Block Parameter: g_sat
Type: character vector
Values: six-element vector
Default:'[-inf -inf -inf inf inf inf]'
Noise
Noise on - White noise
on (default) | off
To apply white noise to acceleration and gyroscope readings, select this check box.
Programmatic Use
Block Parameter: a_rand
Type: character vector
Values: 'on'|'off'
Default: 'on'
Noise seeds - Noise seeds
[23093 23094230952309623097 23098] (default) | six-element vector
Scalar seeds for the Gaussian noise generator for each axis of the accelerometer and gyroscope, specified as a six-element vector.

Programmatic Use
Block Parameter: a_seeds
Type: character vector
Values: six-element vector
Default: '[23093 23094230952309623097 23098]'

## Dependencies

To enable this parameter, select Noise on.

Noise power - Noise power

## [0.001 0.001 0.001 0.0001 0.0001 0.0001] (default)| six-element vector

Height of the power spectral density (PSD) of the white noise for each axis of the accelerometer and gyroscope, specified as a six-element vector, in:

- ( $\mathrm{m} / \mathrm{s}^{2}$ )/Hz for Metric (MKS)
- (ft/s²)/Hz for English

Programmatic Use
Block Parameter: a_pow
Type: character vector
Values: six-element vector
Default: '[0.001 0.001 0.001 0.0001 0.0001 0.0001]'
Dependencies
To enable this parameter, select Noise on.

## Version History

Introduced in R2020a

## References

[1] Rogers, R. M., Applied Mathematics in Integrated Navigation Systems, AIAA Education Series, 2000.

## Extended Capabilities

C/C++ Code Generation
Generate C and C++ code using Simulink ${ }^{\circledR}$ Coder ${ }^{\mathrm{TM}}$.

## See Also

Three-axis Gyroscope | Three-axis Accelerometer

## Motorcycle Body Longitudinal In-Plane

Longitudinal in-plane motorcycle vehicle motion


## Libraries:

Powertrain Blockset / Vehicle Dynamics
Vehicle Dynamics Blockset / Vehicle Body

## Description

The Motorcycle Body Longitudinal In-Plane block implements a longitudinal in-plane motorcycle body model to calculate longitudinal, vertical, and pitch motion. The block accounts for:

- Mass of the frame, rear arm, front upper fork, front lower fork, front wheel, and rear wheel
- In-plane dynamic effects of the frame, front lower fork, front wheel, rear wheel, rear suspension, front suspension, rear wheel damper, rear arm, and chain
- External forces, external moments, and aerodynamic drag
- Road incline
- Weight distribution between the axles due to acceleration

Consider using this block to represent motorcycle motion in powertrain and fuel economy studies, for example, in studies with heavy breaking or acceleration or road profiles that contain larger vertical changes.

The block uses rigid-body vehicle motion, suspension system forces, and wind and drag forces to calculate the forces on the motorcycle frames. The block then determines the position and velocity of motorcycle at the front and rear contact patches.

## Layout

To determine the rigid-body motorcycle motion, the block uses right-handed (RH) Cartesian reference frames systems attached to the motorcycle. $i, j$, and $k$ are orthogonal unit vectors attached to the frames.


| Frame | Variable in Figure | Description |
| :---: | :---: | :---: |
| Road | $x, z$ | Road-fixed coordinate system. $x$ is along road grade, and $z$ points downward. |
| Motorcycle main frame <br> - $i_{F r m}$ - Forward along vector given by $\theta_{f r m}$ <br> - $k_{\text {Frm }}$ - Downward <br> - $j_{\text {Frm }}$ - Orthogonal to motorcycle plane | $O_{\text {Frm }}$ | Main frame origin |
|  | $G_{\text {Frm }}$ | Center of mass (CM) of the main frame with respect to $O_{F r m}$, along $i_{F r m}$ and $k_{F r m}$, respectively |
|  | $G_{\text {Rdr }}$ | CM of the rider with respect to $O_{\text {Frm }}$, along $i_{F r m}$ and $k_{F r m}$, respectively |
|  | $\theta_{f r m}$ | Main frame rotation about $j_{\text {Frm }}$ |
| Upper fork <br> - $i_{\text {FrkU }}$ - Forward along vector given by $\theta_{f r m}$ <br> - $k_{\text {FrkUp }}$ - Downward | $O_{\text {FrkUp }}$ | Upper fork origin |


| Frame | Variable in Figure | Description |
| :---: | :---: | :---: |
| - $j_{F r k U p}$ - Orthogonal to motorcycle plane | $G_{\text {FrkUp }}$ | CM of the upper fork with respect to $O_{F r k U p}$, along $i_{F r k U_{p}}$ and $k_{F r k U_{p}}$, respectively |
| Lower fork <br> - $i_{\text {FrkLw }}$ - Forward along vector given by $\theta_{f r m}$ <br> - $k_{\text {FrkLw }}$ - Downward <br> - $j_{\text {FrkLw }}$ - Orthogonal to motorcycle plane | $O_{F}$ | Lower fork origin |
|  | $G_{\text {FrkLw }}$ | CM of the lower fork with respect to $O_{\text {FrkLw }}$, along $i_{F r k L w}$ and $k_{F r k L w}$, respectively |
| Rear arm <br> - $i_{\text {ArmRr }}$ - Forward along vector given by $\theta_{r a}$ <br> - $k_{\text {ArmRr }}$ - Downward <br> - $j_{\text {ArmRr }}$ - Orthogonal to motorcycle plane | $O_{\text {ArmRr }}$ | Rear arm origin |
|  | $G_{\text {ArmRr }}$ | CM of the rear arm with respect to $O_{\text {ArmRr }}$, along $i_{\text {ArmRr }}$ and $k_{\text {ArmRr }}$, respectively |
|  | $\theta_{r a}$ | Rear arm rotation about $j_{A r m R r}$ |
| Front wheel contact patch <br> - $i_{C P F}$ - Forward along vector given by road-fixed $x$ - axis <br> - $k_{C P F}$ - Downward along vector given by road-fixed $z$ - axis <br> - $j_{C P F}$ - Orthogonal to motorcycle plane | $O_{C p F}$ | Front wheel contact patch origin |
| Rear wheel contact patch <br> - $i_{C p R}$ - Forward along vector given by road-fixed $x$ - axis <br> - $k_{C P R}$ - Downward along vector given by road-fixed $z$ - axis <br> - $j_{C p R}$ - Orthogonal to motorcycle plane | $O_{C p R}$ | Rear wheel contact patch origin |

Use the parameters in this table to specify the geometric layout of your motorcycle.

| Parameter |  |  | Variable in Figure |
| :---: | :---: | :---: | :---: |
| Initial conditions | Position | Rear contact patch longitudinal coordinate, CpRrX0 | $O_{C P R}$ with respect to road-fixed coordinate system, along $x$ |
|  |  | Rear contact patch vertical coordinate, CpRrZo | $O_{C P R}$ with respect to road-fixed coordinate system, along z |
|  |  | Pitch angle of rear arm, ArmRrAng0 | $\theta_{r a}$ |
|  |  | Pitch angle of main frame, FrmAng0 | $\theta_{\text {Frm }}$ |


| Parameter |  |  | Variable in Figure $d_{f}$ |
| :---: | :---: | :---: | :---: |
|  |  | Fork length, FrkFrL0 |  |
| Frame |  | Center of mass location, FrmCmPxz | $G_{F r m}$ with respect to $O_{\text {Frm }}$, along $i_{\text {Frm }}$ and $k_{F r m}$, respectively |
|  |  | Length, FrmLen | FrmLen |
| Rider |  | Center of mass location, RdrCmPxz | $G_{\text {Rdr }}$ with respect to $O_{\text {Frm }}$, along $i_{\text {Frm }}$ and $k_{F r m}$, respectively |
| Front Fork | Upper | Position, FrkUpCmPxz | $G_{F r k U p}$ with respect to $O_{F r k U p}$, along $i_{F r k U p}$ and $k_{F r k U p}$, respectively |
|  |  | Offset, FrkOfs | FrkOfs |
|  | Lower | Position, FrkLwCmPxz | $G_{\text {FrkLw }}$ with respect to $O_{\text {FrkLw }}$, along $i_{F r k L w}$ and $k_{F r k L w}$, respectively |
| Rear Arm |  | Position, ArmRrCmPxz | $G_{\text {ArmRr }}$ with respect to $O_{\text {ArmRr }}$, along $i_{A r m R r}$ and $k_{A r m R r}$, respectively |
|  |  | Length, ArmRrLen | ArmRrLen |
| Wheels | Front | Radius, WhlFrR | WhlFrR |
|  | Rear | Radius, WhlRrR | WhlRrR |
| Suspension | Front | Equilibrium length, FrkLwL0 | $d_{f}$ |
|  | Rear | Equilibrium angle, ShkRrAng0 | $\theta_{\text {Frm }}$ |

## Input Signals

You can use these block parameters to create additional input ports. This table summarizes the settings.

| Input Signals Pane Parameter | Input Port | Description |
| :--- | :--- | :--- |
| External forces | FExt | External longitudinal and vertical forces <br> applied at equivalent rider and motorcycle <br> center of mass (CM). |
| External moments | MExt | External moment about equivalent rider and <br> motorcycle CM, for example, moment due to <br> rider physical motion. |
| External front wheel moment | MWhlF | External moment at the front wheel $G_{\text {WhlFr, for }}$ <br> example, wheel motors and external <br> intermittent friction-related disturbances. |
| External rear wheel moment | MWhlR | External moment at the rear wheel $G_{\text {WhlRr, }}$ for <br> example, wheel motors and external <br> intermittent friction-related disturbances. |
| Grade angle | Grade | Road grade angle. |
| Wind velocity | WindXYZ | Wind speed. |
| Ambient temperature | Temp | Ambient air temperature. Consider this option <br> if you want to vary the temperature during run- <br> time. |

## Suspension System

Use the Suspension type parameter to specify the type of suspension.

| Setting | Description |
| :--- | :--- |
| Simple | Block models the suspension force and moment as a spring- <br> damper system: <br> - <br> - Suspension force at the upper fork |
| User-defined | Input the suspension force and moment: <br> - FSuspF - Suspension force at the upper fork <br> - MSuspR - Suspension moment at the rear arm |

## Wind and Drag Forces

The block subtracts the wind speeds from the vehicle velocity components to obtain a net relative airspeed. To calculate the drag force and moments acting on the motorcycle, the block uses the net relative airspeed.

## Use in 3D Environment

To co-simulate in the Unreal Engine ${ }^{\circledR}$ and provide a motorcycle with the motion calculated by the Motorcycle Body Longitudinal In-Plane block:

1 Put the Simulation 3D Motorcycle block in your model.
2 Route these the Info bus port signals to the Simulation 3D Motorcycle input ports Translation and Rotation.

- PosOrgInert
- PosFwBdy
- PosRwBdy
- AngOrgInert


For more information about using the block in the 3D environment, see "Longitudinal Motorcycle Braking Test".

## Power Accounting

The block accounts for the power transferred, not transferred, and stored.

| Bus Signal |  |  | Description |
| :---: | :---: | :---: | :---: |
| PwrInfo | PwrTrnsfrd - Power transferred between blocks <br> - Positive signals indicate flow into block <br> - Negative signals indicate flow out of block | PwrFxExt | Mechanical power from longitudinal external force |
|  |  | PwrFzExt | Mechanical power from vertical external force |
|  |  | PwrMyExt | Mechanical power from external pitch moment |
|  | PwrNotTrnsfrd - Power crossing the block boundary, but not transferred <br> - Positive signals indicate an input <br> - Negative signals indicate a loss | PwrFxDrag | Mechanical power loss from longitudinal drag force |
|  |  | PwrFzDrag | Mechanical power loss from vertical lift |
|  |  | PwrMyDrag | Mechanical power loss from pitch moment drag |
|  | PwrStored - Stored energy rate of change <br> - Positive signals indicate an increase <br> - Negative signals indicate a decrease | PwrStoredGrvty | Rate change in gravitational potential energy |
|  |  | PwrStoredxdot | Rate of change of longitudinal kinetic energy |
|  |  | PwrStoredzdot | Rate of change of vertical kinetic energy |
|  |  | PwrStoredq | Rate of change of rotational pitch kinetic energy |
|  |  | PwrStoredFsFzSprng | Stored spring energy from front suspension |
|  |  | PwrStoredFsRzSprng | Stored spring energy from rear suspension |

## Ports

## Input

FCpF - Longitudinal and vertical forces at front wheel contact patch

## vector

Longitudinal and vertical forces at front wheel contact patch $O_{C P F}$, along $i_{C P F}$ and $k_{C p F}$, in N. Signal vector dimensions are [1×2] or [ $2 \times 1$ ].

FCpR - Longitudinal and vertical forces at rear wheel contact patch

## vector

Longitudinal and vertical forces at rear wheel contact patch $O_{C p R}$, along $i_{C p R}$ and $k_{C p R}$, in N. Signal vector dimensions are [ $1 \times 2$ ] or [ $2 \times 1$ ].

MDrvArmR - Drive chain moment at rear arm
scalar
Drive chain moment at rear arm $O_{A r m R r}$, about $j_{A r m R r}$, in $N \cdot \mathrm{~m}$.
MDrvFrm - Drive chain moment at frame
scalar
Drive chain moment at the frame $O_{F r m}$, about $j_{F r m}$, in $\mathrm{N} \cdot \mathrm{m}$.
FExt - External longitudinal and vertical forces at frame
vector
External longitudinal and vertical forces applied at equivalent rider and motorcycle center of mass (CM), along $i_{F r m}$ and $k_{F r m}$, in N. Signal vector dimensions are [ $1 \times 2$ ] or [ $2 \times 1$ ].

## Dependencies

To create this port, select External forces.
MExt - External moment about frame
scalar

External moment about equivalent rider and motorcycle $\mathrm{CM}, j_{F r m}$, for example, moment due to rider physical motion, in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

To create this port, select External moments.
MBrkF - Brake moment at front wheel
scalar
Brake moment at the front wheel $G_{W h l F r}$, about $j_{W h l F r}$, in $\mathrm{N} \cdot \mathrm{m}$.
MBrkR - Brake moment at rear wheel
scalar
Brake moment at the rear wheel $G_{W h l R r}$, about $j_{W h l R r}$, in $\mathrm{N} \cdot \mathrm{m}$.
MWhIF - External moment at front wheel
scalar
External moment at the front wheel $G_{W h l F r}$, in $\mathrm{N} \cdot \mathrm{m}$.
Dependencies
To create this port, select External front wheel moment.
MWhIR - External moment at rear wheel
scalar

External moment at the rear wheel $G_{W h l R r}$, in $\mathrm{N} \cdot \mathrm{m}$.
Dependencies
To create this port, select External rear wheel moment.

FSuspF - External suspension force at upper fork scalar

External suspension force at upper fork $O_{\text {FrkUp }}$, along $k_{F r k U p}$, in N .

## Dependencies

To create this port, set Suspension type to User-defined.
MSuspR - External suspension moment at rear arm
scalar
External suspension force at upper fork $O_{A r m R r}$, about $j_{A r m R r}$, in $\mathrm{N} \cdot \mathrm{m}$.

## Dependencies

To create this port, set Suspension type to User-defined.
Grade - Road grade angle scalar

Road grade angle, $\gamma$, in deg.

## Dependencies

To create this port, select Grade angle.
WindXYZ - Wind speed
array
Wind speed, $W_{X}, W_{Y}, W_{Z}$ along earth-fixed $X$-, $Y$-, and $Z$-axes, in $\mathrm{m} / \mathrm{s}$. Signal vector dimensions are [1×3] or [3×1].

## Dependencies

To create this port, select Wind velocity.
Temp - Ambient air temperature
scalar
Ambient air temperature, $T_{\text {air }}$, in K . Considering this option if you want to vary the temperature during run-time.

## Dependencies

To create this port, select Ambient temperature.

## Output

Info - Bus signal
bus
Bus signal containing these block calculations.

| Signal | Signal | Units |  |
| :--- | :--- | :--- | :--- |
| Geom | Pos0rgInert | Main frame position along <br> the earth-fixed axes | m |






| Signal |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Signal |  |  |  |  |  | Acc |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  |  | dfddot | Signal | Fork length acceleration | $\mathrm{m} / \mathrm{s}^{2}$ |  |
| Susp | Genrl | Rear | Moments | Mthetafrm | Rear suspension moment <br> at frame | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | Frnt | Forces | Fdf | Suspensive force at upper <br> fork | N |

VCpF - Longitudinal, lateral, and vertical velocity at front wheel contact patch vector

Longitudinal, lateral, and vertical velocity at front wheel contact patch $O_{C P F}$, along $i_{C P F}$ and $k_{C p F}$, in $\mathrm{m} / \mathrm{s}$. Signal vector dimensions are [1x3] or [3x1]. The lateral component is set to 0 .
$\mathbf{P C p F}$ - Longitudinal, lateral, and vertical position at front wheel contact patch vector

Longitudinal, lateral, and vertical position at front wheel contact patch $O_{C P F}$, along $i_{C P F}$ and $k_{C p F}$, in $m$. Signal vector dimensions are [ $1 \times 3$ ] or [ $3 \times 1$ ]. The lateral component is set to 0 .

VCpR - Longitudinal, lateral, and vertical velocity at rear wheel contact patch vector

Longitudinal,lateral, and vertical velocity at rear wheel contact patch $O_{C P R}$, along $i_{C P R}$ and $k_{C P R}$, in $\mathrm{m} / \mathrm{s}$. Signal vector dimensions are [ $1 \times 3$ ] or [ $3 \times 1$ ]. The lateral component is set to 0 .

PCpR - Longitudinal, lateral, and vertical position at rear wheel contact patch vector

Longitudinal, lateral, and vertical position at rear wheel contact patch $O_{C p R}$, along $i_{C p R}$, and $k_{C p R}$, in m . Signal vector dimensions are [ $1 \times 3$ ] or [ $3 \times 1$ ]. The lateral component is set to 0 .

ThetaFrm - Main frame pitch angle

## scalar

Main frame pitch angle, $\Theta_{\text {frm }}$, in rad.
ThetaArmR - Rear arm pitch angle
scalar
Rear arm pitch angle, $\Theta_{r a}$ in rad.

## Parameters

## Options

## Suspension type - Type of suspension

Simple (default) | User-defined
Use the Suspension type parameter to specify the type of suspension.

| Setting | Description |
| :--- | :--- |
| Simple | Block models the suspension force and moment as a spring- <br> damper system: |
|  | - Suspension force at the upper fork <br> - <br> User-defined <br> Input the suspension force and moment: <br> - FSuspF - Suspension force at the upper fork <br> - MSuspR - Suspension moment at the rear arm |

## Input signals

External forces - FExt input port
off (default) | on
Specify to create input port FExt.
External moments - MExt input port
off (default) | on
Specify to create input port MExt.
External front wheel moment - MWhlF input port
off (default) | on
Specify to create input port MWhlF. Consider using this port to input external moments such as wheel motors and external intermittent friction-related disturbances.

External rear wheel moment - MWhlR input port
off (default) | on
Specify to create input port MWhlR. Consider using this port to input external moments such as wheel motors and external intermittent friction-related disturbances.

Grade angle - Grade input port
on (default) | off
Specify to create input port Grade.
Wind velocity - WindXYZ input port
on (default) | off
Specify to create input port WindXYZ.
Ambient temperature - Temp input port off (default) | on

Specify to create input port Temp.

Layout


Use the parameters in this table to specify the geometric layout of your motorcycle.

| Parameter |  |  | Variable in Figure $O_{C P R}$ with respect to road-fixed coordinate system, along $x$ |
| :---: | :---: | :---: | :---: |
| Initial conditions | Position | Rear contact patch longitudinal coordinate, CpRrX0 |  |
|  |  | Rear contact patch vertical coordinate, CpRrZ0 | $O_{C p R}$ with respect to road-fixed coordinate system, along z |
|  |  | Pitch angle of rear arm, ArmRrAng0 | $\theta_{\text {ra }}$ |
|  |  | Pitch angle of main frame, FrmAng0 | $\theta_{\text {Frm }}$ |
|  |  | Fork length, FrkFrL0 | $d_{f}$ |


| Parameter |  |  | Variable in Figure |
| :---: | :---: | :---: | :---: |
| Frame |  | Center of mass location, FrmCmPxz | $G_{F r m}$ with respect to $O_{F r m}$, along $i_{F r m}$ and $k_{F r m}$, respectively |
|  |  | Length, FrmLen | FrmLen |
| Rider |  | Center of mass location, RdrCmPxz | $G_{\text {Rdr }}$ with respect to $O_{\text {Frm }}$, along $i_{\text {Frm }}$ and $k_{F r m}$, respectively |
| Front Fork | Upper | Position, FrkUpCmPxz | $G_{F r k U p}$ with respect to $O_{F r k U p}$, along $i_{F r k U_{p}}$ and $k_{F r k U_{p}}$, respectively |
|  |  | Offset, FrkOfs | FrkOfs |
|  | Lower | Position, FrkLwCmPxz | $G_{\text {FrkLw }}$ with respect to $O_{\text {FrkLw }}$, along $i_{F r k L w}$ and $k_{F r k L w}$, respectively |
| Rear Arm |  | Position, ArmRrCmPxz | $G_{\text {ArmRr }}$ with respect to $O_{\text {ArmRr }}$, along $i_{\text {ArmRr }}$ and $k_{\text {ArmRr }}$, respectively |
|  |  | Length, ArmRrLen | ArmRrLen |
| Wheels | Front | Radius, WhlFrR | WhlFrR |
|  | Rear | Radius, WhlRrR | WhlRrR |
| Suspension | Front | Equilibrium length, FrkLwL0 | $d_{f}$ |
|  | Rear | Equilibrium angle, ShkRrAng0 | $\theta_{\text {Frm }}$ |

## Frame

Center of mass location, FrmCmPxz - Frame location
[0.255, -0.02] (default)|vector
Center of mass location of the frame, $G_{F r m}$. Specified as a vector with respect to $O_{F r m}$, along $i_{\text {Frm }}$ and $k_{\text {Frm }}$, respectively.

Mass, FrmMass - Frame mass
223 (default) | scalar
Frame mass, FrmMass, in kg.
Mass moment of inertia, Frmlyy - Frame inertia
26.2 (default) | scalar

Mass moment of inertia, FrmIyy, in $\mathrm{kg} \cdot \mathrm{m}^{2}$.
Length, FrmLen - Frame length
0.730 (default) | scalar

Length of the frame, FrmLen, in m.

## Rider

Center of mass location, RdrCmPxz - Rider location
[0.275, -0.61] (default)|vector
Center of mass location of the rider, $G_{R d r}$. Specified as a vector with respect to $O_{F r m}$, along $i_{F r m}$ and $k_{\text {Frm }}$, respectively.

Mass, RdrMass - Rider mass
78 (default) | scalar
Rider mass, RdrMass, in kg.
Mass moment of inertia, Rdrlyy - Rider inertia
26.2 (default) | scalar

Rider mass moment of inertia, RdrIyy, in $\mathrm{kg} \cdot \mathrm{m}^{2}$.
Front Fork - Upper
Position, FrkUpCmPxz - Upper fork location
[0.023, -0.098] (default)| vector
Center of mass location of the upper fork, $G_{F r k U p}$. Specified as a vector with respect to $O_{\text {FrkUp }}$, along $i_{F r k U_{p}}$ and $k_{F r k U p}$, respectively.

Mass, FrkUpMass - Upper fork mass
8.8 (default) | scalar

Upper fork mass, FrkUpMass, in kg.
Mass moment of inertia, Frmlyy - Upper fork inertia
0.14 (default) | scalar

Upper fork mass moment of inertia, FrkUpIyy, in $\mathrm{kg} \cdot \mathrm{m}^{2}$.
Offset, FrkOfs - Upper fork offset
0.034 (default) | scalar

Upper fork offset, FrkOfs, in m.

## Front Fork - Lower

Position, FrkLwCmPxz - Lower fork location
[-0.029, -0.189] (default) | vector
Center of mass location of the lower fork, $G_{F r k L w}$. Specified as a vector with respect to $O_{\text {FrkLw, }}$ along $i_{\text {FrkLw }}$ and $k_{\text {FrkLw, }}$, respectively.

Mass, FrkLwMass - Lower fork mass
7.0 (default) | scalar

Lower fork mass, FrkLwMass, in kg.
Mass moment of inertia, FrkLwlyy - Lower fork inertia 0.18 (default) | scalar

Lower fork mass moment of inertia, FrkLwIyy, in $\mathrm{kg} \cdot \mathrm{m}^{2}$.

## Rear Arm

Position, ArmRrCmPxz - Rear arm location
[0.275, - 0.052] (default) | vector

Center of mass location of the rear arm, $G_{A r m R r}$. Specified as a vector with respect to $O_{A r m R r}$, along $i_{\text {ArmRr }}$ and $k_{\text {ArmRr }}$, respectively.

Mass, ArmRrMass - Rear arm mass
10 (default) | scalar
Rear arm mass, ArmRrMass, in kg.
Mass moment of inertia, ArmRrlyy - Rear arm inertia
0.8 (default) | scalar

Rear arm mass moment of inertia, ArmRrIyy, in $\mathrm{kg} \cdot \mathrm{m}^{2}$.
Length, ArmRrLen - Rear arm length
0.535 (default) | scalar

Rear arm length, ArmRrLen, in m.
Wheels - Front
Mass, WhIFrMass - Front wheel mass
12 (default) | scalar
Front wheel mass, WhlFrMass, in kg.
Radius, WhIFrR - Front wheel radius
0.3 (default) | scalar

Front wheel radius, WhlFrR, in m.

## Wheels - Rear

Mass, WhIRrMass - Rear wheel mass
16.2 (default) | scalar

Rear wheel mass, WhlRrMass, in kg.
Radius, WhIRrR - Rear wheel radius
0.33 (default) | scalar

Rear wheel radius, $W h l R r R$, in $m$.

## Suspension - Front

Stiffness, SuspFrK - Front suspension stiffness
25e3 (default) | scalar
Front suspension stiffness at $O_{F r k U p}$, along $k_{F r k U p}$, in $\mathrm{N} / \mathrm{m}$.
Damping, SuspFrC - Front suspension damping
1250 (default) | scalar
Front suspension damping, at $O_{F r k U p}$, along $k_{F r k U p}$, in $\mathrm{N} \cdot \mathrm{s} / \mathrm{m}$.
Equilibrium length, FrkLwLO - Front suspension equilibrium length
0.473 (default) | scalar

Front suspension equilibrium length, $d_{f}$, in $m$.
Suspension - Rear
Stiffness, SuspRrK - Rear arm suspension stiffness
1500 (default) | scalar
Rear arm suspension stiffness at $O_{A r m R r}$, about $j_{\text {ArmRr }}$, in $\mathrm{N} / \mathrm{rad}$.
Damping, SuspRrC - Rear arm suspension damping
150 (default) | scalar
Rear arm suspension damping at $O_{\text {ArmRr, }}$, about $j_{A r m R r}$, in $\mathrm{N} \cdot \mathrm{s} / \mathrm{rad}$.
Equilibrium angle, ShkRrAng0 - Rear suspension equilibrium angle
0 (default) | scalar
Rear suspension equilibrium angle, $\theta_{\text {Frm }}$, in rad.

## Aerodynamic

## Longitudinal drag area, Af - Area

2 (default) | scalar
Effective vehicle cross-sectional area, $A_{f}$ to calculate the aerodynamic drag force on the vehicle, in $\mathrm{m}^{2}$.

## Longitudinal drag coefficient, Cd - Drag

. 2 (default) | scalar
Air drag coefficient, $C_{d}$, dimensionless.
Longitudinal lift coefficient, CI - Lift
. 1 (default) | scalar
Air lift coefficient, $C_{l}$, dimensionless.
Longitudinal drag pitch moment, Cpm - Pitch drag
. 1 (default) | scalar
Longitudinal drag pitch moment coefficient, $C_{p m}$, dimensionless.
Pitch moment length, Lcpm - Pitch drag
2 (default) | scalar
Pitch moment length, Lcpm, in m.

## Environment

Gravitational acceleration, $\mathbf{g}$ - Gravity
9.80665 (default) | scalar

Gravitational acceleration, $g$, in $\mathrm{m} / \mathrm{s}^{2}$.
Absolute air pressure, Pabs - Pressure
101325 (default) | scalar

Environmental air absolute pressure, $P_{\text {abs }}$, in Pa.
Air temperature, Tair - Ambient air temperature
273 (default) | scalar
Ambient air temperature, $T_{\text {air }}$, in K.

## Dependencies

To enable this parameter, clear Ambient temperature.

## Initial conditions

## Position

Rear contact patch longitudinal coordinate, CpRrX0 - Longitudinal coordinate
0 (default) | scalar
Rear contact patch longitudinal coordinate, $O_{C p R}$, with respect to road-fixed coordinate system, along $x$, in m.

Rear contact patch vertical coordinate, CpRrZO - Vertical coordinate
0 (default) | scalar
Rear contact patch vertical coordinate, $O_{C p R}$, with respect to road-fixed coordinate system, along z, in m.

Pitch angle of rear arm, ArmRrAng0 - Rear arm angle
0.0590379 (default) | scalar

Pitch angle of rear arm, $\theta_{r a}$ in rad.
Pitch angle of main frame, FrmAng0 - Angle length
0.377024 (default) | scalar

Pitch angle of main frame, $\theta_{\text {Frm }}$, in rad.
Fork length, FrkFrLO - Fork length
0.4262193 (default) | scalar

Fork length, $d_{f}$ in m .

## Velocity

Longitudinal velocity of rear contact patch - Longitudinal velocity
0 (default) | scalar
Rear contact patch longitudinal coordinate, $\dot{O}_{C p R}$, with respect to road-fixed coordinate system, along $x$, in $\mathrm{m} / \mathrm{s}$.

Vertical velocity of rear contact patch, CpRrVz0 - Vertical velocity
0 (default) | scalar
Vertical velocity of rear contact patch, $\dot{O}_{C p R}$, with respect to road-fixed coordinate system, along $z$, in $\mathrm{m} / \mathrm{s}$.

Pitch rate of rear arm, ArmRrAngV0 - Pitch rate 0 (default) | scalar

Pitch rate of rear arm, $\dot{\theta}_{r a}$, in rad/s.
Pitch rate of main frame, FrmAngV0 - Pitch rate
0 (default) | scalar
Pitch rate of main frame, $\dot{\theta}_{F r m}$, in rad/s.
Lower fork deformation velocity, FrkLwV0 - Deformation velocity
0 (default) | scalar
Lower fork deformation velocity, $\dot{d}_{f}$, in $\mathrm{m} / \mathrm{s}$.

## Coordinate Offsets

Longitudinal offset, longOff - Longitudinal offset
0 (default) | scalar
Vehicle main frame offset along the earth-fixed $X$-axis, in m.
Lateral offset, latOff - Lateral offset
0 (default) | scalar
Vehicle main frame offset along the earth-fixed $Y$-axis, in $m$.
Vertical offset, vertOff - Vertical offset
0 (default) | scalar
Vehicle main frame offset along the earth-fixed $Z$-axis, in $m$.
Roll offset, pitchOff - Roll offset
0 (default) | scalar
Vehicle main frame offset about the earth-fixed $X$-axis, in rad.
Pitch offset, pitchOff - Pitch offset
0 (default) | scalar
Vehicle main frame offset about the earth-fixed $Y$-axis, in rad.
Yaw offset, pitchOff - Yaw offset
0 (default) | scalar
Vehicle main frame offset about the earth-fixed $Z$-axis, in rad.

Introduced in R2021b

## References

[1] Giner, David Moreno. "Symbolic-Numeric Tools for the Analysis of Motorcycle Dynamics. Development of a Virtual Rider for Motorcycles Based on Model Predictive Control." PhD diss., Universidad Miguel Hernández de Elche, 2016.

## Extended Capabilities

C/C++ Code Generation
Generate C and $\mathrm{C}++$ code using Simulink $®$ Coder $^{\mathrm{TM}}$.

## See Also

Motorcycle Chain
Topics
"Coordinate Systems in Vehicle Dynamics Blockset"
"Longitudinal Motorcycle Braking Test"

## Motorcycle Chain

## Implement motorcycle chain



## Libraries:

Powertrain Blockset / Drivetrain / Couplings
Vehicle Dynamics Blockset / Powertrain / Drivetrain / Couplings

## Description

The Motorcycle Chain block implements the dynamic effects of a motorcycle chain on the Motorcycle Body Longitudinal In-Plane block, including dynamic tension and moment drive coupling.

This figure shows how the chain relates geometrically to the motorcycle frame, rear arm, and rear wheel.


| Frame | Variable in <br> Figure | Description |
| :--- | :--- | :--- |
| Motorcycle main frame | $O_{m}$ | Main frame origin |
| - $x_{m}$ - Forward along vector pointing to front fork |  |  |
| - $z_{m}$ - Downward |  |  |
| - $\quad y_{m}$ - Orthogonal to motorcycle plane |  |  |

## Ports

Input
MDshft - Drive shaft moment on front sprocket
scalar
Drive shaft moment on front sprocket about $y_{m}$, in $\mathrm{N} \cdot \mathrm{m}$.

FCpR - Longitudinal and vertical forces at rear wheel contact patch vector

Longitudinal and vertical forces at rear wheel contact patch $O_{C p R}$, along $i_{C p R}$ and $k_{C p R}$, in N. Signal vector dimensions are [1×2] or [2×1].

ThetaFrm - Main frame pitch angle scalar

Main frame pitch angle, $\Theta_{f r m}$, in rad.
ThetaArmR - Rear arm pitch angle scalar

Rear arm pitch angle, $\Theta_{r a}$, in rad.
MBrkR — Brake moment at rear wheel
scalar
Brake moment at the rear wheel $G_{W h l R r}$, about $j_{W h l R r}$, in $\mathrm{N} \cdot \mathrm{m}$.
AngAWhIR - Rear wheel angular acceleration
scalar
Rear wheel angular acceleration, in rad/s ${ }^{2}$.

## Output

Info - Bus signal
bus
Bus signal containing these block calculations.

| Signal | Description | Units |
| :--- | :--- | :--- |
| FChn | Chain force applied to rear arm | N |
| AngVSprtR | Angular velocity of rear <br> sprocket | $\mathrm{rad} / \mathrm{s}$ |
| MDrvSprtR | Wheel damper moment applied <br> to rear sprocket | $\mathrm{N} \cdot \mathrm{m}$ |
| WhlDmpAng | Angle between rear sprocket <br> and rear wheel | rad |

MDrvSprtR - Wheel damper moment at rear sprocket
scalar
Wheel damper moment applied to rear sprocket, in $N \cdot m$.
MDrvArmR - Drive chain moment at rear arm
scalar
Drive chain moment at rear arm $O_{A r m R r}$, about $j_{A r m R r}$, in $N \cdot \mathrm{~m}$.
MDrvFrm - Drive chain moment at frame
scalar

Drive chain moment at the frame $O_{\text {Frm }}$, about $j_{F r m}$, in $\mathrm{N} \cdot \mathrm{m}$.

## Parameters

This figure shows how the chain relates geometrically to the motorcycle frame, rear arm, and rear wheel.


## Front Sprocket

Coordinates, SprktFrPxz - Front sprocket position
[0.05-0.05] (default) | vector
Position of front sprocket, SprktFrPxz, along $x_{m} z_{m}$, respectively, in $m$.
Mass moment of inertia, SprktFrlyy - Front sprocket inertia
0.005 (default) | scalar

Front sprocket mass moment of inertia, SprktFrIyy, in $\mathrm{kg} \cdot \mathrm{m}^{2}$.
Radius, SprktFrR - Front sprocket radius
0.04 (default) | scalar

Front sprocket radius, SprktFrR, in m.

## Rear Sprocket

Mass moment of inertia, SprktRrlyy - Rear sprocket inertia
0.01 (default) | scalar

Rear sprocket mass moment of inertia, SprktRrIyy, in $\mathrm{kg} \cdot \mathrm{m}^{2}$.
Radius, SprktRrR - Rear sprocket radius
0.12 (default) | scalar

Rear sprocket radius, SprktRrR, in m.

## Rear Wheel

Mass moment of inertia, WhIRrlyy - Rear wheel inertia
0.66 (default) | scalar

Rear wheel mass moment of inertia, WhlRrIyy, in $\mathrm{kg} \cdot \mathrm{m}^{2}$.

Radius, WhIRrR - Rear wheel radius
0.33 (default) | scalar

Rear wheel radius, WhlRrR, in m.

## Swing Arm

Arm length, ArmRrLen - Swing arm length
0.535 (default) | scalar

Arm length, ArmRrLen, in m.

## Wheel Damper

Stiffness, WhIDmpK - Wheel damper stiffness
le4 (default) | scalar
Wheel damper stiffness, WhlDmpK, in N/rad.
Damping, WhIDmpC - Wheel damping
1e2 (default) | scalar
Wheel damper damping, WhlDmpC, in $\mathrm{N} \cdot \mathrm{s} / \mathrm{rad}$.
Equilibrium angle - Wheel damper equilibrium angle
-15e-3 (default) | scalar
Equilibrium angle, WhlDmpAng0, in rad.
Initial Conditions
Rear sprocket angular velocity, SprktRrAngV0 - Angular velocity
0 (default) | scalar
Rear sprocket angular velocity, SprktRrAngV0, in rad/s.
Rear wheel angular velocity, WhIRrAngV0 - Angular velocity
0 (default) | scalar
Rear wheel angular velocity, WhlRrAngV0, in rad/s.

## Version History

Introduced in R2021b

## References

[1] Giner, David Moreno. "Symbolic-Numeric Tools for the Analysis of Motorcycle Dynamics. Development of a Virtual Rider for Motorcycles Based on Model Predictive Control." PhD diss., Universidad Miguel Hernández de Elche, 2016.

## Extended Capabilities

C/C++ Code Generation
Generate C and C++ code using Simulink ${ }^{\circledR}$ Coder $^{\mathrm{TM}}$.

## See Also

Motorcycle Body Longitudinal In-Plane

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"

## Vehicle Scenario Blocks

## Drive Cycle Source

Standard or specified longitudinal drive cycle


## Libraries:

Powertrain Blockset / Vehicle Scenario Builder
Vehicle Dynamics Blockset / Vehicle Scenarios / Drive Cycle and Maneuvers

## Description

The Drive Cycle Source block generates a standard or user-specified longitudinal drive cycle. The block output is the specified vehicle longitudinal speed, which you can use to:

- Predict the engine torque and fuel consumption that a vehicle requires to achieve desired speed and acceleration for a given gear shift reference.
- Produce realistic velocity and shift references for closed loop acceleration and braking commands for vehicle control and plant models.
- Study, tune, and optimize vehicle control, system performance, and system robustness over multiple drive cycles.
- Identify the faults within tolerances specified by standardized tests, including:
- EPA dynamometer driving schedules ${ }^{1}$
- Worldwide Harmonised Light Vehicle Test Procedure (WLTP) laboratory tests ${ }^{2}$

For the drive cycles, you can use:

- Drive cycles from predefined sources. By default, the block includes the FTP-75 drive cycle. To install additional drive cycles from a support package, see "Support Package for Maneuver and Drive Cycle Data". The support package has drive cycles that include the gear shift schedules, for example JC08 and CUEDC.
- Workspace variables that define your own drive cycles.
- .mat, .xls, .xlsx, or .txt files.
- Wide open throttle (WOT) parameters, including initial and nominal reference speed, deceleration start time, and final reference speed.

To achieve the goals listed in the table, use the specified Drive Cycle Source block parameter options.

| Goal | Action |
| :--- | :--- |
| Repeat the drive cycle if the <br> simulation run time exceeds <br> the drive cycle length. | Select Repeat cyclically. |
| Output the acceleration, as <br> calculated by Savitzky-Golay <br> differentiation. | Select Output acceleration. |


| Goal | Action |
| :---: | :---: |
| Specify a sample period for discrete applications. | Specify a Output sample period (0 for continuous), dt parameter. |
| Update the simulation run time so that it equals the length of the drive cycle. | Click Update simulation time. If a model configuration reference exists, the block does not enable this option. |
| Plot the drive cycle in a MATLAB ${ }^{\circledR}$ figure. | Click Plot drive cycle. |
| Specify the drive cycle using a workspace variable. | Click Specify variable. The block: <br> - Sets the Drive cycle source parameter to Workspace variable. <br> - Enables the From workspace parameter. <br> Specify the workspace variable so that it contains time, velocity, and, optionally, the gear shift schedule. For examples, see "Create Drive Cycles Using Workspace Variables" on page 6-5. |
| Specify the drive cycle using a file. | Click Select file. The block: <br> - Sets the Drive cycle source parameter to .mat, .xls, .xlsx or .txt file. <br> - Enables the Drive cycle source file parameter. <br> Specify a file that contains time, velocity, and, optionally, the gear shift schedule. |
| Output drive cycle gear. | Specify a drive cycle that contains a gear shift schedule. You can use: <br> - A support package to install standard drive cycles that include the gear shift schedules, for example JC08 and CUEDC. <br> - Workspace variables. <br> - .mat, .xls, .xlsx, or .txt files. <br> Click Output gear shift data. |
| Install additional drive cycles from a support package. | Click Install additional drive cycles. The block enables the parameter if you can install additional drive cycles from a support package. |
| Identify drive cycle faults within tolerances specified by standardized tests. | On the Fault Tracking tab, use the parameters to specify the fault tolerances. If the vehicle speed is not within the allowable speed range, the block sets a fault condition. |

## Fault and Failure Tracking

On the Fault Tracking tab, use the parameters to specify the fault tolerances. If the vehicle speed or time is not within the allowable range, the block sets a fault condition.

| Parameter | Description | Setting | WLTP Tests $^{\mathbf{2}}$ |
| :--- | :--- | :--- | :--- |
|  | EPA Standard ${ }^{\mathbf{1}}$ | $2.0 \mathrm{~km} / \mathrm{h}$ |  |
| Speed tolerance | Speed tolerance <br> above the highest <br> point and below the <br> lowest point of the <br> drive cycle speed <br> trace within the time <br> tolerance. | 2.0 mph | 1.0 s |
| Time tolerance | Time that the block <br> uses to determine the <br> speed tolerance. | 1.0 s | 10 |
| Maximum number of <br> faults | Maximum number of <br> faults during the drive <br> cycle. | Not specified | 1.0 s |
| Maximum single fault <br> time | Maximum fault <br> duration. | 2.0 s | Not specified |
| Maximum total fault <br> time | Maximum <br> accumulated time <br> spent under fault <br> condition. | Not specified |  |

These figures illustrate how the block uses the velocity and time tolerances to determine the allowable speed range.


## Create Drive Cycles Using Workspace Variables

If you set Drive cycle source to Workspace variable, you can specify a workspace variable that defines the drive cycle.

This table provides examples for using workspace variables to create your own drive cycles.




## Ports

## Input

VelFdbk - Vehicle longitudinal speed scalar

Longitudinal vehicle speed.

## Dependencies

To enable this port, on the Fault Tracking tab, select Enable fault tracking. Set the Velocity feedback units, inUnit parameter to the VelFdbk input port signal units.

Output
Info - Bus signal
bus
Bus signal containing these block calculations.

| Signal |  | Description |
| :---: | :---: | :---: |
| Reference Speed |  | Vehicle reference speed |
| Reference Accel |  | Vehicle reference acceleration |
| Gear |  | Vehicle gear |
| Fault | UpprBnd | Upper bound of allowable vehicle speed range. |
|  | LowerBnd | Lower bound of allowable vehicle speed range. |
|  | Fault | Boolean value indicating fault condition: <br> - 1 - Fault <br> - 0 - No fault <br> If the vehicle speed is not within the allowable speed range, the block sets a fault condition. |
|  | FaultCnt | Number of faults. |
|  | CumFaultTime | Cumulative time spent in fault condition. |
|  | SnglFaultTime | Tim spent in a single fault. |
|  | Fail | Boolean value indicating fault failure: <br> - 1 - Failure <br> - 0 - No failure <br> If the fault conditions exceed the maximum number of faults, maximum single fault time, or maximum total fault time, the block sets a fault failure. |

## Dependencies

To enable this port, on the Fault Tracking tab, select Enable fault tracking.
RefSpd - Vehicle reference speed
scalar
Vehicle reference speed, in units that you specify. To specify the units, use the Output velocity units parameter.

RefAcc - Vehicle reference acceleration
scalar

To calculate the acceleration, the block implements Savitzky-Golay differentiation using a secondorder polynomial with a three-sample point filter.

## Dependencies

To create the output acceleration port, select Output acceleration. Selecting Output acceleration enables the Output acceleration units parameter.

## Gear - Vehicle gear

scalar

## Dependencies

To enable this port:
1 Specify a drive cycle that contains a gear shift schedule. You can use:

- A support package to install standard drive cycles that include the gear shift schedules, for example JC08 and CUEDC.
- Workspace variables.
- .mat, .xls, .xlsx, or .txt files.


## 2 Select Output gear shift data.

## Parameters

## Cycle Setup

## Setup

Drive cycle source - Select the drive cycle source
FTP75 (default)|Wide Open Throttle (WOT)|Workspace variable|.mat, .xls, .xlsx or .txt file

- FTP75 - Load the FTP75 drive cycle from a .mat file into a 1-D Lookup Table block. The FTP75 represents a city drive cycle that you can use to determine tailpipe emissions and fuel economy of passenger cars. To install additional drive cycles from a support package, see "Support Package for Maneuver and Drive Cycle Data".
- Wide Open Throttle (WOT) - Use WOT parameters to specify a drive cycle for performance testing.
- Workspace variable - Specify time, speed, and, optionally, gear data as a structure, 2-D array, or time series object.
- .mat, .xls, .xlsx or .txt file - Specify a file that contains time, speed and, optionally, gear data in column format.

Once you have installed additional cycles, you can use set_param to set the drive cycle. For example, to use drive cycle US06:

```
set_param([gcs '/Drive Cycle Source'],'cycleVar','US06')
```


## Dependencies

The table summarizes the parameter dependencies.

| Drive Cycle Source | Enables Parameter |
| :--- | :--- |
| Wide Open Throttle (WOT) | Start time, t_wot1 |
|  | Initial reference speed, xdot_woto |
|  | Nominal reference speed, xdot_wot1 |
|  | Time to start deceleration, wot2 |
|  | Final reference speed, xdot_wot2 |
|  | WOT simulation time, t_wotend |
| Source velocity units |  |
|  |  |
|  | Drive cycle source file |
|  | Source velocity units |
|  | Output gear shift data, if drive cycle includes gear shift <br> schedule |

## From workspace - Workspace

variable
Monotonically increasing time, velocity, and, optionally, gear data, specified by a structure, 2-D array, or time series object. Enter units for velocity in the Source velocity units parameter field.

A valid point must exist for each corresponding time value. You cannot specify inf, empty, or NaN.
This table provides examples for using workspace variables to create your own drive cycles.




## Dependencies

To enable this parameter, select Workspace variable from Drive cycle source.
Drive cycle source file - File name
.mat, .xls, .xlsx or .txt

File containing monotonically increasing time, velocity, and, optionally, gear in column or commaseparated format. The block ignores units in the file. Enter units for velocity in the Source velocity units parameter field.




If you provide the gear schedule using $\mathbf{P}, \mathbf{R}, \mathbf{N}, \mathbf{D}, \mathbf{L}, \mathbf{O D}$, the block maps the gears to integers.

| Gear | Integer |
| :--- | :--- |
| P | 80 |
| R | -1 |
| N | 0 |
| L | 1 |
| D | 2 |
| OD | Next integer after highest specified gear. |

For example, the block converts the gear schedule P P N L D 345654567 OD 7 to 80 8001234565456787.

## Dependencies

To enable this parameter, select .mat, .xls, .xlsx or .txt file from Drive cycle source.
Repeat cyclically - Repeat drive cycle
off (default) | on

Repeat the drive cycle if the simulation run time exceeds the length of the drive cycle.
Output acceleration - Output the acceleration off (default)

To calculate the acceleration, the block implements Savitzky-Golay differentiation using a secondorder polynomial with a three-sample point filter.

## Dependencies

To create the output acceleration port, select Output acceleration. Selecting Output acceleration enables the Output acceleration units parameter.

Output gear shift data - Output the gear
off (default) | on

## Dependencies

- Specify a drive cycle that contains a gear shift schedule. You can use:
- A support package to install standard drive cycles that include the gear shift schedules, for example JC08 and CUEDC.
- Workspace variables.
- .mat, .xls, .xlsx, or .txt files.
- Clicking this parameter creates input port Gear.
wOT
Start time, t_wot1 - Drive cycle start time
5 (default) | scalar
Drive cycle start time, in s. For example, this plot shows a drive cycle with a start time of 10 s .



## Dependencies

To enable this parameter, select the Drive cycle source parameter Wide Open Throttle (WOT).

Initial reference speed, xdot_woto - Speed
0 (default) | scalar
Initial reference speed, in units that you specify with the Source velocity units parameter. For example, this plot shows a drive cycle with an initial reference speed of $4 \mathrm{~m} / \mathrm{s}$.


## Dependencies

To enable this parameter, select the Drive cycle source parameter Wide Open Throttle (WOT).
Nominal reference speed, xdot_wot1 - Speed
30 (default) | scalar
Nominal reference speed, in units that you specify with the Source velocity units parameter. For example, this plot shows a drive cycle with a nominal reference speed of $30 \mathrm{~m} / \mathrm{s}$.


## Dependencies

To enable this parameter, select the Drive cycle source parameter Wide Open Throttle (WOT).
Time to start deceleration, wot2 - Time
20 (default) | scalar
Time to start vehicle deceleration, in s. For example, this plot shows a drive cycle with vehicle deceleration starting at 25 s .


## Dependencies

To enable this parameter, select the Drive cycle source parameter Wide Open Throttle (WOT).
Final reference speed, xdot_wot2 - Speed
0 (default) | scalar
Final reference speed, in units that you specify with the Source velocity units parameter. For example, this plot shows a drive cycle with a final reference speed of $2 \mathrm{~m} / \mathrm{s}$.


## Dependencies

To enable this parameter, select the Drive cycle source parameter Wide Open Throttle (WOT).
WOT simulation time, t_wotend - Time
30 (default) | scalar
Drive cycle WOT simulation time, in s. For example, this plot shows a drive cycle with a simulation time of 50 s .


## Dependencies

To enable this parameter, select the Drive cycle source parameter Wide Open Throttle (WOT).

## Units and Sample Period

Source velocity units - Specify velocity units
$\mathrm{m} / \mathrm{s}$ (default)
Input velocity units.

## Dependencies

To enable this parameter, select the Drive cycle source parameter Wide Open Throttle (WOT), Workspace variable, or .mat, .xls, .xlsx or .txt file.

Output velocity units - Specify velocity units
m/s (default)
Output velocity units.
Output acceleration units - Specify acceleration units $\mathrm{m} / \mathrm{s}^{\wedge} 2$ (default)

Specify the output acceleration units.

## Dependencies

To enable this parameter, select Output acceleration.
Output sample period (0) for continuous - Sample rate
0 (default) | scalar
Sample rate. Set to 0 for continuous sample period. For a discrete period, specify a non-zero rate.

## Fault Tracking

Fault Settings
Enable fault tracking - Enable fault tracking
off (default) | on
Select this parameter to enable drive cycle fault tracking. Use the parameters to specify the fault tolerances. If the vehicle speed is not within the allowable speed range, the block sets a fault condition.

## Dependencies

Selecting this parameter enables these parameters:

- Speed tolerance, velBnd
- Speed tolerance units, velBndUnit
- Velocity feedback units, inUnit
- Time tolerance, timeBnd

Speed tolerance, velBnd - Drive cycle speed tolerance
2.0 (default) | scalar

The speed tolerance above the highest point and below the lowest point of the drive cycle speed trace within the time tolerance. If the vehicle speed is not within the allowable speed range, the block sets a fault condition. For the tolerances specified by the standardized tests, use these settings:

- EPA dynamometer driving schedules - 2.0
- WLTP tests - 2.0

These figures illustrate how the block uses the velocity and time tolerances to determine the allowable speed range.


## Dependencies

To enable this parameter, on the Fault Tracking tab, select Enable fault tracking.
Speed tolerance units, velBndUnit - Set units
mph (default)
Speed tolerance units. For the units specified by the standardized tests, use these units:

- EPA dynamometer driving schedules - m/s
- WLTP tests - km/h


## Dependencies

To enable this parameter, on the Fault Tracking tab, select Enable fault tracking.
Velocity feedback units, inUnit - Set velocity feedback units
m/s (default)
Velocity feedback units. Set the value to the VelFdbk input port signal units.

## Dependencies

To enable this parameter, on the Fault Tracking tab, select Enable fault tracking.

Time tolerance, timeBnd - Time tolerance

## 1.0 (default) | scalar

Time that the block uses to determine the speed tolerance. If the vehicle speed is not within the allowable speed range, the block sets a fault condition. For the time tolerances specified by the standardized tests, use these settings:

- EPA dynamometer driving schedules - 1.0
- WLTP tests - 1.0

These figures illustrate how the block uses the velocity and time tolerances to determine the allowable speed range.


## Dependencies

To enable this parameter, on the Fault Tracking tab, select Enable fault tracking.

## Failure Settings

Enable failure tracking - Enable failure tracking
off (default) | on
Select this parameter to enable drive cycle failure tracking.

## Dependencies

To enable this parameter, select Enable fault tracking. Selecting Enable failure tracking parameter enables these parameters:

- Stop simulation when trace fails, stopSim
- Maximum number of faults, maxFaultCnt
- Maximum single fault time, maxFaultTime
- Maximum total fault time, maxTotFaultTime

Maximum number of faults, maxFaultCnt - Maximum number of faults
10 (default) | scalar
Maximum number of faults during the drive cycle. For the number specified by the standardized tests, use these settings:

- EPA dynamometer driving schedules - Not specified
- WLTP tests - 10

If the number of faults exceeds the maximum number of faults, the block sets a fault failure.

## Dependencies

To enable this parameter, on the Fault Tracking tab, select Enable failure tracking.
Maximum single fault time, maxFaultTime - Maximum duration of single fault
2.0 (default) | scalar

Maximum duration of single fault, in s. For the time specified by the standardized tests, use these settings:

- EPA dynamometer driving schedules - 2.0
- WLTP tests - 1.0

If the fault duration exceeds the maximum single fault time, the block sets a fault failure.

## Dependencies

To enable this parameter, on the Fault Tracking tab, select Enable failure tracking.
Maximum total fault time, maxTotFaultTime - Maximum total fault time
15.0 (default) | scalar

Maximum accumulated time spent under fault condition, in s.
If the accumulated time spent under fault condition exceeds the maximum total fault time, the block sets a fault failure.

## Dependencies

To enable this parameter, on the Fault Tracking tab, select Enable failure tracking.

## Simulation Trace

Display simulation trace - Display velocity trace
off (default) |on
Select this parameter to display a velocity trace window. Selecting this parameter can slow the simulation time.

## Dependencies

Selecting this parameter enables these parameters:

- Simulation trace update rate, dtTrace
- Simulation trace display window, traceWindow

Simulation trace update rate, dtTrace - Trace update rate
1 (default) | scalar
Simulation trace update rate, in s. Set to 0 for continuous sample period. For a discrete period, specify a non-zero rate.

## Dependencies

To enable this parameter, on the Fault Tracking tab, select Display simulation trace.
Simulation trace display window, traceWindow - Trace window update rate
10 (default) | scalar
Simulation trace window update rate, in s.

## Dependencies

To enable this parameter, on the Fault Tracking tab, select Display simulation trace.

## Version History

Introduced in R2017a

## References

[1] Environmental Protection Agency (EPA). EPA urban dynamometer driving schedule. 40 CFR 86.115-78, July 1, 2001.
[2] European Union Commission. "Speed trace tolerances". European Union Commission Regulation. 32017R1151, Sec 1.2.6.6, June 1, 2017.

## Extended Capabilities

C/C++ Code Generation
Generate C and C++ code using Simulink ${ }^{\circledR}$ Coder ${ }^{\mathrm{TM}}$.

## See Also

Lateral Driver | Longitudinal Driver | Predictive Driver
Topics
"Support Package for Maneuver and Drive Cycle Data"
"Time Series Objects and Collections"

## Longitudinal Driver

## Longitudinal speed-tracking controller



## Libraries:

Powertrain Blockset / Vehicle Scenario Builder
Vehicle Dynamics Blockset / Vehicle Scenarios / Driver

## Description

The Longitudinal Driver block implements a longitudinal speed-tracking controller. Based on reference and feedback velocities, the block generates normalized acceleration and braking commands that can vary from 0 through 1 . You can use the block to model the dynamic response of a driver or to generate the commands necessary to track a longitudinal drive cycle.

## Configurations

## External Actions

Use the External Actions parameters to create input ports for signals that can disable, hold, or override the closed-loop acceleration or deceleration commands. The block uses this priority order for the input commands: disable (highest), hold, override.

This table summarizes the external action parameters.

| Goal | External Action <br> Parameter | Input Ports | Data Type |
| :--- | :--- | :--- | :--- |
| Override the accelerator <br> command with an input <br> acceleration command. | Accelerator <br> override | EnablAccel0vr | Boolean |
| Hold the acceleration command <br> at the current value. | Accel0rator <br> hold | AccelHld | double |
| Disable the acceleration <br> command. | Accelerator <br> disable | AccelZero | Boolean |
| Override the decelerator <br> command with an input <br> deceleration command. | Decelerator <br> override | EnablDecel0vr | Boolean |
| Hold the decelerator command at <br> current value. | Decelerator <br> hold | DecelHld | double |
| Disable the decelerator <br> command. | Decelerator <br> disable | DecelZero | Boolean |

## Controller

Use the Control type, cntrlType parameter to specify one of these control options.

| Setting | Block Implementation |
| :--- | :--- |
| PI | Proportional-integral (PI) control with tracking windup and feed-forward <br> gains. |
| Scheduled PI | PI control with tracking windup and feed-forward gains that are a function <br> of vehicle velocity. |
| Predictive | Optimal single-point preview (look ahead) control model developed by C. C. <br> MacAdam $1,2,3$. The model represents driver steering control behavior <br> during path-following and obstacle avoidance maneuvers. Drivers preview <br> (look ahead) to follow a predefined path. To implement the MacAdam model, <br> the block: |
| - Represents the dynamics as a linear single track (bicycle) vehicle <br> - Minimizes the previewed error signal at a single point $T^{*}$ seconds ahead <br> in time |  |
| Accounts for the driver lag deriving from perceptual and neuromuscular <br> mechanisms |  |

## Shift

Use the Shift type, shftType parameter to specify one of these shift options.

| Setting | Block Implementation |
| :--- | :--- |
| None | No transmission. Block outputs a constant gear of 1. <br> Use this setting to minimize the number of parameters you need to generate <br> acceleration and braking commands to track forward vehicle motion. This <br> setting does not allow reverse vehicle motion. |
| Reverse, Neutral, <br> Drive | Block uses a Stateflow ${ }^{\circledR}$ chart to model reverse, neutral, and drive gear shift <br> scheduling. |
| Use this setting to generate acceleration and braking commands to track <br> forward and reverse vehicle motion using simple reverse, neutral, and drive <br> gear shift scheduling. Depending on the vehicle state and vehicle velocity <br> feedback, the block uses the initial gear and time required to shift to shift <br> the vehicle up into drive or down into reverse or neutral. |  |
| For neutral gears, the block uses braking commands to control the vehicle <br> speed. For reverse gears, the block uses an acceleration command to <br> generate torque and a brake command to reduce vehicle speed. |  |


| Setting | Block Implementation |
| :--- | :--- |
| Scheduled | Block uses a Stateflow chart to model reverse, neutral, park, and N-speed <br> gear shift scheduling. <br> Use this setting to generate acceleration and braking commands to track <br> forward and reverse vehicle motion using reverse, neutral, park, and N- <br> speed gear shift scheduling. Depending on the vehicle state and vehicle <br> velocity feedback, the block uses these parameters to determine the: <br> - $\quad$ Initial gear |
|  | - Upshift and downshift accelerator pedal positions <br> - <br> - Upshift and downshift velocity |
|  | For neutral gears, the block uses braking commands to control the vehicle <br> speed. For reverse gears, the block uses an acceleration command to <br> generate torque and a brake command to reduce vehicle speed. |
| External | Block uses the input gear, vehicle state, and velocity feedback to generate <br> acceleration and braking commands to track forward and reverse vehicle <br> motion. |
| For neutral gears, the block uses braking commands to control the vehicle <br> speed. For reverse gears, the block uses an acceleration command to <br> generate torque and a brake command to reduce vehicle speed. |  |

## Gear Signal

Use the Output gear signal parameter to create the GearCmd output port. The GearCmd signal contains the integer value of the commanded vehicle gear.

| Gear | Integer |
| :--- | :--- |
| Park | 80 |
| Reverse | -1 |
| Neutral | 0 |
| Drive | 1 |
| Gear | Gear number |

## Controller: PI Speed-Tracking

If you set the control type to PI or Scheduled PI, the block implements proportional-integral (PI) control with tracking windup and feed-forward gains. For the Scheduled PI configuration, the block uses feed forward gains that are a function of vehicle velocity.

To calculate the speed control output, the block uses these equations.

| Setting | Equation |
| :--- | :---: |
| PI | $y=\frac{K_{f f}}{v_{\text {nom }}} v_{r e f}+\frac{K_{p} e_{r e f}}{v_{\text {nom }}}+\int\left(\frac{K_{i} e_{r e f}}{v_{\text {nom }}}+K_{a w} e_{o u t}\right) d t+K_{g} \theta$ |

## Setting Equation

| Scheduled PI | $y=\frac{K_{f f}(v)}{v_{\text {nom }}} v_{\text {ref }}+\frac{K_{p}(v) e_{\text {ref }}}{v_{\text {nom }}}+\int\left(\frac{K_{i}(v) e_{\text {ref }}}{v_{\text {nom }}}+K_{\text {aw }} e_{o u t}\right) e_{r e f} d t+K_{g}(v) \theta$. |
| :--- | :--- |

where:

$$
\begin{aligned}
& e_{\text {ref }}=v_{\text {ref }}-v \\
& e_{\text {out }}=y_{\text {sat }}-y \\
& y_{\text {sat }}=\left\{\begin{array}{cc}
-1 & y<-1 \\
y & -1 \leq y \leq 1 \\
1 & 1<y
\end{array}\right.
\end{aligned}
$$

The velocity error low-pass filter uses this transfer function.

$$
H(s)=\frac{1}{\tau_{e r r} s+1} \text { for } \tau_{\text {err }}>0
$$

To calculate the acceleration and braking commands, the block uses these equations.

$$
\begin{aligned}
& y_{\text {acc }}=\left\{\begin{array}{cc}
0 & y_{\text {sat }}<0 \\
y_{\text {sat }} & 0 \leq y_{\text {sat }} \leq 1 \\
1 & 1<y_{\text {sat }}
\end{array}\right. \\
& y_{\text {dec }}=\left\{\begin{array}{cc}
0 & y_{\text {sat }}>0 \\
-y_{\text {sat }} & -1 \leq y_{\text {sat }} \leq 0 \\
1 & y_{\text {sat }}<-1
\end{array}\right.
\end{aligned}
$$

The equations use these variables.

| $v_{\text {nom }}$ | Nominal vehicle speed |
| :--- | :--- |
| $K_{p}$ | Proportional gain |
| $K_{i}$ | Integral gain |
| $K_{a w}$ | Anti-windup gain |
| $K_{f f}$ | Velocity feed-forward gain |
| $K_{g}$ | Grade angle feed-forward gain |
| $\theta$ | Grade angle |
| $\tau_{\text {err }}$ | Error filter time constant |
| $y$ | Nominal control output magnitude |
| $y_{\text {sat }}$ | Saturated control output magnitude |
| $e_{\text {ref }}$ | Velocity error |
| $e_{\text {out }}$ | Difference between saturated and nominal control outputs |
| $y_{a c c}$ | Acceleration signal |
| $y_{d e c}$ | Braking signal |
| $v$ | Velocity feedback signal |

$v_{\text {ref }} \quad$ Reference velocity signal

## Controller: Predictive Speed-Tracking

If you set the Control type, cntrlType parameter to Predictive, the block implements an optimal single-point preview (look ahead) control model developed by C. C. MacAdam ${ }^{1,2,3}$. The model represents driver steering control behavior during path-following and obstacle avoidance maneuvers. Drivers preview (look ahead) to follow a predefined path. To implement the MacAdam model, the block:

- Represents the dynamics as a linear single track (bicycle) vehicle
- Minimizes the previewed error signal at a single point T* seconds ahead in time
- Accounts for the driver lag deriving from perceptual and neuromuscular mechanisms


## Vehicle Dynamics

For longitudinal motion, the block implements these linear dynamics.

$$
\begin{aligned}
& x_{1}=v \\
& \dot{x}_{1}=x_{2}=\frac{K_{p t}}{m}-g \sin (\gamma)+F_{r} x_{1}
\end{aligned}
$$

In matrix notation:

$$
\dot{x}=F x+g \bar{u}
$$

where:

$$
\begin{aligned}
& x=\left[\begin{array}{l}
x_{1} \\
x_{2}
\end{array}\right] \\
& F=\left[\begin{array}{cc}
0 & 1 \\
\frac{F_{r}}{m} & 0
\end{array}\right] \\
& g=\left[\begin{array}{c}
0 \\
\frac{K_{p t}}{m}
\end{array}\right] \\
& \bar{u}=u-\frac{m^{2}}{K_{p t}} g \sin (\gamma)
\end{aligned}
$$

The block uses this equation for the rolling resistance.

$$
F_{r}=-\left[\tanh \left(x_{1}\right)\left(\frac{a_{r}}{x_{1}}+c_{r} x_{1}\right)+b_{r}\right]
$$

The single-point model assumes a minimum previewed error signal at a single point $T^{*}$ seconds ahead in time. $a^{*}$ is the driver ability to predict the future vehicle response based on the current steering control input. $b^{*}$ is the driver ability to predict the future vehicle response based on the current vehicle state. The block uses these equations.

$$
\begin{aligned}
& a^{*}=\left(T^{*}\right) m^{T}\left[I+\sum_{n=1}^{\infty} \frac{F^{n}\left(T^{*}\right)^{n}}{(n+1)!}\right] g e \\
& b^{*}=m^{T}\left[I+\sum_{n=1}^{\infty} \frac{F^{n}\left(T^{*}\right)^{n}}{n!}\right]
\end{aligned}
$$

where:

$$
m^{T}=\left[\begin{array}{ll}
1 & 1
\end{array}\right]
$$

The equations use these variables.

| $a, b$ | Forward and rearward tire location, respectively |
| :--- | :--- |
| $m$ | Vehicle mass |
| $I$ | Vehicle rotational inertia |
| $a^{*}, \boldsymbol{b}^{*}$ | Driver prediction scalar and vector gain, respectively |
| $\boldsymbol{x}$ | Predicted vehicle state vector |
| $v$ | Longitudinal velocity |
| $\boldsymbol{F}$ | System matrix |
| $K_{p t}$ | Tractive force and brake limit |
| $\gamma$ | Grade angle |
| $\boldsymbol{g}$ | Control coefficient vector |
| $g$ | Gravitational constant |
| $T^{*}$ | Preview time window |
| $f\left(t+T^{*}\right)$ | Previewed path input T* seconds ahead |
| $U$ | Forward vehicle velocity |
| $\boldsymbol{m}^{T}$ | Constant observer vector; provides vehicle lateral position |
| $F_{r}$ | Rolling resistance |
| $a_{r}$ | Static rolling and driveline resistance |
| $b_{r}$ | Linear rolling and driveline resistance |
| $c_{r}$ | Aerodynamic rolling and driveline resistance |

## Optimization

The single-point model implemented by the block finds the steering command that minimizes a local performance index, $J$, over the current preview interval, $(t, t+T)$.

$$
J=\frac{1}{T} \int^{t+T}[f(\eta)-y(\eta)]^{2} d \eta
$$

To minimize $J$ with respect to the steering command, this condition must be met.

$$
\frac{d J}{d u}=0
$$

You can express the optimal control solution in terms of a current non-optimal and corresponding nonzero preview output error $T^{*}$ seconds ahead ${ }^{1,2,3}$.

$$
u^{o}(t)=u(t)+\frac{e\left(t+T^{*}\right)}{a^{*}}
$$

The block uses the preview distance and vehicle longitudinal velocity to determine the preview time window.

$$
T^{*}=\frac{L}{U}
$$

The equations use these variables.

| $T^{*}$ | Preview time window |
| :--- | :--- |
| $f\left(t+T^{*}\right)$ | Previewed path input $T^{*} \sec$ ahead |
| $y\left(t+T^{*}\right)$ | Previewed plant output $T^{*}$ sec ahead |
| $e\left(t+T^{*}\right)$ | Previewed error signal $T^{*}$ sec ahead |
| $u(t), u^{o}(t)$ | Steer angle and optimal steer angle, respectively |
| $L$ | Preview distance |
| $J$ | Performance index |
| $U$ | Forward (longitudinal) vehicle velocity |

## Driver Lag

The single-point model implemented by the block introduces a driver lag. The driver lag accounts for the delay when the driver is tracking tasks. Specifically, it is the transport delay deriving from perceptual and neuromuscular mechanisms. To calculate the driver transport delay, the block implements this equation.

$$
H(s)=e^{-s \tau}
$$

The equations use these variables.

| $\tau$ | Driver transport delay |
| :--- | :--- |
| $y\left(t+T^{*}\right)$ | Previewed plant output $T^{*} \sec$ ahead |
| $e\left(t+T^{*}\right)$ | Previewed error signal $T^{*}$ sec ahead |
| $u(t), u^{o}(t)$ | Steer angle and optimal steer angle, respectively |
| $J$ | Performance index |

## Ports

Input
VelRef - Reference vehicle velocity
scalar
Reference velocity, $v_{\text {ref, }}$ in $\mathrm{m} / \mathrm{s}$.
EnbIAcceIOvr - Enable acceleration command override scalar

Enable acceleration command override.

## Dependencies

To enable this port, select Acceleration override.
Data Types: Boolean
AccelOvrCmd - Acceleration override command scalar

Acceleration override command, normalized from 0 through 1.

## Dependencies

To enable this port, select Acceleration override.
Data Types: double
AccelHId - Acceleration hold
scalar
Boolean signal that holds the acceleration command at the current value.

## Dependencies

To enable this port, select Acceleration hold.
Data Types: Boolean
AccelZero - Disable acceleration command scalar

Disable acceleration command.

## Dependencies

To enable this port, select Acceleration disable.
Data Types: Boolean
EnblDecelOvr - Enable deceleration command override
scalar
Enable deceleration command override.

## Dependencies

To enable this port, select Deceleration override.
Data Types: Boolean
DecelOvrCmd - Deceleration override command scalar

Deceleration override command, normalized from 0 through 1.

## Dependencies

To enable this port, select Deceleration override.
Data Types: double

DecelHId - Deceleration hold scalar

Boolean signal that holds the deceleration command at the current value.

## Dependencies

To enable this port, select Deceleration hold.
Data Types: Boolean
DecelZero - Disable deceleration command
scalar
Disable deceleration command.

## Dependencies

To enable this port, select Deceleration disable.

## Data Types: Boolean

ExtGear - Gear
scalar

| Gear | Integer |
| :--- | :--- |
| Park | 80 |
| Reverse | -1 |
| Neutral | 0 |
| Drive | 1 |
| Gear | Gear number |

## Dependencies

To enable this port, set Shift type, shftType to External.
VelFdbk - Longitudinal vehicle velocity
scalar
Longitudinal vehicle velocity, $U$, in the vehicle-fixed frame, in $\mathrm{m} / \mathrm{s}$.
Grade - Road grade angle
scalar
Road grade angle, $\theta$ or $\gamma$, in deg.
Output
Info - Bus signal
bus
Bus signal containing these block calculations.

| Signal |  | Variable | Description |
| :---: | :---: | :---: | :---: |
| Accel |  | $y_{a c c}$ | Commanded vehicle acceleration, normalized from 0 through 1 |
| Decel |  | $y_{\text {dec }}$ | Commanded vehicle deceleration, normalized from 0 through 1 |
| Gear |  |  | Integer value of commanded gear |
| Clutch |  |  | Clutch command |
| Err |  | $e_{\text {ref }}$ | Difference in reference vehicle speed and vehicle speed |
| ErrSqrSum |  | $\int_{0}^{t} e_{r e f}{ }^{2} d t$ | Integrated square of error |
| ErrMax |  | $\max \left(e_{r e f}(t)\right)$ | Maximum error during simulation |
| ErrMin |  | $\min \left(e_{r e f}(t)\right)$ | Minimum error during simulation |
| ExtActions | EnblAccel0vr |  | Override the accelerator command with an input acceleration command |
|  | Accel0vrCmd |  | Input accelerator override command |
|  | AccelHld |  | Hold the acceleration command at the current value |
|  | AccelZero |  | Disable the acceleration command |
|  | EnblDecel0vr |  | Override the decelerator command with an input deceleration command |
|  | Decel0vrCmd |  | Input deceleration override command |
|  | DecelHld |  | Hold the decelerator command at current value |
|  | DecelZero |  | Disable the decelerator command |

## AccelCmd - Commanded vehicle acceleration

## scalar

Commanded vehicle acceleration, $y_{a c c}$, normalized from 0 through 1.
DecelCmd - Commanded vehicle deceleration
scalar
Commanded vehicle deceleration, $y_{\text {dec }}$, normalized from 0 through 1.
GearCmd - Commanded vehicle gear
scalar
Integer value of commanded vehicle gear.

| Gear | Integer |
| :--- | :--- |
| Park | 80 |
| Reverse | -1 |


| Gear | Integer |
| :--- | :--- |
| Neutral | 0 |
| Drive | 1 |
| Gear | Gear number |

## Dependencies

To enable this port, select Output gear signal.

## Parameters

## External Actions

Accelerator override - Override acceleration command
off (default) | on
Select to override the acceleration command with an input acceleration command.

## Dependencies

Selecting this parameter creates the EnblAccelOvr and AccelOvrCmd input ports.
Accelerator hold - Hold acceleration command
off (default) | on
Select to hold the acceleration command.

## Dependencies

Selecting this parameter creates the AccelHld input port.
Accelerator disable - Disable acceleration command
off (default) | on
Select to disable the acceleration command.

## Dependencies

Selecting this parameter creates the AccelZero input port.
Decelerator override - Override deceleration command
off (default) | on
Select to override the deceleration command with an input deceleration command.

## Dependencies

Selecting this parameter creates the EnblDecelOvr and DecelOvrCmd input ports.
Decelerator hold - Hold deceleration command
off (default) | on
Select to hold the deceleration command.

## Dependencies

Selecting this parameter creates the DecelHld input port.
Decelerator disable - Disable deceleration command
off (default) | on
Select to disable the deceleration command.

## Dependencies

Selecting this parameter creates the DecelZero input port.

## Configuration

Control type, cntriType - Longitudinal control
PI (default) | Scheduled PI|Predictive
Type of longitudinal control.

| Setting | Block Implementation |
| :--- | :--- |
| PI | Proportional-integral (PI) control with tracking windup and feed-forward <br> gains. |
| Scheduled PI | PI control with tracking windup and feed-forward gains that are a function <br> of vehicle velocity. |
| Predictive | Optimal single-point preview (look ahead) control model developed by C. C. <br> MacAdam $1,2,3$ <br> during path-following model represents driver steering control behavior <br> (look ahead) to follow a predefined avoidance maneuvers. Drivers preview <br> the block: implement the MacAdam model, |
| - Represents the dynamics as a linear single track (bicycle) vehicle <br> - Minimizes the previewed error signal at a single point $T^{*}$ seconds ahead <br> in time |  |
| Accounts for the driver lag deriving from perceptual and neuromuscular <br> mechanisms |  |

Shift type, shftType - Shift type
None (default)|Reverse, Neutral, Drive|Scheduled|External
Shift type.

| Setting | Block Implementation |
| :--- | :--- |
| None | No transmission. Block outputs a constant gear of 1. |
| Use this setting to minimize the number of parameters you need to generate <br> acceleration and braking commands to track forward vehicle motion. This <br> setting does not allow reverse vehicle motion. |  |


| Setting | Block Implementation |
| :--- | :--- |
| Reverse, Neutral, <br> Drive | Block uses a Stateflow chart to model reverse, neutral, and drive gear shift <br> scheduling. <br> Use this setting to generate acceleration and braking commands to track <br> forward and reverse vehicle motion using simple reverse, neutral, and drive <br> gear shift scheduling. Depending on the vehicle state and vehicle velocity <br> feedback, the block uses the initial gear and time required to shift to shift <br> the vehicle up into drive or down into reverse or neutral. |
| For neutral gears, the block uses braking commands to control the vehicle <br> speed. For reverse gears, the block uses an acceleration command to <br> generate torque and a brake command to reduce vehicle speed. |  |
| Block uses a Stateflow chart to model reverse, neutral, park, and N-speed <br> gear shift scheduling. |  |
| Use this setting to generate acceleration and braking commands to track <br> forward and reverse vehicle motion using reverse, neutral, park, and N- <br> speed gear shift scheduling. Depending on the vehicle state and vehicle <br> velocity feedback, the block uses these parameters to determine the: |  |
| - Initial gear |  |
| - Upshift and downshift accelerator pedal positions |  |
| - Upshift and downshift velocity |  |
| - Timing for shifting and engaging forward and reverse from neutral |  |
| For neutral gears, the block uses braking commands to control the vehicle |  |
| speed. For reverse gears, the block uses an acceleration command to |  |
| generate torque and a brake command to reduce vehicle speed. |  |

## Reference and feedback units, velUnits - Velocity units

$\mathrm{m} / \mathrm{s}$ (default)
Vehicle velocity reference and feedback units.

## Dependencies

If you set Control type, cntrlType control type to Scheduled or Scheduled PI, the block uses the Reference and feedback units, velUnits for the Nominal speed, vnom parameter dimension.

If you set Shift Type, shftType to Scheduled, the block uses the Longitudinal velocity units, velUnits for these parameter dimensions:

## - Upshift velocity data table, upShftTbl

- Downshift velocity data table, dwnShftTbl

Output gear signal - Create GearCmd output port
off (default) | on
Specify to create output port GearCmd.

## Control

Longitudinal
Proportional gain, Kp - Gain
10 (default) | scalar
Proportional gain, $K_{p}$, dimensionless.

## Dependencies

To create this parameter, set Control type to PI.
Integral gain, Ki - Gain
5 (default) | scalar
Proportional gain, $K_{i}$, dimensionless.

## Dependencies

To create this parameter, set Control type to PI.
Velocity feed-forward, Kff - Gain
. 1 (default) | scalar
Velocity feed-forward gain, $K_{f f}$, dimensionless.

## Dependencies

To create this parameter, set Control type to PI.
Grade angle feed-forward, Kg - Gain
0 (default) | scalar
Grade angle feed-forward gain, $K_{g}$, in 1/deg.

## Dependencies

To create this parameter, set Control type to PI.
Velocity gain breakpoints, VehVelVec - Breakpoints
[0 100] (default)|vector
Velocity gain breakpoints, VehVelVec, dimensionless.

## Dependencies

To create this parameter, set Control type to Scheduled PI.
Velocity feed-forward gain values, KffVec - Gain
[. 1 . 1] (default) |vector

Velocity feed-forward gain values, KffVec, as a function of vehicle velocity, dimensionless.

## Dependencies

To create this parameter, set Control type to Scheduled PI.
Proportional gain values, KpVec - Gain
[10 10] (default) | vector
Proportional gain values, $K p V e c$, as a function of vehicle velocity, dimensionless.

## Dependencies

To create this parameter, set Control type to Scheduled PI.
Integral gain values, KiVec - Gain
[5 5] (default) | vector
Integral gain values, KiVec, as a function of vehicle velocity, dimensionless.

## Dependencies

To create this parameter, set Control type to Scheduled PI.
Grade angle feed-forward values, KgVec - Grade gain
[0 0] (default) | vector
Grade angle feed-forward values, KgVec , as a function of vehicle velocity, in 1/deg.

## Dependencies

To create this parameter, set Control type to Scheduled PI.
Nominal speed, vnom - Nominal vehicle speed
5 (default) | scalar
Nominal vehicle speed, $v_{\text {nom }}$, in units specified by the Reference and feedback units, velUnits parameter. The block uses the nominal speed to normalize the controller gains.

## Dependencies

To create this parameter, set Control type to PI or Scheduled PI.
Anti-windup, Kaw - Gain
1 (default) | scalar
Anti-windup gain, $K_{\text {aw }}$, dimensionless.
Dependencies
To create this parameter, set Control type to PI or Scheduled PI.
Error filter time constant, tauerr - Filter
. 01 (default) | scalar
Error filter time constant, $\tau_{\text {err }}$, in s . To disable the filter, enter 0.

## Dependencies

To create this parameter, set Control type to PI or Scheduled PI.

## Predictive

Vehicle mass, m - Mass
1500 (default) | scalar
Vehicle mass, $m$, in kg.

## Dependencies

To create this parameter, set Longitudinal control type, cntrlType to Predictive.
Effective vehicle total tractive force, Kpt - Tractive force
3000 (default) | scalar
Effective vehicle total tractive force, $K_{p t}$, in N.

## Dependencies

To create this parameter, set Longitudinal control type, cntrlType to Predictive.
Driver response time, tau - Tau
. 1 (default) | scalar
Driver response time, $\tau$, in s.
Dependencies
To create this parameter, set Longitudinal control type, cntrlType to Predictive.
Preview distance, L - Distance
2 (default) | scalar
Driver preview distance, $L$, in $m$.

## Dependencies

To create this parameter, set Longitudinal control type, cntrlType to Predictive.
Rolling resistance coefficient, aR - Resistance
200 (default) | scalar
Static rolling and driveline resistance coefficient, $a_{R}$, in N. Block uses the parameter to estimate the constant acceleration or braking effort.

## Dependencies

To create this parameter, set Longitudinal control type, cntrlType to Predictive.
Rolling and driveline resistance coefficient, bR - Resistance
2.5 (default) | scalar

Rolling and driveline resistance coefficient, $b_{R}$, in $N \cdot \mathrm{~s} / \mathrm{m}$. Block uses the parameter to estimate the linear velocity-dependent acceleration or braking effort.

## Dependencies

To create this parameter, set Longitudinal control type, cntrlType to Predictive.
Aerodynamic drag coefficient, cR - Drag
. 5 (default) | scalar
Aerodynamic drag coefficient, $c_{R}$, in $\mathrm{N} \cdot \mathrm{s}^{\wedge} 2 / \mathrm{m}^{\wedge} 2$. Block uses the parameter to estimate the quadratic velocity-dependent acceleration or braking effort.

## Dependencies

To create this parameter, set Longitudinal control type, cntrlType to Predictive.
Gravitational constant, $\mathbf{g}$ - Gravitational constant
9.81 (default) | scalar

Gravitational constant, g , in $\mathrm{m} / \mathrm{s}^{\wedge} 2$.

## Dependencies

To create this parameter, set Longitudinal control type, cntrlType to Predictive.

## Shift

Reverse, Neutral, Drive
Initial gear, GearInit - Initial gear
0 (default) | scalar
Integer value of the initial gear. The block uses the initial gear to generate acceleration and braking commands to track forward and reverse vehicle motion.

| Gear | Integer |
| :--- | :--- |
| Park | 80 |
| Reverse | -1 |
| Neutral | 0 |
| Drive | 1 |
| Gear | Gear number |

## Dependencies

To create this parameter, set Shift type, shftType to Reverse, Neutral, Drive or Scheduled. If you specify Reverse, Neutral, Drive, the Initial Gear, GearInit parameter value can be only -1, 0, or 1.

Time required to shift, tShift - Time

## . 1 (default)| scalar

Time required to shift, $t$ Shift, in s. The block uses the time required to shift to generate acceleration and braking commands to track forward and reverse vehicle motion using reverse, neutral, and drive gear shift scheduling.

## Dependencies

To create this parameter, set Shift type, shftType to Reverse, Neutral, Drive.
Scheduled
Initial gear, GearInit - Initial gear
0 (default) | scalar
Integer value of the initial gear. The block uses the initial gear to generate acceleration and braking commands to track forward and reverse vehicle motion.

| Gear | Integer |
| :--- | :--- |
| Park | 80 |
| Reverse | -1 |
| Neutral | 0 |
| Drive | 1 |
| Gear | Gear number |

## Dependencies

To create this parameter, set Shift type, shftType to Reverse, Neutral, Drive or Scheduled. If you specify Reverse, Neutral, Drive, the Initial Gear, GearInit parameter value can be only -1, 0 , or 1 .

Up and down shift accelerator pedal positions, pdIVec - Pedal position breakpoints
[0.1 0.4 0.5 0.9] (default)|[1-by-m] vector
Pedal position breakpoints for lookup tables when calculating upshift and downshift velocities, dimensionless. Vector dimensions are 1 by the number of pedal position breakpoints, $m$.

## Dependencies

To create this parameter, set Shift type, shftType to Scheduled.
Upshift velocity data table, upShftTbI - Table
[m-by-n] array
Upshift velocity data as a function of pedal position and gear, in units specified by the Reference and feedback units, velUnits parameter. Upshift velocities indicate the vehicle velocity at which the gear should increase by 1 .

The array dimensions are $m$ pedal positions by $n$ gears. The first column of data, when $n$ equals 1 , is the upshift velocity for the neutral gear.

## Dependencies

To create this parameter, set Shift type, shftType to Scheduled.
Downshift velocity data table, dwnShftTbl - Table
[m-by-n] array
Downshift velocity data as a function of pedal position and gear, in units specified by the Reference and feedback units, velUnits parameter. Downshift velocities indicate the vehicle velocity at which the gear should decrease by 1 .

The array dimensions are m pedal positions by n gears. The first column of data, when n equals 1 , is the downshift velocity for the neutral gear.

## Dependencies

To create this parameter, set Shift type, shftType to Scheduled.
Time required to shift, tClutch - Time
. 5 (default) | scalar
Time required to shift, $t_{\text {Clutch }}$, in s .

## Dependencies

To create this parameter, set Shift type, shftType to Scheduled.
Time required to engage reverse from neutral, tRev - Time

```
. 5 (default) | scalar
```

Time required to engage reverse from neutral, $t_{\text {Rev, }}$ in s .

## Dependencies

To create this parameter, set Shift type, shftType to Scheduled.
Time required to engage park from neutral, tPark - Time

## 120 (default) | scalar

Time required to engage park from neutral, $t_{\text {Park, }}$, in s .

## Dependencies

To create this parameter, set Shift type, shftType to Scheduled.

## Version History

## Introduced in R2017a

## References

[1] MacAdam, C. C. "An Optimal Preview Control for Linear Systems". Journal of Dynamic Systems, Measurement, and Control. Vol. 102, Number 3, Sept. 1980.
[2] MacAdam, C. C. "Application of an Optimal Preview Control for Simulation of Closed-Loop Automobile Driving ". IEEE Transactions on Systems, Man, and Cybernetics. Vol. 11, Issue 6, June 1981.
[3] MacAdam, C. C. Development of Driver/Vehicle Steering Interaction Models for Dynamic Analysis. Final Technical Report UMTRI-88-53. Ann Arbor, Michigan: The University of Michigan Transportation Research Institute, Dec. 1988.

## Extended Capabilities

C/C++ Code Generation
Generate C and C++ code using Simulink $\circledR_{\circledR}$ Coder ${ }^{\mathrm{TM}}$.

## See Also

Drive Cycle Source | Lateral Driver | Predictive Driver

## Lateral Driver

Lateral path-tracking controller


## Libraries:

Vehicle Dynamics Blockset / Vehicle Scenarios / Driver

## Description

The Lateral Driver block implements a control model to generate normalized steering commands that track a lateral reference displacement. The normalized steering commands can vary between -1 to 1 . To model the dynamics, the block uses a linear single track (bicycle) model. Use the Lateral Driver block to:

- Close the loop between a predefined path and actual vehicle motion.
- Generate steering commands that track predefined paths. You can connect the Lateral Driver block output to steering block inputs.


## Configurations

## External Actions

Use the External Actions parameters to create input ports for signals that can disable, hold, or override the closed-loop steering command. The block uses this priority order for the input commands: disable (highest), hold, override. The block uses this priority order for the input commands: disable (highest), hold, override.

This table summarizes the external action parameters.

| Goal | External Action <br> Parameter | Input Ports | Data Type |
| :--- | :--- | :--- | :--- |
| Override the steering command <br> with an input steering command. | Steering <br> override | EnblSteer0vr | Boolean |
|  | Steer0vrCmd | double |  |
| Hold the steering command at <br> the current value. | Steering hold | SteerHld | Boolean |
| Disable the steering command. | Steering <br> disable | SteerZero | Boolean |

Use the Output handwheel angle parameter to specify the units for the steering ports.

| Setting | Block Implementation | Port |
| :--- | :--- | :--- |
| off (default) | Commanded steer angle, normalized from -1 <br> through 1. The block uses the tire wheel angle <br> saturation limit Tire wheel angle limit, <br> theta parameter to normalize the command. | SteerCmd - Output |
|  | Overrides the steering command with an input <br> steering command normalized from -1 through <br> 1. | Steer0vrCmd - Input |
| on | Commanded steer angle, in units specified by <br> Angular units, angUnits. | SteerCmd - Output |
|  | Overrides the steering command with an input <br> steering command, in units specified by <br> Angular units, angUnits. | Steer0vrCmd - Input |

Also, you can specify a tire wheel angle saturation limit using the Tire wheel angle limit, theta parameter.

## Control Type and Units

Use the Lateral control type, controlTypeLat parameter to specify the type of lateral control. The table specifies the block implementation.

| Setting | Block Implementation |
| :--- | :--- |
| Predictive (default) | Optimal single-point preview (look ahead) control model developed by C. <br> C. MacAdam <br> duri, 3. The model represents driver steering control behavior <br> during path-following and obstacle avoidance maneuvers. Drivers <br> preview (look ahead) to follow a predefined path. |


| Setting | Block Implementation |  |
| :---: | :---: | :---: |
| Stanley | Controller that uses the Stanley ${ }^{4}$ method to minimize the position error and the angle error of the current pose with respect to the reference pose. <br> On the Reference Control pane, use the: <br> - Vector input for poses parameter to input the to specify the input. |  |
|  | Setting | Implementation |
|  | off (default) | Block uses the longitudinal, lateral, and yaw reference (LongRef, LatRef, LatRef) input ports and the feedback (LongFdbk, LatFdbk, LatFdbk) input ports for the reference and feedback pose. |
|  | on | Block uses input ports, RefPose and CurrPose, for the reference and feedback pose, respectively. |
|  | - Include dynamics parameter to specify the type of model for the controller to use. |  |
|  | Setting | Implementation |
|  | off (default) | Controller uses a kinematic bicycle model that is suitable for path following in low-speed environments such as parking lots, where inertial effects are minimal. |
|  | on | Controller uses a dynamic bicycle model that is suitable for path following in high-speed environments such as highways, where inertial effects are more pronounced. |

Use the Angular units, angUnits parameter to specify the angular units for the input and output ports.

## Controller: Predictive Lateral Path-Tracking

If you set Lateral control type, controlTypeLat to Predictive, the Lateral Driver block implements an optimal single-point preview (look ahead) control model developed by C. C. MacAdam ${ }^{1,}$ ${ }^{2,3}$. The model represents driver steering control behavior during path-following and obstacle avoidance maneuvers. Drivers preview (look ahead) to follow a predefined path. To implement the MacAdam model, the block:

- Represents the dynamics as a linear single track (bicycle) vehicle
- Minimizes the previewed error signal at a single point T* seconds ahead in time
- Accounts for the driver lag deriving from perceptual and neuromuscular mechanisms

This figure illustrates the block implementation of the single-point version of the driver model.


## Vehicle Dynamics

For lateral and yaw motion, the block implements these linear dynamic equations.

$$
\begin{aligned}
& \dot{y}=v+U \psi \\
& \dot{v}=\left[-\frac{2\left(C_{\alpha F}+C_{\alpha R}\right)}{m U}\right] v+\left[\frac{2\left(b C_{\alpha R}-a C_{\alpha F}\right)}{m U}-U\right] r+\left(\frac{2 C_{\alpha F}}{m}\right) \delta_{F} \\
& \dot{r}=\left[\frac{2\left(b C_{\alpha R}-a C_{\alpha F}\right)}{I U}\right] v+\left[-\frac{2\left(a^{2} C_{\alpha F}+b^{2} C_{\alpha R}\right)}{I U}\right] r+\left(\frac{2 a C_{\alpha F}}{I}\right) \delta_{F} \\
& \dot{\psi}=r
\end{aligned}
$$

In matrix notation:

$$
\dot{x}=F x+g \delta_{F}
$$

where:

$$
\chi=\left[\begin{array}{l}
y \\
v \\
r \\
\psi
\end{array}\right]
$$

$$
F=\left[\begin{array}{cccc}
0 & 1 & 0 & U \\
0 & -2 \frac{C_{\alpha F}+C_{\alpha R}}{m U} & 2 \frac{b C_{\alpha R}-a C_{\alpha F}}{m U}-U & 0 \\
0 & 2 \frac{b C_{\alpha R}-a C_{\alpha F}}{I U} & -2 \frac{a^{2} C_{\alpha F}+b^{2} C_{\alpha R}}{I U} & 0 \\
0 & 0 & 1 & 0
\end{array}\right]
$$

$$
x=\left[\begin{array}{l}
0 \\
\frac{2 C_{\alpha F}}{m} \\
\frac{2 a C_{\alpha F}}{I} \\
0
\end{array}\right]
$$

The single-point model assumes a minimum previewed error signal at a single point $\mathrm{T}^{*}$ seconds ahead in time. a* is the driver ability to predict the future vehicle response based on the current steering control input. b* is the driver ability to predict the future vehicle response based on the current vehicle state. The block uses these equations.

$$
\begin{aligned}
& a^{*}=T^{*} m^{T}\left[I+\sum_{n=1}^{\infty} \frac{F^{n}\left(T^{*}\right)^{n}}{(n+1)!}\right] g \\
& b^{*}=m^{T}\left[I+\sum_{n=1}^{\infty} \frac{F^{n}\left(T^{*}\right)^{n}}{n!}\right]
\end{aligned}
$$

where:

$$
m^{T}=\left[\begin{array}{llll}
1 & 0 & 0 & 0
\end{array}\right]
$$

The equations use these variables.

| $a, b$ | Forward and rearward tire location, respectively |
| :--- | :--- |
| $m$ | Vehicle mass |
| $I$ | Vehicle rotational inertia |
| $C_{\alpha F}$ | Front tire cornering coefficient |
| $C_{\alpha R}$ | Rear tire cornering coefficient |
| $a^{*}, \boldsymbol{b}^{*}$ | Driver prediction scalar and vector gain, respectively |
| $\boldsymbol{x}$ | Predicted vehicle state vector |
| $v$ | Lateral velocity |


| $r$ | Yaw rate |
| :--- | :--- |
| $\Psi$ | Front wheel heading angle |
| $y$ | Lateral displacement |
| $\boldsymbol{F}$ | System matrix |
| $\delta, \delta_{F}$ | Steer angle and front axle steer angle, respectively |
| $\boldsymbol{g}$ | Control coefficient vector |
| $U$ | Forward (longitudinal) vehicle velocity |
| $T^{*}$ | Preview time window |
| $f\left(t+T^{*}\right)$ | Previewed path input T* seconds ahead |
| $U$ | Forward vehicle velocity |
| $\boldsymbol{m}^{T}$ | Constant observer vector; provides vehicle lateral position |
| Optimization |  |

The single-point model implemented by the block finds the steering command that minimizes a local performance index, $J$, over the current preview interval, $(t, t+T)$.

$$
J=\frac{1}{T} \int^{t+T}[f(\eta)-y(\eta)]^{2} d \eta
$$

To minimize $J$ with respect to the steering command, this condition must be met.

$$
\frac{d J}{d u}=0
$$

You can express the optimal control solution in terms of a current non-optimal and corresponding nonzero preview output error $T^{*}$ seconds ahead ${ }^{1,2,3}$.

$$
u^{o}(t)=u(t)+\frac{e\left(t+T^{*}\right)}{a^{*}}
$$

The block uses the preview distance and vehicle longitudinal velocity to determine the preview time window.

$$
T^{*}=\frac{L}{U}
$$

The equations use these variables.

| $T^{*}$ | Preview time window |
| :--- | :--- |
| $f\left(t+T^{*}\right)$ | Previewed path input $T^{*} \sec$ ahead |
| $y\left(t+T^{*}\right)$ | Previewed plant output $T^{*}$ sec ahead |
| $e\left(t+T^{*}\right)$ | Previewed error signal $T^{*}$ sec ahead |
| $u(t), u^{o}(t)$ | Steer angle and optimal steer angle, respectively |
| $L$ | Preview distance |
| $J$ | Performance index |
| $U$ | Forward (longitudinal) vehicle velocity |

## Driver Lag

The single-point model implemented by the block introduces a driver lag. The driver lag accounts for the delay when the driver is tracking tasks. Specifically, it is the transport delay deriving from perceptual and neuromuscular mechanisms. To calculate the driver transport delay, the block implements this equation.

$$
H(s)=e^{-s \tau}
$$

The equations use these variables.

| $\tau$ | Driver transport delay |
| :--- | :--- |
| $y\left(t+T^{*}\right)$ | Previewed plant output $T^{*} \sec$ ahead |
| $e\left(t+T^{*}\right)$ | Previewed error signal $T^{*}$ sec ahead |
| $u(t), u^{o}(t)$ | Steer angle and optimal steer angle, respectively |
| $J$ | Performance index |

## Controller: Stanley Lateral Path-Tracking

If you set Lateral control type, controlTypeLat to Stanley, the block implements the Stanley method ${ }^{4}$. To compute the steering angle command, the Stanley controller minimizes the position error and the angle error of the current pose with respect to the reference pose. The driving direction of the vehicle determines these error values.

To compute the steering angle command, the controller minimizes the position error and the angle error of the current pose with respect to the reference pose.

- The position error is the lateral distance from the vehicle center-of-gravity (CG) to the reference point on the path.
- The angle error is the angle of the vehicle with respect to reference path.


## Ports

## Input

LongRef - Longitudinal displacement reference
scalar
Longitudinal center of mass (CM) displacement reference, in the inertial reference frame, in m .

## Dependencies

To enable this port:

- Set Lateral control type, controlTypeLat to Stanley
- Clear Vector input for poses

LatRef - Lateral displacement reference
scalar
Lateral center of mass (CM) displacement reference, in the inertial reference frame, in m .

## Dependencies

To enable this port, do either of these:

- Set Lateral control type, controlTypeLat to Stanley and clear Vector input for poses.
- Set Lateral control type, controlTypeLat to Predictive.

EnblSteerOvr - Enable steering command override
scalar
Enable steering command override.

## Dependencies

To enable this port, select Steering override.
Data Types: Boolean
SteerOvrCmd - Steering override command
scalar
Steering override command.
Use the Output handwheel angle parameter to specify the units for the steering ports.

| Setting | Block Implementation | Port |
| :--- | :--- | :--- |
| off (default) | Commanded steer angle, normalized from -1 <br> through 1. The block uses the tire wheel angle <br> saturation limit Tire wheel angle limit, <br> theta parameter to normalize the command. | SteerCmd - Output |
|  | Overrides the steering command with an input <br> steering command normalized from -1 through <br> 1. | SteerOvrCmd - Input |
| on | Commanded steer angle, in units specified by <br> Angular units, angUnits. | SteerCmd - Output |
|  | Overrides the steering command with an input <br> steering command, in units specified by <br> Angular units, angUnits. | SteerOvrCmd - Input |

## Dependencies

To enable this port, select Steering override.

## Data Types: double

SteerHId - Steering hold
scalar
Boolean signal that holds the steering command at the current value.

## Dependencies

To enable this port, select Steering hold.
Data Types: Boolean

SteerZero - Disable steering command
scalar
Disable steering command.
Dependencies
To enable this port, select Steering disable.
Data Types: Boolean
YawRef - Yaw angle reference
scalar
Vehicle yaw angle, $\Psi_{o}$, in the inertial reference frame, in units specified by Angular units, angUnits.

## Dependencies

To enable this port:

- Set Lateral control type, controlTypeLat to Stanley
- Clear Vector input for poses

RefPose - Reference pose
$[x, y, \Theta]$ vector
Reference pose, specified as an $[x, y, \Theta]$ vector. $x$ and $y$ are in meters, and $\Theta$ are in units specified by Angular units, angUnits.
$x$ and $y$ specify the reference point to steer the vehicle toward. $\Theta$ specifies the orientation angle of the path at this reference point and is positive in the counterclockwise direction.

The reference point is the point on the path that is closest to the vehicle CG. You can use the either the Z-up or Z-down vehicle coordinate system, as long you use the same coordinate system (Z-up or Z-down) for block inputs and parameters.


## Dependencies

To enable this port, set Lateral control type, controlTypeLat to Stanley and select Vector input for poses.

## Data Types: single|double

VelFdbk - Longitudinal vehicle velocity
scalar
Longitudinal vehicle velocity, $U$, in the vehicle-fixed frame, in m/s.
CurrPose - Current pose
$[x, y, \Theta]$ vector
Current pose of the vehicle, specified as an $[x, y, \Theta]$ vector. $x$ and $y$ are in meters, and $\Theta$ is in units specified by Angular units, angUnits.
$x$ and $y$ specify the location of the vehicle, which is defined as the vehicle CG. You can use the either the Z-up or Z-down vehicle coordinate system, as long you use the same coordinate system (Z-up or Z-down) for block inputs and parameters.


## Dependencies

To enable this port, set Lateral control type, controlTypeLat to Stanley and select Vector input for poses.

Data Types: single | double
LatFdbk - Lateral displacement
scalar
Lateral CM displacement, $y_{o}$, in the inertial reference frame, in $m$.

## Dependencies

To enable this port, do either of these:

- Set Lateral control type, controlTypeLat to Stanley and clear Vector input for poses.
- Set Lateral control type, controlTypeLat to Predictive.

LatVelFdbk - Lateral vehicle velocity
scalar
Lateral vehicle velocity, $v_{o}$, in the vehicle-fixed frame, in $\mathrm{m} / \mathrm{s}$.

## Dependencies

To enable this port, Set Lateral control type, controlTypeLat to Predictive.
YawFdbk - Vehicle yaw angle
scalar

Vehicle yaw angle, $\Psi_{o}$, in the inertial reference frame, in units specified by Angular units, angUnits.

## Dependencies

To enable this port, do either of these:

- Set Lateral control type, controlTypeLat to Stanley and clear Vector input for poses.
- Set Lateral control type, controlTypeLat to Predictive.

YawVelFdbk - Yaw rate
scalar
Yaw rate, $r_{0}$, in the vehicle-fixed frame, in units specified by Angular units, angUnits per sec.

## Dependencies

To enable this port, Set Lateral control type, controlTypeLat to Predictive.

## Output

Info - Bus signal
bus
Bus signal containing these block calculations.

| Signal |  | Variable | Description |
| :---: | :---: | :---: | :---: |
| Predicted | y | y | Predicted lateral displacement, in the vehicle-fixed frame. |
|  | ydot | $v$ | Predicted lateral velocity, in the vehicle-fixed frame. |
|  | psi | $\Psi$ | Predicted front wheel heading angle. |
|  | r | $r$ | Predicted yaw rate, in the vehicle-fixed frame. |
| SteerCmd |  | $\delta_{F}$ | Commanded steer angle. |
| Err |  | $e_{\text {ref }}$ | Difference in reference vehicle position and vehicle position. |
| ErrSqrSum |  | $\int_{0}^{t} e_{r e f}{ }^{2} d t$ | Integrated square of error. |
| ErrMax |  | $\max \left(e_{\text {ref }}(t)\right)$ | Maximum error during simulation. |
| ErrMin |  | $\min \left(e_{r e f}(t)\right)$ | Minimum error during simulation. |
| ExtActions | EnblSteer0vr |  | Override the steering command with an input deceleration command. |
|  | Steer0vrCmd |  | Input steering override command |
|  | SteerHld |  | Hold the steering command at the current value |
|  | SteerZero |  | Disable the steering command |

SteerCmd - Steer angle command
scalar
Commanded steer angle, $\delta_{F}$.

Use the Output handwheel angle parameter to specify the units for the steering ports.

| Setting | Block Implementation | Port |
| :--- | :--- | :--- |
| off (default) | Commanded steer angle, normalized from -1 <br> through 1. The block uses the tire wheel angle <br> saturation limit Tire wheel angle limit, <br> theta parameter to normalize the command. | SteerCmd - Output |
|  | Overrides the steering command with an input <br> steering command normalized from -1 through <br> 1. | SteerOvrCmd - Input |
| on | Commanded steer angle, in units specified by <br> Angular units, angUnits. | SteerCmd - Output |
|  | Overrides the steering command with an input <br> steering command, in units specified by <br> Angular units, angUnits. | SteerOvrCmd - Input |

## Parameters

## Configuration

Steering override - Override steering command
off (default) | on
Select to override the steering command with an input steering command.

## Dependencies

Selecting this parameter creates the EnblSteerOvr and SteerOvrCmd input ports.
Steering hold - Hold steering command
off (default) | on
Select to hold the steering command.

## Dependencies

Selecting this parameter creates the SteerHld input port.
Steering disable - Disable steering command
off (default) | on
Select to disable the steering command.

## Dependencies

Selecting this parameter creates the SteerZero input port.
Output handwheel angle - Steering port units in rad
off (default) | on
Use the Output handwheel angle parameter to specify the units for the steering ports.

| Setting | Block Implementation | Port |
| :--- | :--- | :--- |
| off (default) | Commanded steer angle, normalized from -1 <br> through 1. The block uses the tire wheel angle <br> saturation limit Tire wheel angle limit, <br> theta parameter to normalize the command. | SteerCmd - Output |
|  | Overrides the steering command with an input <br> steering command normalized from -1 through <br> 1. | Steer0vrCmd - Input |
| on | Commanded steer angle, in units specified by <br> Angular units, angUnits. | SteerCmd - Output |
|  | Overrides the steering command with an input <br> steering command, in units specified by <br> Angular units, angUnits. | Steer0vrCmd - Input |

## Dependencies

To create the SteerOvrCmd input port, select Steering override.
Lateral control type, controlTypeLat - Controller
Predictive (default) | Stanley
Use the Lateral control type, controlTypeLat parameter to specify the type of lateral control. The table specifies the block implementation.

| Setting | Block Implementation |
| :--- | :--- |
| Predictive (default) | Optimal single-point preview (look ahead) control model developed by C. <br> C. MacAdam <br> duri,3. The model represents driver steering control behavior <br> during path-following and obstacle avoidance maneuvers. Drivers <br> preview (look ahead) to follow a predefined path. |


| Setting | Block Implementation |  |
| :---: | :---: | :---: |
| Stanley | Controller that uses the Stanley ${ }^{4}$ method to minimize the position error and the angle error of the current pose with respect to the reference pose. <br> On the Reference Control pane, use the: <br> - Vector input for poses parameter to input the to specify the input. |  |
|  | Setting | Implementation |
|  | off (default) | Block uses the longitudinal, lateral, and yaw reference (LongRef, LatRef, LatRef) input ports and the feedback (LongFdbk, LatFdbk, LatFdbk) input ports for the reference and feedback pose. |
|  | on | Block uses input ports, RefPose and CurrPose, for the reference and feedback pose, respectively. |
|  | - Include dynami controller to use. | arameter to specify the type of model for the |
|  | Setting | Implementation |
|  | off (default) | Controller uses a kinematic bicycle model that is suitable for path following in low-speed environments such as parking lots, where inertial effects are minimal. |
|  | on | Controller uses a dynamic bicycle model that is suitable for path following in high-speed environments such as highways, where inertial effects are more pronounced. |

Angular units, angUnits - Input and output port angular units

## rad (default) | deg

Input and output port angular units.

## Reference Control

## Predictive

Driver response time, tau - Response time
0.1 (default) | scalar

Driver response time, $\tau$, in s.

## Dependencies

To enable this parameter, Set Lateral control type, controlTypeLat to Predictive.
Preview distance, L - Distance
3 (default) | scalar

Driver preview distance, $L$, in m . Used to determine the preview time window, $T^{*}$.

## Dependencies

To enable this parameter, Set Lateral control type, controlTypeLat to Predictive.

## Stanley

Vector input for poses - Select to create RefPose and CurrPose input ports
off (default) | on
Select this parameter to create the RefPose and CurrPose input ports.

## Dependencies

To enable this parameter, Set Lateral control type, controlTypeLat to Stanley.
Include dynamics - Select to include dynamics
off (default) | on
The controller computes this command using the Stanley method, whose control law is based on both a kinematic and dynamic bicycle model. To change between models, use this parameter.

| Setting | Implementation |
| :--- | :--- |
| off | Controller uses a kinematic bicycle model that is suitable for path <br> following in low-speed environments such as parking lots, where <br> inertial effects are minimal. |
| on | Controller uses a dynamic bicycle model that is suitable for path <br> following in high-speed environments such as highways, where inertial <br> effects are more pronounced. |

## Dependencies

To enable this parameter, Set Lateral control type, controlTypeLat to Stanley.
Position gain of forward motion, PositionGainF - Position gain of vehicle in forward motion
2.5 (default) | positive real scalar

Position gain of the vehicle when it is in forward motion, specified as a positive scalar. This value determines how much the position error affects the steering angle. Typical values are in the range [1, 5]. Increase this value to increase the magnitude of the steering angle.

## Dependencies

To enable this parameter, Set Lateral control type, controlTypeLat to Stanley.
Position gain of reverse motion, PositionGainF - Position gain of vehicle in reverse motion 2.5 (default) | positive real scalar

Position gain of the vehicle when it is in reverse motion, specified as a positive scalar. This value determines how much the position error affects the steering angle. Typical values are in the range [1, 5]. Increase this value to increase the magnitude of the steering angle.

## Dependencies

To enable this parameter, Set Lateral control type, controlTypeLat to Stanley.

Yaw rate feedback gain, YawRateGain - Yaw rate feedback gain

## . 2 (default) | nonnegative real scalar

Yaw rate feedback gain, specified as a nonnegative real scalar. This value determines how much weight is given to the current yaw rate of the vehicle when the block computes the steering angle command.

## Dependencies

To enable this parameter, Set Lateral control type, controlTypeLat to Stanley and select Include dynamics.

Steering angle feedback gain, DelayGain - Steering angle feedback gain
. 2 (default) | nonnegative real scalar
Steering angle feedback gain, specified as a nonnegative real scalar. This value determines how much the difference between the current steering angle command, SteerCmd, and the current steering angle, CurrSteer, affects the next steering angle command.

## Dependencies

To enable this parameter, Set Lateral control type, controlTypeLat to Stanley and select Include dynamics.

## Vehicle Parameters

Forward location of tire, a - Along vehicle longitudinal axis
1.41 (default) | scalar

Forward location of tire, $a$, in m . Distance from vehicle cg to forward tire location, along vehicle longitudinal axis.

Rearward location of tire, $\mathbf{b}$ - Along vehicle longitudinal axis
1.41 (default) | scalar

Rearward location of tire, $b$, in m. Absolute value of distance from vehicle cg to rearward tire location, along vehicle longitudinal axis.

Vehicle mass, $\mathbf{m}$ - Mass
2016 (default) | scalar
Vehicle mass, $m$, in kg.

## Dependencies

To enable this port, do either of these:

- Set Lateral control type, controlTypeLat to Stanley and select Include dynamics.
- Set Lateral control type, controlTypeLat to Predictive.

Front tire cornering coefficient, Cy_f - Coefficient
25266 (default) | scalar
Cornering stiffness coefficient, $C_{\alpha F}$, in $\mathrm{N} / \mathrm{rad}$.

## Dependencies

To enable this port, do either of these:

- Set Lateral control type, controlTypeLat to Stanley and select Include dynamics.
- Set Lateral control type, controlTypeLat to Predictive.

Rear tire cornering coefficient, Cy_r - Coefficient
70933 (default) | scalar
Cornering stiffness coefficient, $C_{\alpha R}$, in $\mathrm{N} / \mathrm{rad}$.
Dependencies
To enable this port, set Lateral control type, controlTypeLat to Predictive.
Vehicle rotational inertia, I - Inertia about yaw axis
4013 (default) | scalar
Vehicle rotational inertia, $I$, about the vehicle yaw axis, in $N \cdot m \cdot s^{\wedge} 2$.

## Dependencies

To enable this parameter, Set Lateral control type, controlTypeLat to Predictive.
Nominal steering ratio, Ksteer - Steering ratio
18 (default) | scalar
Steering ratio, $K_{\text {steer }}$. The value has no dimension.

## Dependencies

To enable this parameter, select Output handwheel angle.
Tire wheel angle limit, theta - Angle limit
45*pi/180 (default) | scalar
Tire wheel angle limit, $\theta$, in rad.

## Version History

## Introduced in R2018a

## References

[1] MacAdam, C. C. "An Optimal Preview Control for Linear Systems". Journal of Dynamic Systems, Measurement, and Control. Vol. 102, Number 3, Sept. 1980.
[2] MacAdam, C. C. "Application of an Optimal Preview Control for Simulation of Closed-Loop Automobile Driving ". IEEE Transactions on Systems, Man, and Cybernetics. Vol. 11, Issue 6, June 1981.
[3] MacAdam, C. C. Development of Driver/Vehicle Steering Interaction Models for Dynamic Analysis. Final Technical Report UMTRI-88-53. Ann Arbor, Michigan: The University of Michigan Transportation Research Institute, Dec. 1988.
[4] Hoffmann, Gabriel M., Claire J. Tomlin, Michael Montemerlo, and Sebastian Thrun. "Autonomous Automobile Trajectory Tracking for Off-Road Driving: Controller Design, Experimental Validation and Racing." American Control Conference. 2007, pp. 2296-2301. doi:10.1109/ ACC.2007.4282788

## Extended Capabilities

C/C++ Code Generation
Generate C and C++ code using Simulink ${ }^{\circledR}$ Coder ${ }^{\mathrm{TM}}$.

## See Also

Longitudinal Driver | Predictive Driver

## Predictive Driver

Predictive driver controller to track longitudinal speed and lateral path


Libraries:
Vehicle Dynamics Blockset / Vehicle Scenarios / Driver

## Description

The Predictive Driver block implements a controller that generates normalized steering, acceleration, and braking commands to track longitudinal velocity and a lateral reference displacement. The normalized commands can vary between -1 to 1 . The controller uses a single-track (bicycle) model for optimal single-point preview control.

## Configurations

## External Actions

Use the External Actions parameters to create input ports for signals that you can use to simulate standard test maneuvers. The block uses this priority order for the input commands: disable (highest), hold, override.

This table summarizes the external action parameters.

| Goal | External Action <br> Parameter | Input Ports | Data Type |
| :--- | :--- | :--- | :--- |
| Override the accelerator <br> command with an input <br> acceleration command. | Accelerator <br> override | EnablAccel0vr | Boolean |
| Hold the acceleration command <br> at the current value. | Accel0vrCmd <br> hold | AccelHld | double |
| Disable the acceleration <br> command. | Accelerator <br> disable | AccelZero | Boolean |
| Override the decelerator <br> command with an input <br> deceleration command. | Decelerator <br> override | EnablDecel0vr | Boolean |
|  | Decel0vrCmd | double |  |
| Hold the decelerator command at <br> current value. | Decelerator <br> hold | DecelHld | Boolean |
| Disable the decelerator <br> command. | Decelerator <br> disable | DecelZero | Boolean |


| Goal | External Action <br> Parameter | Input Ports | Data Type |
| :--- | :--- | :--- | :--- |
| Override the steering command <br> with an input steering command. | Steering <br> override | EnblSteerOvr | Boolean |
|  | Steer0vrCmd | double |  |
| Hold the steering command at <br> the current value. | Steering hold | SteerHld | Boolean |
| Disable the steering command. | Steering <br> disable | SteerZero | Boolean |

## Controllers

Use the Longitudinal control type, cntrlType parameter to specify one of these control options.

| Setting | Block Implementation |
| :--- | :--- |
| PI | Proportional-integral (PI) control with tracking windup and feed-forward <br> gains. |
| Scheduled PI | PI control with tracking windup and feed-forward gains that are a function <br> of vehicle velocity. |
| Predictive | Optimal single-point preview (look ahead) control model developed by C. C. <br> MacAdam 1,2, . The model represents driver steering control behavior <br> during path-following and obstacle avoidance maneuvers. Drivers preview <br> (look ahead) to follow a predefined path. To implement the MacAdam model, <br> the block: |
| - Represents the dynamics as a linear single track (bicycle) vehicle <br> - Minimizes the previewed error signal at a single point $T^{*}$ seconds ahead <br> in time |  |
| Accounts for the driver lag deriving from perceptual and neuromuscular <br> mechanisms |  |

Use the Lateral control type, controlTypeLat parameter to specify the type of lateral control. The table specifies the block implementation.

| Setting | Block Implementation |
| :--- | :--- |
| Predictive (default) | Optimal single-point preview (look ahead) control model developed by C. <br> C. MacAdam <br> 1,2,3. The model represents driver steering control behavior <br> during path-following and obstacle avoidance maneuvers. Drivers <br> preview (look ahead) to follow a predefined path. |


| Setting | Block Implementation |  |
| :---: | :---: | :---: |
| Stanley | Controller that uses the Stanley ${ }^{4}$ method to minimize the position error and the angle error of the current pose with respect to the reference pose. <br> On the Reference Control pane, use the: <br> - Vector input for poses parameter to input the to specify the input. |  |
|  | Setting | Implementation |
|  | off (default) | Block uses the longitudinal, lateral, and yaw reference (LongRef, LatRef, LatRef) input ports and the feedback (LongFdbk, LatFdbk, LatFdbk) input ports for the reference and feedback pose. |
|  | on | Block uses input ports, RefPose and CurrPose, for the reference and feedback pose, respectively. |
|  | - Include dynamics parameter to specify the type of model for the controller to use. |  |
|  | Setting | Implementation |
|  | off (default) | Controller uses a kinematic bicycle model that is suitable for path following in low-speed environments such as parking lots, where inertial effects are minimal. |
|  | on | Controller uses a dynamic bicycle model that is suitable for path following in high-speed environments such as highways, where inertial effects are more pronounced. |

## Shift

Use the Shift type, ShftType parameter to specify one of these shift options.

| Setting | Block Implementation |
| :--- | :--- |
| None | No transmission. Block outputs a constant gear of 1. |
| Use this setting to minimize the number of parameters you need to generate <br> acceleration and braking commands to track forward vehicle motion. This <br> setting does not allow reverse vehicle motion. |  |


| Setting | Block Implementation |
| :--- | :--- |
| Reverse, Neutral, <br> Drive | Block uses a Stateflow chart to model reverse, neutral, and drive gear shift <br> scheduling. <br> Use this setting to generate acceleration and braking commands to track <br> forward and reverse vehicle motion using simple reverse, neutral, and drive <br> gear shift scheduling. Depending on the vehicle state and vehicle velocity <br> feedback, the block uses the initial gear and time required to shift to shift <br> the vehicle up into drive or down into reverse or neutral. |
| For neutral gears, the block uses braking commands to control the vehicle <br> speed. For reverse gears, the block uses an acceleration command to <br> generate torque and a brake command to reduce vehicle speed. |  |
| Block uses a Stateflow chart to model reverse, neutral, park, and N-speed <br> gear shift scheduling. |  |
| Use this setting to generate acceleration and braking commands to track <br> forward and reverse vehicle motion using reverse, neutral, park, and N- <br> speed gear shift scheduling. Depending on the vehicle state and vehicle <br> velocity feedback, the block uses these parameters to determine the: |  |
| - Initial gear |  |
| - Upshift and downshift accelerator pedal positions |  |
| - Upshift and downshift velocity |  |
| - Timing for shifting and engaging forward and reverse from neutral |  |
| For neutral gears, the block uses braking commands to control the vehicle |  |$|$| speed. For reverse gears, the block uses an acceleration command to |
| :--- |
| generate torque and a brake command to reduce vehicle speed. |

## Units

Use the and Longitudinal velocity units, velUnits and Angular units, angUnits parameter to specify the units for the input and output ports.

## Gear Signal

Use the Output gear signal parameter to create the GearCmd output port. The GearCmd signal contains the integer value of the commanded vehicle gear.

| Gear | Integer |
| :--- | :--- |
| Park | 80 |
| Reverse | -1 |


| Gear | Integer |
| :--- | :--- |
| Neutral | 0 |
| Drive | 1 |
| Gear | Gear number |

Output Handwheel Angle
Use the Output handwheel angle parameter to specify the units for the steering ports.

| Setting | Block Implementation | Port |
| :--- | :--- | :--- |
| off (default) | Commanded steer angle, normalized from -1 <br> through 1. The block uses the tire wheel angle <br> saturation limit Tire wheel angle limit, <br> theta parameter to normalize the command. | SteerCmd - Output |
|  | Overrides the steering command with an input <br> steering command normalized from -1 through <br> 1. | SteerOvrCmd - Input |
| on | Commanded steer angle, in units specified by <br> Angular units, angUnits. | SteerCmd - Output |
| Overrides the steering command with an input <br> steering command, in units specified by <br> Angular units, angUnits. | SteerOvrCmd - Input |  |

## Controller: PI Speed-Tracking

If you set the control type to PI or Scheduled PI, the block implements proportional-integral (PI) control with tracking windup and feed-forward gains. For the Scheduled PI configuration, the block uses feed forward gains that are a function of vehicle velocity.

To calculate the speed control output, the block uses these equations.

| Setting | Equation |
| :--- | :---: |
| PI | $y=\frac{K_{f f}}{v_{\text {nom }}} v_{r e f}+\frac{K_{p} e_{r e f}}{v_{\text {nom }}}+\int\left(\frac{K_{i} e_{r e f}}{v_{\text {nom }}}+K_{a w} e_{o u t}\right) d t+K_{g} \theta$ |
| Scheduled PI | $y=\frac{K_{f f}(v)}{v_{\text {nom }}} v_{r e f}+\frac{K_{p}(v) e_{r e f}}{v_{\text {nom }}}+\int\left(\frac{K_{i}(v) e_{r e f}}{v_{\text {nom }}}+K_{a w} e_{o u t}\right) e_{r e f} d t+K_{g}(v) \theta$ |

where:

$$
\begin{aligned}
& e_{\text {ref }}=v_{\text {ref }}-v \\
& e_{\text {out }}=y_{\text {sat }}-y \\
& y_{\text {sat }}=\left\{\begin{array}{cc}
-1 & y<-1 \\
y & -1 \leq y \leq 1 \\
1 & 1<y
\end{array}\right.
\end{aligned}
$$

The velocity error low-pass filter uses this transfer function.

$$
H(s)=\frac{1}{\tau_{e r r} s+1} \text { for } \tau_{\text {err }}>0
$$

To calculate the acceleration and braking commands, the block uses these equations.

$$
\begin{aligned}
& y_{\text {acc }}=\left\{\begin{array}{cc}
0 & y_{\text {sat }}<0 \\
y_{\text {sat }} & 0 \leq y_{\text {sat }} \leq 1 \\
1 & 1<y_{\text {sat }}
\end{array}\right. \\
& y_{\text {dec }}=\left\{\begin{array}{cc}
0 & y_{\text {sat }}>0 \\
-y_{\text {sat }} & -1 \leq y_{\text {sat }} \leq 0 \\
1 & y_{\text {sat }}<-1
\end{array}\right.
\end{aligned}
$$

The equations use these variables.

| $v_{\text {nom }}$ | Nominal vehicle speed |
| :--- | :--- |
| $K_{p}$ | Proportional gain |
| $K_{i}$ | Integral gain |
| $K_{a w}$ | Anti-windup gain |
| $K_{f f}$ | Velocity feed-forward gain |
| $K_{g}$ | Grade angle feed-forward gain |
| $\theta$ | Grade angle |
| $\tau_{\text {err }}$ | Error filter time constant |
| $y$ | Nominal control output magnitude |
| $y_{\text {sat }}$ | Saturated control output magnitude |
| $e_{r e f}$ | Velocity error |
| $e_{\text {out }}$ | Difference between saturated and nominal control outputs |
| $y_{a c c}$ | Acceleration signal |
| $y_{d e c}$ | Braking signal |
| $v$ | Velocity feedback signal |
| $v_{r e f}$ | Reference velocity signal |

## Controller: Predictive Speed-Tracking

If you set the Longitudinal control type, cntrlType or Lateral control type, cntrlType to Predictive, the block implements an optimal single-point preview (look ahead) control model developed by C. C. MacAdam ${ }^{1,2,3}$. The model represents driver steering control behavior during pathfollowing and obstacle avoidance maneuvers. Drivers preview (look ahead) to follow a predefined path. To implement the MacAdam model, the block:

- Represents the dynamics as a linear single track (bicycle) vehicle
- Minimizes the previewed error signal at a single point $T^{*}$ seconds ahead in time
- Accounts for the driver lag deriving from perceptual and neuromuscular mechanisms


## Vehicle Dynamics

For lateral and yaw motion, the block implements these linear dynamic equations.
$x_{1}=U$
$\dot{x}_{1}=x_{2}=\frac{K_{p t}}{m}+v r-g \sin (\gamma)+F_{r} \chi_{1}$
$\dot{y}=v+U \psi$
$\dot{v}=\left[-\frac{2\left(C_{\alpha F}+C_{\alpha R}\right)}{m U}\right] v+\left[\frac{2\left(b C_{\alpha R}-a C_{\alpha F}\right)}{m U}-U\right] r+\left(\frac{2 C_{\alpha F}}{m}\right) \delta_{F}$
$\dot{r}=\left[\frac{2\left(b C_{\alpha R}-a C_{\alpha F}\right)}{I U}\right] v+\left[-\frac{2\left(a^{2} C_{\alpha F}+b^{2} C_{\alpha R}\right)}{I U}\right] r+\left(\frac{2 a C_{\alpha F}}{I}\right) \delta_{F}$
$\dot{\psi}=r$
In matrix notation:
$\dot{x}=F x+g u$
where:
$x=\left[\begin{array}{l}x_{1} \\ x_{2} \\ y \\ v \\ r \\ \psi\end{array}\right]$
$F=\left[\begin{array}{cccccc}0 & 1 & 0 & 0 & 0 & 0 \\ \frac{F_{r}}{m} & 0 & 0 & 0 & v & 0 \\ 0 & 0 & 0 & 1 & 0 & U \\ 0 & 0 & 0 & -\frac{2\left(C_{\alpha F}+C_{\alpha R}\right)}{m U} & \frac{2\left(b C_{\alpha R}-a C_{\alpha F}\right)}{m U}-U & 0 \\ 0 & 0 & 0 & \frac{2\left(b C_{\alpha R}-a C_{\alpha F}\right)}{I U} & -\frac{2\left(a^{2} C_{\alpha F}+b^{2} C_{\alpha R}\right)}{I U} & 0 \\ 0 & 0 & 0 & 0 & 1 & 0\end{array}\right]$
$g=\left[\begin{array}{cc}0 & 0 \\ \frac{K_{p t}}{m} & 0 \\ 0 & 0 \\ 0 & \frac{2 C_{\alpha F}}{m} \\ 0 & \frac{2 a C_{\alpha F}}{I} \\ 0 & 0\end{array}\right]$
$u=\left[\begin{array}{l}\bar{u} \\ \delta_{F}\end{array}\right]$
$\bar{u}=u-\frac{m^{2}}{K_{p t}} g \sin (\gamma)$

The single-point model assumes a minimum previewed error signal at a single point $T^{*}$ seconds ahead in time. $a^{*}$ is the driver ability to predict the future vehicle response based on the current steering control input. $b^{*}$ is the driver ability to predict the future vehicle response based on the current vehicle state. The block uses these equations.

$$
\begin{aligned}
& a^{*}=\left(T^{*}\right) m^{T}\left[I+\sum_{n=1}^{\infty} \frac{F^{n}\left(T^{*}\right)^{n}}{(n+1)!}\right] g \\
& b^{*}=m^{T}\left[I+\sum_{n=1}^{\infty} \frac{F^{n}\left(T^{*}\right)^{n}}{n!}\right] \\
& m^{T}=\left[\begin{array}{lllll}
1 & 1 & 1 & 0 & 0
\end{array}\right]
\end{aligned}
$$

The equations use these variables.

| $a, b$ | Forward and rearward tire location, respectively |
| :--- | :--- |
| $m$ | Vehicle mass |
| $I$ | Vehicle rotational inertia |
| $C_{\alpha F}$ | Front tire cornering coefficient |
| $C_{\alpha R}$ | Rear tire cornering coefficient |
| $a^{*}, \boldsymbol{b}^{*}$ | Driver prediction scalar and vector gain, respectively |
| $\boldsymbol{x}$ | Predicted vehicle state vector |
| $v$ | Lateral velocity |
| $r$ | Yaw rate |
| $\Psi$ | Front wheel heading angle |
| $y$ | Lateral displacement |
| $\boldsymbol{F}$ | System matrix |
| $\delta, \delta_{F}$ | Steer angle and front axle steer angle, respectively |
| $\gamma$ | Grade angle |
| $\boldsymbol{g}$ | Control coefficient vector |
| $U$ | Forward (longitudinal) vehicle velocity |
| $T^{*}$ | Preview time window |
| $f\left(t+T^{*}\right)$ | Previewed path input T* seconds ahead |
| $\boldsymbol{u}$ | Tractive force |
| $\boldsymbol{m}^{T}$ | Constant observer vector; provides vehicle lateral position |
| $a_{r}$ | Static rolling and driveline resistance |
| $b_{r}$ | Linear rolling and driveline resistance |
| $c_{r}$ | Aerodynamic rolling and driveline resistance |
| $F_{r}$ | Rolling resistance |

## Optimization

The single-point model implemented by the block finds the steering command that minimizes a local performance index, $J$, over the current preview interval, $(t, t+T)$.

$$
J=\frac{1}{T} \int^{t+T}[f(\eta)-y(\eta)]^{2} d \eta
$$

To minimize $J$ with respect to the steering command, this condition must be met.

$$
\frac{d J}{d u}=0
$$

You can express the optimal control solution in terms of a current non-optimal and corresponding nonzero preview output error $T^{*}$ seconds ahead ${ }^{1,2,3}$.

$$
u^{o}(t)=u(t)+\frac{e\left(t+T^{*}\right)}{a^{*}}
$$

The block uses the preview distance and vehicle longitudinal velocity to determine the preview time window.

$$
T^{*}=\frac{L}{U}
$$

The equations use these variables.

| $T^{*}$ | Preview time window |
| :--- | :--- |
| $f\left(t+T^{*}\right)$ | Previewed path input $T^{*} \sec$ ahead |
| $y\left(t+T^{*}\right)$ | Previewed plant output $T^{*}$ sec ahead |
| $e\left(t+T^{*}\right)$ | Previewed error signal $T^{*}$ sec ahead |
| $u(t), u^{o}(t)$ | Steer angle and optimal steer angle, respectively |
| $L$ | Preview distance |
| $J$ | Performance index |
| $U$ | Forward (longitudinal) vehicle velocity |

## Driver Lag

The single-point model implemented by the block introduces a driver lag. The driver lag accounts for the delay when the driver is tracking tasks. Specifically, it is the transport delay deriving from perceptual and neuromuscular mechanisms. To calculate the driver transport delay, the block implements this equation.

$$
H(s)=e^{-s \tau}
$$

The equations use these variables.

| $\tau$ | Driver transport delay |
| :--- | :--- |
| $y\left(t+T^{*}\right)$ | Previewed plant output $T^{*}$ sec ahead |
| $e\left(t+T^{*}\right)$ | Previewed error signal $T^{*}$ sec ahead |
| $u(t), u^{\circ}(t)$ | Steer angle and optimal steer angle, respectively |
| $J$ | Performance index |

## Controller: Stanley Lateral Path-Tracking

If you set Lateral control type, controlTypeLat to Stanley, the block implements the Stanley method ${ }^{4}$. To compute the steering angle command, the Stanley controller minimizes the position error
and the angle error of the current pose with respect to the reference pose. The driving direction of the vehicle determines these error values.

To compute the steering angle command, the controller minimizes the position error and the angle error of the current pose with respect to the reference pose.

- The position error is the lateral distance from the vehicle center-of-gravity (CG) to the reference point on the path.
- The angle error is the angle of the vehicle with respect to reference path.


## Ports

Input
VelRef - Reference vehicle velocity
scalar
Reference velocity, $v_{\text {ref }}$, in units specified by Longitudinal velocity units, velUnits.
LongRef - Longitudinal displacement reference
scalar
Longitudinal center of mass (CM) displacement reference, in the inertial reference frame, in m .

## Dependencies

To enable this port:
1 Set Lateral control type, controlTypeLat to Stanley.
2 Clear Vector input for poses.
LatRef - Lateral displacement reference
scalar
Lateral center of mass (CM) displacement reference, in the inertial reference frame, in m .

## Dependencies

To enable this port, do one of these:

- Set Lateral control type, controlTypeLat to Stanley and clear Vector input for poses.
- Set Lateral control type, controlTypeLat to Predictive.

YawRef - Yaw angle reference
scalar
Vehicle yaw angle, $\Psi_{o}$, in the inertial reference frame, in units specified by Angular units, angUnits.

## Dependencies

To enable this port:

- Set Lateral control type, controlTypeLat to Stanley
- Clear Vector input for poses

EnblSteerOvr - Enable steering command override scalar

Enable steering command override.

## Dependencies

To enable this port, select Steering override.
Data Types: Boolean
SteerOvrCmd - Steering override command scalar

Steering override command.
Use the Output handwheel angle parameter to specify the units for the steering ports.

| Setting | Block Implementation | Port |
| :--- | :--- | :--- |
| off (default) | Commanded steer angle, normalized from -1 <br> through 1. The block uses the tire wheel angle <br> saturation limit Tire wheel angle limit, <br> theta parameter to normalize the command. | SteerCmd - Output |
|  | Overrides the steering command with an input <br> steering command normalized from -1 through <br> 1. | SteerOvrCmd - Input |
| on | Commanded steer angle, in units specified by <br> Angular units, angUnits. | SteerCmd - Output |
| Overrides the steering command with an input <br> steering command, in units specified by <br> Angular units, angUnits. | SteerOvrCmd - Input |  |

## Dependencies

To enable this port, select Steering override.
Data Types: double
SteerHId - Steering hold
scalar
Boolean signal that holds the steering command at the current value.

## Dependencies

To enable this port, select Steering hold
Data Types: Boolean
SteerZero - Disable steering command
scalar
Disable steering command.

## Dependencies

To enable this port, select Steering disable.
Data Types: Boolean
EnblAccelOvr - Enable acceleration command override
scalar
Enable acceleration command override.
Dependencies
To enable this port, select Acceleration override.
Data Types: Boolean
AccelOvrCmd - Acceleration override command
scalar
Acceleration override command, normalized from 0 through 1.

## Dependencies

To enable this port, select Acceleration override.
Data Types: double
AccelHId - Acceleration hold
scalar
Boolean signal that holds the acceleration command at the current value.
Dependencies
To enable this port, select Acceleration hold.
Data Types: Boolean
AccelZero - Disable acceleration command
scalar
Disable acceleration command.

## Dependencies

To enable this port, select Acceleration disable.
Data Types: Boolean
EnbIDeceIOvr - Enable deceleration command override scalar

Enable deceleration command override.

## Dependencies

To enable this port, select Deceleration override.
Data Types: Boolean

DecelOvrCmd - Deceleration override command scalar

Deceleration override command, normalized from 0 through 1.

## Dependencies

To enable this port, select Deceleration override.
Data Types: double
DecelHId - Deceleration hold
scalar
Boolean signal that holds the deceleration command at the current value.

## Dependencies

To enable this port, select Deceleration hold.
Data Types: Boolean
DecelZero - Disable deceleration command
scalar
Disable deceleration command.

## Dependencies

To enable this port, select Deceleration disable.
Data Types: Boolean
ExtGear - Gear
scalar

| Gear | Integer |
| :--- | :--- |
| Park | 80 |
| Reverse | -1 |
| Neutral | 0 |
| Drive | 1 |
| Gear | Gear number |

## Dependencies

To enable this port, set Shift type, shftType to External.
Grade - Road grade angle scalar

Road grade angle, $\gamma$, in deg.
RefPose - Reference pose
$[x, y, \Theta]$ vector

Reference pose, specified as an $[x, y, \Theta]$ vector. $x$ and $y$ are in meters, and $\Theta$ are in units specified by Angular units, angUnits.
$x$ and $y$ specify the reference point to steer the vehicle toward. $\Theta$ specifies the orientation angle of the path at this reference point and is positive in the counterclockwise direction.

The reference point is the point on the path that is closest to the vehicle CG. You can use the either the Z-up or Z-down vehicle coordinate system, as long you use the same coordinate system (Z-up or Z-down) for block inputs and parameters.


## Dependencies

To enable this port:
1 Set Lateral control type, controlTypeLat to Stanley.
2 Select Vector input for poses.
Data Types: single | double
VeIFdbk - Longitudinal vehicle velocity
scalar
Longitudinal vehicle velocity, $U$, in the vehicle-fixed frame, in units specified by Longitudinal velocity units, velUnits.

CurrPose - Current pose
$[x, y, \Theta]$ vector

Current pose of the vehicle, specified as an $[x, y, \Theta]$ vector. $x$ and $y$ are in meters, and $\Theta$ is in units specified by Angular units, angUnits.
$x$ and $y$ specify the location of the vehicle, which is defined as the vehicle CG. You can use the either the Z-up or Z-down vehicle coordinate system, as long you use the same coordinate system (Z-up or Z-down) for block inputs and parameters.


## Dependencies

To enable this port, set Lateral control type, controlTypeLat to Stanley and select Vector input for poses.
Data Types: single | double
LatFdbk - Lateral displacement
scalar
Lateral CM displacement, $y_{o}$, in the inertial reference frame, in $m$.

## Dependencies

To enable this port, do either of these:

- Set Lateral control type, controlTypeLat to Stanley and clear Vector input for poses.
- Set Lateral control type, controlTypeLat to Predictive.

LatVeIFdbk - Lateral vehicle velocity
scalar
Lateral vehicle velocity, $v_{0}$, in the vehicle-fixed frame, in $\mathrm{m} / \mathrm{s}$.

## Dependencies

To enable this port, Set Lateral control type, controlTypeLat to Predictive.
YawFdbk - Vehicle yaw angle
scalar
Vehicle yaw angle, $\Psi_{o}$, in the inertial reference frame, in units specified by Angular units, angUnits.

## Dependencies

To enable this port, do either of these:

- Set Lateral control type, controlTypeLat to Stanley and clear Vector input for poses.
- Set Lateral control type, controlTypeLat to Predictive.

YawVelFdbk - Yaw rate
scalar
Yaw rate, $r_{0}$, in the vehicle-fixed frame, in units specified by Angular units, angUnits per sec.

## Dependencies

To enable this port, Set Lateral control type, controlTypeLat to Predictive.

## Output

Info - Bus signal
bus
Bus signal containing these block calculations.

| Signal |  |  | Variable | Description |
| :---: | :---: | :---: | :---: | :---: |
| Steer |  |  | $\delta_{F}$ | Commanded steer angle, normalized from 0 through 1 |
| Accel |  |  | $y_{\text {acc }}$ | Commanded vehicle acceleration, normalized from 0 through 1 |
| Decel |  |  | $y_{\text {dec }}$ | Commanded vehicle deceleration, normalized from 0 through 1 |
| Gear |  |  |  | Integer value of commanded gear |
| Clutch |  |  |  | Clutch command |
| Err | LatErr | Err | $e_{\text {ref }}$ | Difference in reference vehicle position and vehicle position. |
|  |  | ErrSqrSum | $\int_{0}^{t} e_{r e f^{2} d t}$ | Integrated square of error. |
|  |  | ErrMax | $\max _{\mathrm{m})}\left(e_{r e f}(t\right.$ | Maximum error during simulation. |
|  |  | ErrMin | $\min _{)}\left(e_{r e f}(t\right.$ | Minimum error during simulation. |
|  | LngErr | Err | $e_{\text {ref }}$ | Difference in reference vehicle speed and vehicle speed |


| Signal |  | Variable | Description |
| :---: | :---: | :---: | :---: |
|  | ErrSqrSum | $\int_{0}^{t} e_{r e f^{2} d t}$ | Integrated square of error |
|  | ErrMax | $\max _{)}\left(e_{r e f}(t\right.$ | Maximum error during simulation |
|  | ErrMin | $\left.\min _{\mathrm{m}}\right)\left(e_{r e f}(t\right.$ | Minimum error during simulation |
| ExtAct ions | EnblSteer0vr |  | Override the steering command with an input deceleration command |
|  | SteerOvrCmd |  | Input steering override command |
|  | SteerHld |  | Hold the steering command at the current value |
|  | SteerZero |  | Disable the steering command |
|  | EnblAccel0vr |  | Override the accelerator command with an input acceleration command |
|  | Accel0vrCmd |  | Input accelerator override command |
|  | Accelhld |  | Hold the acceleration command at the current value |
|  | AccelZero |  | Disable the acceleration command |
|  | EnblDecel0vr |  | Override the decelerator command with an input deceleration command |
|  | Decel0vrCmd |  | Input deceleration override command |
|  | Decelhld |  | Hold the decelerator command at current value |
|  | DecelZero |  | Disable the decelerator command |

SteerCmd - Steer angle command
scalar
Commanded steer angle, $\delta_{F}$.
Use the Output handwheel angle parameter to specify the units for the steering ports.

| Setting | Block Implementation | Port |
| :--- | :--- | :--- |
| off (default) | Commanded steer angle, normalized from -1 <br> through 1. The block uses the tire wheel angle <br> saturation limit Tire wheel angle limit, <br> theta parameter to normalize the command. | SteerCmd - Output |
|  | Overrides the steering command with an input <br> steering command normalized from -1 through <br> 1. | SteerOvrCmd - Input |
| on | Commanded steer angle, in units specified by <br> Angular units, angUnits. | SteerCmd - Output |
|  | Overrides the steering command with an input <br> steering command, in units specified by <br> Angular units, angUnits. | SteerOvrCmd - Input |

AccelCmd - Commanded vehicle acceleration scalar

Commanded vehicle acceleration, $y_{\text {acc }}$, normalized from 0 through 1.
DecelCmd - Commanded vehicle deceleration
scalar
Commanded vehicle deceleration, $y_{d e c}$, normalized from 0 through 1.
GearCmd - Commanded vehicle gear
scalar
Integer value of commanded vehicle gear.

| Gear | Integer |
| :--- | :--- |
| Park | 80 |
| Reverse | -1 |
| Neutral | 0 |
| Drive | 1 |
| Gear | Gear number |

## Dependencies

To enable this port, select Output gear signal.

## Parameters

## Configuration

## External Actions

Accelerator override - Override acceleration command
off (default) | on
Select to override the acceleration command with an input acceleration command.

## Dependencies

Selecting this parameter creates the EnblAccelOvr and AccelOvrCmd input ports.

## Accelerator hold - Hold acceleration command

off (default) | on
Select to hold the acceleration command.

## Dependencies

Selecting this parameter creates the AccelHld input port.
Accelerator disable - Disable acceleration command
off (default) | on
Select to disable the acceleration command.

## Dependencies

Selecting this parameter creates the AccelZero input port.
Decelerator override - Override deceleration command off (default) | on

Select to override the deceleration command with an input deceleration command.

## Dependencies

Selecting this parameter creates the EnblDecelovr and DecelovrCmd input ports.
Decelerator hold - Hold deceleration command
off (default) |on
Select to hold the deceleration command.

## Dependencies

Selecting this parameter creates the DecelHld input port.
Decelerator disable - Disable deceleration command
off (default) | on
Select to disable the deceleration command.

## Dependencies

Selecting this parameter creates the DecelZero input port.
Steering override - Override steering command
off (default) | on
Select to override the steering command with an input steering command.

## Dependencies

Selecting this parameter creates the EnblSteerOvr and SteerOvrCmd input ports.
Steering hold - Hold steering command
off (default) | on
Select to hold the steering command.

## Dependencies

Selecting this parameter creates the SteerHld input port.
Steering disable - Disable steering command
off (default) |on
Select to disable the steering command.

## Dependencies

Selecting this parameter creates the SteerZero input port.

## Control and Shift

Longitudinal control type, cntriType - Longitudinal control
PI (default) | Scheduled PI | Predictive
Type of longitudinal control.

| Setting | Block Implementation |
| :--- | :--- |
| PI | Proportional-integral (PI) control with tracking windup and feed-forward <br> gains. |
| Scheduled PI | PI control with tracking windup and feed-forward gains that are a function <br> of vehicle velocity. |
| Predictive | Optimal single-point preview (look ahead) control model developed by C. C. <br> MacAdam 1,2, . The model represents driver steering control behavior <br> during path-following and obstacle avoidance maneuvers. Drivers preview <br> (look ahead) to follow a predefined path. To implement the MacAdam model, <br> the block: |
| - Represents the dynamics as a linear single track (bicycle) vehicle <br> - Minimizes the previewed error signal at a single point $T^{*}$ seconds ahead <br> in time |  |
| Accounts for the driver lag deriving from perceptual and neuromuscular <br> mechanisms |  |

## Lateral control type, controlTypeLat - Controller

Predictive (default) | Stanley
Use the Lateral control type, controlTypeLat parameter to specify the type of lateral control. The table specifies the block implementation.

| Setting | Block Implementation |
| :--- | :--- |
| Predictive (default) | Optimal single-point preview (look ahead) control model developed by C. <br> C. MacAdam <br> 1,2,3. The model represents driver steering control behavior <br> during path-following and obstacle avoidance maneuvers. Drivers <br> preview (look ahead) to follow a predefined path. |


| Setting | Block Implementat |  |
| :---: | :---: | :---: |
| Stanley | Controller that uses the Stanley ${ }^{4}$ method to minimize the position error and the angle error of the current pose with respect to the reference pose. <br> On the Reference Control pane, use the: <br> - Vector input for poses parameter to input the to specify the input. |  |
|  | Setting | Implementation |
|  | off (default) | Block uses the longitudinal, lateral, and yaw reference (LongRef, LatRef, LatRef) input ports and the feedback (LongFdbk, LatFdbk, LatFdbk) input ports for the reference and feedback pose. |
|  | on | Block uses input ports, RefPose and CurrPose, for the reference and feedback pose, respectively. |
|  | - Include dynamics parameter to specify the type of model for the controller to use. |  |
|  | Setting | Implementation |
|  | off (default) | Controller uses a kinematic bicycle model that is suitable for path following in low-speed environments such as parking lots, where inertial effects are minimal. |
|  | on | Controller uses a dynamic bicycle model that is suitable for path following in high-speed environments such as highways, where inertial effects are more pronounced. |

Shift type, shftType - Shift type
None (default)|Reverse, Neutral, Drive|Scheduled|External
Shift type

| Setting | Block Implementation |
| :--- | :--- |
| None | No transmission. Block outputs a constant gear of 1. |
| Use this setting to minimize the number of parameters you need to generate <br> acceleration and braking commands to track forward vehicle motion. This <br> setting does not allow reverse vehicle motion. |  |


| Setting | Block Implementation |
| :--- | :--- |
| Reverse, Neutral, <br> Drive | Block uses a Stateflow chart to model reverse, neutral, and drive gear shift <br> scheduling. <br> Use this setting to generate acceleration and braking commands to track <br> forward and reverse vehicle motion using simple reverse, neutral, and drive <br> gear shift scheduling. Depending on the vehicle state and vehicle velocity <br> feedback, the block uses the initial gear and time required to shift to shift <br> the vehicle up into drive or down into reverse or neutral. |
| For neutral gears, the block uses braking commands to control the vehicle <br> speed. For reverse gears, the block uses an acceleration command to <br> generate torque and a brake command to reduce vehicle speed. |  |
| Block uses a Stateflow chart to model reverse, neutral, park, and N-speed <br> gear shift scheduling. |  |
| Use this setting to generate acceleration and braking commands to track <br> forward and reverse vehicle motion using reverse, neutral, park, and N- <br> speed gear shift scheduling. Depending on the vehicle state and vehicle <br> velocity feedback, the block uses these parameters to determine the: |  |
| - Initial gear |  |
| - Upshift and downshift accelerator pedal positions |  |
| - Upshift and downshift velocity |  |
| - Timing for shifting and engaging forward and reverse from neutral |  |
| For neutral gears, the block uses braking commands to control the vehicle |  |
| speed. For reverse gears, the block uses an acceleration command to |  |
| generate torque and a brake command to reduce vehicle speed. |  |

## Longitudinal velocity units, velUnits - Velocity units

$\mathrm{m} / \mathrm{s}$ (default)
Vehicle velocity reference and feedback units.

## Dependencies

If you set Longitudinal control type, CntrlType control type to Scheduled or Scheduled PI, the block uses the Longitudinal velocity units, velUnits for the Nominal speed, vnom parameter dimension.

If you set Shift Type, shftType to Scheduled, the block uses the Longitudinal velocity units, velUnits for these parameter dimensions:

## - Upshift velocity data table, upShftTbl

## - Downshift velocity data table, dwnShftTbl

Angular units, angUnits - Input and output port angular units

## rad (default) | deg

Input and output port angular units.
Output gear signal - Create GearCmd output port
off (default) | on
Specify to create output port GearCmd.
Output handwheel angle - Steering port units in rad
off (default) | on
Use the Output handwheel angle parameter to specify the units for the steering ports.

| Setting | Block Implementation | Port |
| :--- | :--- | :--- |
| off (default) | Commanded steer angle, normalized from -1 <br> through 1. The block uses the tire wheel angle <br> saturation limit Tire wheel angle limit, <br> theta parameter to normalize the command. | SteerCmd - Output |
|  | Overrides the steering command with an input <br> steering command normalized from -1 through <br> 1. | SteerOvrCmd - Input |
| on | Commanded steer angle, in units specified by <br> Angular units, angUnits. | SteerCmd - Output |
|  | Overrides the steering command with an input <br> steering command, in units specified by <br> Angular units, angUnits. | SteerOvrCmd - Input |

## Dependencies

To create the SteerOvrCmd input port, select Steering override.

## Reference Control

## Longitudinal

Proportional gain, Kp - Gain
10 (default) | scalar
Proportional gain, $K_{p}$, dimensionless.

## Dependencies

To create this parameter, set Control type to PI.
Integral gain, Ki - Gain
5 (default) | scalar
Proportional gain, $K_{i}$, dimensionless.

## Dependencies

To create this parameter, set Control type to PI.
Velocity feed-forward, Kff - Gain
. 1 (default) | scalar
Velocity feed-forward gain, $K_{f f}$, dimensionless.

## Dependencies

To create this parameter, set Control type to PI.
Grade angle feed-forward, $\mathbf{K g}$ - Gain
0 (default) | scalar
Grade angle feed-forward gain, $K_{g}$, in $1 /$ deg.

## Dependencies

To create this parameter, set Control type to PI.
Velocity gain breakpoints, VehVelVec - Breakpoints
[0 100] (default)|vector
Velocity gain breakpoints, VehVelVec, dimensionless.

## Dependencies

To create this parameter, set Control type to Scheduled PI.
Velocity feed-forward gain values, KffVec - Gain
[. 1 . 1] (default) |vector
Velocity feed-forward gain values, KffVec, as a function of vehicle velocity, dimensionless.

## Dependencies

To create this parameter, set Control type to Scheduled PI.
Proportional gain values, KpVec - Gain
[10 10] (default) | vector
Proportional gain values, $K p V e c$, as a function of vehicle velocity, dimensionless.

## Dependencies

To create this parameter, set Control type to Scheduled PI.
Integral gain values, KiVec - Gain
[5 5] (default)| vector
Integral gain values, KiVec, as a function of vehicle velocity, dimensionless.

## Dependencies

To create this parameter, set Control type to Scheduled PI.

## Grade angle feed-forward values, $\mathbf{K g V e c}$ - Grade gain

[0 0] (default)| vector
Grade angle feed-forward values, KgVec , as a function of vehicle velocity, in $1 / \mathrm{deg}$.

## Dependencies

To create this parameter, set Control type to Scheduled PI.
Nominal speed, vnom - Nominal vehicle speed
5 (default) | scalar
Nominal vehicle speed, $v_{\text {nom }}$, in units specified by the Reference and feedback units, velUnits parameter. The block uses the nominal speed to normalize the controller gains.

## Dependencies

To create this parameter, set Control type to PI or Scheduled PI.
Anti-windup, Kaw - Gain
1 (default) | scalar
Anti-windup gain, $K_{a w}$, dimensionless.

## Dependencies

To create this parameter, set Control type to PI or Scheduled PI.
Error filter time constant, tauerr - Filter
. 01 (default) | scalar
Error filter time constant, $\tau_{\text {err }}$, in s. To disable the filter, enter 0.

## Dependencies

To create this parameter, set Control type to PI or Scheduled PI.

## Predictive

Driver response time, tau - Response time
0.1 (default) | scalar

Driver response time, $\tau$, in s.

## Dependencies

To enable this parameter, Set Longitudinal control type, cntrlType or Lateral control type, controlTypeLat to Predictive.

Preview distance, L - Distance
3 (default) | scalar
Driver preview distance, $L$, in m . Used to determine the preview time window, $T^{*}$.

## Dependencies

To enable this parameter, Set Longitudinal control type, cntrlType or Lateral control type, controlTypeLat to Predictive.

Effective vehicle total tractive force, Kpt - Tractive force
3000 (default) | scalar
Effective vehicle total tractive force, $K_{p t}$, in N.

## Dependencies

To create this parameter, set Longitudinal control type, cntrlType to Predictive.
Rolling resistance coefficient, aR - Resistance
200 (default) | scalar
Static rolling and driveline resistance coefficient, $a_{R}$, in N. Block uses the parameter to estimate the constant acceleration or braking effort.

## Dependencies

To create this parameter, set Longitudinal control type, cntrlType to Predictive.
Rolling and driveline resistance coefficient, bR - Resistance
2.5 (default) | scalar

Rolling and driveline resistance coefficient, $b_{R}$, in $\mathrm{N} \cdot \mathrm{s} / \mathrm{m}$. Block uses the parameter to estimate the linear velocity-dependent acceleration or braking effort.

## Dependencies

To create this parameter, set Longitudinal control type, cntrlType to Predictive.

## Aerodynamic drag coefficient, cR - Drag

. 5 (default) | scalar
Aerodynamic drag coefficient, $c_{R}$, in $\mathrm{N} \cdot \mathrm{s}^{\wedge} 2 / \mathrm{m}^{\wedge} 2$. Block uses the parameter to estimate the quadratic velocity-dependent acceleration or braking effort.

## Dependencies

To create this parameter, set Longitudinal control type, cntrlType to Predictive.
Gravitational constant, $\mathbf{g}$ - Gravitational constant
9.81 (default) | scalar

Gravitational constant, g , in $\mathrm{m} / \mathrm{s}^{\wedge} 2$.

## Dependencies

To create this parameter, set Longitudinal control type, cntrlType to Predictive.
Stanley
Vector input for poses - Select to create RefPose and CurrPose input ports off (default) | on

Select this parameter to create the RefPose and CurrPose input ports.

## Dependencies

To enable this parameter, Set Lateral control type, controlTypeLat to Stanley.

## Include dynamics - Select to include dynamics

off (default) | on
The controller computes this command using the Stanley method, whose control law is based on both a kinematic and dynamic bicycle model. To change between models, use this parameter.

| Setting | Implementation |
| :--- | :--- |
| off | Controller uses a kinematic bicycle model that is suitable for path <br> following in low-speed environments such as parking lots, where <br> inertial effects are minimal. |
| on | Controller uses a dynamic bicycle model that is suitable for path <br> following in high-speed environments such as highways, where inertial <br> effects are more pronounced. |

## Dependencies

To enable this parameter, Set Lateral control type, controlTypeLat to Stanley.
Position gain of forward motion, PositionGainF - Position gain of vehicle in forward motion 2.5 (default) | positive real scalar

Position gain of the vehicle when it is in forward motion, specified as a positive scalar. This value determines how much the position error affects the steering angle. Typical values are in the range [1, 5]. Increase this value to increase the magnitude of the steering angle.

## Dependencies

To enable this parameter, Set Lateral control type, controlTypeLat to Stanley.
Position gain of reverse motion, PositionGainF - Position gain of vehicle in reverse motion 2.5 (default) | positive real scalar

Position gain of the vehicle when it is in reverse motion, specified as a positive scalar. This value determines how much the position error affects the steering angle. Typical values are in the range [1, 5]. Increase this value to increase the magnitude of the steering angle.

## Dependencies

To enable this parameter, Set Lateral control type, controlTypeLat to Stanley.
Yaw rate feedback gain, YawRateGain - Yaw rate feedback gain
. 2 (default) | nonnegative real scalar
Yaw rate feedback gain, specified as a nonnegative real scalar. This value determines how much weight is given to the current yaw rate of the vehicle when the block computes the steering angle command.

## Dependencies

To enable this parameter, Set Lateral control type, controlTypeLat to Stanley and select Include dynamics.

## Steering angle feedback gain, DelayGain - Steering angle feedback gain

.2 (default) | nonnegative real scalar

Steering angle feedback gain, specified as a nonnegative real scalar. This value determines how much the difference between the current steering angle command, SteerCmd, and the current steering angle, CurrSteer, affects the next steering angle command.

## Dependencies

To enable this parameter, Set Lateral control type, controlTypeLat to Stanley and select Include dynamics.

## Vehicle Parameters

Forward location of tire, a - Along vehicle longitudinal axis

### 1.41 (default) | scalar

Forward location of tire, $a$, in m . Distance from vehicle cg to forward tire location, along vehicle longitudinal axis.

Rearward location of tire, $\mathbf{b}$ - Along vehicle longitudinal axis
1.41 (default) | scalar

Rearward location of tire, $b$, in $m$. Absolute value of distance from vehicle cg to rearward tire location, along vehicle longitudinal axis.

Vehicle mass, m - Mass
2016 (default) | scalar
Vehicle mass, $m$, in kg.

## Dependencies

To enable this port, do either of these:

- Set Lateral control type, controlTypeLat to Stanley and select Include dynamics.
- Set Lateral control type, controlTypeLat to Predictive.

Front tire cornering coefficient, Cy_f - Coefficient
25266 (default) | scalar
Cornering stiffness coefficient, $C_{\alpha F}$, in $\mathrm{N} / \mathrm{rad}$.

## Dependencies

To enable this port, do either of these:

- Set Lateral control type, controlTypeLat to Stanley and select Include dynamics.
- Set Lateral control type, controlTypeLat to Predictive.

Rear tire cornering coefficient, Cy_r - Coefficient
70933 (default) | scalar
Cornering stiffness coefficient, $C_{\alpha R}$, in $\mathrm{N} / \mathrm{rad}$.

## Dependencies

To enable this port, set Lateral control type, controlTypeLat to Predictive.

Vehicle rotational inertia, I - Inertia about yaw axis
4013 (default) | scalar
Vehicle rotational inertia, $I$, about the vehicle yaw axis, in $N \cdot m \cdot s^{\wedge} 2$.

## Dependencies

To enable this parameter, Set Lateral control type, controlTypeLat to Predictive.
Nominal steering ratio, Ksteer - Steering ratio
18 (default) | scalar
Steering ratio, $K_{\text {steer }}$. The value has no dimension.

## Dependencies

To enable this parameter, select Output handwheel angle.
Tire wheel angle limit, theta - Angle limit
45*pi/180 (default) | scalar
Tire wheel angle limit, $\theta$, in rad.

## Shift

Reverse, Neutral, Drive
Initial gear, GearInit - Initial gear
0 (default) | scalar
Integer value of the initial gear. The block uses the initial gear to generate acceleration and braking commands to track forward and reverse vehicle motion.

| Gear | Integer |
| :--- | :--- |
| Park | 80 |
| Reverse | -1 |
| Neutral | 0 |
| Drive | 1 |
| Gear | Gear number |

## Dependencies

To create this parameter, set Shift type, shftType to Reverse, Neutral, Drive or Scheduled. If you specify Reverse, Neutral, Drive, the Initial Gear, GearInit parameter value can be only -1, 0 , or 1 .

Time required to shift, tShift - Time

## . 1 (default) | scalar

Time required to shift, $t$ Shift, in s. The block uses the time required to shift to generate acceleration and braking commands to track forward and reverse vehicle motion using reverse, neutral, and drive gear shift scheduling.

## Dependencies

To create this parameter, set Shift type, shftType to Reverse, Neutral, Drive.
Scheduled
Initial gear, GearInit - Initial gear
0 (default) | scalar
Integer value of the initial gear. The block uses the initial gear to generate acceleration and braking commands to track forward and reverse vehicle motion.

| Gear | Integer |
| :--- | :--- |
| Park | 80 |
| Reverse | -1 |
| Neutral | 0 |
| Drive | 1 |
| Gear | Gear number |

## Dependencies

To create this parameter, set Shift type, shftType to Reverse, Neutral, Drive or Scheduled. If you specify Reverse, Neutral, Drive, the Initial Gear, GearInit parameter value can be only -1, 0 , or 1 .

Up and down shift accelerator pedal positions, pdIVec - Pedal position breakpoints
[0.1 0.4 0.5 0.9] (default)|[1-by-m] vector
Pedal position breakpoints for lookup tables when calculating upshift and downshift velocities, dimensionless. Vector dimensions are 1 by the number of pedal position breakpoints, $m$.

## Dependencies

To create this parameter, set Shift type, shftType to Scheduled.

## Upshift velocity data table, upShftTbI - Table <br> [m-by-n] array

Upshift velocity data as a function of pedal position and gear, in units specified by the Reference and feedback units, velUnits parameter. Upshift velocities indicate the vehicle velocity at which the gear should increase by 1 .

The array dimensions are m pedal positions by n gears. The first column of data, when n equals 1 , is the upshift velocity for the neutral gear.

## Dependencies

To create this parameter, set Shift type, shftType to Scheduled.

## Downshift velocity data table, dwnShftTbl - Table

[m-by-n] array
Downshift velocity data as a function of pedal position and gear, in units specified by the Reference and feedback units, velUnits parameter. Downshift velocities indicate the vehicle velocity at which the gear should decrease by 1 .

The array dimensions are m pedal positions by n gears. The first column of data, when n equals 1 , is the downshift velocity for the neutral gear.

## Dependencies

To create this parameter, set Shift type, shftType to Scheduled.
Time required to shift, tClutch - Time
. 5 (default) | scalar
Time required to shift, $t_{\text {Clutch }}$, in s .

## Dependencies

To create this parameter, set Shift type, shftType to Scheduled.
Time required to engage reverse from neutral, tRev - Time

## . 5 (default) | scalar

Time required to engage reverse from neutral, $t_{\text {Rev, }}$ in s .

## Dependencies

To create this parameter, set Shift type, shftType to Scheduled.

## Time required to engage park from neutral, tPark - Time

120 (default) | scalar
Time required to engage park from neutral, $t_{\text {Park }}$ in s .

## Dependencies

To create this parameter, set Shift type, shftType to Scheduled.

## Version History

## Introduced in R2018a

## References

[1] MacAdam, C. C. "An Optimal Preview Control for Linear Systems". Journal of Dynamic Systems, Measurement, and Control. Vol. 102, Number 3, Sept. 1980.
[2] MacAdam, C. C. "Application of an Optimal Preview Control for Simulation of Closed-Loop Automobile Driving ". IEEE Transactions on Systems, Man, and Cybernetics. Vol. 11, Issue 6, June 1981.
[3] MacAdam, C. C. Development of Driver/Vehicle Steering Interaction Models for Dynamic Analysis. Final Technical Report UMTRI-88-53. Ann Arbor, Michigan: The University of Michigan Transportation Research Institute, Dec. 1988.
[4] Hoffmann, Gabriel M., Claire J. Tomlin, Michael Montemerlo, and Sebastian Thrun. "Autonomous Automobile Trajectory Tracking for Off-Road Driving: Controller Design, Experimental Validation and Racing." American Control Conference. 2007, pp. 2296-2301. doi:10.1109/ ACC.2007.4282788

## Extended Capabilities

C/C++ Code Generation
Generate C and C++ code using Simulink ${ }^{\circledR}$ Coder ${ }^{\mathrm{TM}}$.

## See Also

Lateral Driver | Longitudinal Driver

## 3D Simulation Blocks

## Simulation 3D Actor Transform Get

Get actor translation, rotation, scale


## Libraries:

Vehicle Dynamics Blockset / Vehicle Scenarios / Sim3D / Sim3D Core Aerospace Blockset / Animation / Simulation 3D
Simulink 3D Animation / Simulation 3D

## Description

The Simulation 3D Actor Transform Get block provides the actor translation, rotation, and scale for the Simulink simulation environment.

The block uses a vehicle-fixed coordinate system that is initially aligned with the inertial world coordinate system.


| Axis | Description |
| :--- | :--- |
| $X$ | Forward direction of the vehicle <br> Roll $~-~ R i g h t-h a n d e d ~ r o t a t i o n ~ a b o u t ~$ <br> $X$ |
| $Y$ | Extends to the right of the vehicle, initially parallel to the ground plane <br> Pitch $~-~ R i g h t-h a n d e d ~ r o t a t i o n ~ a b o u t ~$ -axis |$|$| $Z$ | Extends upwards |
| :--- | :--- |
| Yaw - Left-handed rotation about Z-axis |  |

Actors are scene objects that support 3D translation, rotation, and scale. Parts are actor components. Components do not exist by themselves; they are associated with an actor.

Tip Verify that the Simulation 3D Scene Configuration block executes before the Simulation 3D Actor Transform Get block. That way, the Unreal Engine 3D visualization environment prepares the data
before the Simulation 3D Actor Transform Get block receives it. To check the block execution order, right-click the blocks and select Properties. On the General tab, confirm these Priority settings:

- Simulation 3D Scene Configuration - 0
- Simulation 3D Actor Transform Get - 1

For more information about execution order, see "Control and Display Execution Order".

## Ports

## Output

Translation - Actor translation
array
Actor translation, in m. Array dimensions are number of parts per actor-by-3.

- Translation(1,1), Translation(1,2), and Translation(1,3) - Vehicle displacement along world $X$-, $Y$, and $Z$ - axes, respectively.
- Translation(...,1), Translation(...,2), and Translation(..., 3) - Actor displacement relative to vehicle, in vehicle-fixed coordinate system initially aligned with world $X$-, $Y$, and $Z$ - axes, respectively.

For example, consider a vehicle actor with a vehicle body and four wheels. The Translation signal:

- Dimensions are [5x3].
- Contains translation information according to the axle and wheel locations, relative to vehicle.
Translation $=\left[\begin{array}{ccc}X_{v} & Y_{v} & Z_{v} \\ X_{F L} & Y_{F L} & Z_{F L} \\ X_{F R} & Y_{F R} & Z_{F R} \\ X_{R L} & Y_{R L} & Z_{R L} \\ X_{R R} & Y_{R R} & Z_{R R}\end{array}\right]$

| Translation | Array Element |
| :--- | :--- |
| Vehicle, $X_{v}$ | Translation $(1,1)$ |
| Vehicle, $Y_{v}$ | Translation(1,2) |
| Vehicle, $Z_{v}$ | Translation(1,3) |
| Front left wheel, $X_{F L}$ | Translation(2,1) |
| Front left wheel, $Y_{F L}$ | Translation(2,2) |
| Front left wheel, $Z_{F L}$ | Translation(2,3) |
| Front right wheel, $X_{F R}$ | Translation(3,1) |
| Front right wheel, $Y_{F R}$ | Translation(3,2) |
| Front right wheel, $Z_{F R}$ | Translation(3,3) |
| Rear left wheel, $X_{R L}$ | Translation(4,1) |
| Rear left wheel, $Y_{R L}$ | Translation(4,2) |


| Translation | Array Element |
| :--- | :--- |
| Rear left wheel, $Z_{R L}$ | Translation $(4,3)$ |
| Rear right wheel, $X_{R R}$ | Translation(5,1) |
| Rear right wheel, $Y_{R R}$ | Translation(5,2) |
| Rear right wheel, $Z_{R R}$ | Translation(5,3) |

Rotation - Actor rotation
array
Actor rotation across a [-pi/2, pi/2] range, in rad. Array dimensions are number of parts per actor-by-3.

- Rotation(1,1), Rotation(1,2), and Rotation(1,3) - Vehicle rotation about vehicle-fixed pitch, roll, and yaw $Y$-, $Z$-, and $X$ - axes, respectively.
- Rotation(...,1), Rotation(...,2), and Rotation(...,3) - Actor rotation about vehiclefixed pitch, roll, and yaw $Y$-, $Z$-, and $X$ - axes, respectively.

For example, consider a vehicle actor with a vehicle body and four wheels. The Rotation signal:

- Dimensions are [5x3].
- Contains rotation information according to the axle and wheel locations.

$$
\text { Rotation }=\left[\begin{array}{ccc}
\text { Pitch }_{v} & \text { Roll }_{v} & \text { Yaw }_{v} \\
\text { Pitch }_{F L} & \text { Roll }_{F L} & \text { Yaw }_{F L} \\
\text { Pitch }_{F R} & \text { Roll }_{F R} & \text { Yaw }_{F R} \\
\text { Pitch }_{R L} & \text { Roll }_{R L} & \text { Yaw }_{R L} \\
\text { Pitch }_{R R} & \text { Roll }_{R R} & \text { Yaw }_{R R}
\end{array}\right]
$$

| Rotation | Array Element |
| :--- | :--- |
| Vehicle, Pitch $_{v}$ | Rotation(1,1) |
| Vehicle, Roll $v$ | Rotation(1,2) |
| Vehicle, Yaw | Rotation(1,3) |
| Front left wheel, Pitch $_{F L}$ | Rotation(2,1) |
| Front left wheel, Roll $_{F L}$ | Rotation(2,2) |
| Front left wheel, Yaw | RL |$\quad$ Rotation(2,3) | Front right wheel, Pitch $_{F R}$ | Rotation(3,1) |
| :--- | :--- |
| Front right wheel, Roll $_{F R}$ | Rotation(3,2) |
| Front right wheel, Yaw $_{F R}$ | Rotation(3,3) |
| Rear left wheel, Pitch $_{R L}$ | Rotation(4,1) |
| Rear left wheel, Roll $_{R L}$ | Rotation(4,2) |
| Rear left wheel, Yaw | Rotation(4,3) |
| Rear right wheel, Pitch $_{R R}$ | Rotation(5,1) |
| Rear right wheel, Roll $_{R R}$ | Rotation(5,2) |


| Rotation | Array Element |
| :--- | :--- |
| Rear right wheel, $\operatorname{Yaw}_{R R}$ | Rotation(5,3) |

## Scale - Actor scale

array
Actor scale. Array dimensions are number of number of parts per actor-by-3.

- Scale ( 1,1 ), Scale ( 1,2 ), and Scale ( 1,3 ) - Vehicle scale along world $X$-, $Y$-, and $Z$ - axes, respectively.
- Scale(...,1), Scale(...,2), and Scale(...,3) - Actor scale along world $X$-, $Y$-, and Zaxes, respectively.

For example, consider a vehicle actor with a vehicle body and four wheels. The Scale signal:

- Dimensions are [5x3].
- Contains scale information according to the axle and wheel locations.

$$
\text { Scale }=\left[\begin{array}{ccc}
X_{V_{\text {scale }}} & Y_{V_{\text {scale }}} & Z_{V_{\text {scale }}} \\
X_{F L_{\text {scale }}} & Y_{F L_{\text {scale }}} & Z_{F L_{\text {scale }}} \\
X_{F R_{\text {scale }}} & Y_{F R_{\text {scale }}} & Z_{F R_{\text {scale }}} \\
X_{R L_{\text {scale }}} & Y_{R L_{\text {scale }}} & Z_{R L_{\text {scale }}} \\
X_{R R_{\text {scale }}} & Y_{R R_{\text {scale }}} & Z_{R R_{\text {scale }}}
\end{array}\right]
$$

| Scale | Array Element |
| :---: | :---: |
| Vehicle, $X_{V_{\text {scale }}}$ | Scale(1,1) |
| Vehicle, $Y_{V_{\text {sale }}}$ | Scale(1,2) |
| Vehicle, $Z_{V_{\text {sale }}}$ | Scale(1,3) |
| Front left wheel, $X_{F L_{\text {scale }}}$ | Scale (2,1) |
| Front left wheel, $Y_{F L_{\text {scale }}}$ | Scale(2,2) |
| Front left wheel, $Z_{F L_{\text {sclue }}}$ | Scale(2,3) |
| Front right wheel, $X_{F R_{\text {sale }}}$ | Scale(3,1) |
| Front right wheel, $Y_{F R_{\text {sace }}}$ | Scale(3,2) |
| Front right wheel, $Z_{F R_{\text {sacale }}}$ | Scale(3,3) |
| Rear left wheel, $X_{R L_{\text {scole }}}$ | Scale(4,1) |
| Rear left wheel, $Y_{R L_{\text {sace }}}$ | Scale(4,2) |
| Rear left wheel, $Z_{R L_{\text {scale }}}$ | Scale(4,3) |
| Rear right wheel, $X_{R R_{\text {sale }}}$ | Scale (5,1) |
| Rear right wheel, $Y_{\text {RR }{ }_{\text {scale }}}$ | Scale (5,2) |
| Rear right wheel, $Z_{R R_{\text {scale }}}$ | Scale(5,3) |

## Parameters

Tag for actor in 3D scene, ActorTag - Name
SimulinkActorl (default)| character vector
Actor name.
Actors are scene objects that support 3D translation, rotation, and scale. Parts are actor components. Components do not exist by themselves; they are associated with an actor.

The block does not support multiple instances of the same actor tag. To refer to the same scene actor when you use the 3D block pairs (e.g. Simulation 3D Actor Transform Get and Simulation 3D Actor Transform Set), specify the same Tag for actor in 3D scene, ActorTag parameter.

## Number of parts per actor to get, NumberOfParts - Name

1 (default) | scalar
Number of parts per actor. Actors are scene objects that support 3D translation, rotation, and scale. Parts are actor components. Components do not exist by themselves; they are associated with an actor. Typically, a vehicle actor with a body and four wheels has 5 parts.

The block does not support multiple instances of the same actor tag. To refer to the same scene actor when you use the 3D block pairs (e.g. Simulation 3D Actor Transform Get and Simulation 3D Actor Transform Set), specify the same Tag for actor in 3D scene, ActorTag parameter.

Sample time - Sample time

- 1 (default) | scalar

Sample time, $T_{s}$. The graphics frame rate is the inverse of the sample time.

## Version History

Introduced in R2018a

## See Also

Simulation 3D Actor Transform Set | Simulation 3D Camera Get | Simulation 3D Scene Configuration | Vehicle Terrain Sensor

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"
"How 3D Simulation for Vehicle Dynamics Blockset Works"
"Unreal Engine Simulation Environment Requirements and Limitations"

## Simulation 3D Actor Transform Set

Set actor translation, rotation, scale


## Libraries:

Vehicle Dynamics Blockset / Vehicle Scenarios / Sim3D / Sim3D Core
Aerospace Blockset / Animation / Simulation 3D
Simulink 3D Animation / Simulation 3D

## Description

The Simulation 3D Actor Transform Set block sets the actor translation, rotation, and scale in the 3D visualization environment.

The block uses a vehicle-fixed coordinate system that is initially aligned with the inertial world coordinate system.


| Axis | Description |
| :--- | :--- |
| $X$ | Forward direction of the vehicle <br> Roll - Right-handed rotation about $X$-axis |
| $Y$ | Extends to the right of the vehicle, initially parallel to the ground plane <br> Pitch $~-~ R i g h t-h a n d e d ~ r o t a t i o n ~ a b o u t ~$ -axis |$|$| Extends upwards |
| :--- | :--- |
| Yaw - Left-handed rotation about $Z$-axis |

Actors are scene objects that support 3D translation, rotation, and scale. Parts are actor components. Components do not exist by themselves; they are associated with an actor.

Tip Verify that the Simulation 3D Actor Transform Set block executes before the Simulation 3D Scene Configuration block. That way, Simulation 3D Actor Transform Set prepares the signal data
before the Unreal Engine 3D visualization environment receives it. To check the block execution order, right-click the blocks and select Properties. On the General tab, confirm these Priority settings:

- Simulation 3D Scene Configuration - 0
- Simulation 3D Actor Transform Set - - 1

For more information about execution order, see "Control and Display Execution Order".

## Ports

## Input

Translation - Actor translation
array
Actor translation, in m. Array dimensions are number of parts per actor-by-3.

- Translation(1, 1), Translation(1,2), and Translation(1,3) - Vehicle displacement along world $X$-, $Y$, and $Z$ - axes, respectively.
- Translation(...,1), Translation(...,2), and Translation(...,3) - Actor displacement relative to vehicle, in vehicle-fixed coordinate system initially aligned with world $X$-, $Y$, and $Z$ - axes, respectively.

For example, consider a vehicle actor with a vehicle body and four wheels. The Translation signal:

- Dimensions are [5x3].
- Contains translation information according to the axle and wheel locations, relative to vehicle.

Translation $=\left[\begin{array}{ccc}X_{v} & Y_{v} & Z_{v} \\ X_{F L} & Y_{F L} & Z_{F L} \\ X_{F R} & Y_{F R} & Z_{F R} \\ X_{R L} & Y_{R L} & Z_{R L} \\ X_{R R} & Y_{R R} & Z_{R R}\end{array}\right]$

| Translation | Array Element |
| :--- | :--- |
| Vehicle, $X_{v}$ | Translation(1,1) |
| Vehicle, $Y_{v}$ | Translation(1,2) |
| Vehicle, $Z_{v}$ | Translation(1,3) |
| Front left wheel, $X_{F L}$ | Translation(2,1) |
| Front left wheel, $Y_{F L}$ | Translation(2,2) |
| Front left wheel, $Z_{F L}$ | Translation(2,3) |
| Front right wheel, $X_{F R}$ | Translation(3,1) |
| Front right wheel, $Y_{F R}$ | Translation(3,2) |
| Front right wheel, $Z_{F R}$ | Translation(3,3) |
| Rear left wheel, $X_{R L}$ | Translation(4,1) |


| Translation | Array Element |
| :--- | :--- |
| Rear left wheel, $Y_{R L}$ | Translation (4, 2) |
| Rear left wheel, $Z_{R L}$ | Translation(4, 3) |
| Rear right wheel, $X_{R R}$ | Translation(5, 1) |
| Rear right wheel, $Y_{R R}$ | Translation(5, 2) |
| Rear right wheel, $Z_{R R}$ | Translation(5, 3) |

## Rotation - Actor rotation

array
Actor rotation across a [-pi/2, pi/2] range, in rad. Array dimensions are number of parts per actor-by-3.

- Rotation(1,1), Rotation(1,2), and Rotation(1,3) - Vehicle rotation about vehicle-fixed pitch, roll, and yaw $Y$-, $Z$-, and $X$ - axes, respectively.
- Rotation(..., 1), Rotation(...,2), and Rotation (..., 3) - Actor rotation about vehiclefixed pitch, roll, and yaw $Y$-, $Z$-, and $X$ - axes, respectively.

For example, consider a vehicle actor with a vehicle body and four wheels. The Rotation signal:

- Dimensions are [5×3].
- Contains rotation information according to the axle and wheel locations.

Rotation $=\left[\begin{array}{ccc}\text { Pitch }_{v} & \text { Roll }_{v} & \text { Yaw }_{v} \\ \text { Pitch }_{F L} & \text { Roll }_{F L} & \text { Yaw }_{F L} \\ \text { Pitch }_{F R} & \text { Roll }_{F R} & \text { Yaw }_{F R} \\ \text { Pitch }_{R L} & \text { Roll }_{R L} & \text { Yaw }_{R L} \\ \text { Pitch }_{R R} & \text { Roll }_{R R} & \text { Yaw }_{R R}\end{array}\right]$

| Rotation | Array Element |
| :--- | :--- |
| Vehicle, Pitch $_{v}$ | Rotation(1,1) |
| Vehicle, Roll $_{v}$ | Rotation(1,2) |
| Vehicle, Yaw $_{v}$ | Rotation(1,3) |
| Front left wheel, Pitch $_{F L}$ | Rotation(2,1) |
| Front left wheel, Roll $_{F L}$ | Rotation(2,2) |
| Front left wheel, Yaw | Rotation(2,3) |
| Front right wheel, Pitch $_{F R}$ | Rotation(3,1) |
| Front right wheel, Roll $_{F R}$ | Rotation(3,2) |
| Front right wheel, Yaw | RR |
| Rear left wheel, Pitch $_{R L}$ | Rotation(3,3) |
| Rear left wheel, Roll $_{R L}$ | Rotation(4,1) |
| Rear left wheel, Yaw Pot | Rotation(4,2) |
| Rear right wheel, Pitch $_{R R}$ | Rotation(4,3) |


| Rotation | Array Element |
| :--- | :--- |
| Rear right wheel, $\operatorname{Roll}_{R R}$ | Rotation(5,2) |
| Rear right wheel, $\operatorname{Yaw}_{R R}$ | Rotation(5,3) |

## Scale - Actor scale

array
Actor scale. Array dimensions are number of number of parts per actor-by-3.

- Scale (1, 1), Scale (1, 2), and Scale (1,3) - Vehicle scale along world $X$-, $Y$-, and $Z$ - axes, respectively.
- Scale (..., 1), Scale (...,2), and Scale(...,3) - Actor scale along world $X$-, $Y$-, and Zaxes, respectively.

For example, consider a vehicle actor with a vehicle body and four wheels. The Scale signal:

- Dimensions are [5×3].
- Contains scale information according to the axle and wheel locations.
Scale $=\left[\begin{array}{ccc}X_{V_{\text {scale }}} & Y_{V_{\text {scale }}} & Z_{V_{\text {scale }}} \\ X_{F L_{\text {scale }}} & Y_{F L_{\text {scale }}} & Z_{F L_{\text {scale }}} \\ X_{F R_{\text {scale }}} & Y_{F R_{\text {scale }}} & Z_{F R_{\text {scale }}} \\ X_{R L_{\text {scale }}} & Y_{R L_{\text {scale }}} & Z_{R L_{\text {scale }}} \\ X_{R R_{\text {scale }}} & Y_{R R_{\text {scale }}} & Z_{R R_{\text {scale }}}\end{array}\right]$

| Scale | Array Element |
| :---: | :---: |
| Vehicle, $X_{V_{\text {scade }}}$ | Scale(1,1) |
| Vehicle, $Y_{V_{\text {sale }}}$ | Scale(1,2) |
| Vehicle, $Z_{V_{\text {scale }}}$ | Scale(1,3) |
| Front left wheel, $X_{F L_{\text {scale }}}$ | Scale(2,1) |
| Front left wheel, $Y_{F L_{\text {scale }}}$ | Scale(2,2) |
| Front left wheel, $Z_{F L_{\text {scale }}}$ | Scale (2,3) |
| Front right wheel, $X_{F R_{\text {sace }}}$ | Scale(3,1) |
| Front right wheel, $Y_{F R_{\text {sade }}}$ | Scale(3,2) |
| Front right wheel, $Z_{F R_{\text {sace }}}$ | Scale(3,3) |
| Rear left wheel, $X_{R L_{\text {sale }}}$ | Scale (4,1) |
| Rear left wheel, $Y_{R L_{\text {scale }}}$ | Scale(4,2) |
| Rear left wheel, $Z_{R L_{\text {scale }}}$ | Scale(4,3) |
| Rear right wheel, $X_{\text {RRsale }}$ | Scale (5,1) |
| Rear right wheel, $Y_{R R_{\text {scale }}}$ | Scale (5,2) |
| Rear right wheel, $Z_{R R_{\text {sale }}}$ | Scale(5,3) |

## Parameters

## Actor Setup

Tag for actor in 3D scene, ActorTag - Name
SimulinkActor1 (default) | character vector
Actor name.
Actors are scene objects that support 3D translation, rotation, and scale. Parts are actor components. Components do not exist by themselves; they are associated with an actor.

The block does not support multiple instances of the same actor tag. To refer to the same scene actor when you use the 3D block pairs (e.g. Simulation 3D Actor Transform Get and Simulation 3D Actor Transform Set), specify the same Tag for actor in 3D scene, ActorTag parameter.

## Number of parts per actor to set, NumberOfParts - Name

1 (default) | scalar
Number of parts per actor. Actors are scene objects that support 3D translation, rotation, and scale. Parts are actor components. Components do not exist by themselves; they are associated with an actor. Typically, a vehicle actor with a body and four wheels has 5 parts.

The block does not support multiple instances of the same actor tag. To refer to the same scene actor when you use the 3D block pairs (e.g. Simulation 3D Actor Transform Get and Simulation 3D Actor Transform Set), specify the same Tag for actor in 3D scene, ActorTag parameter.

Initial Values
Initial array values to translate actor per part, Translation - Actor initial position
[0 0 0] (default) |array
Actor initial position, along world $X$-, $Y$-, and $Z$ - axes, in $m$.
Array dimensions are number of parts per actor-by-3.

- Translation(1,1), Translation(1,2), and Translation(1,3) - Vehicle displacement along world $X$-, $Y$, and $Z$ - axes, respectively.
- Translation(...,1), Translation(...,2), and Translation(..., 3) - Actor displacement relative to vehicle, in vehicle-fixed coordinate system initially aligned with world $X$-, $Y$, and $Z$ - axes, respectively.

For example, consider a vehicle actor with a vehicle body and four wheels. The parameter:

- Dimensions are [5×3].
- Contains translation information according to the axle and wheel locations, relative to vehicle.

$$
\text { Translation }=\left[\begin{array}{ccc}
X_{V} & Y_{v} & Z_{V} \\
X_{F L} & Y_{F L} & Z_{F L} \\
X_{F R} & Y_{F R} & Z_{F R} \\
X_{R L} & Y_{R L} & Z_{R L} \\
X_{R R} & Y_{R R} & Z_{R R}
\end{array}\right]
$$

| Translation | Array Element |
| :--- | :--- |
| Vehicle, $X_{v}$ | Translation(1, 1) |
| Vehicle, $Y_{v}$ | Translation(1, 2) |
| Vehicle, $Z_{v}$ | Translation(1, 3) |
| Front left wheel, $X_{F L}$ | Translation(2, 1) |
| Front left wheel, $Y_{F L}$ | Translation(2,2) |
| Front left wheel, $Z_{F L}$ | Translation(2, 3) |
| Front right wheel, $X_{F R}$ | Translation(3, 1) |
| Front right wheel, $Y_{F R}$ | Translation(3, 2) |
| Front right wheel, $Z_{F R}$ | Translation(3, 3) |
| Rear left wheel, $X_{R L}$ | Translation(4, 1) |
| Rear left wheel, $Y_{R L}$ | Translation(4, 2) |
| Rear left wheel, $Z_{R L}$ | Translation(4, 3) |
| Rear right wheel, $X_{R R}$ | Translation(5, 1) |
| Rear right wheel, $Y_{R R}$ | Translation(5, 2) |
| Rear right wheel, $Z_{R R}$ | Translation(5, 3) |

Initial array values to rotate actor per part, Rotation - Actor initial rotation
[0 0 0] (default) |array
Actor initial rotation about world $X-, Y$-, and $Z$ - axes across a $[-\mathrm{pi} / 2$, pi/2] range, in rad.
Array dimensions are number of parts per actor-by-3.

- Rotation(1,1), Rotation(1,2), and Rotation(1,3) - Vehicle rotation about vehicle-fixed pitch, roll, and yaw $Y$-, $Z$-, and $X$ - axes, respectively.
- Rotation(...,1), Rotation(...,2), and Rotation(...,3) - Actor rotation about vehiclefixed pitch, roll, and yaw $Y$-, $Z$-, and $X$ - axes, respectively.

For example, consider a vehicle actor with a vehicle body and four wheels. The parameter:

- Dimensions are [5×3].
- Contains rotation information according to the axle and wheel locations.
Rotation $=\left[\begin{array}{ccc}\text { Pitch }_{\nu} & \text { Roll }_{V} & \text { Yaw }_{\nu} \\ \text { Pitch }_{F L} & \text { Roll }_{F L} & \text { Yaw }_{F L} \\ \text { Pitch }_{F R} & \text { Roll }_{F R} & Y a w_{F R} \\ \text { Pitch }_{R L} & \text { Roll }_{R L} & \text { Yaw }_{R L} \\ \text { Pitch }_{R R} & \text { Roll }_{R R} & \text { Yaw }_{R R}\end{array}\right]$

| Rotation | Array Element |
| :--- | :--- |
| Vehicle, Pitch $_{v}$ | Rotation(1,1) |
| Vehicle, Roll $_{v}$ | Rotation(1,2) |
| Vehicle, Yaw $_{v}$ | Rotation(1,3) |


| Rotation | Array Element |
| :---: | :---: |
| Front left wheel, Pitch $_{\text {FL }}$ | Rotation (2,1) |
| Front left wheel, Roll $_{F L}$ | Rotation (2,2) |
| Front left wheel, Yaw $_{F L}$ | Rotation(2,3) |
| Front right wheel, Pitch $_{F R}$ | Rotation(3,1) |
| Front right wheel, Roll $_{F R}$ | Rotation (3, 2 ) |
| Front right wheel, Yaw $_{\text {FR }}$ | Rotation(3, 3) |
| Rear left wheel, Pitch $_{\text {RL }}$ | Rotation(4,1) |
| Rear left wheel, Roll $_{\text {RL }}$ | Rotation (4, 2 ) |
| Rear left wheel, Yaw $_{R L}$ | Rotation(4, 3) |
| Rear right wheel, Pitch $_{\text {RR }}$ | Rotation(5,1) |
| Rear right wheel, Roll $_{R R}$ | Rotation (5,2) |
| Rear right wheel, Yaw $_{\text {RR }}$ | Rotation(5, 3) |

Initial array values to scale actor per part, Scale - Actor initial scale
[1 1 1] (default)|array
Actor initial scale.
Array dimensions are number of number of parts per actor-by-3.

- Scale (1, 1), Scale (1, 2), and Scale (1, 3) - Vehicle scale along world $X$-, $Y$, and $Z$ - axes, respectively.
- Scale(...,1), Scale(...,2), and Scale(...,3) - Actor scale along world $X$-, $Y$, and $Z$ axes, respectively.

For example, consider a vehicle actor with a vehicle body and four wheels. The parameter:

- Dimensions are [5x3].
- Contains scale information according to the axle and wheel locations.

$$
\text { Scale }=\left[\begin{array}{ccc}
X_{V_{\text {scale }}} & Y_{V_{\text {scale }}} & Z_{V_{\text {scale }}} \\
X_{F L_{\text {scale }}} & Y_{F L_{\text {scale }}} & Z_{F L_{\text {scale }}} \\
X_{F R_{\text {scale }}} & Y_{F R_{\text {scale }}} & Z_{F R_{\text {scale }}} \\
X_{R L_{\text {scale }}} & Y_{R L_{\text {scale }}} & Z_{R L_{\text {scale }}} \\
X_{R R_{\text {scale }}} & Y_{R R_{\text {scale }}} & Z_{R R_{\text {scale }}}
\end{array}\right]
$$

| Scale | Array Element | Scale Axis |
| :--- | :--- | :--- |
| Vehicle, $X_{V_{\text {scale }}}$ | Scale $(1,1)$ | World $X$-axis |
| Vehicle, $V_{V_{\text {scal }}}$ | Scale $(1,2)$ | World $Y$-axis |
| Vehicle, $Z_{V_{\text {scal }}}$ | Scale $(1,3)$ | World $Z$-axis |
| Front left wheel, $X_{F L_{\text {scale }}}$ | Scale $(2,1)$ | World $X$-axis |
| Front left wheel, $Y_{F L_{\text {cole }}}$ | Scale $(2,2)$ | World $Y$-axis |


| Scale | Array Element | Scale Axis |
| :--- | :--- | :--- |
| Front left wheel, $Z_{F L_{\text {scal }}}$ | $\operatorname{Scale}(2,3)$ | World $Z$-axis |
| Front right wheel, $X_{F R_{\text {scal }}}$ | $\operatorname{Scale}(3,1)$ | World $X$-axis |
| Front right wheel, $Y_{F R_{\text {sale }}}$ | $\operatorname{Scale}(3,2)$ | World $Y$-axis |
| Front right wheel, $Z_{F R_{\text {sale }}}$ | Scale $(3,3)$ | World $Z$-axis |
| Rear left wheel, $X_{R L_{\text {scale }}}$ | $\operatorname{Scale}(4,1)$ | World $X$-axis |
| Rear left wheel, $Y_{R L_{\text {sale }}}$ | $\operatorname{Scale}(4,2)$ | World $Y$-axis |
| Rear left wheel, $Z_{R L_{\text {scale }}}$ | $\operatorname{Scale}(4,3)$ | World $Z$-axis |
| Rear right wheel, $X_{R R_{\text {scal }}}$ | $\operatorname{Scale}(5,1)$ | World $X$-axis |
| Rear right wheel, $Y_{R R_{\text {scale }}}$ | $\operatorname{Scale}(5,2)$ | World $Y$-axis |
| Rear right wheel, $Z_{R R_{\text {sade }}}$ | $\operatorname{Scale}(5,3)$ | World $Z$-axis |

Sample time - Sample time

- 1 (default) | scalar

Sample time, $T_{s}$. The graphics frame rate is the inverse of the sample time.

## Version History

## Introduced in R2018a

## See Also

Simulation 3D Actor Transform Get | Simulation 3D Camera Get | Simulation 3D Scene Configuration | Vehicle Terrain Sensor

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"
"How 3D Simulation for Vehicle Dynamics Blockset Works"
"Unreal Engine Simulation Environment Requirements and Limitations"

## Simulation 3D Camera Get

Camera image


## Libraries:

Vehicle Dynamics Blockset / Vehicle Scenarios / Sim3D / Sim3D Core
Aerospace Blockset / Animation / Simulation 3D
Simulink 3D Animation / Simulation 3D

## Description

The Simulation 3D Camera Get block provides an interface to an ideal camera in the 3D visualization environment. The image output is a red, green, and blue (RGB) array.

If you set the sample time to -1, the block uses the sample time specified in the Simulation 3D Scene Configuration block. To use this sensor, ensure that the Simulation 3D Scene Configuration block is in your model.

Tip Verify that the Simulation 3D Scene Configuration block executes before the Simulation 3D Camera Get block. That way, the Unreal Engine 3D visualization environment prepares the data before the Simulation 3D Camera Get block receives it. To check the block execution order, right-click the blocks and select Properties. On the General tab, confirm these Priority settings:

- Simulation 3D Scene Configuration - 0
- Simulation 3D Camera Get - 1

For more information about execution order, see "Control and Display Execution Order".

## Ports

## Output

Image - 3D output camera image
$m$-by- $n$-by-3 array of RGB triplet values
3D output camera image, returned as an $m$-by- $n$-by- 3 array of RGB triplet values. $m$ is the vertical resolution of the image, and $n$ is the horizontal resolution of the image.
Data Types: int8 |uint8

## Parameters

Mounting
Sensor identifier - Number to identify unique sensor
0 (default) | positive integer
Unique sensor identifier, specified as a positive integer. This number is used to identify a specific sensor. The sensor identifier distinguishes between sensors in a multi-sensor system.

## Example: 2

## Vehicle name - Name of a vehicle

Scene Origin (default) | character vector
Vehicle name. Block provides a list of vehicles in the model. If you select Scene Origin, the block places a sensor at the scene origin.

Example: SimulinkVehicle1
Vehicle mounting location - Sensor mounting location
Origin (default)|Front bumper|Rear bumper|Right mirror|Left mirror|Rearview mirror|Hood center|Roof center

Sensor mounting location.

- When Vehicle name is Scene Origin, the block mounts the sensor to the origin of the scene, and Mounting location can be set to Origin only. During simulation, the sensor remains stationary.
- When Vehicle name is the name of a vehicle (for example, SimulinkVehicle1) the block mounts the sensor to one of the predefined mounting locations described in the table. During simulation, the sensor travels with the vehicle.

| Vehicle Mounting Location | Description | Orientation Relative to <br> Vehicle Origin [Roll, Pitch, <br> Yaw] (deg) |
| :--- | :--- | :--- |
| Origin | Forward-facing sensor mounted <br> to the vehicle origin, which is on <br> the ground and at the geometric <br> center of the vehicle (see <br> "Coordinate Systems in Vehicle <br> Dynamics Blockset") | $[0,0]$ |
|  |  |  |


| Vehicle Mounting Location | Description | Orientation Relative to <br> Vehicle Origin [Roll, Pitch, <br> Yaw] (deg) |
| :--- | :--- | :--- |
| Front bumper | Forward-facing sensor mounted <br> to the front bumper | $[0,0,0]$ |
| Rear bumper |  |  |


| Vehicle Mounting Location | Description | Orientation Relative to <br> Vehicle Origin [Roll, Pitch, <br> Yaw] (deg) |
| :--- | :--- | :--- |
| Right mirror | Downward-facing sensor <br> mounted to the right side-view <br> mirror | $[0,-90,0]$ |
|  |  |  |


| Vehicle Mounting Location | Description | Orientation Relative to <br> Vehicle Origin [Roll, Pitch, <br> Yaw] (deg) |
| :--- | :--- | :--- |
| Hood center | Forward-facing sensor mounted <br> to the center of the hood | $[0,0,0]$ |

The $(X, Y, Z)$ location of the sensor relative to the vehicle depends on the vehicle type. To specify the vehicle type, use the Type parameter of the Simulation 3D Scene Configuration block to which you are mounting. The tables show the $X, Y$, and $Z$ locations of sensors in the vehicle coordinate system. In this coordinate system:

- The $X$-axis points forward from the vehicle.
- The $Y$-axis points to the left of the vehicle, as viewed when facing forward.
- The $Z$-axis points up from the ground.
- Roll, pitch, and yaw are clockwise-positive when looking in the positive direction of the $X$-axis, $Y$ axis, and $Z$-axis, respectively. When looking at a vehicle from the top down, then the yaw angle (that is, the orientation angle) is counterclockwise-positive, because you are looking in the negative direction of the axis.

Box Truck - Sensor Locations Relative to Vehicle Origin

| Mounting Location | $\mathbf{X ( m )}$ | $\mathbf{Y}(\mathbf{m})$ | $\mathbf{Z}(\mathbf{m})$ |
| :--- | :--- | :--- | :--- |
| Front bumper | 5.10 | 0 | 0.60 |
| Rear bumper | -5 | 0 | 0.60 |
| Right mirror | 2.90 | 1.60 | 2.10 |
| Left mirror | 2.90 | -1.60 | 2.10 |
| Rearview mirror | 2.60 | 0.20 | 2.60 |
| Hood center | 3.80 | 0 | 2.10 |
| Roof center | 1.30 | 0 | 4.20 |

Hatchback - Sensor Locations Relative to Vehicle Origin

| Mounting Location | $\mathbf{X ( m )}$ | $\mathbf{Y}(\mathbf{m})$ | $\mathbf{Z}(\mathbf{m})$ |
| :--- | :--- | :--- | :--- |
| Front bumper | 1.93 | 0 | 0.51 |
| Rear bumper | -1.93 | 0 | 0.51 |
| Right mirror | 0.43 | -0.84 | 1.01 |
| Left mirror | 0.43 | 0.84 | 1.01 |
| Rearview mirror | 0.32 | 0 | 1.27 |
| Hood center | 1.44 | 0 | 1.01 |
| Roof center | 0 | 0 | 1.57 |

## Muscle Car - Sensor Locations Relative to Vehicle Origin

| Mounting Location | $\mathbf{X ( m )}$ | $\mathbf{Y}(\mathbf{m})$ | $\mathbf{Z}(\mathbf{m})$ |
| :--- | :--- | :--- | :--- |
| Front bumper | 2.47 | 0 | 0.45 |
| Rear bumper | -2.47 | 0 | 0.45 |
| Right mirror | 0.43 | -1.08 | 1.01 |
| Left mirror | 0.43 | 1.08 | 1.01 |
| Rearview mirror | 0.32 | 0 | 1.20 |
| Hood center | 1.28 | 0 | 1.14 |
| Roof center | -0.25 | 0 | 1.58 |

Sedan - Sensor Locations Relative to Vehicle Origin

| Mounting Location | $\mathbf{X}(\mathbf{m})$ | $\mathbf{Y}(\mathbf{m})$ | $\mathbf{Z}(\mathbf{m})$ |
| :--- | :--- | :--- | :--- |
| Front bumper | 2.42 | 0 | 0.51 |
| Rear bumper | -2.42 | 0 | 0.51 |
| Right mirror | 0.59 | -0.94 | 1.09 |
| Left mirror | 0.59 | 0.94 | 1.09 |
| Rearview mirror | 0.43 | 0 | 1.31 |
| Hood center | 1.46 | 0 | 1.11 |
| Roof center | -0.45 | 0 | 1.69 |

Small Pickup Truck - Sensor Locations Relative to Vehicle Origin

| Mounting Location | $\mathbf{X}(\mathbf{m})$ | $\mathbf{Y}(\mathbf{m})$ | $\mathbf{Z}(\mathbf{m})$ |
| :--- | :--- | :--- | :--- |
| Front bumper | 3.07 | 0 | 0.51 |
| Rear bumper | -3.07 | 0 | 0.51 |
| Right mirror | 1.10 | -1.13 | 1.52 |
| Left mirror | 1.10 | 1.13 | 1.52 |
| Rearview mirror | 0.85 | 0 | 1.77 |
| Hood center | 2.22 | 0 | 1.59 |
| Roof center | 0 | 0 | 2.27 |

Sport Utility Vehicle - Sensor Locations Relative to Vehicle Origin

| Mounting Location | $\mathbf{X ( m )}$ | $\mathbf{Y}(\mathbf{m})$ | $\mathbf{Z}(\mathbf{m})$ |
| :--- | :--- | :--- | :--- |
| Front bumper | 2.42 | 0 | 0.51 |
| Rear bumper | -2.42 | 0 | 0.51 |
| Right mirror | 0.60 | -1 | 1.35 |
| Left mirror | 0.60 | 1 | 1.35 |
| Rearview mirror | 0.39 | 0 | 1.55 |
| Hood center | 1.58 | 0 | 1.39 |
| Roof center | -0.56 | 0 | 2 |

Example: Origin
Specify offset - Specify offset from mounting location
off (default) | on
Select this parameter to specify an offset from the mounting location.
Relative translation [ $\mathbf{X}, \mathbf{Y}, \mathbf{Z}$ ] - Translation offset from mounting location
[0,0,0] (default) | real-valued 1-by-3 vector
Specify a translation offset from the mount location, about the vehicle coordinate system $X, Y$, and $Z$ axes. Units are in meters.

- The $X$-axis points forward from the vehicle.
- The $Y$-axis points to the left of the vehicle, as viewed when facing forward.
- The $Z$-axis points up.

Example: [0,0,0.01]
Dependencies
To enable this parameter, select Specify offset.
Relative rotation [Roll, Pitch, Yaw] - Rotational offset from mounting location
[0, 0, 0] (default) | real-valued 1-by-3 vector
Specify a rotational offset from the mounting location, about the vehicle coordinate system $X, Y$, and $Z$ axes. Units are in degrees.

- Roll angle is the angle of rotation about the $X$-axis of the vehicle coordinate system. A positive roll angle corresponds to a clockwise rotation when looking in the positive direction of the $X$-axis.
- Pitch angle is the angle of rotation about the $Y$-axis of the vehicle coordinate system. A positive pitch angle corresponds to a clockwise rotation when looking in the positive direction of the $Y$ axis.
- Yaw angle is the angle of rotation about the $Z$ of the vehicle coordinate system. A positive yaw angle corresponds to a clockwise rotation when looking in the positive direction of the $Z$-axis.

Example: [0, 0, 10]

## Dependencies

To enable this parameter, select Specify offset.

## Sample time - Sample time

-1 (default) | positive scalar
Sample time of the block in seconds. The 3D simulation environment frame rate is the inverse of the sample time.

If you set the sample time to -1 , the block uses the sample time specified in the Simulation 3D Scene Configuration block.

Parameter
Horizontal resolution - Pixels
uint32(1280) (default) | scalar
Horizontal image resolution, in pixels.
Vertical resolution - Pixels
uint32(720) (default) | scalar
Vertical image resolution, in pixels.
Horizontal field of view - Field of view
single(60) (default) | scalar
Horizontal field of view (FOV), in deg.

## Tips

- To understand how to set tag of Sim 3d Scene Cap and how it the tag is related to the block, see "Place Cameras on Actors in the Unreal Editor".


## Version History

Introduced in R2018a

## See Also

Simulation 3D Actor Transform Get | Simulation 3D Actor Transform Set | Simulation 3D Scene Configuration | Vehicle Terrain Sensor

## Topics

"How 3D Simulation for Vehicle Dynamics Blockset Works"
"Scene Interrogation in 3D Environment"
"Unreal Engine Simulation Environment Requirements and Limitations"

## Simulation 3D Scene Configuration

Scene configuration for 3D simulation environment


Libraries:
Vehicle Dynamics Blockset / Vehicle Scenarios / Sim3D / Sim3D Core
Aerospace Blockset / Animation / Simulation 3D
Automated Driving Toolbox / Simulation 3D
UAV Toolbox / Simulation 3D
Simulink 3D Animation / Simulation 3D

## Description

The Simulation 3D Scene Configuration block implements a 3D simulation environment that is rendered by using the Unreal Engine from Epic Games ${ }^{\circledR}$. Vehicle Dynamics Blockset integrates the 3D simulation environment with Simulink so that you can query the world around the vehicle and virtually test perception, control, and planning algorithms. Using this block, you can also control the position of the sun and the weather conditions of a scene. For more details, see Sun Position and Weather on page 7-36.

You can simulate from a set of prebuilt scenes or from your own custom scenes. Scene customization requires the Vehicle Dynamics Blockset Interface for Unreal Engine 4 Projects support package. For more details, see "Customize 3D Scenes for Vehicle Dynamics Simulations".

Note The Simulation 3D Scene Configuration block must execute after blocks that send data to the 3D environment and before blocks that receive data from the 3D environment. To verify the execution order of such blocks, right-click the blocks and select Properties. Then, on the General tab, confirm these Priority settings:

- For blocks that send data to the 3D environment, such as Simulation 3D Vehicle with Ground Following blocks, Priority must be set to -1 . That way, these blocks prepare their data before the 3D environment receives it.
- For the Simulation 3D Scene Configuration block in your model, Priority must be set to 0 .
- For blocks that receive data from the 3D environment, such as Simulation 3D Message Get blocks, Priority must be set to 1 . That way, the 3D environment can prepare the data before these blocks receive it.

For more information about execution order, see "Control and Display Execution Order".

## Parameters

## Scene

## Scene Selection

Scene source - Source of scene
Default Scenes (default)|Unreal Executable|Unreal Editor

Source of the scene in which to simulate, specified as one of the options in the table.

| Option | Description |
| :--- | :--- |
| Default Scenes | Simulate in one of the default, prebuilt scenes <br> specified in the Scene name parameter. |
| Unreal Executable | Simulate in a scene that is part of an Unreal <br> Engine executable file. Specify the executable file <br> in the Project name parameter. Specify the <br> scene in the Scene parameter. |
| Unreal Editor | Select this option to simulate in custom scenes <br> that have been packaged into an executable for <br> faster simulation. |
| Simulate in a scene that is part of an Unreal <br> Engine project (. uproject) file and is open in <br> the Unreal® Editor. Specify the project file in the <br> Project parameter. |  |
| Select this option when developing custom <br> scenes. By clicking Open Unreal Editor, you can <br> co-simulate within Simulink and the Unreal <br> Editor and modify your scenes based on the <br> simulation results. |  |

## Scene name - Name of prebuilt 3D scene

Straight road (default)|Curved road|Parking lot|Double lane change|Open surface|US city block|US highway|Virtual Mcity|Large parking lot

Name of the prebuilt 3D scene in which to simulate, specified as one of these options. For details about a scene, see its listed corresponding reference page.

- Straight road - Straight Road
- Curved road - Curved Road
- Parking lot - Parking Lot
- Double lane change - Double Lane Change
- Open surface - Open Surface
- US city block - US City Block
- US highway - US Highway
- Virtual Mcity - Virtual Mcity
- Large parking lot - Large Parking Lot

The Vehicle Dynamics Blockset Interface for Unreal Engine 4 Projects contains customizable versions of these scenes. For details about customizing scenes, see "Customize 3D Scenes for Vehicle Dynamics Simulations".

## Dependencies

To enable this parameter, set Scene source to Default Scenes.

Project name - Name of Unreal Engine executable file
VehicleSimulation.exe (default) | valid executable file name
Name of the Unreal Engine executable file, specified as a valid executable project file name. You can either browse for the file or specify the full path to the project file, using backslashes. To specify a scene from this file to simulate in, use the Scene parameter.

By default, Project name is set to VehicleSimulation.exe, which is on the MATLAB search path.

## Example: C:\Local\WindowsNoEditor\AutoVrtlEnv.exe

## Dependencies

To enable this parameter, set Scene source to Unreal Executable.
Select ASAM OpenDRIVE file - Specify an ASAM OpenDRIVE file
off (default) | on
Specify an ASAM OpenDRIVE ${ }^{\circledR}$ file. Select the Simulation 3D Scene Configuration block parameter Select ASAM OpenDRIVE file to specify an ASAM OpenDRIVE file. You will need an ASAM OpenDRIVE file if you want to perform any lane detection applications with custom scenes using the Simulation 3D Vision Detection Generator block.

## Dependencies

This parameter is available when you set Scene Source is set to either Unreal Executable or Unreal Engine.
Data Types: Boolean
Scene - Name of scene from executable file
/Game/Maps/HwStrght (default) | path to valid scene name
Name of a scene from the executable file specified by the Project name parameter, specified as a path to a valid scene name.

When you package scenes from an Unreal Engine project into an executable file, the Unreal Editor saves the scenes to an internal folder within the executable file. This folder is located at the path / Game/Maps. Therefore, you must prepend /Game/Maps to the scene name. You must specify this path using forward slashes. For the file name, do not specify the . umap extension. For example, if the scene from the executable in which you want to simulate is named myScene. umap, specify Scene as /Game/Maps/myScene.

Alternatively, you can browse for the scene in the corresponding Unreal Engine project. These scenes are typically saved to the Content/Maps subfolder of the project. This subfolder contains all the scenes in your project. The scenes have the extension . umap. Select one of the scenes that you packaged into the executable file specified by the Project name parameter. Use backward slashes and specify the . umap extension for the scene.

By default, Scene is set to /Game/Maps/HwStrght, which is a scene from the default VehicleSimulation. exe executable file specified by the Project name parameter. This scene corresponds to the prebuilt Straight Road scene.

Example: /Game/Maps/scenel

## Example: C:\Local\myProject\Content \Maps\scene1.umap

## Dependencies

To enable this parameter, set Scene source to Unreal Executable.
Project - Name of Unreal Engine project file
valid project file name
Name of the Unreal Engine project file, specified as a valid project file name. You can either browse for the file or specify the full path to the file, using backslashes. The file must contain no spaces. To simulate scenes from this project in the Unreal Editor, click Open Unreal Editor. If you have an Unreal Editor session open already, then this button is disabled.

To run the simulation, in Simulink, click Run. Before you click Play in the Unreal Editor, wait until the Diagnostic Viewer window displays this confirmation message:

```
In the Simulation 3D Scene Configuration block, you set the scene source to 'Unreal Editor'.
```

In Unreal Editor, select 'Play' to view the scene.

This message confirms that Simulink has instantiated the scene actors, including the vehicles and cameras, in the Unreal Engine 3D environment. If you click Play before the Diagnostic Viewer window displays this confirmation message, Simulink might not instantiate the actors in the Unreal Editor.

## Dependencies

To enable this parameter, set Scene source to Unreal Editor.

## Scene Parameters

Scene view - Configure placement of virtual camera that displays scene

## Scene Origin|vehicle name

Configure the placement of the virtual camera that displays the scene during simulation.

- If your model contains no Simulation 3D Vehicle or Simulation 3D Vehicle with Ground Following blocks, then during simulation, you view the scene from a camera positioned at the scene origin.
- If your model contains at least one vehicle block, then by default, you view the scene from behind the first vehicle that was placed in your model. To change the view to a different vehicle, set
Scene view to the name of that vehicle. The Scene view parameter list is populated with all the Name parameter values of the vehicle blocks contained in your model.

If you add a Simulation 3D Scene Configuration block to your model before adding any vehicle blocks, the virtual camera remains positioned at the scene. To reposition the camera to follow a vehicle, update this parameter.

When Scene view is set to a vehicle name, during simulation, you can change the location of the camera around the vehicle.

To smoothly change the camera views, use these key commands.


| Key | Camera Vie |  |
| :---: | :---: | :---: |
| 2 | Back | View Animated GIF |
| 3 | Back right |  |
| 4 | Left |  |
| 5 | Internal |  |
| 6 | Right |  |
| 7 | Front left |  |
| 8 | Front |  |
| 9 | Front right |  |
| 0 | Overhead |  |

For additional camera controls, use these key commands.

| Key | Camera Control |
| :--- | :--- |
| Tab | Cycle the view between all vehicles in the scene. <br> View Animated GIF |
|  |  |
|  |  |
|  |  |


| Key | Camera Control |
| :--- | :--- |
| Mouse scroll wheel | Control the camera distance from the vehicle. <br> View Animated GIF |
| L | Toggle a camera lag effect on or off. When you enable the lag effect, the <br> camera view includes: <br> Position lag, based on the vehicle translational acceleration <br> Rotation lag, based on the vehicle rotational velocity <br> This lag enables improved visualization of overall vehicle acceleration and <br> rotation. <br> View Animated GIF |


| Key | Camera Control |
| :--- | :--- |
| F | Toggle the free camera mode on or off. When you enable the free camera <br> mode, you can use the mouse to change the pitch and yaw of the camera. <br> This mode enables you to orbit the camera around the vehicle. <br> View Animated GIF |

Sample time - Sample time of visualization engine
. 02 (default) | scalar greater than or equal to 0.01
Sample time, $T_{s^{\prime}}$ of the visualization engine, specified as a scalar greater than or equal to 0.01 . Units are in seconds.

The graphics frame rate of the visualization engine is the inverse of the sample time. For example, if
Sample time is $1 / 60$, then the visualization engine solver tries to achieve a frame rate of 60 frames per second. However, the real-time graphics frame rate is often lower due to factors such as graphics card performance and model complexity.

By default, blocks that receive data from the visualization engine, such as Simulation 3D Message blocks, inherit this sample rate.

Display 3D simulation window - Unreal Engine visualization

```
on (default)| off
```

Select whether to run simulations in the 3D visualization environment without visualizing the results, that is, in headless mode.

Consider running in headless mode in these cases:

- You want to run multiple 3D simulations in parallel to test models in different Unreal Engine scenarios.
- You want to optimize model parameters without visualizing the results. For example, consider using headless mode if you want to tune vehicle suspension parameters over a terrain scenario defined in Unreal Engine.


## Dependencies

To enable this parameter, set Scene source to Default Scenes or Unreal Executable.

## Weather

Override scene weather - Control the scene weather and sun position
off (default) |on
Select whether to control the scene weather and sun position during simulation. Use the enabled parameters to change the sun position, clouds, fog, and rain.

This table summarizes sun position settings for specific times of day.

| Time of Day | Settings | Unreal Editor Environment |
| :---: | :---: | :---: |
| Midnight | Sun altitude: -90 Sun azimuth: 180 |  |
| Sunrise in the | Sun altitude: 0 |  |
| Noon | Sun altitude: 90 |  |
|  | Sun azimuth: 180 |  |
|  |  | $v$ |

This table summarizes settings for specific cloud conditions.

| Cloud <br> Condition | Settings | Unreal Editor Environment |
| :--- | :--- | :--- |
| Clear | Cloud opacity: 0 |  |
|  |  |  |
| Heavy | Cloud opacity: 85 |  |
|  |  | $\ddots$ |

This table summarizes settings for specific fog conditions.

| Fog Condition | Settings | Unreal Editor Environment |
| :--- | :--- | :--- |
| None | Fog density: 0 |  |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |

This table summarizes settings for specific rain conditions.

| Rain Condition | Settings | Unreal Editor Environment |  |
| :--- | :--- | :--- | :--- |
| Light | Cloud opacity: 10 |  |  |
|  | Rain density: 25 |  |  |
| Heavy | Cloud opacity: 10 |  |  |
|  | Rain density: 80 |  |  |

Sun altitude - Altitude angle between sun and horizon
40 (default) | any value between -90 and 90
Altitude angle in a vertical plane between the sun's rays and the horizontal projection of the rays, in deg.


Use the Sun altitude and Sun azimuth parameters to control the time of day in the scene. For example, to specify sunrise in the north, set Sun altitude to 0 deg and Sun azimuth to 180 deg.

## Dependencies

To enable this parameter, select Override scene weather.
Sun azimuth - Azimuth angle from south to horizontal projection of the sun ray
90 (default) | any value between 0 and 360
Azimuth angle in the horizontal plane measured from the south to the horizontal projection of the sun rays, in deg.


Use the Sun altitude and Sun azimuth parameters to control the time of day in the scene. For example, to specify sunrise in the north, set Sun altitude to 0 deg and Sun azimuth to 180 deg.

## Dependencies

To enable this parameter, select Override scene weather.
Cloud opacity - Unreal Editor Cloud Opacity global actor target value
10 (default) | any value between 0 and 100
Parameter that corresponds to the Unreal Editor Cloud Opacity global actor target value, in percent. Zero is a cloudless scene.


Use the Cloud opacity and Cloud speed parameters to control clouds in the scene.

## Dependencies

To enable this parameter, select Override scene weather.
Cloud speed - Unreal Editor Cloud Speed global actor target value
1 (default) | any value between - 100 and 100
Parameter that corresponds to the Unreal Editor Cloud Speed global actor target value. The clouds move from west to east for positive values and east to west for negative values.


Use the Cloud opacity and Cloud speed parameters to control clouds in the scene.
Dependencies
To enable this parameter, select Override scene weather.
Fog density - Unreal Editor Set Fog Density and Set Start Distance target values
0 (default) | any value between 0 and 100
Parameter that corresponds to the Unreal Editor Set Fog Density and Set Start Distance target values, in percent.


## Dependencies

To enable this parameter, select Override scene weather.
Rain density - Unreal Editor local actor controlling rain density, wetness, rain puddles, and ripples
0 (default) | any value between 0 and 100
Parameter corresponding to the Unreal Editor local actor that controls rain density, wetness, rain puddles, and ripples, in percent.


Use the Cloud opacity and Rain density parameters to control rain in the scene.
Dependencies
To enable this parameter, select Override scene weather.

## More About

## Sun Position and Weather

To control the scene weather and sun position, on the Weather tab, select Override scene weather.
Use the enabled parameters to change the sun position, clouds, fog, and rain during the simulation.

## Sun Position

Use Sun altitude and Sun azimuth to control the sun position.

- Sun altitude - Altitude angle in a vertical plane between the sun rays and the horizontal projection of the rays.
- Sun azimuth - Azimuth angle in the horizontal plane measured from the south to the horizontal projection of the sun rays.


This table summarizes sun position settings for specific times of day.

| Time of Day | Settings | Unreal Editor Environment |
| :--- | :--- | :--- | :--- |
| Midnight | Sun altitude: -90 |  |
| Sun azimuth: 180 |  |  |

## Clouds

Use Cloud opacity and Cloud speed to control clouds in the scene.

- Cloud opacity - Unreal Editor Cloud Opacity global actor target value. Zero is a cloudless scene.
- Cloud speed - Unreal Editor Cloud Speed global actor target value. The clouds move from west to east for positive values and east to west for negative values.


This table summarizes settings for specific cloud conditions.

| Cloud <br> Condition | Settings | Unreal Editor Environment |
| :--- | :--- | :--- |
| Clear | Cloud opacity: 0 |  |
|  |  |  |
|  |  |  |
| Heavy | Cloud opacity: 85 |  |
|  |  | $\ddots$ |

Fog
Use Fog density to control fog in the scene. Fog density corresponds to the Unreal Editor Set Fog Density.


This table summarizes settings for specific fog conditions.

| Fog Condition | Settings | Unreal Editor Environment |
| :--- | :--- | :--- |
| None | Fog density: 0 |  |
|  |  |  |
|  |  |  |
| Heavy |  |  |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |

## Rain

Use Cloud opacity and Rain density to control rain in the scene.

- Cloud opacity - Unreal Editor Cloud Opacity global actor target value.
- Rain density - Unreal Editor local actor that controls rain density, wetness, rain puddles, and ripples.


This table summarizes settings for specific rain conditions.

| Rain Condition | Settings | Unreal Editor Environment |
| :---: | :---: | :---: |
| Light | Cloud opacity: 10 Rain density: 25 |  |
| Heavy | Cloud opacity: 10 Rain density: 80 |  |

## Version History

## Introduced in R2018a

## See Also

Simulation 3D Vehicle with Ground Following | Simulation 3D Vehicle

## Topics

"How 3D Simulation for Vehicle Dynamics Blockset Works"
"Scene Interrogation in 3D Environment"
"Unreal Engine Simulation Environment Requirements and Limitations"
"Customize 3D Scenes for Vehicle Dynamics Simulations"
"Prepare Custom Vehicle Mesh for the Unreal Editor"

## Vehicle Terrain Sensor

Vehicle and tire distances to objects


## Libraries:

Vehicle Dynamics Blockset / Vehicle Scenarios / Sim3D / Sim3D Vehicle / Components

## Description

The Vehicle Terrain Sensor block implements ray tracing to detect the terrain below the tires and objects in front of the vehicle. Specifically, for these actor components, the block returns the hit location (in the world coordinate system) and the distance to an object.

- Vehicle body
- Left front wheel
- Right front wheel
- Left rear wheel
- Right rear wheel

Tip Verify that the Vehicle Terrain Sensor block executes before the Simulation 3D Fisheye Camera block. That way, the Unreal Engine 3D visualization environment prepares the data before the Vehicle Terrain Sensor block receives it. To check the block execution order, right-click the blocks and select Properties. On the General tab, confirm these Priority settings:

- Simulation 3D Scene Configuration - 0
- Vehicle Terrain Sensor - 1

For more information about execution order, see "Control and Display Execution Order".

Actors are scene objects that support 3D translation, rotation, and scale. Parts are actor components. Components do not exist by themselves; they are associated with an actor.

## Hit Distance

To calculate the hit distances shown in the illustration, the block implements these equations.

| Front of vehicle to object, | DistToHitVh = GetLength(CntrLocVh, HitLocVh) |
| :--- | :--- |
| DistToHitVhAdjust | DistToHitVhAdjust = DistToHitVh - VehCntrLngthVal |
|  | EndLocVh = CntrLocVh + VehRayLngth - VehRayOffset <br>  <br>  <br>  <br>  <br> VehRayOffset = CntrLocVh - StartLocVh <br> VehRayLngth = StartLocVh - EndLocVh |


| Tires to terrain, |  |
| :--- | :--- |
| DistToHitTrAdjust | DistToHitTr $=$ GetLength(CntrLocTr, HitLocTr) |
| DistToHitTrAdjust $=$ DistToHitTr - TireRadiiVal |  |
| EndLocTr = CntrLocTr + LengthTr - OffsetTr |  |
| OffsetTr = CntrLocTr - StartLocTr |  |
| LengthTr = StartLocTr - EndLocTr |  |



This illustration and equations use these variables.

| CntrLocVh | Vehicle center location |
| :--- | :--- |
| DistToHitVh | Distance from vehicle center location to object |
| DistToHitVhAdjust | Distance from the front of the vehicle to object |
| EndLocVh | Vehicle ray trace end |
| HitLocVh | Vehicle hit location |
| OffsetVh | Vehicle trace offset |
| StartLocVh | Vehicle ray trace start |
| VehRayLngth | Vehicle trace length |
| VehCntrLngthVal | Distance from vehicle center to front |
| CntrLocTr | Tire center location |
| DistToHitTr | Distance from tire center location to terrain |
| DistToHitTrAdjust | Distance from tire to terrain |
| HitLocTr | Tire hit location |
| EndLocTr | Tire ray trace end |
| OffsetTr | Tire trace offset |
| StartLocTr | Tire ray trace start |


| LengthTr | Tire trace length |
| :--- | :--- |
| TireRadiiVal | Tire radius |

## Hit Event

To determine a hit event, the block uses the ray trace. The block provides the hit location in the world coordinate system.


## Miss Event

To determine a miss event, the block uses the ray trace.


## Ports

Input
VehCntr - Vehicle distance from center to front
scalar
Distance from the vehicle center to front, VehCntrLngthVal, in m.

## Dependencies

| Distance to vehicle <br> center | Creates Port | Creates Parameter |
| :--- | :--- | :--- |
| Constant | None | Distance from vehicle center to front, <br> VehCntrLngthVal |
| External input | VehCntr | None |

TireRadii - Tire radii
array
Tire radii, TireRadiiVal, in m.

Dependencies

| Distance to tire center <br> Setting | Creates Port | Creates Parameter |
| :--- | :--- | :--- |
| Constant | None | Distance from tire center to ground, <br> TireRadiiVal |
| External input | TireRadii | None |

## Output

Info - Bus signal
bus
Bus signal containing block values. The signals are arrays that depend on the wheel location.

| Signal | Description | Variable | Units |
| :---: | :---: | :---: | :---: |
| HitFlg | Vehicle and wheel hit flag: <br> - Hit an object - 1 <br> - Miss an object - 0 | $\left[\begin{array}{c}\text { Vehicle } \\ \text { FrontLeft } \\ \text { FrontRight } \\ \text { RearLeft } \\ \text { RearRight }\end{array}\right]$ | NA |
| HitLoc | Vehicle, HitLocVh, and tire, HitLocTr, hit locations, in world coordinate system $X$-, $Y$, and Z- axes, respectively | $\left[\begin{array}{ccc}\text { Vehicle }_{X} & \text { Vehicle }_{Y} & \text { Vehicle }_{Z} \\ \text { FrontLeft }_{X} & \text { FrontLeft }_{Y} & \text { FrontLeft }_{Z} \\ \text { FrontRight }_{X} & \text { FrontRight }_{Y} & \text { FrontRight }_{Z}\end{array}\right]$ | m |
| StartLoc | Vehicle, StartLocVh, and tire, StartLocTr, ray trace start locations, in world coordinate system $X$-, $Y$, and $Z$ - axes, respectively | $\left[\begin{array}{lll}\text { RearLeft }_{X} & \text { RearLeft }_{Y} & \text { RearLeft }_{Z} \\ \text { RearRear }_{X} & \text { RearRear }_{Y} & \text { RearRear }_{Z}\end{array}\right]$ | m |

VehHitDist - Front of vehicle distance to object
scalar
Distance from the front of the vehicle to object, DistToHitVhAdjust, in m.
TireHitDist - Tire distance to terrain
vector
Distance from tire to terrain, DistToHitTrAdjust, in m.
DistToHitTrAdjust $=[$ FrontLeft FrontRight RearLef RearRight $]$

## Parameters

## Actor Setup

Tag for actor in 3D scene, ActorTag - Name
SimulinVehicle1 (default) | character vector
Actor name.

Actors are scene objects that support 3D translation, rotation, and scale. Parts are actor components. Components do not exist by themselves; they are associated with an actor.

The block does not support multiple instances of the same actor tag. To refer to the same scene actor when you use the 3D block pairs (e.g. Simulation 3D Actor Transform Get and Simulation 3D Actor Transform Set), specify the same Tag for actor in 3D scene, ActorTag parameter.

Distance to vehicle center - Selection
Constant (default)|External input
Configure how to provide the distance to the vehicle center.
Dependencies

| Distance to vehicle <br> center | Creates Port | Creates Parameter |
| :--- | :--- | :--- |
| Constant | None | Distance from vehicle center to front, <br> VehCntrLngthVal |
| External input | VehCntr | None |

Distance to tire center - Selection
Constant (default)|External input
Configure how to provide the distance to the tire center.

## Dependencies

| Distance to tire center <br> Setting | Creates Port | Creates Parameter |
| :--- | :--- | :--- |
| Constant | None | Distance from tire center to ground, <br> TireRadiiVal |
| External input | TireRadii | None |

Distance from vehicle center to front, VehCntrLngthVal - Vehicle center
0 (default) | scalar
Distance from the vehicle center to front, VehCntrLngthVal, in m.

## Dependencies

| Distance to vehicle <br> center | Creates Port | Creates Parameter |
| :--- | :--- | :--- |
| Constant | None | Distance from vehicle center to front, <br> VehCntrLngthVal |
| External input | VehCntr | None |

## Distance from tire center to ground, TireRadiiVal - Tire radii

0 (default) | scalar
Tire radius, TireRadiiVal, in m.

Dependencies

| Distance to tire center <br> Setting | Creates Port | Creates Parameter |
| :--- | :--- | :--- |
| Constant | None | Distance from tire center to ground, <br> TireRadiiVal |
| External input | TireRadii | None |

## Trace Lengths

Vehicle body x-axis trace length, VehRayLngth - Trace length
5 (default) | scalar
Vehicle body trace length, VehRayLngth, in m.

## Left front wheel $\mathbf{z}$-axis trace length, LfRayLngth - Trace length

5 (default) | scalar
Left front wheel trace length, LfRayLngth and LengthTr, in m.
Right front wheel z-axis trace length, RfRayLngth - Trace length
5 (default) | scalar
Right front wheel trace length, RfRayLngth and LengthTr, in m.
Left rear wheel z-axis trace length, LrRayLngth - Trace length
5 (default) | scalar
Left rear wheel trace length, LrRayLngth and LengthTr, in m.
Right rear wheel z-axis trace length, RrRayLngth - Trace length
5 (default) | scalar
Right rear wheel trace length, RrRayLngth and LengthTr, in m.

## Starting Point Offsets

Vehicle body x-axis trace offset, VehRayOffset - Offset the vehicle ray trace
0 (default) | scalar
Vehicle body trace offset, OffsetVh, in m.
Left front wheel z-axis trace offset, LfRayOffset - Offset the left front wheel ray trace 0 (default) | scalar

Left front wheel trace offset, LfRayOffset and OffsetTr, in m.
Right front wheel z-axis trace offset, RfRayOffset - Offset the right front wheel ray trace
0 (default) | scalar
Right front wheel trace offset, RfRayOffset and OffsetTr, in m.
Left rear wheel z-axis trace offset, LrRayOffset - Offset the left rear wheel ray trace 0 (default) | scalar

Left rear wheel trace offset, LrRayOffset and OffsetTr, in m.

Right rear wheel z-axis trace offset, RrRayOffset - Offset the right rear wheel ray trace 0 (default) | scalar

Right rear wheel trace offset, RrRayOffset and OffsetTr, in m.
Enable Traces
Vehicle body - Enable vehicle body ray tracing
on (default) | off
Enable vehicle body ray tracing.
Left front tire - Enable left front tire ray tracing
on (default) | off
Enable left front tire ray tracing.
Right front tire - Enable right front tire ray tracing
on (default) | off
Enable right front tire ray tracing.
Left rear tire - Enable left rear tire ray tracing
on (default) | off
Enable left rear tire ray tracing.
Right rear tire - Enable right rear tire ray tracing
on (default) | off
Enable right rear tire ray tracing.
Trace line visualization - Visualize ray traces
on (default) | off
Enable trace line visualization.
Sample time - Sample time

- 1 (default) | scalar

Sample time, $T_{s}$. The graphics frame rate is the inverse of the sample time.

## Version History <br> Introduced in R2018a

## See Also

Simulation 3D Camera Get | Simulation 3D Scene Configuration | Simulation 3D Vehicle | Simulation 3D Vehicle with Ground Following

## Topics

"Scene Interrogation in 3D Environment"

## External Websites

Unreal Engine

## Simulation 3D Vehicle with Ground Following

Implement vehicle that follows ground in 3D environment


## Libraries:

Automated Driving Toolbox / Simulation 3D
Vehicle Dynamics Blockset / Vehicle Scenarios / Sim3D / Sim3D Vehicle /
Components

## Description

The Simulation 3D Vehicle with Ground Following block implements a vehicle with four wheels in a 3D simulation environment. This environment is rendered using the Unreal Engine from Epic Games. The block uses the input ( $X, Y$ ) position and yaw angle of the vehicle to adjust the elevation, roll angle, and pitch angle of the vehicle so that it follows the ground terrain. The block determines the vehicle velocity and heading and adjusts the steering angle and rotation for each wheel. Use this block for automated driving applications.

To use this block, ensure that the Simulation 3D Scene Configuration block is in your model. If you set the Sample time parameter of the Simulation 3D Vehicle with Ground Following block to -1, the block inherits the sample time specified in the Simulation 3D Scene Configuration block.

The block input uses the vehicle Z-down right-handed (RH) Cartesian coordinate system defined in SAE J670 ${ }^{1}$. The coordinate system is inertial and initially aligned with the vehicle geometric center:

- $X$-axis - Along vehicle longitudinal axis, points forward
- $Y$-axis - Along vehicle lateral axis, points to the right
- Z-axis - Points downward

Note The Simulation 3D Vehicle with Ground Following block must execute before the Simulation 3D Scene Configuration block. That way, the Simulation 3D Vehicle with Ground Following block prepares the signal data before the Unreal Engine 3D visualization environment receives it. To check the block execution order, right-click the blocks and select Properties. On the General tab, confirm these Priority settings:

- Simulation 3D Scene Configuration - 0
- Simulation 3D Vehicle with Ground Following - - 1

For more information about execution order, see "Control and Display Execution Order".

You can configure the Simulation 3D Vehicle with Ground Following block to import custom meshes on page 7-56 and control vehicle lights on page 7-57.

## Ports

## Input

$\mathbf{X}$ - Longitudinal position of vehicle
scalar
Longitudinal position of the vehicle along the $X$-axis of the scene. $\mathbf{X}$ is in the inertial Z-down coordinate system. Units are in meters.

Y - Lateral position of vehicle
scalar
Lateral position of the vehicle along the $Y$-axis of the scene. $\mathbf{Y}$ is in the inertial $Z$-down coordinate system. Units are in meters.

Yaw - Yaw orientation angle of vehicle
scalar
Yaw orientation angle of the vehicle along the $Z$-axis of the scene. Yaw is in the $Z$-down coordinate system. Units are in radians.

Light controls - Vehicle lights on or off
1-by-6 vector
Light controls input signal, specified as a 1-by-6 Boolean vector. Each element of the vector turns a specific vehicle light on or off, as indicated in this table. A value of 1 turns the light on; a value of 0 turns the light off

| Vector Element | Vehicle Light |
| :--- | :--- |
| $(1,1)$ | Headlight high beam |
| $(1,2)$ | Headlight low beam |
| $(1,3)$ | Brake |
| $(1,4)$ | Reverse |
| $(1,5)$ | Left signal |
| $(1,6)$ | Right signal |

## Dependencies

To create this port, on the Light Controls tab, select Enable light controls.
Data Types: Boolean

## Parameters

## Vehicle Parameters

Type - Type of vehicle
Muscle car (default) | Sedan|Sport utility vehicle|Small pickup truck|Hatchback|
Box truck|Formula Student Vehicle|Custom

Select the type of vehicle. To obtain the dimensions of each vehicle type, see these reference pages:

- Muscle car - Muscle Car
- Sedan - Sedan
- Sport utility vehicle - Sport Utility Vehicle
- Small pickup truck - Small Pickup Truck
- Hatchback - Hatchback
- Box truck - Box Truck
- Formula Student Vehicle - Formula Student Vehicle


## Dependencies

Selecting Custom enables parameters that allow you to import a custom mesh for your vehicle.
Path to custom mesh, MeshPath - Path to custom mesh
/MathWorksSimulation/Vehicles/Muscle/Meshes/SK_MuscleCar.SK_MuscleCar (default)| valid path

Path to custom mesh.
To create a custom vehicle mesh, see "Prepare Custom Vehicle Mesh for the Unreal Editor".
Example: /MathWorksSimulation/Vehicles/Muscle/Meshes/SK_Sedan.SK_Sedan

## Dependencies

To enable this parameter, set Type to Custom.
Track width in custom mesh, TrackWidth - Track width
1.9 (default) | scalar

Track width in custom mesh, in m.

## Dependencies

To enable this parameter, set Type to Custom.
Wheel base in custom mesh, WheelBase - Wheel base
3 (default) | scalar
Wheel base in custom mesh, in $m$.

## Dependencies

To enable this parameter, set Type to Custom.
Wheel radius in custom mesh, WheelRadius - Wheel radius
0.35 (default) | scalar

Wheel radius in custom mesh, in m.

## Dependencies

To enable this parameter, set Type to Custom.

Color - Color of vehicle
Red (default) | Orange | Yellow | Green | Blue | Black | White | Silver
Select the color of the vehicle.
Initial position [X, Y, Z], InitialPos (m) - Initial vehicle position
[0, 0, 0] (default) | real-valued 1-by-3 vector
Initial vehicle position along the $X$-axis, $Y$-axis, and $Z$-axis in the inertial $Z$-down coordinate system, in m.

Initial rotation [Roll, Pitch, Yaw], InitialRot (rad) - Initial angle of vehicle rotation
[0, 0, 0] (default) | real-valued 1-by-3 vector
Initial angle of vehicle rotation, in rad. The angle of rotation is defined by the roll, pitch, and yaw of the vehicle.

```
Name, ActorName - Name of vehicle
SimulinkVehicle1 (default) | vehicle name
```

Name of vehicle. By default, when you use the block in your model, the block sets the Name parameter to SimulinkVehicle $X$. The value of $X$ depends on the number of Simulation 3D Vehicle with Ground Following blocks that you have in your model.

## Sample time, SampleTime - Sample time

- 1 (default) | positive scalar

Sample time, $T_{s}$. The graphics frame rate is the inverse of the sample time.
If you set the sample time to -1 , the block uses the sample time specified in the Simulation 3D Scene Configuration block.

## Light Controls

Enable light controls, VehLightsControl - Control vehicle lights
off (default) | on
Select whether to control the vehicle headlights. Use the enabled parameters to set the light parameters, including headlight intensity.

## Dependencies

Selecting this parameter:

- Creates the input port Light controls
- Enables these light parameters.

| Lights | Light Parameters |
| :---: | :---: |
| Headlights | - Headlight color <br> - High beam intensity <br> - Low beam intensity <br> - High beam cone half angle <br> - Low beam cone half angle <br> - Left headlight beam orientation <br> - Right headlight beam orientation |
| Brake lights | Brake light intensity |
| Reverse lights | Reverse light intensity |
| Turn signal lights | - Turn signal light intensity <br> - Period <br> - Pulse width |

## Headlights

Headlight color [R,G,B], HeadlightColor - Headlight color
[1,1,1] (default) | 1-by-3 vector of RGB triplet values
Headlight color, specified as a normalized 1-by-3 vector of RGB triplet values.

## Dependencies

To enable this parameter, select Enable light controls.

## Data Types: int8 |uint8

High beam intensity, HighBeamIntensity - High beam intensity
100000 (default) | positive scalar
High beam intensity, in cd.

## Dependencies

To enable this parameter, select Enable light controls.
Data Types: double
Low beam intensity, LowBeamIntensity - Low beam intensity
60000 (default) | positive scalar
Low beam intensity, in cd.

## Dependencies

To enable this parameter, select Enable light controls.
Data Types: double
High beam cone half angle, HighBeamConeAngle - High beam cone half angle
1.22 (default) | positive scalar less than pi/2

High beam cone half angle, in rad.

## Dependencies

To enable this parameter, select Enable light controls.

## Data Types: double

Low beam cone half angle, LowBeamConeAngle - Low beam cone half angle
1.22 (default) | positive scalar less than pi/2

Low beam cone half angle, in rad.

## Dependencies

To enable this parameter, select Enable light controls.

## Data Types: double

Left headlight beam orientation [Pitch, Yaw], LeftHeadlightOrientation - Left headlight beam orientation
[0,0] (default) | 1-by-2 vector greater with values between -pi and pi
Pitch and yaw orientation of the left headlight beam orientation in the Z-down coordinate system, specified as a 1-by-2 vector, in rad. The first element of the vector, [1, 1], is the pitch angle. The second element of the vector, [1,2] is the yaw angle.

## Dependencies

To enable this parameter, select Enable light controls.

## Data Types: double

Right headlight beam orientation [Pitch, Yaw], RightHeadlightOrientation - Right headlight beam orientation

```
[0,0] (default) | 1-by-2 vector greater with values between -pi and pi
```

Pitch and yaw orientation of the right headlight beam orientation in the $Z$-down coordinate system, specified as a 1-by-2 vector, in rad. The first element of the vector, [1, 1], is the pitch angle. The second element of the vector, $[1,2]$ is the yaw angle.

## Dependencies

To enable this parameter, select Enable light controls.

## Brake Lights

Brake light intensity, BrakelightIntensity - Intensity
500 (default) | positive scalar
Brake light intensity, in $\mathrm{cd} / \mathrm{m}^{\wedge} 2$.

## Dependencies

To enable this parameter, select Enable light controls.

## Data Types: double

## Reverse Lights

Reverse light intensity, ReverselightIntensity - Intensity
500 (default) | positive scalar

Reverse light intensity, in cd/m^2.

## Dependencies

To enable this parameter, select Enable light controls.
Data Types: double
Turn Signal Lights
Turn signal light intensity, SignallightIntensity - Intensity
500 (default) | positive scalar
Turn signal light intensity, in $\mathrm{cd} / \mathrm{m}^{\wedge} 2$.

## Dependencies

To enable this parameter, select Enable light controls.

## Data Types: double

Period, SignallightPeriod - Turn signal light period
1 (default) | positive scalar
Turn signal light period, in s.

## Dependencies

To enable this parameter, select Enable light controls.
Data Types: double
Pulse width, SignalPulseWidth - Pulse width
50 (default) | positive scalar less than 100
Turn signal light pulse width, as a percent of the period.

## Dependencies

To enable this parameter, select Enable light controls.

## Data Types: double

## More About <br> Import Custom Meshes

To import custom meshes for defining custom vehicles, follow these steps:
1 Install the Vehicle Dynamics Blockset Interface for Unreal Engine 4 Projects support package. See "Customize 3D Scenes for Vehicle Dynamics Simulations".
2 On the block Parameters tab, set Type to Custom.
3 In the Path to custom mesh field, enter the path to the vehicle mesh in the Unreal Engine project. For example, enter /MathWorksSimulation/Vehicles/Muscle/Meshes/ SK_MuscleCar.SK_MuscleCar.

To create a custom vehicle mesh, see "Prepare Custom Vehicle Mesh for the Unreal Editor".

4 Use the vehicle dimensions in the custom mesh to enter the dimensions in the corresponding block parameter fields.

## Control Vehicle Lights

To control the lights of vehicles in a scene, follow these steps:
1 Install the Vehicle Dynamics Blockset Interface for Unreal Engine 4 Projects support package. See "Customize 3D Scenes for Vehicle Dynamics Simulations".
2 On the block Light Controls tab, select Enable light controls.
3 Use the enabled parameters to specify the vehicle light for:

- Headlights
- Brake lights
- Reverse lights
- Turn signal lights

4 Connect Boolean light control signals to the Signal lights input port.

## Version History

Introduced in R2019b

## References

[1] Vehicle Dynamics Standards Committee. Vehicle Dynamics Terminology. SAE J670. Warrendale, PA: Society of Automotive Engineers, 2008.
[2] Technical Committee. Road vehicles - Vehicle dynamics and road-holding ability - Vocabulary. ISO 8855:2011. Geneva, Switzerland: International Organization for Standardization, 2011.

## See Also

Simulation 3D Scene Configuration | Simulation 3D Vehicle

## Topics

"How 3D Simulation for Vehicle Dynamics Blockset Works"
"Prepare Custom Vehicle Mesh for the Unreal Editor"
"Scene Interrogation in 3D Environment"
"Unreal Engine Simulation Environment Requirements and Limitations"

## Simulation 3D Vehicle

Implement vehicle in 3D environment


## Libraries:

Vehicle Dynamics Blockset / Vehicle Scenarios / Sim3D / Sim3D Vehicle / Components

## Description

The Simulation 3D Vehicle block implements a vehicle with four wheels in the 3D simulation environment.

To use this block, ensure that the Simulation 3D Scene Configuration block is in your model. If you set the Sample time parameter of this block to -1, the block uses the sample time specified in the Simulation 3D Scene Configuration block.

The block input uses the vehicle Z-down right-handed (RH) Cartesian coordinate system defined in SAE J670 ${ }^{1}$. The coordinate system is inertial and initially aligned with the vehicle geometric center:

- $X$-axis - Along vehicle longitudinal axis, points forward
- $Y$-axis - Along vehicle lateral axis, points to the right
- Z-axis - Points downward

Tip Verify that the Simulation 3D Vehicle block executes before the Simulation 3D Scene Configuration block. That way, Simulation 3D Vehicle prepares the signal data before the Unreal Engine 3D visualization environment receives it. To check the block execution order, right-click the blocks and select Properties. On the General tab, confirm these Priority settings:

- Simulation 3D Scene Configuration - 0
- Simulation 3D Vehicle - - 1

For more information about execution order, see "Control and Display Execution Order".

You can configure the Simulation 3D Vehicle with Ground Following block to import custom meshes on page 7-68 and control vehicle lights on page 7-68.

## Ports

## Input

Translation - Vehicle translation
5-by-3 array
Vehicle and wheel translation, in m. Array dimensions are 5-by-3.

- Translation(1,1), Translation(1,2), and Translation(1,3) - Vehicle translation along the inertial vehicle Z-down $X$-, $Y$-, and $Z$ - axes, respectively.
- Translation(...,1), Translation(...,2), and Translation(...,3) - Wheel translation relative to vehicle, along the vehicle Z-down $X$-, $Y$-, and $Z$ - axes, respectively.

The signal contains translation information according to the axle and wheel locations.

$$
\text { Translation }=\left[\begin{array}{ccc}
X_{v} & Y_{v} & Z_{v} \\
X_{F L} & Y_{F L} & Z_{F L} \\
X_{F R} & Y_{F R} & Z_{F R} \\
X_{R L} & Y_{R L} & Z_{R L} \\
X_{R R} & Y_{R R} & Z_{R R}
\end{array}\right]
$$

| Translation | Array Element | Translation Axis |
| :--- | :--- | :--- |
| Vehicle, $X_{v}$ | Translation(1,1) | Inertial vehicle Z-down $X$-axis |
| Vehicle, $Y_{v}$ | Translation(1,2) | Inertial vehicle Z-down $Y$-axis |
| Vehicle, $Z_{v}$ | Translation(1,3) | Inertial vehicle Z-down Z-axis |
| Front left wheel, $X_{F L}$ | Translation(2,1) | Vehicle Z-down $X$-axis |
| Front left wheel, $Y_{F L}$ | Translation(2,2) | Vehicle Z-down $Y$-axis |
| Front left wheel, $Z_{F L}$ | Translation(2,3) | Vehicle Z-down Z-axis |
| Front right wheel, $X_{F R}$ | Translation(3,1) | Vehicle Z-down $X$-axis |
| Front right wheel, $Y_{F R}$ | Translation(3,2) | Vehicle Z-down $Y$-axis |
| Front right wheel, $Z_{F R}$ | Translation(3,3) | Vehicle Z-down Z-axis |
| Rear left wheel, $X_{R L}$ | Translation(4,1) | Vehicle Z-down $X$-axis |
| Rear left wheel, $Y_{R L}$ | Translation(4,2) | Vehicle Z-down $Y$-axis |
| Rear left wheel, $Z_{R L}$ | Translation(4,3) | Vehicle Z-down Z-axis |
| Rear right wheel, $X_{R R}$ | Translation(5,1) | Vehicle Z-down $X$-axis |
| Rear right wheel, $Y_{R R}$ | Translation(5,2) | Vehicle Z-down $Y$-axis |
| Rear right wheel, $Z_{R R}$ | Translation(5,3) | Vehicle Z-down Z-axis |

Rotation - Vehicle rotation
5-by-3 array
Vehicle and wheel rotation, in rad. Array dimensions are 5-by-3.

- Rotation(1,1), Rotation(1,2), and Rotation(1,3) - Vehicle rotation about the inertial vehicle Z-down $X$-, $Y$-, and $Z$ - axes, respectively.
- Rotation(...,1), Rotation(...,2), and Rotation(...,3) - Wheel rotation relative to vehicle, about the vehicle Z-down $X$-, $Y$-, and $Z$ - axes, respectively.

The signal contains rotation information according to the axle and wheel locations.

$$
\text { Rotation }=\left[\begin{array}{ccc}
\text { Roll }_{v} & \text { Pitch }_{v} & \text { Yaw }_{v} \\
\text { Roll }_{F L} & \text { Pitch }_{F L} & \text { Yaw }_{F L} \\
\text { Roll }_{F R} & \text { Pitch }_{F R} & \text { Yaw }_{F R} \\
\text { Roll }_{R L} & \text { Pitch }_{R L} & \text { Yaw }_{R L} \\
\text { Roll }_{R R} & \text { Pitch }_{R R} & \text { Yaw }_{R R}
\end{array}\right]
$$

| Rotation | Array Element | Rotation Axis |
| :---: | :---: | :---: |
| Vehicle, Roll ${ }_{v}$ | Rotation(1,1) | Inertial vehicle Z-down $X$-axis |
| Vehicle, Pitch ${ }_{v}$ | Rotation(1,2) | Inertial vehicle Z-down $Y$-axis |
| Vehicle, Yaw ${ }_{v}$ | Rotation(1,3) | Inertial vehicle Z-down $Z$-axis |
| Front left wheel, Roll $_{F L}$ | Rotation(2,1) | Vehicle Z-down $X$-axis |
| Front left wheel, Pitch $_{F L}$ | Rotation(2,2) | Vehicle Z-down $Y$-axis |
| Front left wheel, Yaw $_{F L}$ | Rotation(2,3) | Vehicle Z-down Z -axis |
| Front right wheel, Roll $_{F R}$ | Rotation(3,1) | Vehicle Z-down X-axis |
| Front right wheel, Pitch $_{\text {FR }}$ | Rotation(3,2) | Vehicle Z-down Y-axis |
| Front right wheel, Yaw $_{\text {FR }}$ | Rotation(3,3) | Vehicle Z-down Z -axis |
| Rear left wheel, Roll $_{R L}$ | Rotation(4,1) | Vehicle Z-down X-axis |
| Rear left wheel, Pitch $_{R L}$ | Rotation(4,2) | Vehicle Z-down Y-axis |
| Rear left wheel, Yaw ${ }_{\text {RL }}$ | Rotation(4,3) | Vehicle Z-down Z-axis |
| Rear right wheel, Roll $_{\text {RR }}$ | Rotation(5,1) | Vehicle Z-down X-axis |
| Rear right wheel, Pitch $_{\text {RR }}$ | Rotation(5,2) | Vehicle Z-down Y-axis |
| Rear right wheel, Yaw ${ }_{\text {RR }}$ | Rotation(5,3) | Vehicle Z-down Z -axis |

## Scale - Vehicle scale

5-by-3
Vehicle and wheel scale, dimensionless. Array dimensions are 5-by-3.

- Scale(1,1), Scale(1,2), and Scale(1,3) - Vehicle scale along the inertial vehicle Z-down $X-, Y$-, and $Z$ - axes, respectively.
- Scale(...,1), Scale(...,2), and Scale(...,3) - Wheel scale relative to vehicle, along vehicle Z-down $X$-, $Y$-, and $Z$ - axes, respectively.

The signal contains scale information according to the axle and wheel locations.

$$
\text { Scale }=\left[\begin{array}{ccc}
X_{V_{\text {scale }}} & Y_{V_{\text {scale }}} & Z_{V_{\text {scale }}} \\
X_{F L_{\text {scale }}} & Y_{F L_{\text {scale }}} & Z_{F L_{\text {scale }}} \\
X_{F R_{\text {scale }}} & Y_{F R_{\text {scale }}} & Z_{F R_{\text {scale }}} \\
X_{R L_{\text {scale }}} & Y_{R L_{\text {scale }}} & Z_{R L_{\text {scale }}} \\
X_{R R_{\text {scale }}} & Y_{R R_{\text {scale }}} & Z_{R R_{\text {scale }}}
\end{array}\right]
$$

| Scale | Array Element | Scale Axis |
| :--- | :--- | :--- |
| Vehicle, $X_{v_{\text {scale }}}$ | Scale $(1,1)$ | Vehicle Z-down $X$-axis |
| Vehicle, $Y_{V_{\text {scale }}}$ | Scale $(1,2)$ | Vehicle Z-down $Y$-axis |
| Vehicle, $Z_{v_{\text {scale }}}$ | Scale $(1,3)$ | Vehicle Z-down $Z$-axis |
| Front left wheel, $X_{F L_{\text {scal }}}$ | Scale $(2,1)$ | Vehicle Z-down $X$-axis |
| Front left wheel, $Y_{F L_{\text {scal }}}$ | Scale $(2,2)$ | Vehicle Z-down $Y$-axis |


| Scale | Array Element | Scale Axis |
| :---: | :---: | :---: |
| Front left wheel, $Z_{F L_{\text {scale }}}$ | Scale(2,3) | Vehicle Z-down Z-axis |
| Front right wheel, $X_{F R_{\text {scale }}}$ | Scale(3,1) | Vehicle Z-down $X$-axis |
| Front right wheel, $Y_{F R_{\text {scale }}}$ | Scale(3, 2 ) | Vehicle Z-down $Y$-axis |
| Front right wheel, $Z_{F R_{\text {scale }}}$ | Scale(3,3) | Vehicle Z-down Z-axis |
| Rear left wheel, $X_{R L_{\text {scale }}}$ | Scale(4,1) | Vehicle Z-down $X$-axis |
| Rear left wheel, $Y_{R L_{\text {scale }}}$ | Scale(4,2) | Vehicle Z-down $Y$-axis |
| Rear left wheel, $Z_{R L_{\text {scale }}}$ | Scale(4,3) | Vehicle Z-down Z-axis |
| Rear right wheel, $X_{R R_{\text {scale }}}$ | Scale(5,1) | Vehicle Z-down $X$-axis |
| Rear right wheel, $Y_{R R_{\text {scale }}}$ | Scale(5,2) | Vehicle Z-down $Y$-axis |
| Rear right wheel, $Z_{R R_{\text {scale }}}$ | Scale(5,3) | Vehicle Z-down Z-axis |

Light controls - Vehicle lights on or off
1-by-6 vector
Light controls input signal, specified as a 1-by-6 Boolean vector. Each element of the vector turns a specific vehicle light on or off, as indicated in this table. A value of 1 turns the light on; a value of 0 turns the light off

| Vector Element | Vehicle Light |
| :--- | :--- |
| $(1,1)$ | Headlight high beam |
| $(1,2)$ | Headlight low beam |
| $(1,3)$ | Brake |
| $(1,4)$ | Reverse |
| $(1,5)$ | Left signal |
| $(1,6)$ | Right signal |

## Dependencies

To create this port, on the Light Controls tab, select Enable light controls.
Data Types: Boolean

## Parameters

## Vehicle Parameters

## Type - Type

Muscle car (default) | Sedan | Sport utility vehicle|Small pickup truck|Hatchback| Box truck|Formula student vehicle

If you set Actor type to Passenger vehicle, use the Vehicle type parameter to specify the vehicle. This table provides links to the vehicle dimensions.

| Vehicle type Setting | Vehicle Dimensions |
| :--- | :--- |
| Muscle car | Muscle Car |


| Vehicle type Setting | Vehicle Dimensions |
| :--- | :--- |
| Sedan | Sedan |
| Sport utility vehicle | Sport Utility Vehicle |
| Small pickup truck | Small Pickup Truck |
| Hatchback | Hatchback |
| Box truck | Box Truck |
| Formula student vehicle | Formula Student Vehicle |

## Dependencies

Selecting Custom enables parameters that allow you to import a custom mesh for your vehicle.
Path to custom mesh, MeshPath - Path to custom mesh
/MathWorksSimulation/Vehicles/Muscle/Meshes/SK_MuscleCar.SK_MuscleCar (default)| valid path

Path to custom mesh.
To create a custom vehicle mesh, see "Prepare Custom Vehicle Mesh for the Unreal Editor".
Example: /MathWorksSimulation/Vehicles/Muscle/Meshes/SK_Sedan.SK_Sedan

## Dependencies

To enable this parameter, set Type to Custom.
Color - Color of vehicle
Red (default) | Orange | Yellow|Green | Blue | Black | White | Silver
Select the color of the vehicle.
Name - Name of vehicle
SimulinkVehicle1 (default)| character vector
Name of vehicle. By default, when you use the block in your model, the block sets the Name parameter to SimulinkVehicle $X$. The value of $X$ depends on the number of Simulation 3D Vehicle with Ground Following and Simulation 3D Vehicle blocks that you have in your model.

Sample time - Sample time

- 1 (default) | scalar

Sample time, $T_{s}$. The graphics frame rate is the inverse of the sample time.

## Light Controls

Enable light controls, VehLightsControl - Control vehicle lights
off (default) | on
Select whether to control the vehicle headlights. Use the enabled parameters to set the light parameters, including headlight intensity.

## Dependencies

Selecting this parameter:

- Creates the input port Light controls
- Enables these light parameters.

| Lights | Light Parameters |
| :--- | :--- |
| Headlights | $\bullet \quad$ Headlight color |
|  | $\bullet \quad$ High beam intensity |
|  | $\bullet \quad$ Low beam intensity |
|  | $\bullet \quad$ Low beam cone half angle |
|  | $\bullet \quad$ Left headlight beam orientation |
|  | $\bullet \quad$ Right headlight beam orientation |
| Brake lights | Brake light intensity |
| Reverse lights | Reverse light intensity |
| Turn signal lights | $\bullet \quad$ Turn signal light intensity |
|  | $\bullet \quad$ Period |
|  |  |

## Headlights

Headlight color [R,G,B], HeadlightColor - Headlight color
[1, 1, 1] (default) | 1-by-3 vector of RGB triplet values
Headlight color, specified as a normalized 1-by-3 vector of RGB triplet values.

## Dependencies

To enable this parameter, select Enable light controls.
Data Types: int8|uint8
High beam intensity, HighBeamIntensity - High beam intensity
100000 (default) | positive scalar
High beam intensity, in cd.

## Dependencies

To enable this parameter, select Enable light controls.
Data Types: double
Low beam intensity, LowBeamIntensity - Low beam intensity
60000 (default) | positive scalar
Low beam intensity, in cd.

## Dependencies

To enable this parameter, select Enable light controls.

## Data Types: double

High beam cone half angle, HighBeamConeAngle - High beam cone half angle 1.22 (default) | positive scalar less than pi/2

High beam cone half angle, in rad.

## Dependencies

To enable this parameter, select Enable light controls.

## Data Types: double

Low beam cone half angle, LowBeamConeAngle - Low beam cone half angle
1.22 (default) | positive scalar less than pi/2

Low beam cone half angle, in rad.

## Dependencies

To enable this parameter, select Enable light controls.

## Data Types: double

Left headlight beam orientation [Pitch, Yaw], LeftHeadlightOrientation - Left headlight beam orientation
[0,0] (default) | 1-by-2 vector greater with values between -pi and pi
Pitch and yaw orientation of the left headlight beam orientation in the Z-down coordinate system, specified as a 1 -by-2 vector, in rad. The first element of the vector, [1,1], is the pitch angle. The second element of the vector, [1,2] is the yaw angle.

## Dependencies

To enable this parameter, select Enable light controls.
Data Types: double
Right headlight beam orientation [Pitch, Yaw], RightHeadlightOrientation - Right headlight beam orientation

```
[0,0] (default) | 1-by-2 vector greater with values between -pi and pi
```

Pitch and yaw orientation of the right headlight beam orientation in the Z-down coordinate system, specified as a 1 -by- 2 vector, in rad. The first element of the vector, [1,1], is the pitch angle. The second element of the vector, [1,2] is the yaw angle.

## Dependencies

To enable this parameter, select Enable light controls.

## Brake Lights

Brake light intensity, BrakelightIntensity - Intensity
500 (default) | positive scalar
Brake light intensity, in $\mathrm{cd} / \mathrm{m}^{\wedge} 2$.

## Dependencies

To enable this parameter, select Enable light controls.

## Data Types: double

Reverse Lights
Reverse light intensity, ReverselightIntensity - Intensity
500 (default) | positive scalar
Reverse light intensity, in $\mathrm{cd} / \mathrm{m}^{\wedge} 2$.

## Dependencies

To enable this parameter, select Enable light controls.

## Data Types: double

## Turn Signal Lights

Turn signal light intensity, SignallightIntensity - Intensity
500 (default) | positive scalar
Turn signal light intensity, in $\mathrm{cd} / \mathrm{m}^{\wedge} 2$.
Dependencies
To enable this parameter, select Enable light controls.
Data Types: double
Period, SignallightPeriod - Turn signal light period
1 (default) | positive scalar
Turn signal light period, in s.

## Dependencies

To enable this parameter, select Enable light controls.
Data Types: double
Pulse width, SignalPulseWidth - Pulse width
50 (default) | positive scalar less than 100
Turn signal light pulse width, as a percent of the period.

## Dependencies

To enable this parameter, select Enable light controls.
Data Types: double
Initial Values
Initial array values to translate vehicle per part, Translation - Vehicle initial translation zeros( 5, 3 ) (default) | 5-by-3 array

Initial vehicle and wheel translation, in m. Array dimensions are 5-by-3.

- Translation(1,1), Translation(1,2), and Translation(1,3) - Initial vehicle translation along the inertial vehicle Z-down coordinate system $X-, Y$-, and $Z$ - axes, respectively.
- Translation(...,1), Translation(...,2), and Translation(...,3) - Initial wheel translation relative to vehicle, along the vehicle Z-down $X$-, $Y$-, and $Z$ - axes, respectively.

The parameter contains translation information according to the axle and wheel locations.

$$
\text { Translation }=\left[\begin{array}{ccc}
X_{v} & Y_{v} & Z_{v} \\
X_{F L} & Y_{F L} & Z_{F L} \\
X_{F R} & Y_{F R} & Z_{F R} \\
X_{R L} & Y_{R L} & Z_{R L} \\
X_{R R} & Y_{R R} & Z_{R R}
\end{array}\right]
$$

| Translation | Array Element | Translation Axis |
| :--- | :--- | :--- |
| Vehicle, $X_{v}$ | Translation(1,1) | Inertial vehicle Z-down $X$-axis |
| Vehicle, $Y_{v}$ | Translation(1,2) | Inertial vehicle Z-down $Y$-axis |
| Vehicle, $Z_{v}$ | Translation(1,3) | Inertial vehicle Z-down Z-axis |
| Front left wheel, $X_{F L}$ | Translation(2,1) | Vehicle Z-down $X$-axis |
| Front left wheel, $Y_{F L}$ | Translation(2,2) | Vehicle Z-down $Y$-axis |
| Front left wheel, $Z_{F L}$ | Translation(2,3) | Vehicle Z-down Z-axis |
| Front right wheel, $X_{F R}$ | Translation(3,1) | Vehicle Z-down $X$-axis |
| Front right wheel, $Y_{F R}$ | Translation(3,2) | Vehicle Z-down $Y$-axis |
| Front right wheel, $Z_{F R}$ | Translation(3,3) | Vehicle Z-down Z-axis |
| Rear left wheel, $X_{R L}$ | Translation(4,1) | Vehicle Z-down $X$-axis |
| Rear left wheel, $Y_{R L}$ | Translation(4,2) | Vehicle Z-down $Y$-axis |
| Rear left wheel, $Z_{R L}$ | Translation(4,3) | Vehicle Z-down Z-axis |
| Rear right wheel, $X_{R R}$ | Translation(5,1) | Vehicle Z-down $X$-axis |
| Rear right wheel, $Y_{R R}$ | Translation(5,2) | Vehicle Z-down $Y$-axis |
| Rear right wheel, $Z_{R R}$ | Translation(5,3) | Vehicle Z-down Z-axis |

Initial array values to rotate vehicle per part, Rotation - Vehicle initial rotation zeros( 5, 3 ) (default) | 5-by-3 array

Initial vehicle and wheel rotation, about the vehicle Z-down $X$-, $Y$-, and $Z$ - axes.
Array dimensions are 5-by-3.

- Rotation(1, 1), Rotation(1,2), and Rotation(1,3) - Initial vehicle rotation about the inertial vehicle Z-down coordinate system $X$-, $Y$-, and $Z$ - axes, respectively.
- Rotation(..., 1), Rotation(...,2), and Rotation(...,3) - Initial wheel rotation relative to vehicle, about the vehicle Z-down $X$-, $Y$-, and $Z$ - axes, respectively.

The parameter contains rotation information according to the axle and wheel locations.

Rotation $=\left[\begin{array}{ccc}\text { Roll }_{v} & \text { Pitch }_{\nu} & \text { Yaw }_{\nu} \\ \text { Roll }_{F L} & \text { Pitch }_{F L} & \text { Yaw }_{F L} \\ \text { Roll }_{F R} & \text { Pitch }_{F R} & \text { Yaw }_{F R} \\ \text { Roll }_{R L} & \text { Pitch }_{R L} & \text { Yaw }_{R L} \\ \text { Roll }_{R R} & \text { Pitch }_{R R} & \text { Yaw }_{R R}\end{array}\right]$

| Rotation | Array Element | Rotation Axis |
| :---: | :---: | :---: |
| Vehicle, Roll ${ }_{v}$ | Rotation(1,1) | Inertial vehicle Z-down $X$-axis |
| Vehicle, Pitch ${ }_{v}$ | Rotation(1,2) | Inertial vehicle Z-down $Y$-axis |
| Vehicle, Yaw $_{v}$ | Rotation(1,3) | Inertial vehicle Z-down $Z$-axis |
| Front left wheel, Roll ${ }_{F L}$ | Rotation(2,1) | Vehicle Z-down $X$-axis |
| Front left wheel, Pitch $_{F L}$ | Rotation(2,2) | Vehicle Z-down $Y$-axis |
| Front left wheel, Yaw $_{F L}$ | Rotation (2,3) | Vehicle Z-down Z-axis |
| Front right wheel, Roll $_{F R}$ | Rotation(3,1) | Vehicle Z-down $X$-axis |
| Front right wheel, Pitch $_{\text {FR }}$ | Rotation(3,2) | Vehicle Z-down Y-axis |
| Front right wheel, Yaw $_{F R}$ | Rotation(3,3) | Vehicle Z-down Z-axis |
| Rear left wheel, Roll $_{R L}$ | Rotation(4,1) | Vehicle Z-down X-axis |
| Rear left wheel, Pitch $_{\text {RL }}$ | Rotation(4,2) | Vehicle Z-down Y-axis |
| Rear left wheel, Yaw ${ }_{R L}$ | Rotation(4,3) | Vehicle Z-down Z-axis |
| Rear right wheel, Roll $_{R R}$ | Rotation(5,1) | Vehicle Z-down $X$-axis |
| Rear right wheel, Pitch $_{\text {RR }}$ | Rotation(5,2) | Vehicle Z-down Y-axis |
| Rear right wheel, Yaw ${ }_{\text {RR }}$ | Rotation(5,3) | Vehicle Z-down Z -axis |

Initial array values to scale vehicle per part, Scale - Vehicle initial scale
ones( 5, 3 ) (default) | 5-by-3 array
Initial vehicle and wheel scale, dimensionless. Array dimensions are 5-by-3.

- Scale(1,1), Scale(1,2), and Scale(1,3) - Initial vehicle scale along the inertial vehicle Zdown $X$-, $Y$-, and $Z$ - axes, respectively.
- Scale(..., 1), Scale (...,2), and Scale(...,3) - Initial wheel scale relative to vehicle, along vehicle Z-down $X$-, $Y$-, and $Z$ - axes, respectively.

The parameter contains scale information according to the axle and wheel locations.

$$
\text { Scale }=\left[\begin{array}{ccc}
X_{V_{\text {scale }}} & Y_{V_{\text {scale }}} & Z_{V_{\text {scale }}} \\
X_{F L_{\text {scale }}} & Y_{F L_{\text {scale }}} & Z_{F L_{\text {scale }}} \\
X_{F R_{\text {scale }}} & Y_{F R_{\text {scale }}} & Z_{F R_{\text {scale }}} \\
X_{R L_{\text {scale }}} & Y_{R L_{\text {scale }}} & Z_{R L_{\text {scale }}} \\
X_{R R_{\text {scale }}} & Y_{R R_{\text {scale }}} & Z_{R R_{\text {scale }}}
\end{array}\right]
$$

| Scale | Array Element | Scale Axis |
| :---: | :---: | :---: |
| Vehicle, $X_{V_{\text {scale }}}$ | Scale(1,1) | Vehicle Z-down $X$-axis |
| Vehicle, $Y_{V_{\text {scale }}}$ | Scale(1,2) | Vehicle Z-down $Y$-axis |
| Vehicle, $Z_{v_{\text {scale }}}$ | Scale(1,3) | Vehicle Z-down Z-axis |
| Front left wheel, $X_{F L_{\text {scale }}}$ | Scale(2,1) | Vehicle Z-down $X$-axis |
| Front left wheel, $Y_{F L_{\text {scale }}}$ | Scale (2,2) | Vehicle Z-down $Y$-axis |
| Front left wheel, $Z_{F L_{\text {scale }}}$ | Scale(2,3) | Vehicle Z-down Z-axis |
| Front right wheel, $X_{F R_{\text {sade }}}$ | Scale(3,1) | Vehicle Z-down $X$-axis |
| Front right wheel, $Y_{F R_{\text {sade }}}$ | Scale(3,2) | Vehicle Z-down Y-axis |
| Front right wheel, $Z_{F R_{\text {scale }}}$ | Scale (3, 3) | Vehicle Z-down Z-axis |
| Rear left wheel, $X_{R L_{\text {scale }}}$ | Scale(4,1) | Vehicle Z-down $X$-axis |
| Rear left wheel, $Y_{\text {RLscale }}$ | Scale(4,2) | Vehicle Z-down Y-axis |
| Rear left wheel, $Z_{\text {RLsale }}$ | Scale (4,3) | Vehicle Z-down Z-axis |
| Rear right wheel, $X_{R R_{\text {scale }}}$ | Scale (5,1) | Vehicle Z-down $X$-axis |
| Rear right wheel, $Y_{R R_{\text {sale }}}$ | Scale(5,2) | Vehicle Z-down $Y$-axis |
| Rear right wheel, $Z_{R R_{\text {scale }}}$ | Scale (5,3) | Vehicle Z-down Z-axis |

## More About

## Import Custom Meshes

To import custom meshes for defining custom vehicles, follow these steps:
1 Install the Vehicle Dynamics Blockset Interface for Unreal Engine 4 Projects support package. See "Customize 3D Scenes for Vehicle Dynamics Simulations".
2 On the block Parameters tab, set Type to Custom.
3 In the Path to custom mesh field, enter the path to the vehicle mesh in the Unreal Engine project. For example, enter /MathWorksSimulation/Vehicles/Muscle/Meshes/ SK_MuscleCar.SK_MuscleCar.

To create a custom vehicle mesh, see "Prepare Custom Vehicle Mesh for the Unreal Editor".
4 Use the vehicle dimensions in the custom mesh to enter the dimensions in the corresponding block parameter fields.

## Control Vehicle Lights

To control the lights of vehicles in a scene, follow these steps:
1 Install the Vehicle Dynamics Blockset Interface for Unreal Engine 4 Projects support package. See "Customize 3D Scenes for Vehicle Dynamics Simulations".
2 On the block Light Controls tab, select Enable light controls.
3 Use the enabled parameters to specify the vehicle lights for:

- Headlights
- Brake lights
- Reverse lights
- Turn signal lights

4 Connect Boolean light control signals to the Signal lights input port.

## Version History

Introduced in R2019b

## References

[1] Vehicle Dynamics Standards Committee. Vehicle Dynamics Terminology. SAE J670. Warrendale, PA: Society of Automotive Engineers, 2008.
[2] Technical Committee. Road vehicles - Vehicle dynamics and road-holding ability - Vocabulary. ISO 8855:2011. Geneva, Switzerland: International Organization for Standardization, 2011.

## See Also

Simulation 3D Vehicle with Ground Following | Simulation 3D Scene Configuration

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"
"How 3D Simulation for Vehicle Dynamics Blockset Works"
"Prepare Custom Vehicle Mesh for the Unreal Editor"
"Unreal Engine Simulation Environment Requirements and Limitations"

## Simulation 3D Message Get

Retrieve data from Unreal Engine visualization environment

## Libraries:

Vehicle Dynamics Blockset / Vehicle Scenarios / Sim3D / Sim3D Core Aerospace Blockset / Animation / Simulation 3D

## Description

The Simulation 3D Message Get block retrieves data from the Unreal Engine 3D visualization environment. In your model, ensure that the Simulation 3D Scene Configuration block is at the same level as the Simulation 3D Message Get block.

Tip Verify that the Simulation 3D Scene Configuration block executes before the Simulation 3D Message Get block. That way, the Unreal Engine 3D visualization environment prepares the data before the Simulation 3D Message Get block receives it. To check the block execution order, rightclick the blocks and select Properties. On the General tab, confirm these Priority settings:

- Simulation 3D Scene Configuration - 0
- Simulation 3D Message Get - 1

For more information about execution order, see "Control and Display Execution Order".

## Configure Scenes to Send Data

To use the block, you must configure scenes in the Unreal Engine environment to send data to the Simulink model:

1 Install the "Customize 3D Scenes for Vehicle Dynamics Simulations".
2 In the Unreal Editor, follow these general workflows to send data to Simulink. For detailed information, see "Get Started Communicating with the Unreal Engine Visualization Environment".

| Unreal Engine User | Workflow |
| :---: | :---: |
| Blueprint | a Instantiate the Sim3DSet actor that corresponds to the data type you want to send to the Simulink model. This example shows the Unreal Editor Sim3DSet data types. <br> b Specify an actor tag name that matches the Simulation 3D Message Get block Signal name parameter. <br> c Navigate to the Level Blueprint. <br> d Find the blueprint method for the Sim3DSet actor class based on the data type and size specified by the Simulation 3D Message Get block Data type and Message size parameters. <br> For example, in Unreal Editor, this diagram shows that Write Array Boolean is the method for the Sim3DSetBoolean actor class that sends Boolean data type of array size 30 . <br> Compile and save the scene. |
|  | Note By default, the Double Lane Change scene has a Sim3DSetBoolean actor with tag name NumOfConesHit. |


| Unreal Engine User | Workflow |
| :---: | :---: |
| C++ class | a Create a new actor class for the mesh or asset that you want the Simulink model to interact with. Derive it from ASim3dActor. <br> b In the new actor class: <br> - Declare a pointer to the signal name as a class field. <br> - Get the class tag. <br> - Create a signal writer and assign the pointer in the method Sim3dSetup. <br> - In the method Sim3dStep, invoke the WriteSimulation3DMessage function to write the data to the Simulink model. <br> - Delete the signal writer in the method Sim3dRelease of the actor. |

For more information about the Unreal Editor, see the Unreal Engine 4 Documentation.

## Ports

## Output

ReadMsg - Data retrieved from scene
scalar|array
Data retrieved from the 3D visualization environment scene data. In the Unreal Engine environment, you can use the Sim3DSet class to configure scene actors to send data to the Simulink model.

For example, in the Unreal Editor, the Double Lane Change scene has a Sim3DSetBoolean actor with tag name NumOfConesHit. Use it to retrieve the number of cones the vehicle hits during a double-lane change maneuver.

This table provides the Double Lane Change scene cone name that corresponds to the ReadMsg array element.

| Simulation 3D Message Get Block ReadMsg Value | Unreal Editor Cone Name | Simulation 3D <br> Message Get Block <br> Array Element | Unreal Editor Cone Name |
| :---: | :---: | :---: | :---: |
| ReadMsg(1,1) | SM_Cone5 | ReadMsg (2,1) | SM_Cone10 |
| ReadMsg(1,2) | SM_Cone4 | ReadMsg(2,2) | SM_Cone09 |
| ReadMsg(1,3) | SM_Cone3 | ReadMsg(2,3) | SM_Cone08 |
| ReadMsg (1,4) | SM_Cone2 | ReadMsg $(2,4)$ | SM_Cone07 |
| ReadMsg(1,5) | SM_Cone01 | ReadMsg (2,5) | SM_Cone06 |
| ReadMsg(1,6) | SM_Cone15 | ReadMsg (2,6) | SM_Cone20 |
| ReadMsg (1,7) | SM_Cone14 | ReadMsg $(2,7)$ | SM_Cone19 |
| ReadMsg(1,8) | SM_Cone13 | ReadMsg $(2,8)$ | SM_Cone18 |


| Simulation 3D <br> Message Get Block <br> ReadMsg Value | Unreal Editor Cone <br> Name | Simulation 3D <br> Message Get Block <br> Array Element | Unreal Editor Cone <br> Name |
| :--- | :--- | :--- | :--- |
| ReadMsg $(1,9)$ | SM_Cone12 | ReadMsg $(2,9)$ | SM_Cone17 |
| ReadMsg $(1,10)$ | SM_Cone11 | ReadMsg $(2,10)$ | SM_Cone16 |
| ReadMsg $(1,11)$ | SM_Cone25 | $\operatorname{ReadMsg(2,11)}$ | SM_Cone30 |
| ReadMsg $(1,12)$ | SM_Cone24 | ReadMsg(2,12) | SM_Cone29 |
| ReadMsg $(1,13)$ | SM_Cone23 | $\operatorname{ReadMsg(2,13)}$ | SM_Cone28 |
| ReadMsg(1,14) | SM_Cone22 | $\operatorname{ReadMsg(2,14)}$ | SM_Cone27 |
| ReadMsg(1,15) | SM_Cone21 | $\operatorname{ReadMsg(2,15)}$ | SM_Cone26 |

## Parameters

Signal name, SigName - Message signal name
mySignal (default)
Specifies the signal name in the 3D visualization environment. In the Unreal Engine environment, use the Sim3DSet actor class 'Tags' property located in the 'Details' pane.

For example, you can retrieve data from the double-lane change scene that indicates if cones are hit during a double-lane change maneuver. To retrieve cone hit data from the double-lane change scene, set this parameter to NumOfConesHit. In the double-lane change scene, the Sim3DSet actor class 'Tags' property is set to NumOfConesHit.

Data type, DataType - Message data type
double* | single | int8*| uint8* | int16* | uint16* | int32 | uint32* | boolean
3D visualization environment signal data type. The supported data types depend on the Unreal Engine workflow.

| Workflow | Supported Data Types |
| :--- | :--- |
| Blueprint | single |
|  | int32 |
|  | Boolean |


| Workflow | Supported Data Types |
| :--- | :--- |
| ${ }^{*}$ C++ class | double |
|  | single |
|  | int8 |
|  | uint8 |
|  | int16 |
|  | uint16 |
| int32 |  |
|  | uint32 |
|  | Boolean |

In the Unreal Engine environment, instantiate the Sim3DSet actor class for the data type that you want to send to the Simulink model. For example, you can retrieve data from the double-lane change scene that indicates if cones are hit during a double-lane change maneuver. To retrieve cone hit data from the double-lane change scene, set this parameter to boolean. In the double-lane change scene, the Sim3DSetBoolean actor class is instantiated to send the cone hit or miss boolean data.

Message size, MsgSize - Message dimension
[1 1] (default)|scalar|array
3D visualization environment signal dimension. In the Unreal Engine environment blueprint, set the input to the node of the Sim3DSet actor class to specify the dimensions of data that you want to send to the Simulink model.

For example, you can retrieve data from the double-lane change scene that indicates if cones are hit during a double-lane change maneuver. To retrieve cone hit data from the double-lane change scene, set this parameter to [2 15]. In the double-lane change scene, the input to the blueprint node for the Sim3DSetBoolean actor class is set to 30, the number of cones in the scene.

## Sample time - Sample time

0.02 (default) | - 1 | scalar

Sample time, in s. The graphics frame rate is the inverse of the sample time. If you set the sample time to -1, the block uses the sample time specified in the Simulation 3D Scene Configuration block.

## Version History

Introduced in R2019b

See Also<br>Double Lane Change | Simulation 3D Scene Configuration | Simulation 3D Message Set<br>Topics<br>"Get Started Communicating with the Unreal Engine Visualization Environment"<br>"Send and Receive Double-Lane Change Scene Data"

"Customize 3D Scenes for Vehicle Dynamics Simulations"
External Websites
Unreal Engine

## Simulation 3D Message Set

Send data to Unreal Engine visualization environment


## Libraries:

Vehicle Dynamics Blockset / Vehicle Scenarios / Sim3D / Sim3D Core
Aerospace Blockset / Animation / Simulation 3D
Simulink 3D Animation / Simulation 3D

## Description

The Simulation 3D Message Set block sends data to the Unreal Engine 3D visualization environment. In your model, ensure that the Simulation 3D Scene Configuration block is at the same level as the Simulation 3D Message Set block.

Tip Verify that the Simulation 3D Message Set block executes before the Simulation 3D Scene Configuration block. That way, Simulation 3D Message Set prepares the signal data before the Unreal Engine 3D visualization environment receives it. To check the block execution order, right-click the blocks and select Properties. On the General tab, confirm these Priority settings:

- Simulation 3D Scene Configuration - 0
- Simulation 3D Message Set - - 1

For more information about execution order, see "Control and Display Execution Order".

## Configure Scenes to Receive Data

To use the block, you must configure scenes in the Unreal Engine environment to receive data from the Simulink model:

1 Install the "Customize 3D Scenes for Vehicle Dynamics Simulations".
2 In the Unreal Editor, follow these general workflows to receive data from Simulink. For detailed information, see "Get Started Communicating with the Unreal Engine Visualization Environment".

| Unreal Engine User | Workflow |
| :---: | :---: |
| Blueprint | a Instantiate the Sim3DGet actor that corresponds to the data type you want to receive from the Simulink model. This example shows the Unreal Editor Sim3DGet data types. <br> b Specify an actor tag name that matches the Simulation 3D Message Set block Signal name parameter. <br> c Navigate to the Level Blueprint. <br> d Find the blueprint method for the Sim3DGet actor class based on the data type and size that you want to receive from the Simulink model. <br> For example, in Unreal Editor, this diagram shows that Read Scalar Integer is the method for Sim3DGetInteger actor class to receive int32 data type of size scalar. <br> Compile and save the scene. |
|  | Note By default, the Double Lane Change scene has a Sim3DGetInteger actor with tag name TrafficLight1. |


| Unreal Engine User | Workflow |
| :---: | :---: |
| C++ class | a Create a new actor class for the mesh or asset that you want the Simulink model to interact with. Derive it from ASim3dActor. <br> b In the new actor class: <br> - Declare a pointer to the signal name as a class field. <br> - Get the class tag. <br> - Create a signal reader and assign the pointer in the method Sim3dSetup. <br> - In the method Sim3dStep, invoke the ReadSimulation3DMessage function to read the data from a Simulink model. <br> - Delete the signal reader in the method Sim3dRelease of the actor. |

For more information about the Unreal Editor, see the Unreal Engine 4 Documentation.

## Ports

## Input

WriteMsg - Data sent to scene
scalar|array
Data sent to the 3D visualization environment scene. In the Unreal Engine environment, you can configure the Sim3DGet class to receive the data from the Simulink model.

For example, in the Unreal Editor, the Double Lane Change scene has a Sim3DGetInteger integer actor with tag name TrafficLight1. The integer actor reads int32 data type from the Simulink model. You can use it to control the traffic signal light color.

This table provides the scene traffic signal light color that corresponds to the WriteMsg value in the Double Lane Change scene.

| Simulation 3D Message Set Block WriteMsg <br> Value | TrafficLight1 Color |
| :--- | :--- |
| 0 | Red |
| 1 | Yellow |
| 2 | Green |

## Parameters

Signal name, SigName - Message signal name
mySignal (default)
Specifies the signal name in the 3D visualization environment. In the Unreal Engine environment, use the Sim3Get actor class 'Tags' property located in the 'Details' pane.

For example, you can send data to the double lane change scene that changes the traffic signal light color to red, yellow, or green. To send data to the traffic signal light, set this parameter to TrafficLight1. In the double lane change scene, the 'Tags' property value for Sim3dGetInteger actor class is set to TrafficLight1.

Sample time - Sample time
0.02 (default) |-1 | scalar

Sample time, in s. The graphics frame rate is the inverse of the sample time. If you set the sample time to -1 , the block uses the sample time specified in the Simulation 3D Scene Configuration block.

## Version History

## Introduced in R2019b

## See Also

Simulation 3D Scene Configuration | Simulation 3D Message Get
Topics
"Get Started Communicating with the Unreal Engine Visualization Environment"
"Send and Receive Double-Lane Change Scene Data"
"Customize 3D Scenes for Vehicle Dynamics Simulations"
External Websites
Unreal Engine

## Simulation 3D Tractor

Implement tractor in 3D environment


## Libraries:

Vehicle Dynamics Blockset / Vehicle Scenarios / Sim3D / Sim3D Vehicle / Components

## Description

The Simulation 3D Tractor block implements a tree-axle tractor in the 3D simulation environment.
To use the Simulation 3D Tractor block, ensure that the Simulation 3D Scene Configuration block is in your model. If you set the Sample time parameter of the Simulation 3D Tractor block to -1, the block uses the sample time specified in the Simulation 3D Scene Configuration block.

The block input uses the vehicle Z-down right-handed (RH) Cartesian coordinate system defined in SAE J670 ${ }^{1}$. The coordinate system is inertial and initially aligned with the vehicle geometric center:

- $X$-axis - Points forward along vehicle longitudinal axis
- $Y$-axis - Points to the right along vehicle lateral axis
- Z-axis - Points downward

Tip Verify that the Simulation 3D Tractor block executes before the Simulation 3D Scene Configuration block. That way, Simulation 3D Vehicle prepares the signal data before the Unreal Engine 3D visualization environment receives it. To check the block execution order, right-click the blocks and select Properties. On the General tab, confirm these Priority settings:

- Simulation 3D Scene Configuration - 0
- Simulation 3D Tractor - - 1

For more information about execution order, see "Control and Display Execution Order".

## Ports

## Input

Translation - Vehicle translation
7-by-3 array
Vehicle and wheel translation, in $m$. The array dimensions are 7-by-3, where:

- Translation(1,1), Translation(1,2), and Translation(1,3) - Vehicle translation along the inertial vehicle Z-down $X$-, $Y$-, and $Z$-axes, respectively.
- Translation(...,1), Translation(...,2), and Translation(...,3) - Wheel translation relative to vehicle, along the vehicle Z-down $X$-, $Y$-, and $Z$-axes, respectively.

The signal contains translation information according to the axle and wheel locations.

$$
\text { Translation }=\left[\begin{array}{ccc}
X_{v} & Y_{v} & Z_{v} \\
X_{F L} & Y_{F L} & Z_{F L} \\
X_{F R} & Y_{F R} & Z_{F R} \\
X_{M L} & Y_{M L} & Z_{M L} \\
X_{M R} & Y_{M R} & Z_{M R} \\
X_{R L} & Y_{R L} & Z_{R L} \\
X_{R R} & Y_{R R} & Z_{R R}
\end{array}\right]
$$

| Translation | Array Element | Translation Axis |
| :--- | :--- | :--- |
| Vehicle, $X_{v}$ | Translation(1,1) | Inertial vehicle Z-down $X$-axis |
| Vehicle, $Y_{v}$ | Translation(1,2) | Inertial vehicle Z-down $Y$-axis |
| Vehicle, $Z_{v}$ | Translation(1,3) | Inertial vehicle Z-down Z-axis |
| Front left wheel, $X_{F L}$ | Translation(2,1) | Vehicle Z-down $X$-axis |
| Front left wheel, $Y_{F L}$ | Translation(2,2) | Vehicle Z-down $Y$-axis |
| Front left wheel, $Z_{F L}$ | Translation(2,3) | Vehicle Z-down Z-axis |
| Front right wheel, $X_{F R}$ | Translation(3,1) | Vehicle Z-down $X$-axis |
| Front right wheel, $Y_{F R}$ | Translation(3,2) | Vehicle Z-down $Y$-axis |
| Front right wheel, $Z_{F R}$ | Translation(3,3) | Vehicle Z-down Z-axis |
| Middle left wheel, $X_{M L}$ | Translation(4,1) | Vehicle Z-down $X$-axis |
| Middle left wheel, $Y_{M L}$ | Translation(4,2) | Vehicle Z-down $Y$-axis |
| Middle left wheel, $Z_{M L}$ | Translation(4,3) | Vehicle Z-down Z-axis |
| Middle right wheel, $X_{M R}$ | Translation(5,1) | Vehicle Z-down $X$-axis |
| Middle right wheel, $Y_{M R}$ | Translation(5,2) | Vehicle Z-down $Y$-axis |
| Middle right wheel, $Z_{M R}$ | Translation(5,3) | Vehicle Z-down Z-axis |
| Rear left wheel, $X_{R L}$ | Translation(6,1) | Vehicle Z-down $X$-axis |
| Rear left wheel, $Y_{R L}$ | Translation(6,2) | Vehicle Z-down $Y$-axis |
| Rear left wheel, $Z_{R L}$ | Translation(6,3) | Vehicle Z-down Z-axis |
| Rear right wheel, $X_{R R}$ | Translation(7,1) | Vehicle Z-down $X$-axis |
| Rear right wheel, $Y_{R R}$ | Translation(7,2) | Vehicle Z-down $Y$-axis |
| Rear right wheel, $Z_{R R}$ | Translation(7,3) | Vehicle Z-down Z-axis |

Rotation - Vehicle rotation
7-by-3 array
Vehicle and wheel rotation, in rad. The array dimensions are 7-by-3, where:

- Rotation(1, 1), Rotation(1,2), and Rotation(1,3) - Vehicle rotation about the inertial vehicle Z-down $X$-, $Y$-, and $Z$-axes, respectively.
- Rotation(...,1), Rotation(...,2), and Rotation(...,3) - Wheel rotation relative to vehicle, about the vehicle Z-down $X$-, $Y$-, and $Z$-axes, respectively.

The signal contains rotation information according to the axle and wheel locations.

$$
\text { Rotation }=\left[\begin{array}{ccc}
\text { Roll }_{v} & \text { Pitch }_{v} & \text { Yaw }_{v} \\
\text { Roll }_{F L} & \text { Pitch }_{F L} & \text { Yaw }_{F L} \\
\text { Roll }_{F R} & \text { Pitch }_{F R} & \text { Yaw }_{F R} \\
\text { Roll }_{M L} & \text { Pitch }_{M L} & \text { Yaw }_{M L} \\
\text { Roll }_{M R} & \text { itch }_{M R} & \text { Yaw }_{M R} \\
\text { Roll }_{R L} & \text { Pitch }_{R L} & \text { Yaw }_{R L} \\
\text { Roll }_{R R} & \text { Pitch }_{R R} & \text { Yaw }_{R R}
\end{array}\right]
$$

| Rotation | Array Element | Rotation Axis |
| :---: | :---: | :---: |
| Vehicle, Rollv | Rotation(1,1) | Inertial vehicle Z-down $X$-axis |
| Vehicle, Pitch ${ }_{v}$ | Rotation(1,2) | Inertial vehicle Z -down $Y$-axis |
| Vehicle, Yaw ${ }_{v}$ | Rotation(1,3) | Inertial vehicle Z-down $Z$-axis |
| Front left wheel, Roll ${ }_{F L}$ | Rotation(2,1) | Vehicle Z-down $X$-axis |
| Front left wheel, Pitch $_{\text {FL }}$ | Rotation(2,2) | Vehicle Z-down Y-axis |
| Front left wheel, Yaw $_{F L}$ | Rotation(2,3) | Vehicle Z-down Z -axis |
| Front right wheel, Roll $_{F R}$ | Rotation(3,1) | Vehicle Z-down $X$-axis |
| Front right wheel, Pitch $_{\text {FR }}$ | Rotation(3,2) | Vehicle Z-down $Y$-axis |
| Front right wheel, Yaw $_{\text {FR }}$ | Rotation(3,3) | Vehicle Z-down $Z$-axis |
| Middle left wheel, Roll $_{\text {ML }}$ | Rotation(4,1) | Vehicle Z-down $X$-axis |
| Middle left wheel, Pitch $_{\text {ML }}$ | Rotation(4,2) | Vehicle Z-down $Y$-axis |
| Middle left wheel, Yaw ${ }_{\text {ML }}$ | Rotation(4,3) | Vehicle Z-down Z -axis |
| Middle right wheel, Roll $_{\text {MR }}$ | Rotation(5,1) | Vehicle Z-down $X$-axis |
| Middle right wheel, Pitch $_{\text {MR }}$ | Rotation(5,2) | Vehicle Z-down $Y$-axis |
| Middle right wheel, Yaw ${ }_{\text {MR }}$ | Rotation(5,3) | Vehicle Z-down Z-axis |
| Rear left wheel, Roll ${ }_{\text {RL }}$ | Rotation(6,1) | Vehicle Z-down $X$-axis |
| Rear left wheel, Pitch $_{\text {RL }}$ | Rotation(6,2) | Vehicle Z-down Y-axis |
| Rear left wheel, Yaw RL | Rotation(6,3) | Vehicle Z-down Z -axis |
| Rear right wheel, Roll $_{R R}$ | Rotation(7,1) | Vehicle Z-down $X$-axis |
| Rear right wheel, Pitch $_{R R}$ | Rotation(7,2) | Vehicle Z-down $Y$-axis |
| Rear right wheel, Yaw $_{\text {RR }}$ | Rotation(7,3) | Vehicle Z-down Z-axis |

## Parameters

## Vehicle Parameters

Type - Tractor type
Conventional tractor (default) | Cab-over tractor
Type of tractor. For the dimensions, see:

## - Cab-Over Tractor

- Conventional Tractor

Color - Vehicle color
Red (default) | Orange | Yellow|Green | Blue | Black | White | Silver
Specify the vehicle color.
Name - Name of vehicle
SimulinkVehicle1 (default) | character vector
Name of the vehicle. By default, when you use the block in your model, the block sets the Name parameter to SimulinkVehicle $X$. The value of $X$ depends on the number of Simulation 3D Vehicle with Ground Following and Simulation 3D Vehicle blocks that you have in your model.

Initial Values
Initial array values to translate vehicle per part, Translation - Vehicle initial translation zeros( 7, 3 ) (default) | 7-by-3 array

Initial vehicle and wheel translation, in m . The array dimensions are 7-by-3, where:

- Translation(1,1), Translation(1,2), and Translation(1,3) - Initial vehicle translation along the inertial vehicle Z-down coordinate system $X-, Y$-, and $Z$-axes, respectively.
- Translation (..., 1), Translation( . . , 2), and Translation(...,3) - Initial wheel translation relative to the vehicle, along the vehicle Z-down $X$-, $Y$-, and $Z$-axes, respectively.

The parameter contains translation information according to the axle and wheel locations.

$$
\text { Translation }=\left[\begin{array}{ccc}
X_{v} & Y_{v} & Z_{v} \\
X_{F L} & Y_{F L} & Z_{F L} \\
X_{F R} & Y_{F R} & Z_{F R} \\
X_{M L} & Y_{M L} & Z_{M L} \\
X_{M R} & Y_{M R} & Z_{M R} \\
X_{R L} & Y_{R L} & Z_{R L} \\
X_{R R} & Y_{R R} & Z_{R R}
\end{array}\right]
$$

| Translation | Array Element | Translation Axis |
| :---: | :---: | :---: |
| Vehicle, $X_{v}$ | Translation(1,1) | Inertial vehicle Z-down $X$-axis |
| Vehicle, $Y_{v}$ | Translation(1,2) | Inertial vehicle Z-down $Y$-axis |
| Vehicle, $Z_{v}$ | Translation(1,3) | Inertial vehicle Z-down $Z$-axis |
| Front left wheel, $X_{F L}$ | Translation(2,1) | Vehicle Z-down $X$-axis |
| Front left wheel, $Y_{F L}$ | Translation(2,2) | Vehicle Z-down $Y$-axis |
| Front left wheel, $Z_{F L}$ | Translation(2,3) | Vehicle Z-down Z-axis |
| Front right wheel, $X_{F R}$ | Translation(3,1) | Vehicle Z-down $X$-axis |
| Front right wheel, $Y_{F R}$ | Translation(3,2) | Vehicle Z-down Y-axis |
| Front right wheel, $Z_{F R}$ | Translation(3,3) | Vehicle Z-down Z -axis |
| Middle left wheel, $X_{M L}$ | Translation(4,1) | Vehicle Z-down $X$-axis |


| Translation | Array Element | Translation Axis |
| :--- | :--- | :--- |
| Middle left wheel, $Y_{M L}$ | Translation(4,2) | Vehicle Z-down $Y$-axis |
| Middle left wheel, $Z_{M L}$ | Translation(4,3) | Vehicle Z-down Z-axis |
| Middle right wheel, $X_{M R}$ | Translation(5,1) | Vehicle Z-down $X$-axis |
| Middle right wheel, $Y_{M R}$ | Translation(5,2) | Vehicle Z-down $Y$-axis |
| Middle right wheel, $Z_{M R}$ | Translation(5,3) | Vehicle Z-down Z-axis |
| Rear left wheel, $X_{R L}$ | Translation(6,1) | Vehicle Z-down $X$-axis |
| Rear left wheel, $Y_{R L}$ | Translation(6,2) | Vehicle Z-down $Y$-axis |
| Rear left wheel, $Z_{R L}$ | Translation(6,3) | Vehicle Z-down Z-axis |
| Rear right wheel, $X_{R R}$ | Translation(7,1) | Vehicle Z-down $X$-axis |
| Rear right wheel, $Y_{R R}$ | Translation(7,2) | Vehicle Z-down Y-axis |
| Rear right wheel, $Z_{R R}$ | Translation(7,3) | Vehicle Z-down Z-axis |

Initial array values to rotate vehicle per part, Rotation - Vehicle initial rotation zeros( 7, 3 ) (default) | 7-by-3 array

Initial vehicle and wheel rotation, about the vehicle Z-down $X$-, $Y$-, and $Z$-axes, in rad.
The array dimensions are 7-by-3.

- Rotation(1,1), Rotation(1,2), and Rotation(1,3) - Initial vehicle rotation about the inertial vehicle Z-down coordinate system $X$-, $Y$-, and $Z$-axes, respectively.
- Rotation( . . , 1), Rotation (..., 2) , and Rotation (...,3) - Initial wheel rotation relative to the vehicle, about the vehicle Z-down $X$-, $Y$-, and $Z$-axes, respectively.

The parameter contains rotation information according to the axle and wheel locations.

$$
\text { Rotation }=\left[\begin{array}{ccc}
\text { Roll }_{v} & \text { Pitch }_{v} & \text { Yaw }_{v} \\
\text { Roll }_{F L} & \text { Pitch }_{F L} & \text { Yaw }_{F L} \\
\text { Roll }_{F R} & \text { Pitch }_{F R} & \text { Yaw }_{F R} \\
\text { Roll }_{M L} & \text { Pitch }_{M L} & \text { Yaw }_{M L} \\
\text { Roll }_{M R} & \text { itch }_{M R} & \text { Yaw }_{M R} \\
\text { Roll }_{R L} & \text { Pitch }_{R L} & \text { Yaw }_{R L} \\
\text { Roll }_{R R} & \text { Pitch }_{R R} & \text { Yaw }_{R R}
\end{array}\right]
$$

| Rotation | Array Element | Rotation Axis |
| :--- | :--- | :--- |
| Vehicle, Roll $_{v}$ | Rotation $(1,1)$ | Inertial vehicle Z-down X-axis |
| Vehicle, Pitch $_{v}$ | Rotation $(1,2)$ | Inertial vehicle Z-down Y-axis |
| Vehicle, Yaw $_{v}$ | Rotation $(1,3)$ | Inertial vehicle Z-down Z-axis |
| Front left wheel, Roll $_{F L}$ | Rotation $(2,1)$ | Vehicle Z-down $X$-axis |
| Front left wheel, Pitch $_{F L}$ | Rotation $(2,2)$ | Vehicle Z-down $Y$-axis |
| Front left wheel, Yaw $_{F L}$ | Rotation $(2,3)$ | Vehicle Z-down Z-axis |
| Front right wheel, Roll $_{F R}$ | Rotation $(3,1)$ | Vehicle Z-down $X$-axis |


| Rotation | Array Element | Rotation Axis |
| :---: | :---: | :---: |
| Front right wheel, Pitch $_{\text {FR }}$ | Rotation(3,2) | Vehicle Z-down Y-axis |
| Front right wheel, Yaw $_{\text {FR }}$ | Rotation(3,3) | Vehicle Z-down Z-axis |
| Middle left wheel, Roll $_{\text {ML }}$ | Rotation(4,1) | Vehicle Z-down X-axis |
| Middle left wheel, Pitch $_{\text {ML }}$ | Rotation(4,2) | Vehicle Z-down Y-axis |
| Middle left wheel, $Y^{\prime} w_{M L}$ | Rotation(4,3) | Vehicle Z-down Z-axis |
| Middle right wheel, Roll $_{\text {MR }}$ | Rotation(5,1) | Vehicle Z-down $X$-axis |
| Middle right wheel, Pitch $_{\text {MR }}$ | Rotation(5,2) | Vehicle Z-down Y-axis |
| Middle right wheel, Yaw $_{\text {MR }}$ | Rotation(5,3) | Vehicle Z-down $Z$-axis |
| Rear left wheel, Roll ${ }_{R L}$ | Rotation(6,1) | Vehicle Z-down $X$-axis |
| Rear left wheel, Pitch $_{\text {RL }}$ | Rotation(6,2) | Vehicle Z-down Y-axis |
| Rear left wheel, Yaw RL | Rotation(6,3) | Vehicle Z-down Z-axis |
| Rear right wheel, Roll $_{R R}$ | Rotation(7,1) | Vehicle Z-down $X$-axis |
| Rear right wheel, Pitch $_{\text {RR }}$ | Rotation(7,2) | Vehicle Z-down Y-axis |
| Rear right wheel, Yaw ${ }_{\text {RR }}$ | Rotation(7,3) | Vehicle Z-down Z-axis |

## Sample time - Sample time

## - 1 (default) | scalar

Sample time, $T_{s}$. The graphics frame rate is the inverse of the sample time.

## Version History

Introduced in R2020b

## References

[1] Vehicle Dynamics Standards Committee. Vehicle Dynamics Terminology. SAE J670. Warrendale, PA: Society of Automotive Engineers, 2008.
[2] Technical Committee. Road vehicles - Vehicle dynamics and road-holding ability - Vocabulary. ISO 8855:2011. Geneva, Switzerland: International Organization for Standardization, 2011.

## See Also

Vehicle Body 3DOF Three Axles | Simulation 3D Trailer | Vehicle Body 6DOF Three Axles | Vehicle Body 3DOF | Vehicle Body 6DOF

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"
"How 3D Simulation for Vehicle Dynamics Blockset Works"

## Simulation 3D Physics Vehicle

Implement controllable 6DOF vehicle 3D environment


## Libraries:

Vehicle Dynamics Blockset / Vehicle Scenarios / Sim3D / Sim3D Vehicle / Components

## Description

The Simulation 3D Physics Vehicle block implements a controllable 10DOF vehicle in the 3D simulation environment, with a vertical DOF for each vehicle and 6DOF for the chassis.

To use the Simulation 3D Physics Vehicle block, ensure that the Simulation 3D Scene Configuration block is in your model. If you set the Sample time parameter of the Simulation 3D Physics Vehicle block to -1, the block uses the sample time specified in the Simulation 3D Scene Configuration block.

The block input uses the vehicle Z-down right-handed (RH) Cartesian coordinate system defined in SAE J670 ${ }^{1}$. The coordinate system is inertial and initially aligned with the vehicle geometric center:

- $X$-axis - Along vehicle longitudinal axis, points forward
- $Y$-axis - Along vehicle lateral axis, points to the right
- Z-axis - Points downward

Tip Verify that the Simulation 3D Scene Configuration block executes before the Simulation 3D Physics Vehicle block. That way, the Unreal Engine 3D visualization environment prepares the data before the Simulation 3D Physics Vehicle block receives it. To check the block execution order, rightclick the blocks and select Properties. On the General tab, confirm these Priority settings:

- Simulation 3D Scene Configuration - 0
- Simulation 3D Physics Vehicle - - 1

For more information about execution order, see "Control and Display Execution Order".

## Ports

Input
SteerCmd - Normalized steer angle
scalar
Normalized steer angle, specified as a scalar. SteerCmd corresponds to the minimum and maximum range of the steering angle as determined by theFront wheel max steer angle and Rear wheel max steer angle parameters, respectively

AccelCmd - Normalized vehicle acceleration
scalar

Normalized acceleration torque request to the vehicle powertrain, specified as a scalar. The exact response will be characterized by the engine, transmission and other vehicle parameters.

## DecelCmd - Normalized vehicle deceleration

scalar
Normalized deceleration torque request to the vehicle braking system, specified as a scalar. The exact braking response will be characterized by the engine, transmission and other vehicle parameters.

GearCmd - Gear input
1|-1|0
Gear input, specified as either $1,-1$, or 0 , with:

- 1 - Forward shift gear.
-     - 1 - Reverse gear.
- 0 - Neutral gear.

If manual shift mode is selected, then the vehicle will shift according to what the signal is, but the values listed will still apply. Any input set that doesn't correspond to a valid gear will be ignored.

## Output

Info - Bus signal
bus
Bus signal containing these block values.

| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| InertFrm | Cg | Disp | X | Vehicle CG displacement along the earth-fixed $X$ axis | Computed | m |
|  |  |  | Y | Vehicle CG displacement along the earth-fixed $Y$ axis | Computed | m |
|  |  |  | Z | Vehicle CG displacement along the earth-fixed $Z$ axis | 0 | m |
|  |  | Vel | Xdot | Vehicle CG velocity along the earth-fixed $X$-axis | Computed | m/s |
|  |  |  | Ydot | Vehicle CG velocity along the earth-fixed $Y$-axis | Computed | m/s |
|  |  |  | Zdot | Vehicle CG velocity along the earth-fixed $Z$-axis | 0 | m/s |
|  |  | Ang | phi | Rotation of the vehiclefixed frame about the earth-fixed $X$-axis (roll) | 0 | rad |


| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | theta | Rotation of the vehiclefixed frame about the earth-fixed $Y$-axis (pitch) | 0 | rad |
|  |  | psi | Rotation of the vehiclefixed frame about the earth-fixed $Z$-axis (yaw) | Computed | rad |
| BdyFrm | Cg |  | Vel | xdot | Vehicle CG velocity along the vehicle-fixed $x$-axis | Computed | m/s |
|  |  | ydot |  | Vehicle CG velocity along the vehicle-fixed $y$-axis | Computed | m/s |
|  |  | zdot |  | Vehicle CG velocity along the vehicle-fixed $z$-axis | 0 | m/s |
|  |  | Ang | Beta | Body slip angle, $\beta$ $\beta=\frac{V_{y}}{V_{x}}$ | Computed | rad |
|  |  | AngVel | p | Vehicle angular velocity about the vehicle-fixed $x$ axis (roll rate) | 0 | rad/s |
|  |  |  | q | Vehicle angular velocity about the vehicle-fixed $y$ axis (pitch rate) | 0 | rad/s |
|  |  |  | r | Vehicle angular velocity about the vehicle-fixed $z$ axis (yaw rate) | Computed | rad/s |
|  |  | Acc | ax | Vehicle CG acceleration along the vehicle-fixed $x$ axis | Computed | gn |
|  |  |  | ay | Vehicle CG acceleration along the vehicle-fixed $y$ axis | Computed | gn |
|  |  |  | az | Vehicle CG acceleration along the vehicle-fixed $z$ axis | 0 | gn |
|  |  |  | xddot | Vehicle CG acceleration along the vehicle-fixed $x$ axis | Computed | $\mathrm{m} / \mathrm{s}^{\wedge} 2$ |
|  |  |  | yddot | Vehicle CG acceleration along the vehicle-fixed $y$ axis | Computed | $\mathrm{m} / \mathrm{s}^{\wedge} 2$ |
|  |  |  | zddot | Vehicle CG acceleration along the vehicle-fixed $z$ axis | 0 | $\mathrm{m} / \mathrm{s}^{\wedge} 2$ |


| Signal |  |  |  |  |  | AngAcc | pdot |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Signal | Description | Variable | Units |  |
| :--- | :--- | :--- | :--- | :--- |
|  | TransGear | Engaged gear | $N$ | N/A |

The Info output parameter is optional.
xdot - Vehicle longitudinal velocity
scalar
Vehicle CG velocity along the vehicle-fixed $x$-axis, in $\mathrm{m} / \mathrm{s}$.
ydot - Vehicle lateral velocity
scalar
Vehicle CG velocity along the vehicle-fixed $y$-axis, in $\mathrm{m} / \mathrm{s}$.
psi - Yaw
scalar
Rotation of the vehicle-fixed frame about the earth-fixed Z-axis (yaw), in rad.
$\mathbf{r}$ - Yaw rate
scalar
Vehicle angular velocity, r , about the vehicle-fixed $z$-axis (yaw rate), in rad/s.

## Parameters

## Chassis

Type - Type
Muscle car (default)|Sedan|Sport utility vehicle|Small pickup truck|Hatchback| Box truck|Custom

Specify the vehicle type. This table provides links to the vehicle dimensions.

| Vehicle type Setting | Vehicle Dimensions |
| :--- | :--- |
| Muscle car | Muscle Car |
| Sedan | Sedan |
| Sport utility vehicle | Sport Utility Vehicle |
| Small pickup truck | Small Pickup Truck |
| Hatchback | Hatchback |
| Box truck | Box Truck |

## Dependencies

Selecting Custom enables parameters that allow you to import a custom mesh for your vehicle.
Color - Color of vehicle
Red (default) | Orange | Yellow | Green | Blue | Black | White | Silver
Select the color of the vehicle.

## Name - Name of vehicle

## SimulinkVehicle1 (default)| character vector

Name of vehicle. By default, when you use the block in your model, the block sets the Name parameter to SimulinkVehicle $X$. The value of $X$ depends on the number of Simulation 3D Physics Vehicle and Simulation 3D Vehicle blocks that you have in your model.

Initial position - Vehicle initial position
[ $0,0,0]$ (default) | 1-by-3 array
Initial vehicle position specified by a 1-by-3 array, in m. Array elements are values along the
Coordinate system parameter $X$-, $Y$-, and $Z$ - axes, respectively.
Initial rotation - Vehicle initial rotation
[ 0, 0, 0 ] (default) | 1-by-3 array
Initial vehicle rotation specified by a 1-by-3 array, in rad. Array elements are values about the Coordinate system parameter $X$-, $Y$-, and $Z$ - axes, respectively.

Mass - Vehicle mass
1500 (default) | scalar
Vehicle mass, in kg . This value does not include the wheel masses.
Drag Coefficient - Vehicle drag coefficient
0.3 (default) | scalar

Vehicle drag coefficient, dimensionless.
Track width - Distance between wheels
2 (default) | scalar
The vehicle track width refers to the distance between the wheels, or the axle length, specified in meters.

## Dependencies

To enable this parameter, set Type to Custom.
Chassis height - Height of chassis
1.5 (default) | scalar

Height of chassis used to calculate drag force, specified in meters.
Center of mass offset - Offset in center of mass
[0, 0, 0] (default) | three element vector
Offset in center of mass, specified as a three element vector, in meters.
Inertia tensor scaling vector - Scaling of inertia tensor
[1, 1, 1] (default) | three element vector
Scaling of inertia tensor, specified as a three element dimensionless vector.
Path to custom mesh - Path to custom mesh
character vector

Path to custom mesh file.

## Dependencies

To enable this parameter, set Type to Custom.
Wheel base in custom mesh - Wheel base in custom mesh
3 (default) | scalar
Wheel base, in meters.

## Dependencies

To enable this parameter, set Type to Custom.
Front Wheel radius - Front Wheel radius
0.30 (default) | scalar

Front wheel radius, in meters.

## Dependencies

To enable this parameter, set Type to Custom.
Rear Wheel radius - Rear Wheel radius
0.30 (default) | scalar

Rear wheel radius, in meters.

## Dependencies

To enable this parameter, set Type to Custom.

## Powertrain and Driveline

## Powertrain

Motor torque indices - Motor torque indices
[ 75, 300, 400, 0 ] (default) | vector
Motor torque indices, in $N \cdot m$. You can use these pre-transmission values to represent either an electric motor or a conventional engine.
Data Types: double
Motor speed breakpoints - Motor speed breakpoints
[ 0, 1000, 5500, 8000 ] (default)|vector
Motor speed breakpoints, in rpm.
Data Types: double
Max powertrain speed - Max powertrain speed
10000 (default) | scalar
Max powertrain speed, in rpm. If you select an automatic transmission option, this value also corresponds to the normalized shift points used in the up and downshift logic.

Data Types: double

Powertrain rotational inertia - Powertrain rotational inertia
1 (default) | scalar
Powertrain rotational inertia, in $\mathrm{kg} \cdot \mathrm{m}^{2}$.
Data Types: double
Powertrain damping at full max torque request - Powertrain damping at full max torque request 0.15 (default)| scalar

Powertrain damping at full max torque request, in $\mathrm{kg} \cdot \mathrm{m}^{2} / \mathrm{s}$.
Data Types: double
Powertrain damping at zero torque request, in gear - Powertrain damping at zero torque request, in gear
2 (default) | scalar
Powertrain damping at zero torque request, in gear, in $\mathrm{kg} \cdot \mathrm{m}^{2} / \mathrm{s}$.
Data Types: double
Powertrain damping at zero torque request, in neutral - Powertrain damping at zero torque request, in neutral
0.35 (default)| scalar

Powertrain damping at zero torque request, in neutral, in $\mathrm{kg} \cdot \mathrm{m}^{2} / \mathrm{s}$.
Data Types: double

## Driveline

Differential type - Differential
Limited Slip (default)|Open
For both Limited Slip and Open differentials, the block implements a differential as a planetary bevel gear train. The block matches the driveshaft bevel gear to the crown (ring) bevel gear.

If you select Limited Slip, the block prevents one of the wheels from slipping by splitting the torque applied to the left and right axles. With different torque applied to the axles, the wheels can move at different angular velocities, preventing slip.

Drivetrain type - Drivetrain
Rear Wheel Drive (default)|Front Wheel Drive|All Wheel Drive
Implement rear wheel, front wheel, or all wheel drive.
Transmission type - Transmission
Automatic (default)|Manual
Implement an automatic or manual transmission.

Note A response is required for the GearCmd input even if Transmission type is set to Automatic.

Clutch slip torque - Clutch slip torque
10 (default) | scalar
Clutch slip torque, specified as a scalar in $\mathrm{N} \cdot \mathrm{m}$.
Data Types: double
Shift time - Time taken to complete a shift
0.5 (default) | scalar

Time taken to complete a shift, specified as a scalar in s.
Data Types: double
Minimum shift latency - Minimum time transmission will stay in newly selected gear
2.0 (default) | scalar

Minimum time the transmission will stay in a newly selected gear to mitigate shift hunting, specified as a scalar in s.

## Data Types: double

Shift up indices - Normalized engine speeds at which a shift up for forward gears begins
[ $0.15,0.65,0.65,0.65,0.65,0.65,0.65,0.65$ ] (default)|vector
Normalized engine speeds with respect to the Max powertrain speed parameter, at which a shift up for forward gears will be initiated, specified as a scalar in s.

## Data Types: double

Shift down indices - Normalized engine speeds at which a shift down for forward gears begins
[ $0.15,0.5,0.5,0.5,0.5,0.5,0.5,0.5$ ] (default) | vector
Normalized engine speeds with respect to the Max powertrain speed parameter, at which a shift down for forward gears will be initiated, specified as a scalar in s.
Data Types: double
Gear ratio vector - Gear ratios
[ $-3.5,1,4.75,3.75,3.25,2.75,2.25,1.5,1,0.75$ ] (default)|vector
Gear ratios, dimensionless.

Note At least one negative ratio is required for reverse gear. A neutral ratio is also required such that the length of the array should correspond to the number of forward gears plus two one for reverse and one for neutral.

Data Types: double
Gear number vector - Gear ratios
[-1, 0, 1, 2, 3, 4, 5, 6, 7, 8] (default)|vector
Gear number vector, dimensionless.
Data Types: double

Front to rear torque split ratio - Front to rear torque split ratio

## 0.5 (default) | scalar

Front to rear torque split ratio, dimensionless.
1 indicates 100\% torque to the front, whereas 0 indicates $100 \%$ to the rear.
Final drive ratio - Final drive ratio
4.0 (default) | scalar

Final drive ratio, dimensionless. This is the post transmission ratio, typically found in a differential or final drive gearbox.
Data Types: double

## Steering and Brakes

## Steering

Front wheel max steer angle - Front wheel max steer angle
pi/4 (default) | scalar
Front wheel max steer angle, in radians. This is the absolute angle which the front wheels will turn with a-1 or 1 steer command input signal

Data Types: double
Rear wheel max steer angle - Rear wheel max steer angle
0 (default) | scalar
Rear wheel max steer angle, in radians. This is the absolute angle which the rear wheels will turn with a - 1 or 1 steer command input signal

Data Types: double
Percent Ackerman, PctAck - Percent Ackerman constant
1.0 (default) | scalar

Constant value of percent Ackerman, in percent. A value of 100 indicates an ideal Ackermann inside or outside steering adjustment, while 0 indicates a pure parallel steer adjustment.
Data Types: double
Maximum steering ratio breakpoints - Maximum steering ratio
[ 1, 0.8, 0.7 ] (default)|vector
Maximum steering ratio breakpoints, dimensionless. This is the gain by which the steering command is affected by the vehicle speed brake points.
Data Types: double
Steering ratio speed breakpoints - Steering ratio speed breakpoints
[ 0, 60, 120 ]./3.6 (default)|vector
Steering ratio speed breakpoints, in $\mathrm{m} / \mathrm{s}$. This is the vehicle forward speed break points used by the steer ratio gains.
Data Types: double

## Brakes

Maximum front wheel torque - Maximum front wheel torque
1500 (default) | scalar
Maximum front wheel torque, in $\mathrm{N} \cdot \mathrm{m}$. This is the maximum braking torque applied to the front wheels corresponding to the normalized DecelCmd input.
Data Types: double
Maximum rear wheel torque - Maximum rear wheel torque 1500 (default) | scalar

Maximum rear wheel torque, in $\mathrm{N} \cdot \mathrm{m}$. This is the maximum braking torque applied to the rear wheels corresponding to the normalized DecelCmd input.

Data Types: double
Front wheels affected by handbrake - Selection
off (default) | on
Front wheels affected by handbrake.
Data Types: Boolean
Rear wheels affected by handbrake - Selection
off (default) | on
Rear wheels affected by handbrake.
Data Types: Boolean
Enable handbrake input - Enable handbrake input
off (default) | on
Enable handbrake input.
Data Types: Boolean

## Suspension, Wheels and Tires

## Suspension

Front suspension force offset - Front suspension force offset
0 (default) | scalar
Front suspension force offset, specified as a scalar in meters.
Maximum front suspension compression - Maximum front suspension compression 0.01 (default) | scalar

Maximum front suspension compression or jounce, specified as a scalar in meters. Jounce is the upward movement or compression of suspension components.

Maximum front suspension extension - Maximum front suspension extension 0.01 (default) | scalar

Maximum front suspension extension or rebound, specified as a scalar in meters. Rebound is the downward movement or extension of suspension components.

Front suspension natural frequency - Natural frequency of front suspension 7 (default) | scalar

Natural frequency of front suspension, in Hz. Suspension frequencies are the rate that a spring oscillates after applying a load (or hitting a bump).

Front suspension damping ratio - Damping ratio of front suspension
1 (default) | scalar
Damping ratio of front suspension, dimensionless. Damping ratio is the coefficient of the damper at its peak level, where the vehicle will be in a completely stable state.

Rear suspension force offset - Rear suspension force offset
0 (default) | scalar
Rear suspension force offset, specified as a scalar in meters.
Maximum rear suspension compression - Maximum rear suspension compression 0.01 (default) | scalar

Maximum rear suspension compression or jounce, specified as a scalar in meters. Jounce is the upward movement or compression of suspension components.

Maximum rear suspension extension - Maximum rear suspension extension 0.01 (default) | scalar

Maximum rear suspension extension or rebound, specified as a scalar in meters. Rebound is the downward movement or extension of suspension components.

Rear suspension natural frequency - Natural frequency of rear suspension
7 (default) | scalar
Natural frequency of rear suspension, in Hz. Suspension frequencies are the rate that a spring oscillates after applying a load (or hitting a bump).

Rear suspension damping ratio - Damping ratio of rear suspension
1 (default) | scalar
Damping ratio of rear suspension, dimensionless. Damping ratio is the coefficient of the damper at its peak level, where the vehicle will be in a completely stable state.

Wheels
Front wheel mass - Front wheel mass
10 (default) | scalar
Front wheel mass, in kg.
Data Types: double
Front wheel damping - Front wheel damping
0.25 (default)| scalar

Front wheel damping, in $\mathrm{N} \cdot \mathrm{m} / \mathrm{s}$.
Data Types: double
Rear wheel mass - Rear wheel mass
10 (default) | scalar
Rear wheel mass, in kg.
Data Types: double
Rear wheel damping - Rear wheel damping
0.25 (default) | scalar

Rear wheel damping, in $\mathrm{N} \cdot \mathrm{m} / \mathrm{s}$.
Data Types: double
Tires
Front tire max lateral stiffness factor - Front tire max lateral stiffness factor
2.0 (default) | scalar

Front tire max lateral stiffness factor, dimensionless.
Data Types: double
Front tire lateral stiffness - Front tire lateral stiffness
17 (default) | scalar
Front tire lateral stiffness, dimensionless.
Data Types: double
Front tire longitudinal stiffness - Front tire longitudinal stiffness
10 (default) | scalar
Front tire longitudinal stiffness, dimensionless.
Data Types: double
Rear tire max lateral stiffness factor - Front tire max lateral stiffness factor 2.0 (default) | scalar

Front tire max lateral stiffness factor, dimensionless.
Data Types: double
Rear tire lateral stiffness - Front tire lateral stiffness
17 (default) | scalar
Rear tire lateral stiffness, dimensionless.
Data Types: double
Rear tire longitudinal stiffness - Front tire longitudinal stiffness
10 (default) | scalar
Front tire longitudinal stiffness, dimensionless.

## Data Types: double

Friction scaling factor - Friction scaling
1.0 (default) | scalar

Nominal friction scale, dimensionless.
Data Types: double

## Light Controls

Enable light controls, VehLightsControl - Control vehicle lights off (default) | on

Select whether to control the vehicle headlights. Use the enabled parameters to set the light parameters, including headlight intensity.

## Dependencies

Selecting this parameter:

- Creates the input port Light controls
- Enables these light parameters.

| Lights | Light Parameters |
| :---: | :---: |
| Headlights | - Headlight color <br> - High beam intensity <br> - Low beam intensity <br> - High beam cone half angle <br> - Low beam cone half angle <br> - Left headlight beam orientation <br> - Right headlight beam orientation |
| Brake lights | Brake light intensity |
| Reverse lights | Reverse light intensity |
| Turn signal lights | - Turn signal light intensity <br> - Period <br> - Pulse width |

## Headlights

Headlight color [R,G,B], HeadlightColor - Headlight color
[1,1,1] (default) | 1-by-3 vector of RGB triplet values
Headlight color, specified as a normalized 1-by-3 vector of RGB triplet values.

## Dependencies

To enable this parameter, select Enable light controls.
Data Types: int8|uint8

High beam intensity, HighBeamIntensity - High beam intensity
100000 (default) | positive scalar
High beam intensity, in cd.

## Dependencies

To enable this parameter, select Enable light controls.
Data Types: double
Low beam intensity, LowBeamIntensity - Low beam intensity
60000 (default) | positive scalar
Low beam intensity, in cd.

## Dependencies

To enable this parameter, select Enable light controls.

## Data Types: double

High beam cone half angle, HighBeamConeAngle - High beam cone half angle
1.22 (default) | positive scalar less than pi/2

High beam cone half angle, in rad.

## Dependencies

To enable this parameter, select Enable light controls.

## Data Types: double

Low beam cone half angle, LowBeamConeAngle - Low beam cone half angle
1.22 (default) | positive scalar less than pi/2

Low beam cone half angle, in rad.

## Dependencies

To enable this parameter, select Enable light controls.
Data Types: double
Left headlight beam orientation [Pitch, Yaw], LeftHeadlightOrientation - Left headlight beam orientation
[0,0] (default) | 1-by-2 vector greater with values between -pi and pi
Pitch and yaw orientation of the left headlight beam orientation in the $Z$-down coordinate system, specified as a 1 -by- 2 vector, in rad. The first element of the vector, [ 1,1 ], is the pitch angle. The second element of the vector, [1,2] is the yaw angle.

## Dependencies

To enable this parameter, select Enable light controls.
Data Types: double

Right headlight beam orientation [Pitch, Yaw], RightHeadlightOrientation - Right headlight beam orientation
[0,0] (default) | 1-by-2 vector greater with values between -pi and pi
Pitch and yaw orientation of the right headlight beam orientation in the Z-down coordinate system, specified as a 1 -by- 2 vector, in rad. The first element of the vector, [ 1,1 ], is the pitch angle. The second element of the vector, [1,2] is the yaw angle.

## Dependencies

To enable this parameter, select Enable light controls.

## Brake Lights

Brake light intensity, BrakelightIntensity - Intensity
500 (default) | positive scalar
Brake light intensity, in $\mathrm{cd} / \mathrm{m}^{\wedge} 2$.

## Dependencies

To enable this parameter, select Enable light controls.
Data Types: double

## Reverse Lights

Reverse light intensity, ReverselightIntensity - Intensity
500 (default) | positive scalar
Reverse light intensity, in $\mathrm{cd} / \mathrm{m}^{\wedge} 2$.

## Dependencies

To enable this parameter, select Enable light controls.

## Data Types: double

## Turn Signal Lights

Turn signal light intensity, SignallightIntensity - Intensity
500 (default) | positive scalar
Turn signal light intensity, in $\mathrm{cd} / \mathrm{m}^{\wedge} 2$.

## Dependencies

To enable this parameter, select Enable light controls.

## Data Types: double

Period, SignallightPeriod - Turn signal light period
1 (default) | positive scalar
Turn signal light period, in s.

## Dependencies

To enable this parameter, select Enable light controls.

## Data Types: double

Pulse width, SignalPulseWidth - Pulse width
50 (default) | positive scalar less than 100
Turn signal light pulse width, as a percent of the period.

## Dependencies

To enable this parameter, select Enable light controls.
Data Types: double
Sample Time
Sample time - Sample time

- 1 (default) | scalar

Sample time, $T_{s}$. The graphics frame rate is the inverse of the sample time.

## Ground Truth

Output location and orientation - Select to return location and orientation off (default) | on

Select to return location and orientation.
Data Types: Boolean
Output nominal vehicle state feedback - Select to return nominal vehicle state feedback off (default) | on

Select to return nominal vehicle state feedback
Data Types: Boolean

## Version History

## Introduced in R2022b

## References

[1] Vehicle Dynamics Standards Committee. Vehicle Dynamics Terminology. SAE J670. Warrendale, PA: Society of Automotive Engineers, 2008.
[2] Technical Committee. Road vehicles - Vehicle dynamics and road-holding ability - Vocabulary. ISO 8855:2011. Geneva, Switzerland: International Organization for Standardization, 2011.

## See Also

Simulation 3D Scene Configuration

## Topics

"Scene Interrogation in 3D Environment"

## External Websites

Unreal Engine

UWheeledVehicleMovementComponent

## Simulation 3D Trailer

Implement trailer in 3D environment


## Libraries:

Vehicle Dynamics Blockset / Vehicle Scenarios / Sim3D / Sim3D Vehicle / Components

## Description

The Simulation 3D Trailer block implements a trailer with one, two or three axles in the 3D simulation environment.

To use the Simulation 3D Trailer block, ensure that the Simulation 3D Scene Configuration block is in your model. If you set the Sample time parameter of the Simulation 3D Trailer block to -1, the block uses the sample time specified in the Simulation 3D Scene Configuration block.

The block input uses the vehicle Z-down right-handed (RH) Cartesian coordinate system defined in SAE J670 ${ }^{1}$. The coordinate system is inertial and initially aligned with the vehicle geometric center:

- $X$-axis - Points forward along vehicle longitudinal axis
- $Y$-axis - Points to the right along vehicle lateral axis
- Z-axis - Points downward

Tip Verify that the Simulation 3D Trailer block executes before the Simulation 3D Scene
Configuration block. That way, Simulation 3D Vehicle prepares the signal data before the Unreal Engine 3D visualization environment receives it. To check the block execution order, right-click the blocks and select Properties. On the General tab, confirm these Priority settings:

- Simulation 3D Scene Configuration - 0
- Simulation 3D Trailer - - 1

For more information about execution order, see "Control and Display Execution Order".

## Ports

## Input

Translation - Vehicle translation
5-by-3 array (default) | 7-by-3 array | 3-by-3 array
Vehicle and wheel translation, in m . The array dimensions are 3-by-3 for a one-axle trailer, 5-by-3 for a two-axle trailer, and 7-by-3 for a three-axle trailer, where:

- Translation(1,1), Translation(1,2), and Translation(1,3) - Vehicle translation along the inertial vehicle Z-down $X$-, $Y$-, and $Z$-axes, respectively.
- Translation(...,1), Translation(...,2), and Translation(...,3) - Wheel translation relative to vehicle, along the vehicle Z-down $X$-, $Y$-, and $Z$-axes, respectively.

The signal contains translation information according to the axle and wheel locations.
For a one-axle trailer:

$$
\text { Translation }=\left[\begin{array}{lll}
X_{v} & Y_{v} & Z_{v} \\
X_{L} & Y_{L} & Z_{L} \\
X_{R} & Y_{R} & Z_{R}
\end{array}\right]
$$

| Translation | Array Element | Translation Axis |
| :--- | :--- | :--- |
| Vehicle, $X_{v}$ | Translation(1,1) | Inertial vehicle Z-down $X$-axis |
| Vehicle, $Y_{v}$ | Translation(1,2) | Inertial vehicle Z-down $Y$-axis |
| Vehicle, $Z_{v}$ | Translation(1,3) | Inertial vehicle Z-down Z-axis |
| Left wheel, $X_{L}$ | Translation $(2,1)$ | Vehicle Z-down $X$-axis |
| Left wheel, $Y_{L}$ | Translation $(2,2)$ | Vehicle Z-down $Y$-axis |
| Left wheel, $Z_{L}$ | Translation(2,3) | Vehicle Z-down Z-axis |
| Right wheel, $X_{R}$ | Translation $(3,1)$ | Vehicle Z-down $X$-axis |
| Right wheel, $Y_{R}$ | Translation(3,2) | Vehicle Z-down $Y$-axis |
| Right wheel, $Z_{R}$ | Translation(3,3) | Vehicle Z-down Z-axis |

For a two-axle trailer:
Translation $=\left[\begin{array}{ccc}X_{v} & Y_{v} & Z_{v} \\ X_{F L} & Y_{F L} & Z_{F L} \\ X_{F R} & Y_{F R} & Z_{F R} \\ X_{R L} & Y_{R L} & Z_{R L} \\ X_{R R} & Y_{R R} & Z_{R R}\end{array}\right]$

| Translation | Array Element | Translation Axis |
| :--- | :--- | :--- |
| Vehicle, $X_{v}$ | Translation(1,1) | Inertial vehicle Z-down $X$-axis |
| Vehicle, $Y_{v}$ | Translation(1,2) | Inertial vehicle Z-down $Y$-axis |
| Vehicle, $Z_{v}$ | Translation(1,3) | Inertial vehicle Z-down Z-axis |
| Front left wheel, $X_{F L}$ | Translation(2,1) | Vehicle Z-down $X$-axis |
| Front left wheel, $Y_{F L}$ | Translation(2,2) | Vehicle Z-down $Y$-axis |
| Front left wheel, $Z_{F L}$ | Translation(2,3) | Vehicle Z-down Z-axis |
| Front right wheel, $X_{F R}$ | Translation (3,1) | Vehicle Z-down $X$-axis |
| Front right wheel, $Y_{F R}$ | Translation(3,2) | Vehicle Z-down $Y$-axis |
| Front right wheel, $Z_{F R}$ | Translation(3,3) | Vehicle Z-down Z-axis |
| Rear left wheel, $X_{R L}$ | Translation(4,1) | Vehicle Z-down $X$-axis |
| Rear left wheel, $Y_{R L}$ | Translation(4,2) | Vehicle Z-down $Y$-axis |
| Rear left wheel, $Z_{R L}$ | Translation(4,3) | Vehicle Z-down Z-axis |
| Rear right wheel, $X_{R R}$ | Translation(5,1) | Vehicle Z-down $X$-axis |


| Translation | Array Element | Translation Axis |
| :--- | :--- | :--- |
| Rear right wheel, $Y_{R R}$ | Translation (5,2) | Vehicle Z-down Y-axis |
| Rear right wheel, $Z_{R R}$ | Translation(5,3) | Vehicle Z-down Z-axis |

For a three-axle trailer:

$$
\text { Translation }=\left[\begin{array}{ccc}
X_{v} & Y_{v} & Z_{v} \\
X_{F L} & Y_{F L} & Z_{F L} \\
X_{F R} & Y_{F R} & Z_{F R} \\
X_{M L} & Y_{M L} & Z_{M L} \\
X_{M R} & Y_{M R} & Z_{M R} \\
X_{R L} & Y_{R L} & Z_{R L} \\
X_{R R} & Y_{R R} & Z_{R R}
\end{array}\right]
$$

| Translation | Array Element | Translation Axis |
| :--- | :--- | :--- |
| Vehicle, $X_{v}$ | Translation(1,1) | Inertial vehicle Z-down $X$-axis |
| Vehicle, $Y_{v}$ | Translation(1,2) | Inertial vehicle Z-down $Y$-axis |
| Vehicle, $Z_{v}$ | Translation(1,3) | Inertial vehicle Z-down Z-axis |
| Front left wheel, $X_{F L}$ | Translation(2,1) | Vehicle Z-down $X$-axis |
| Front left wheel, $Y_{F L}$ | Translation(2,2) | Vehicle Z-down $Y$-axis |
| Front left wheel, $Z_{F L}$ | Translation(2,3) | Vehicle Z-down Z-axis |
| Front right wheel, $X_{F R}$ | Translation(3,1) | Vehicle Z-down $X$-axis |
| Front right wheel, $Y_{F R}$ | Translation(3,2) | Vehicle Z-down $Y$-axis |
| Front right wheel, $Z_{F R}$ | Translation(3,3) | Vehicle Z-down Z-axis |
| Middle left wheel, $X_{M L}$ <br> three-axle trailer) | Translation(4,1) | Vehicle Z-down $X$-axis |
| Middle left wheel, $Y_{M L}$ | Translation(4,2) | Vehicle Z-down $Y$-axis |
| Middle left wheel, $Z_{M L}$ | Translation(4,3) | Vehicle Z-down Z-axis |
| Middle right wheel, $X_{M R}$ | Translation(5,1) | Vehicle Z-down $X$-axis |
| Middle right wheel, $Y_{M R}$ | Translation(5,2) | Vehicle Z-down $Y$-axis |
| Middle right wheel, $Z_{M R}$ | Translation(5,3) | Vehicle Z-down Z-axis |
| Rear left wheel, $X_{R L}$ | Translation(6,1) | Vehicle Z-down $X$-axis |
| Rear left wheel, $Y_{R L}$ | Translation(6,2) | Vehicle Z-down $Y$-axis |
| Rear left wheel, $Z_{R L}$ | Translation(6,3) | Vehicle Z-down Z-axis |
| Rear right wheel, $X_{R R}$ | Translation(7,1) | Vehicle Z-down $X$-axis |
| Rear right wheel, $Y_{R R}$ | Translation(7,2) | Vehicle Z-down $Y$-axis |
| Rear right wheel, $Z_{R R}$ | Translation(7,3) | Vehicle Z-down Z-axis |

Rotation - Vehicle rotation
5-by-3 array (default) | 7-by-3 array | 3-by-3 array

Vehicle and wheel rotation, in rad. The array dimensions are 3-by-3 for a one-axle trailer, 5-by-3 for a two-axle trailer, and 7-by-3 for a three-axle trailer, where:

- Rotation(1,1), Rotation(1,2), and Rotation(1,3) - Vehicle rotation about the inertial vehicle Z-down $X$-, $Y$-, and $Z$-axes, respectively.
- Rotation(...,1), Rotation(...,2), and Rotation(...,3) - Wheel rotation relative to vehicle, about the vehicle Z-down $X$-, $Y$-, and $Z$-axes, respectively.

The signal contains rotation information according to the axle and wheel locations.
For a one-axle trailer:

$$
\text { Rotation }=\left[\begin{array}{lll}
\text { Roll }_{V} & \text { itch }_{v} & \text { Yaw }_{v} \\
\text { Roll }_{L} & \text { Pitch }_{L} & \text { Yaw }_{L} \\
\text { Roll }_{R} & \text { Pitch }_{R} & \text { Yaw }_{R}
\end{array}\right]
$$

| Rotation | Array Element | Rotation Axis |
| :--- | :--- | :--- |
| Vehicle, Roll $_{v}$ | Rotation $(1,1)$ | Inertial vehicle Z-down $X$-axis |
| Vehicle, Pitch $_{v}$ | Rotation(1,2) | Inertial vehicle Z-down Y-axis |
| Vehicle, Yaw $_{v}$ | Rotation(1,3) | Inertial vehicle Z-down Z-axis |
| Left wheel, Roll $_{L}$ | Rotation $(2,1)$ | Vehicle Z-down $X$-axis |
| Left wheel, Pitch $_{L}$ | Rotation $(2,2)$ | Vehicle Z-down $Y$-axis |
| Left wheel, Yaw $_{L}$ | Rotation(2,3) | Vehicle Z-down Z-axis |
| Right wheel, Roll $_{R}$ | Rotation(3,1) | Vehicle Z-down $X$-axis |
| Right wheel, Pitch $_{R}$ | Rotation(3,2) | Vehicle Z-down Y-axis |
| Right wheel, Yaw $_{R}$ | Rotation(3,3) | Vehicle Z-down Z-axis |

For a two-axle trailer:

$$
\text { Rotation }=\left[\begin{array}{ccc}
\text { Roll }_{v} & \text { Pitch }_{v} & \text { Yaw }_{v} \\
\text { Roll }_{F L} & \text { Pitch }_{F L} & \text { Yaw }_{F L} \\
\text { Roll }_{F R} & \text { Pitch }_{F R} & \text { Yaw }_{F R} \\
\text { Roll }_{R L} & \text { Pitch }_{R L} & \text { Yaw }_{R L} \\
\text { Roll }_{R R} & \text { Pitch }_{R R} & \text { Yaw }_{R R}
\end{array}\right]
$$

| Rotation | Array Element | Rotation Axis |
| :--- | :--- | :--- |
| Vehicle, Roll $_{v}$ | Rotation $(1,1)$ | Inertial vehicle Z-down $X$-axis |
| Vehicle, Pitch $_{v}$ | Rotation $(1,2)$ | Inertial vehicle Z-down $Y$-axis |
| Vehicle, Yaw $_{v}$ | Rotation $(1,3)$ | Inertial vehicle Z-down Z-axis |
| Front left wheel, Roll $_{F L}$ | Rotation $(2,1)$ | Vehicle Z-down $X$-axis |
| Front left wheel, Pitch $_{F L}$ | Rotation $(2,2)$ | Vehicle Z-down $Y$-axis |
| Front left wheel, Yaw $_{F L}$ | Rotation $(2,3)$ | Vehicle Z-down Z-axis |
| Front right wheel, Roll $_{F R}$ | Rotation $(3,1)$ | Vehicle Z-down $X$-axis |


| Rotation | Array Element | Rotation Axis |
| :---: | :---: | :---: |
| Front right wheel, Pitch $_{\text {FR }}$ | Rotation(3,2) | Vehicle Z-down Y-axis |
| Front right wheel, Yaw $_{\text {FR }}$ | Rotation(3,3) | Vehicle Z-down Z -axis |
| Rear left wheel, Roll $_{\text {RL }}$ | Rotation(4,1) | Vehicle Z-down $X$-axis |
| Rear left wheel, Pitch $_{\text {RL }}$ | Rotation(4,2) | Vehicle Z-down Y-axis |
| Rear left wheel, Yaw ${ }_{\text {RL }}$ | Rotation(4,3) | Vehicle Z-down Z-axis |
| Rear right wheel, Roll $_{R R}$ | Rotation(5,1) | Vehicle Z-down $X$-axis |
| Rear right wheel, Pitch $_{\text {RR }}$ | Rotation(5,2) | Vehicle Z-down Y-axis |
| Rear right wheel, Yaw $_{\text {RR }}$ | Rotation(5,3) | Vehicle Z-down Z-axis |

For a three-axle trailer:

$$
\text { Rotation }=\left[\begin{array}{ccc}
\text { Roll }_{v} & \text { Pitch }_{v} & \text { Yaw }_{v} \\
\text { Roll }_{F L} & \text { Pitch }_{F L} & \text { Yaw }_{F L} \\
\text { Roll }_{F R} & \text { Pitch }_{F R} & \text { Yaw }_{F R} \\
\text { Roll }_{M L} & \text { Pitch }_{M L} & \text { Yaw }_{M L} \\
\text { Roll }_{M R} & \text { Pitch }_{M R} & \text { Yaw }_{M R} \\
\text { Roll }_{R L} & \text { Pitch }_{R L} & \text { Yaw }_{R L} \\
\text { Roll }_{R R} & \text { Pitch }_{R R} & \text { Yaw }_{R R}
\end{array}\right]
$$

| Rotation | Array Element | Rotation Axis |
| :---: | :---: | :---: |
| Vehicle, Rollv | Rotation(1,1) | Inertial vehicle Z -down $X$-axis |
| Vehicle, Pitch ${ }_{v}$ | Rotation(1,2) | Inertial vehicle Z -down $Y$-axis |
| Vehicle, Yaw ${ }_{v}$ | Rotation(1,3) | Inertial vehicle Z -down Z -axis |
| Front left wheel, Roll $_{F L}$ | Rotation(2,1) | Vehicle Z-down $X$-axis |
| Front left wheel, Pitch $_{F L}$ | Rotation(2,2) | Vehicle Z-down $Y$-axis |
| Front left wheel, Yaw $_{\text {FL }}$ | Rotation(2,3) | Vehicle Z-down $Z$-axis |
| Front right wheel, Roll $_{\text {FR }}$ | Rotation (3,1) | Vehicle Z-down $X$-axis |
| Front right wheel, Pitch $_{\text {FR }}$ | Rotation(3,2) | Vehicle Z-down $Y$-axis |
| Front right wheel, Yaw $_{\text {FR }}$ | Rotation(3,3) | Vehicle Z-down Z -axis |
| Middle left wheel, Roll $_{\text {ML }}$ | Rotation(4,1) | Vehicle Z-down $X$-axis |
| Middle left wheel, Pitch $_{\text {ML }}$ | Rotation(4,2) | Vehicle Z-down $Y$-axis |
| Middle left wheel, Yaw $_{\text {ML }}$ | Rotation(4,3) | Vehicle Z-down $Z$-axis |
| Middle right wheel, Roll $_{\text {MR }}$ | Rotation (5,1) | Vehicle Z-down $X$-axis |
| Middle right wheel, Pitch $_{\text {MR }}$ | Rotation (5,2) | Vehicle Z-down $Y$-axis |
| Middle right wheel, Yaw ${ }_{\text {MR }}$ | Rotation(5,3) | Vehicle Z-down Z-axis |
| Rear left wheel, Roll $_{R L}$ | Rotation(6,1) | Vehicle Z-down $X$-axis |
| Rear left wheel, Pitch $_{\text {RL }}$ | Rotation(6,2) | Vehicle Z-down $Y$-axis |
| Rear left wheel, Yaw ${ }_{\text {RL }}$ | Rotation(6,3) | Vehicle Z-down Z-axis |


| Rotation | Array Element | Rotation Axis |
| :--- | :--- | :--- |
| Rear right wheel, Roll $_{R R}$ | Rotation $(7,1)$ | Vehicle Z-down $X$-axis |
| Rear right wheel, Pitch $_{R R}$ | Rotation $(7,2)$ | Vehicle Z-down Y-axis |
| Rear right wheel, Yaw $_{R R}$ | Rotation $(7,3)$ | Vehicle Z-down Z-axis |

## Parameters

## Vehicle Parameters

Type - Trailer type
Two-axle trailer (default)|Three-axle trailer|One-axle trailer
Trailer type. For the trailer dimensions, see:

- One-Axle Trailer
- Two-Axle Trailer
- Three-Axle Trailer

Name - Name of vehicle
SimulinkVehicle1 (default) | character vector
Name of vehicle. By default, when you use the block in your model, the block sets the Name parameter to SimulinkVehicle $X$. The value of $X$ depends on the number of Simulation 3D Vehicle with Ground Following and Simulation 3D Vehicle blocks that you have in your model.

## Initial Values

Initial array values to translate vehicle per part, Translation - Vehicle initial translation zeros( 5, 3 ) (default) | zeros( 7, 3 ) | zeros( 3, 3 )

Initial vehicle and wheel translation, in $m$. The array dimensions are 3-by-3 for a one-axle trailer, 5-by-3 for a two-axle trailer and 7-by-3 for a three-axle trailer, where:

- Translation(1,1), Translation(1,2), and Translation(1,3) - Initial vehicle translation along the inertial vehicle Z-down coordinate system $X-, Y$-, and $Z$-axes, respectively.
- Translation(...,1), Translation(...,2), and Translation(...,3) - Initial wheel translation relative to vehicle, along the vehicle Z-down $X$-, $Y$-, and $Z$-axes, respectively.

The signal contains translation information according to the axle and wheel locations.
For a one-axle trailer:

$$
\text { Translation }=\left[\begin{array}{lll}
X_{v} & Y_{v} & Z_{v} \\
X_{L} & Y_{L} & Z_{L} \\
X_{R} & Y_{R} & Z_{R}
\end{array}\right]
$$

| Translation | Array Element | Translation Axis |
| :--- | :--- | :--- |
| Vehicle, $X_{v}$ | Translation(1,1) | Inertial vehicle Z-down $X$-axis |
| Vehicle, $Y_{v}$ | Translation(1,2) | Inertial vehicle Z-down $Y$-axis |


| Translation | Array Element | Translation Axis |
| :--- | :--- | :--- |
| Vehicle, $Z_{v}$ | Translation $(1,3)$ | Inertial vehicle Z-down Z-axis |
| Left wheel, $X_{L}$ | Translation $(2,1)$ | Vehicle Z-down $X$-axis |
| Left wheel, $Y_{L}$ | Translation $(2,2)$ | Vehicle Z-down $Y$-axis |
| Left wheel, $Z_{L}$ | Translation $(2,3)$ | Vehicle Z-down Z-axis |
| Right wheel, $X_{R}$ | Translation $(3,1)$ | Vehicle Z-down $X$-axis |
| Right wheel, $Y_{R}$ | Translation(3, 2) | Vehicle Z-down $Y$-axis |
| Right wheel, $Z_{R}$ | Translation(3,3) | Vehicle Z-down Z-axis |

For a two-axle trailer:

$$
\text { Translation }=\left[\begin{array}{ccc}
X_{v} & Y_{v} & Z_{v} \\
X_{F L} & Y_{F L} & Z_{F L} \\
X_{F R} & Y_{F R} & Z_{F R} \\
X_{R L} & Y_{R L} & Z_{R L} \\
X_{R R} & Y_{R R} & Z_{R R}
\end{array}\right]
$$

| Translation | Array Element | Translation Axis |
| :---: | :---: | :---: |
| Vehicle, $X_{v}$ | Translation(1,1) | Inertial vehicle Z-down $X$-axis |
| Vehicle, $Y_{v}$ | Translation(1,2) | Inertial vehicle Z-down Y-axis |
| Vehicle, $Z_{v}$ | Translation(1,3) | Inertial vehicle Z-down $Z$-axis |
| Front left wheel, $X_{F L}$ | Translation(2,1) | Vehicle Z-down $X$-axis |
| Front left wheel, $Y_{\text {FL }}$ | Translation(2,2) | Vehicle Z-down Y-axis |
| Front left wheel, $Z_{F L}$ | Translation(2,3) | Vehicle Z-down Z-axis |
| Front right wheel, $X_{F R}$ | Translation(3,1) | Vehicle Z-down $X$-axis |
| Front right wheel, $Y_{F R}$ | Translation(3,2) | Vehicle Z-down $Y$-axis |
| Front right wheel, $Z_{F R}$ | Translation(3,3) | Vehicle Z-down Z-axis |
| Rear left wheel, $X_{R L}$ | Translation(4,1) | Vehicle Z-down $X$-axis |
| Rear left wheel, $Y_{R L}$ | Translation(4,2) | Vehicle Z-down Y-axis |
| Rear left wheel, $Z_{R L}$ | Translation(4,3) | Vehicle Z-down Z-axis |
| Rear right wheel, $X_{R R}$ | Translation(5,1) | Vehicle Z-down $X$-axis |
| Rear right wheel, $Y_{R R}$ | Translation(5,2) | Vehicle Z-down Y-axis |
| Rear right wheel, $Z_{R R}$ | Translation(5,3) | Vehicle Z-down Z-axis |

For a three-axle trailer:

$$
\text { Translation }=\left[\begin{array}{ccc}
X_{v} & Y_{v} & Z_{v} \\
X_{F L} & Y_{F L} & Z_{F L} \\
X_{F R} & Y_{F R} & Z_{F R} \\
X_{M L} & Y_{M L} & Z_{M L} \\
X_{M R} & Y_{M R} & Z_{M R} \\
X_{R L} & Y_{R L} & Z_{R L} \\
X_{R R} & Y_{R R} & Z_{R R}
\end{array}\right]
$$

| Translation | Array Element | Translation Axis |
| :---: | :---: | :---: |
| Vehicle, $X_{v}$ | Translation(1,1) | Inertial vehicle Z-down $X$-axis |
| Vehicle, $Y_{v}$ | Translation(1,2) | Inertial vehicle Z-down $Y$-axis |
| Vehicle, $Z_{v}$ | Translation(1,3) | Inertial vehicle Z-down $Z$-axis |
| Front left wheel, $X_{F L}$ | Translation(2,1) | Vehicle Z-down $X$-axis |
| Front left wheel, $Y_{F L}$ | Translation(2,2) | Vehicle Z-down Y-axis |
| Front left wheel, $Z_{F L}$ | Translation(2,3) | Vehicle Z-down Z-axis |
| Front right wheel, $X_{F R}$ | Translation(3,1) | Vehicle Z-down X-axis |
| Front right wheel, $Y_{F R}$ | Translation (3,2) | Vehicle Z-down Y-axis |
| Front right wheel, $Z_{F R}$ | Translation(3,3) | Vehicle Z-down Z-axis |
| Middle left wheel, $X_{M L}$ (for three-axle trailer) | Translation(4,1) | Vehicle Z-down $X$-axis |
| Middle left wheel, $Y_{M L}$ | Translation(4,2) | Vehicle Z-down Y-axis |
| Middle left wheel, $Z_{M L}$ | Translation (4,3) | Vehicle Z-down Z-axis |
| Middle right wheel, $X_{M R}$ | Translation(5,1) | Vehicle Z-down $X$-axis |
| Middle right wheel, $Y_{M R}$ | Translation(5,2) | Vehicle Z-down Y-axis |
| Middle right wheel, $Z_{M R}$ | Translation(5,3) | Vehicle Z-down Z-axis |
| Rear left wheel, $X_{R L}$ | Translation(6,1) | Vehicle Z-down $X$-axis |
| Rear left wheel, $Y_{R L}$ | Translation(6,2) | Vehicle Z-down Y-axis |
| Rear left wheel, $Z_{\text {RL }}$ | Translation(6,3) | Vehicle Z-down Z-axis |
| Rear right wheel, $X_{R R}$ | Translation(7,1) | Vehicle Z-down $X$-axis |
| Rear right wheel, $Y_{R R}$ | Translation(7,2) | Vehicle Z-down Y-axis |
| Rear right wheel, $Z_{R R}$ | Translation(7,3) | Vehicle Z-down Z-axis |

Initial array values to rotate vehicle per part, Rotation - Vehicle initial rotation zeros( 5, 3 ) (default) | zeros( 7, 3 ) | zeros( 3, 3 )

Initial vehicle and wheel rotation, about the vehicle Z-down $X$-, $Y$-, and $Z$-axes, in rad.
The array dimensions are 5-by-3 for a two-axle trailer and 7-by-3 for a three-axle trailer, where:

- Rotation(1,1), Rotation(1,2), and Rotation(1,3) - Initial vehicle rotation about the inertial vehicle Z-down coordinate system $X$-, $Y$-, and $Z$-axes, respectively.
- Rotation(...,1), Rotation(...,2), and Rotation(...,3) - Initial wheel rotation relative to the vehicle, about the vehicle Z-down $X$-, $Y$-, and $Z$-axes, respectively.

The signal contains translation information according to the axle and wheel locations.
For a one-axle trailer:

$$
\text { Rotation }=\left[\begin{array}{lll}
\text { Roll }_{v} & \text { Pitch }_{v} & \text { Yaw }_{v} \\
\text { Roll }_{L} & \text { Pitch }_{L} & \text { Yaw }_{L} \\
\text { Roll }_{R} & \text { itch }_{R} & \text { Yaw }_{R}
\end{array}\right]
$$

| Rotation | Array Element | Rotation Axis |
| :--- | :--- | :--- |
| Vehicle, Roll $_{v}$ | Rotation $(1,1)$ | Inertial vehicle Z-down $X$-axis |
| Vehicle, Pitch $_{v}$ | Rotation(1,2) | Inertial vehicle Z-down Y-axis |
| Vehicle, Yaw $_{v}$ | Rotation(1,3) | Inertial vehicle Z-down Z-axis |
| Left wheel, Roll $_{L}$ | Rotation $(2,1)$ | Vehicle Z-down $X$-axis |
| Left wheel, Pitch $_{L}$ | Rotation $(2,2)$ | Vehicle Z-down $Y$-axis |
| Left wheel, Yaw $_{L}$ | Rotation $(2,3)$ | Vehicle Z-down Z-axis |
| Right wheel, Roll $_{R}$ | Rotation(3,1) | Vehicle Z-down $X$-axis |
| Right wheel, Pitch $_{R}$ | Rotation(3,2) | Vehicle Z-down Y-axis |
| Right wheel, Yaw $_{R}$ | Rotation(3,3) | Vehicle Z-down Z-axis |

For a two-axle trailer:

$$
\text { Rotation }=\left[\begin{array}{ccc}
\text { Roll }_{v} & \text { Pitch }_{v} & \text { Yaw }_{v} \\
\text { Roll }_{F L} & \text { Pitch }_{F L} & \text { Yaw }_{F L} \\
\text { Roll }_{F R} & \text { Pitch }_{F R} & \text { Yaw }_{F R} \\
\text { Roll }_{R L} & \text { Pitch }_{R L} & \text { Yaw }_{R L} \\
\text { Roll }_{R R} & \text { Pitch }_{R R} & \text { Yaw }_{R R}
\end{array}\right]
$$

| Rotation | Array Element | Rotation Axis |
| :---: | :---: | :---: |
| Vehicle, Roll ${ }_{v}$ | Rotation(1,1) | Inertial vehicle Z-down $X$-axis |
| Vehicle, Pitch ${ }_{v}$ | Rotation(1,2) | Inertial vehicle Z-down $Y$-axis |
| Vehicle, Yaw ${ }_{v}$ | Rotation(1,3) | Inertial vehicle Z-down $Z$-axis |
| Front left wheel, Roll $_{F L}$ | Rotation(2,1) | Vehicle Z-down $X$-axis |
| Front left wheel, Pitch $_{F L}$ | Rotation(2,2) | Vehicle Z-down Y-axis |
| Front left wheel, Yaw FL $^{\text {d }}$ | Rotation(2,3) | Vehicle Z-down Z -axis |
| Front right wheel, Roll $_{F R}$ | Rotation(3,1) | Vehicle Z-down $X$-axis |
| Front right wheel, Pitch $_{\text {FR }}$ | Rotation(3,2) | Vehicle Z-down Y-axis |
| Front right wheel, Yaw $_{\text {FR }}$ | Rotation(3,3) | Vehicle Z-down Z -axis |
| Rear left wheel, Roll $_{R L}$ | Rotation(4,1) | Vehicle Z-down $X$-axis |
| Rear left wheel, Pitch $_{\text {RL }}$ | Rotation(4,2) | Vehicle Z-down Y-axis |


| Rotation | Array Element | Rotation Axis |
| :--- | :--- | :--- |
| Rear left wheel, Yaw $_{R L}$ | Rotation $(4,3)$ | Vehicle Z-down Z-axis |
| Rear right wheel, Roll $_{R R}$ | Rotation $(5,1)$ | Vehicle Z-down $X$-axis |
| Rear right wheel, Pitch $_{R R}$ | Rotation (5,2) | Vehicle Z-down Y-axis |
| Rear right wheel, Yaw $_{R R}$ | Rotation (5, 3) | Vehicle Z-down Z-axis |

For a three-axle trailer:

$$
\text { Rotation }=\left[\begin{array}{ccc}
\text { Roll }_{v} & \text { Pitch }_{v} & \text { Yaw }_{v} \\
\text { Roll }_{F L} & \text { Pitch }_{F L} & \text { Yaw }_{F L} \\
\text { Roll }_{F R} & \text { Pitch }_{F R} & \text { Yaw }_{F R} \\
\text { Roll }_{M L} & \text { Pitch }_{M L} & \text { Yaw }_{M L} \\
\text { Roll }_{M R} & \text { Pitch }_{M R} & \text { Yaw }_{M R} \\
\text { Roll }_{R L} & \text { Pitch }_{R L} & \text { Yaw }_{R L} \\
\text { Roll }_{R R} & \text { Pitch }_{R R} & \text { Yaww }_{R R}
\end{array}\right]
$$

| Rotation | Array Element | Rotation Axis |
| :---: | :---: | :---: |
| Vehicle, Roll ${ }_{v}$ | Rotation(1,1) | Inertial vehicle Z-down $X$-axis |
| Vehicle, Pitch ${ }_{v}$ | Rotation(1,2) | Inertial vehicle Z-down $Y$-axis |
| Vehicle, Yaw ${ }_{v}$ | Rotation(1,3) | Inertial vehicle Z-down Z-axis |
| Front left wheel, Roll $_{F L}$ | Rotation(2,1) | Vehicle Z-down $X$-axis |
| Front left wheel, Pitch $_{\text {FL }}$ | Rotation(2,2) | Vehicle Z-down Y-axis |
| Front left wheel, Yaw ${ }_{\text {FL }}$ | Rotation(2,3) | Vehicle Z-down Z-axis |
| Front right wheel, Roll $_{F R}$ | Rotation (3,1) | Vehicle Z-down $X$-axis |
| Front right wheel, Pitch ${ }_{F R}$ | Rotation(3,2) | Vehicle Z-down Y-axis |
| Front right wheel, Yaw $_{\text {FR }}$ | Rotation(3,3) | Vehicle Z-down Z-axis |
| Middle left wheel, Roll $_{\text {ML }}$ | Rotation(4,1) | Vehicle Z-down $X$-axis |
| Middle left wheel, Pitch $_{\text {ML }}$ | Rotation (4, 2) | Vehicle Z-down Y-axis |
| Middle left wheel, Yaw $_{\text {ML }}$ | Rotation(4,3) | Vehicle Z-down Z-axis |
| Middle right wheel, Roll $_{\text {MR }}$ | Rotation(5,1) | Vehicle Z-down $X$-axis |
| Middle right wheel, Pitch ${ }_{M R}$ | Rotation(5,2) | Vehicle Z-down Y-axis |
| Middle right wheel, Yaw $_{\text {MR }}$ | Rotation(5,3) | Vehicle Z-down Z-axis |
| Rear left wheel, Roll $_{R L}$ | Rotation(6,1) | Vehicle Z-down $X$-axis |
| Rear left wheel, Pitch $_{\text {RL }}$ | Rotation (6,2) | Vehicle Z-down $Y$-axis |
| Rear left wheel, $Y^{\prime} w_{\text {RL }}$ | Rotation(6,3) | Vehicle Z-down Z-axis |
| Rear right wheel, Roll $_{R R}$ | Rotation(7,1) | Vehicle Z-down $X$-axis |
| Rear right wheel, Pitch ${ }_{R R}$ | Rotation(7,2) | Vehicle Z-down $Y$-axis |
| Rear right wheel, Yaw $_{R R}$ | Rotation(7,3) | Vehicle Z-down Z-axis |

Sample time - Sample time

- 1 (default) | scalar

Sample time, $T_{s}$. The graphics frame rate is the inverse of the sample time.

## Version History

Introduced in R2020b

## References

[1] Vehicle Dynamics Standards Committee. Vehicle Dynamics Terminology. SAE J670. Warrendale, PA: Society of Automotive Engineers, 2008.
[2] Technical Committee. Road vehicles - Vehicle dynamics and road-holding ability - Vocabulary. ISO 8855:2011. Geneva, Switzerland: International Organization for Standardization, 2011.

## See Also

Vehicle Body 3DOF Three Axles | Simulation 3D Tractor | Trailer Body 3DOF | Trailer Body 6DOF

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"
"How 3D Simulation for Vehicle Dynamics Blockset Works"

## Simulation 3D Motorcycle

Implement motorcycle in 3D environment


## Libraries:

Vehicle Dynamics Blockset / Vehicle Scenarios / Sim3D / Sim3D Vehicle / Components

## Description

The Simulation 3D Motorcycle block implements a motorcycle with two wheels in the 3D simulation environment.

To use this block, ensure that the Simulation 3D Scene Configuration block is in your model. If you set the Sample time parameter of this block to -1, the block uses the sample time specified in the Simulation 3D Scene Configuration block.

The block input uses the vehicle Z-down right-handed (RH) Cartesian coordinate system defined in SAE J670 ${ }^{1}$. The coordinate system is inertial and initially aligned with the vehicle geometric center:

- $X$-axis - Along vehicle longitudinal axis, points forward
- $Y$-axis - Along vehicle lateral axis, points to the right
- Z-axis - Points downward

Tip Verify that the Simulation 3D Motorcycle block executes before the Simulation 3D Scene Configuration block. That way, Simulation 3D Motorcycle prepares the signal data before the Unreal Engine 3D visualization environment receives it. To check the block execution order, right-click each block and select Properties. On the General tab, confirm these Priority settings:

- Simulation 3D Scene Configuration - 0
- Simulation 3D Motorcycle - - 1

For more information about execution order, see "Control and Display Execution Order".

## Ports

Input
Translation - Motorcycle translation
5-by-3 array
Motorcycle and component translation, in m. Array dimensions are 5-by-3.

- Translation(1,1), Translation(1,2), and Translation(1,3) - Motorcycle translation along the inertial vehicle $Z$-down $X$-, $Y$-, and $Z$ - axes, respectively.
- Translation(...,1), Translation(...,2), and Translation(..., 3) - Motorcycle component translation relative to vehicle, along the vehicle Z-down $X$-, $Y$-, and $Z$ - axes, respectively.

The signal contains translation information according to the locations.

$$
\text { Translation }=\left[\begin{array}{ccc}
X_{v} & Y_{v} & Z_{v} \\
X_{H} & Y_{H} & Z_{H} \\
X_{S A} & Y_{S A} & Z_{S A} \\
X_{F} & Y_{F} & Z_{F} \\
X_{R} & Y_{R} & Z_{R}
\end{array}\right]
$$

| Translation | Array Element | Translation Axis |
| :--- | :--- | :--- |
| Motorcycle, $X_{v}$ | Translation(1,1) | Inertial vehicle Z-down $X$-axis |
| Motorcycle, $Y_{v}$ | Translation(1,2) | Inertial vehicle Z-down $Y$-axis |
| Motorcycle, $Z_{v}$ | Translation(1,3) | Inertial vehicle Z-down Z-axis |
| Handlebars, $X_{H}$ | Translation(2,1) | Vehicle Z-down $X$-axis |
| Handlebars, $Y_{H}$ | Translation(2,2) | Vehicle Z-down $Y$-axis |
| Handlebars, $Z_{H}$ | Translation(2,3) | Vehicle Z-down Z-axis |
| Swing arm, $X_{S A}$ | Translation(3,1) | Vehicle Z-down $X$-axis |
| Swing arm, $Y_{S A}$ | Translation(3,2) | Vehicle Z-down $Y$-axis |
| Swing arm, $Z_{S A}$ | Translation(3,3) | Vehicle Z-down Z-axis |
| Front wheel, $X_{F}$ | Translation(4,1) | Vehicle Z-down $X$-axis |
| Front wheel, $Y_{F}$ | Translation(4,2) | Vehicle Z-down $Y$-axis |
| Front wheel, $Z_{F}$ | Translation(4,3) | Vehicle Z-down Z-axis |
| Rear wheel, $X_{R}$ | Translation(5,1) | Vehicle Z-down $X$-axis |
| Rear wheel, $Y_{R}$ | Translation(5,2) | Vehicle Z-down $Y$-axis |
| Rear wheel, $Z_{R}$ | Translation(5,3) | Vehicle Z-down Z-axis |

Rotation - Motorcycle rotation
5-by-3 array
Vehicle and component rotation, in rad. Array dimensions are 5-by-3.

- Rotation(1,1), Rotation(1,2), and Rotation(1,3) - Motorcycle rotation about the inertial vehicle Z-down $X-, Y$-, and $Z$ - axes, respectively.
- Rotation(...,1), Rotation(...,2), and Rotation(...,3) - Motorcycle component rotation relative to vehicle, about the vehicle Z-down $X$-, $Y$-, and Z- axes, respectively.

The signal contains rotation information according to the locations.

$$
\text { Rotation }=\left[\begin{array}{ccc}
\text { Roll }_{\nu} & \text { Pitch }_{V} & \text { Yaw }_{\nu} \\
\text { Roll }_{H} & \text { Pitch }_{H} & \text { Yaw }_{H} \\
\text { Roll }_{S A} & \text { Pitch }_{S A} & \text { Yaw }_{S A} \\
\text { Roll }_{F} & \text { Pitch }_{F} & \text { Yaw }_{F} \\
\text { Roll }_{R} & \text { Pitch }_{R} & \text { Yaw }_{R}
\end{array}\right]
$$

| Rotation | Array Element | Rotation Axis |
| :---: | :---: | :---: |
| Vehicle, Roll ${ }_{v}$ | Rotation(1,1) | Inertial vehicle Z-down $X$-axis |
| Vehicle, Pitch ${ }_{\text {v }}$ | Rotation(1,2) | Inertial vehicle Z-down $Y$-axis |
| Vehicle, Yaw ${ }_{v}$ | Rotation(1,3) | Inertial vehicle Z-down $Z$-axis |
| Handlebar, Roll $_{H}$ | Rotation(2,1) | Vehicle Z-down $X$-axis |
| Handlebar, Pitch $_{H}$ | Rotation(2,2) | Vehicle Z-down $Y$-axis |
| Handlebar, Yaw $_{H}$ | Rotation(2,3) | Vehicle Z-down Z-axis |
| Swing arm, Roll $_{\text {SA }}$ | Rotation(3,1) | Vehicle Z-down $X$-axis |
| Swing arm, Pitch ${ }_{\text {SA }}$ | Rotation(3,2) | Vehicle Z-down Y-axis |
| Swing arm, Yaw ${ }_{\text {SA }}$ | Rotation(3,3) | Vehicle Z-down Z-axis |
| Front wheel, Roll $_{F}$ | Rotation(4,1) | Vehicle Z-down $X$-axis |
| Front wheel, Pitch $_{F}$ | Rotation(4,2) | Vehicle Z-down $Y$-axis |
| Front wheel, Yaw $_{F}$ | Rotation(4,3) | Vehicle Z-down Z-axis |
| Rear wheel, Roll $_{R}$ | Rotation(5,1) | Vehicle Z-down $X$-axis |
| Rear wheel, Pitch $_{R}$ | Rotation(5,2) | Vehicle Z-down Y-axis |
| Rear wheel, Yaw $_{R}$ | Rotation(5,3) | Vehicle Z-down Z -axis |

Light controls - Vehicle lights on or off
1 -by- 5 vector
Light controls input signal, specified as a 1-by-5 Boolean vector. Each element of the vector turns a specific vehicle light on or off, as indicated in this table. A value of 1 turns the light on; a value of 0 turns the light off

| Vector Element | Vehicle Light |
| :--- | :--- |
| $(1,1)$ | Headlight high beam |
| $(1,2)$ | Headlight low beam |
| $(1,3)$ | Brake |
| $(1,4)$ | Left signal |
| $(1,5)$ | Right signal |

## Dependencies

To create this port, on the Light Controls tab, select Enable light controls.
Data Types: Boolean

## Parameters

## Vehicle Parameters

Type - Type
Sports bike (default)|Motor bike|Scooter
Use the Type parameter to specify the motorcycle type. This table provides links to the motorcycle dimensions.

| Vehicle Type Setting | Vehicle Dimensions |
| :--- | :--- |
| Sports bike | Sports Bike |
| Motor bike | Motor Bike |
| Scooter | Scooter |

Color - Color of vehicle
Red (default) | Orange | Yellow|Green | Blue | Black | White | Silver
Select the color of the vehicle.
Name - Name of motorcycle
SimulinkVehicle1 (default)| character vector
Name of motorcycle. By default, when you use the block in your model, the block sets the Name parameter to SimulinkVehicle $X$. The value of $X$ depends on the number of 3D simulation blocks that you have in your model.

Sample time - Sample time

- 1 (default) | scalar

Sample time, $T_{s}$. The graphics frame rate is the inverse of the sample time.

## Light Controls

Enable light controls, VehLightsControl - Control vehicle lights
off (default) | on
Select whether to control the vehicle headlights. Use the enabled parameters to set the light parameters, including headlight intensity.

## Dependencies

Selecting this parameter:

- Creates the input port Light controls
- Enables these light parameters.

| Lights | Light Parameters |
| :--- | :--- |
| Headlights | - |
|  | - |
|  | - High beadlight color intensity |
|  | - Low beam intensity |
|  | - High beam cone half angle |
|  | - Low beam cone half angle |
|  | - Left headlight beam orientation |
|  | Brake light intensity |
| Brake lights |  |


| Lights | Light Parameters |
| :--- | :--- |
| Turn signal lights | $\bullet$ |
|  | $\bullet$ |
|  | $\bullet$ |
|  | Purn signal light intensity |
|  | Pulse width |

## Headlights

Headlight color [R,G,B], HeadlightColor - Headlight color
[1, 1, 1] (default) | 1-by-3 vector of RGB triplet values
Headlight color, specified as a normalized 1-by-3 vector of RGB triplet values.

## Dependencies

To enable this parameter, select Enable light controls.
Data Types: int8|uint8
High beam intensity, HighBeamIntensity - High beam intensity
100000 (default) | positive scalar
High beam intensity, in cd.

## Dependencies

To enable this parameter, select Enable light controls.
Data Types: double
Low beam intensity, LowBeamIntensity - Low beam intensity
60000 (default) | positive scalar
Low beam intensity, in cd.

## Dependencies

To enable this parameter, select Enable light controls.
Data Types: double
High beam cone half angle, HighBeamConeAngle - High beam cone half angle
1.22 (default) | positive scalar less than pi/2

High beam cone half angle, in rad.

## Dependencies

To enable this parameter, select Enable light controls.
Data Types: double
Low beam cone half angle, LowBeamConeAngle - Low beam cone half angle
1.22 (default) | positive scalar less than pi/2

Low beam cone half angle, in rad.

## Dependencies

To enable this parameter, select Enable light controls.

Data Types: double
Left headlight beam orientation [Pitch, Yaw], LeftHeadlightOrientation - Left headlight beam orientation
[0,0] (default) | 1-by-2 vector greater with values between -pi and pi
Pitch and yaw orientation of the left headlight beam orientation in the Z-down coordinate system, specified as a 1 -by- 2 vector, in rad. The first element of the vector, [1,1], is the pitch angle. The second element of the vector, [1,2] is the yaw angle.

## Dependencies

To enable this parameter, select Enable light controls.

## Data Types: double

Right headlight beam orientation [Pitch, Yaw], RightHeadlightOrientation - Right headlight beam orientation
$[0,0]$ (default) | 1-by-2 vector greater with values between -pi and pi
Pitch and yaw orientation of the right headlight beam orientation in the Z-down coordinate system, specified as a 1 -by- 2 vector, in rad. The first element of the vector, [1,1], is the pitch angle. The second element of the vector, [1,2] is the yaw angle.

## Dependencies

To enable this parameter, select Enable light controls.

## Brake Lights

Brake light intensity, BrakelightIntensity - Intensity
500 (default) | positive scalar
Brake light intensity, in $\mathrm{cd} / \mathrm{m}^{\wedge} 2$.

## Dependencies

To enable this parameter, select Enable light controls.
Data Types: double

## Turn Signal Lights

Turn signal light intensity, SignallightIntensity - Intensity
500 (default) | positive scalar
Turn signal light intensity, in $\mathrm{cd} / \mathrm{m}^{\wedge} 2$.

## Dependencies

To enable this parameter, select Enable light controls.

## Data Types: double

Period, SignallightPeriod - Turn signal light period 1 (default) | positive scalar

Turn signal light period, in s.

## Dependencies

To enable this parameter, select Enable light controls.
Data Types: double
Pulse width, SignalPulseWidth - Pulse width
50 (default) | positive scalar less than 100
Turn signal light pulse width, as a percent of the period.

## Dependencies

To enable this parameter, select Enable light controls.
Data Types: double

## Initial Values

Initial array values to translate vehicle per part, Translation - Motorcycle initial translation zeros( 3, 3 ) (default) | 3-by-3 array

Initial motorcycle and component translation, in m. Array dimensions are 5-by-3.

- Translation(1,1), Translation(1,2), and Translation(1,3) - Initial vehicle translation along the inertial vehicle Z-down coordinate system $X-, Y$-, and $Z$ - axes, respectively.
- Translation(...,1), Translation(...,2), and Translation(...,3) - Initial motorcycle component translation relative to vehicle, along the vehicle Z-down $X$-, $Y$-, and $Z$ - axes, respectively.

The parameter contains translation information according to the locations.

$$
\text { Translation }=\left[\begin{array}{ccc}
X_{v} & Y_{v} & Z_{V} \\
X_{H} & Y_{H} & Z_{H} \\
X_{S A} & Y_{S A} & Z_{S A} \\
X_{F} & Y_{F} & Z_{F} \\
X_{R} & Y_{R} & Z_{R}
\end{array}\right]
$$

| Translation | Array Element | Translation Axis |
| :--- | :--- | :--- |
| Motorcycle, $X_{v}$ | Translation $(1,1)$ | Inertial vehicle Z-down $X$-axis |
| Motorcycle, $Y_{v}$ | Translation(1, 2) | Inertial vehicle Z-down $Y$-axis |
| Motorcycle, $Z_{v}$ | Translation $(1,3)$ | Inertial vehicle Z-down Z-axis |
| Handlebars, $X_{H}$ | Translation $(2,1)$ | Vehicle Z-down $X$-axis |
| Handlebars, $Y_{H}$ | Translation $(2,2)$ | Vehicle Z-down $Y$-axis |
| Handlebars, $Z_{H}$ | Translation $(2,3)$ | Vehicle Z-down Z-axis |
| Swing arm, $X_{S A}$ | Translation $(3,1)$ | Vehicle Z-down $X$-axis |
| Swing arm, $Y_{S A}$ | Translation 3,2$)$ | Vehicle Z-down $Y$-axis |
| Swing arm, $Z_{S A}$ | Translation 3,3$)$ | Vehicle Z-down Z-axis |
| Front wheel, $X_{F}$ | Translation 4,1$)$ | Vehicle Z-down $X$-axis |


| Translation | Array Element | Translation Axis |
| :--- | :--- | :--- |
| Front wheel, $Y_{F}$ | Translation(4,2) | Vehicle Z-down $Y$-axis |
| Front wheel, $Z_{F}$ | Translation(4,3) | Vehicle Z-down $Z$-axis |
| Rear wheel, $X_{R}$ | Translation(5,1) | Vehicle Z-down $X$-axis |
| Rear wheel, $Y_{R}$ | Translation(5,2) | Vehicle Z-down $Y$-axis |
| Rear wheel, $Z_{R}$ | Translation(5,3) | Vehicle Z-down Z-axis |

Initial array values to rotate vehicle per part, Rotation - Motorcycle initial rotation zeros( 5, 3 ) (default) | 5-by-3 array

Initial motorcycle and component rotation, about the vehicle Z-down $X$-, $Y$-, and $Z$ - axes.
Array dimensions are 5-by-3.

- Rotation(1, 1), Rotation(1,2), and Rotation(1,3) - Initial motorcycle rotation about the inertial vehicle Z-down coordinate system $X$-, $Y$-, and $Z$ - axes, respectively.
- Rotation(...,1), Rotation(...,2), and Rotation(...,3) - Initial motorcycle component rotation relative to vehicle, about the vehicle Z-down $X$-, $Y$-, and $Z$ - axes, respectively.

The parameter contains rotation information according to the location.

$$
\text { Rotation }=\left[\begin{array}{ccc}
\text { Roll }_{v} & \text { Pitch }_{v} & \text { Yaw }_{v} \\
\text { Roll }_{F L} & \text { Pitch }_{F L} & \text { Yaw }_{F L} \\
\text { Roll }_{F R} & \text { Pitch }_{F R} & \text { Yaw }_{F R} \\
\text { Roll }_{R L} & \text { Pitch }_{R L} & \text { Yaw }_{R L} \\
\text { Roll }_{R R} & \text { Pitch }_{R R} & \text { Yaw }_{R R}
\end{array}\right]
$$

| Rotation | Array Element | Rotation Axis |
| :---: | :---: | :---: |
| Vehicle, Rollv | Rotation(1,1) | Inertial vehicle Z-down $X$-axis |
| Vehicle, Pitch ${ }_{v}$ | Rotation(1,2) | Inertial vehicle Z-down $Y$-axis |
| Vehicle, Yaw ${ }_{v}$ | Rotation(1,3) | Inertial vehicle Z-down $Z$-axis |
| Handlebar, Roll $_{H}$ | Rotation(2,1) | Vehicle Z-down $X$-axis |
| Handlebar, Pitch $_{H}$ | Rotation(2,2) | Vehicle Z-down Y-axis |
| Handlebar, Yaw $_{H}$ | Rotation(2,3) | Vehicle Z-down Z -axis |
| Swing arm, Roll ${ }_{\text {SA }}$ | Rotation(3,1) | Vehicle Z-down $X$-axis |
| Swing arm, Pitch $_{\text {SA }}$ | Rotation(3,2) | Vehicle Z-down Y-axis |
| Swing arm, Yaw $_{\text {SA }}$ | Rotation(3,3) | Vehicle Z-down Z -axis |
| Front wheel, Roll $_{F}$ | Rotation(4,1) | Vehicle Z-down $X$-axis |
| Front wheel, Pitch $_{F}$ | Rotation(4,2) | Vehicle Z-down $Y$-axis |
| Front wheel, Yaw $_{F}$ | Rotation(4,3) | Vehicle Z-down Z -axis |
| Rear wheel, Roll $_{R}$ | Rotation(5,1) | Vehicle Z-down $X$-axis |
| Rear wheel, Pitch $_{R}$ | Rotation(5,2) | Vehicle Z-down $Y$-axis |
| Rear wheel, Yaw $_{R}$ | Rotation(5,3) | Vehicle Z-down Z-axis |

## Version History

Introduced in R2021b

## References

[1] Vehicle Dynamics Standards Committee. Vehicle Dynamics Terminology J670. Warrendale, PA: SAE International, 2008.

## See Also

Motorcycle Body Longitudinal In-Plane | Motorcycle Chain | Simulation 3D Scene Configuration

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"
"How 3D Simulation for Vehicle Dynamics Blockset Works"
"Prepare Custom Vehicle Mesh for the Unreal Editor"
"Unreal Engine Simulation Environment Requirements and Limitations"

## Simulation 3D Dolly

Implement dolly in 3D environment


## Libraries:

Vehicle Dynamics Blockset / Vehicle Scenarios / Sim3D / Sim3D Vehicle / Components

## Description

The Simulation 3D Dolly block implements a dolly in the 3D simulation environment.
To use this block, ensure that the Simulation 3D Scene Configuration block is in your model. If you set the Sample time parameter of this block to -1, the block uses the sample time specified in the Simulation 3D Scene Configuration block.

The block input uses the vehicle Z-down right-handed (RH) Cartesian coordinate system defined in SAE J670 ${ }^{1}$. The coordinate system is inertial and initially aligned with the vehicle geometric center:

- $X$-axis - Along vehicle longitudinal axis, points forward
- $Y$-axis - Along vehicle lateral axis, points to the right
- Z-axis - Points downward

Tip Verify that the Simulation 3D Dolly block executes before the Simulation 3D Scene Configuration block. That way, Simulation 3D Dolly prepares the signal data before the Unreal Engine 3D visualization environment receives it. To check the block execution order, right-click each block and select Properties. On the General tab, confirm these Priority settings:

- Simulation 3D Scene Configuration - 0
- Simulation 3D Dolly - - 1

For more information about execution order, see "Control and Display Execution Order".

## Ports

Input
Translation - Dolly translation
5-by-3 array (default) | 8-by-3 array | 11-by-3 array
Dolly, axle, and wheel translation along the vehicle Z-down $X$-, $Y$-, and $Z$ - axes, respectively, in m. Array dimensions depend on the Type parameter.

| Type Parameter | Array Dimension |
| :--- | :--- |
| One-axle dolly (default) | 5-by-3 array |
| Two-axle dolly | 8-by-3 array |


| Type Parameter | Array Dimension |
| :--- | :--- |
| Three-axle dolly | 11-by-3 array |

The signal contains translation information according to the dolly, axle, and wheel locations.

| Signal Index | Description |
| :---: | :---: |
| $\begin{aligned} & \text { Translation }(1,1) \\ & \text { Translation }(1,2) \\ & \text { Translation }(1,3) \end{aligned}$ | Dolly translation, Vehicle, along the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| $\begin{aligned} & \text { Translation }(2,1) \\ & \text { Translation }(2,2) \\ & \text { Translation }(2,3) \end{aligned}$ | Hitch socket, HitchSocket, translation along the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| ```Translation(3,1) Translation(3,2) Translation(3,3)``` | Axle one, Axle1, translation along the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| $\begin{aligned} & \text { Translation }(4,1) \\ & \text { Translation }(4,2) \\ & \text { Translation }(4,3) \end{aligned}$ | Axle one left wheel, Wheel_L1, translation along the vehicle Z-down $X$-, $Y$-, and $\bar{Z}$ - axes |
| Translation $(5,1)$ Translation $(5,2)$ Translation $(5,3)$ | Axle one right wheel, Wheel_R1, translation along the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| $\begin{aligned} & \hline \text { Translation }(6,1) \\ & \text { Translation }(6,2) \\ & \text { Translation }(6,3) \\ & \hline \end{aligned}$ | Axle two, Axle2, translation along the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| $\begin{aligned} & \text { Translation }(7,1) \\ & \text { Translation }(7,2) \\ & \text { Translation }(7,3) \end{aligned}$ | Axle two left wheel, Wheel L2, translation along the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| $\begin{aligned} & \text { Translation }(8,1) \\ & \text { Translation }(8,2) \\ & \text { Translation }(8,3) \end{aligned}$ | Axle two right wheel, Wheel_R2, translation along the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| $\begin{aligned} & \text { Translation }(9,1) \\ & \text { Translation }(9,2) \\ & \text { Translation }(9,3) \end{aligned}$ | Axle three, Axle3, translation along the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |


| Signal Index | Description |
| :--- | :--- |
| Translation $(10,1)$ | Axle three left wheel, Wheel_L3, translation along the <br> vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| Translation $(10,2)$ |  |
| Translation $(10,3)$ | Axle three right wheel, Wheel_R3, translation along the <br> vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| Translation $(11,1)$ |  |
| Translation $(11,2)$ |  |
| Translation $(11,3)$ |  |

Rotation - Dolly rotation
5-by-3 array (default) | 8-by-3 array | 11-by-3 array
Dolly, axle, and wheel rotation about the vehicle Z-down $X$-, $Y$-, and $Z$ - axes, respectively, in m. Array dimensions depend on the Type parameter.

| Type Parameter | Array Dimension |
| :--- | :--- |
| One-axle dolly (default) | 5-by-3 array |
| Two-axle dolly | 8-by-3 array |
| Three-axle dolly | 11-by-3 array |

The signal contains rotation information according to the dolly, axle, and wheel locations.

| Signal Index | Description |
| :---: | :---: |
| Rotation(1,1) <br> Rotation(1,2) <br> Rotation(1,3) | Dolly rotation, Vehicle, about the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| Rotation $(2,1)$ <br> Rotation $(2,2)$ <br> Rotation(2,3) | Hitch socket, HitchSocket, rotation about the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| Rotation $(3,1)$ <br> Rotation $(3,2)$ <br> Rotation $(3,3)$ | Axle one, Axle1, rotation about the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| Rotation $(4,1)$ <br> Rotation $(4,2)$ <br> Rotation(4,3) | Axle one left wheel, Wheel L1, rotation about the vehicle Z-down $X$-, $Y$-, and $\bar{Z}$ - axes |


| Signal Index | Description |
| :---: | :---: |
| Rotation $(5,1)$ <br> Rotation $(5,2)$ <br> Rotation(5,3) | Axle one right wheel, Wheel_R1, rotation about the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| Rotation (6,1) <br> Rotation $(6,2)$ <br> Rotation(6,3) | Axle two, Axle2, rotation about the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| Rotation(7,1) <br> Rotation $(7,2)$ <br> Rotation(7,3) | Axle two left wheel, Wheel L2, rotation about the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| Rotation(8,1) <br> Rotation (8,2) <br> Rotation(8,3) | Axle two right wheel, Wheel_R2, rotation about the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| Rotation (9,1) <br> Rotation $(9,2)$ <br> Rotation $(9,3)$ | Axle three, Axle3, rotation about the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| Rotation (10,1) <br> Rotation(10,2) <br> Rotation(10,3) | Axle three left wheel, Wheel_L3, rotation about the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| Rotation $(11,1)$ <br> Rotation $(11,2)$ <br> Rotation(11,3) | Axle three right wheel, Wheel_R3, rotation about the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |

## Parameters

## Vehicle Parameters

## Type - Type

One-axle dolly (default)|Two-axle dolly|Three-axle dolly
Use the Type parameter to specify the number of axles on the dolly. This table provides links to the dolly dimensions.

| Type Setting | Dolly Dimensions |
| :--- | :--- |
| One-axle dolly | One-Axle Dolly |
| Two-axle dolly | Two-Axle Dolly |


| Type Setting | Dolly Dimensions |
| :--- | :--- |
| Three-axle dolly | Three-Axle Dolly |
| Name - Name of dolly <br> SimulinkVehiclel (default) \| character vector |  |

Name of dolly. By default, when you use the block in your model, the block sets the Name parameter to SimulinkVehicleX. The value of $X$ depends on the number of simulation 3D vehicle blocks that you have in your model.

Sample time - Sample time

- 1 (default) | scalar

Sample time, $T_{s}$. The graphics frame rate is the inverse of the sample time.

## Initial Values

Initial array values to translate vehicle per part, Translation - Vehicle initial translation zeros( 5, 3 ) (default) | zeros( 8, 3 ) | zeros( 11, 3 )

Initial dolly, axle, and wheel translation along the vehicle Z-down $X$-, $Y$-, and $Z$ - axes, respectively, in m . Array dimensions depend on the Type parameter.

| Type Parameter | Array Dimension |
| :--- | :--- |
| One-axle dolly (default) | 5-by-3 array |
| Two-axle dolly | 8-by-3 array |
| Three-axle dolly | 11-by-3 array |

The parameter contains the initial translation values according to the dolly, axle, and wheel locations.

| Signal Index | Description |
| :---: | :---: |
| Translation(1,1) <br> Translation (1,2) <br> Translation(1,3) | Dolly translation, Vehicle, along the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| Translation $(2,1)$ <br> Translation $(2,2)$ <br> Translation $(2,3)$ | Hitch socket, HitchSocket, translation along the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| Translation $(3,1)$ <br> Translation $(3,2)$ <br> Translation $(3,3)$ | Axle one, Axle1, translation along the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| Translation $(4,1)$ <br> Translation $(4,2)$ <br> Translation(4,3) | Axle one left wheel, Wheel_L1, translation along the vehicle Z-down $X$-, $Y$-, and $\bar{Z}$ - axes |


| Signal Index | Description |
| :---: | :---: |
| Translation $(5,1)$ <br> Translation $(5,2)$ <br> Translation $(5,3)$ | Axle one right wheel, Wheel_R1, translation along the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| ```Translation(6,1) Translation(6,2) Translation(6,3)``` | Axle two, Axle2, translation along the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| Translation $(7,1)$ <br> Translation $(7,2)$ <br> Translation(7,3) | Axle two left wheel, Wheel L2, translation along the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| Translation(8,1) <br> Translation (8,2) <br> Translation(8,3) | Axle two right wheel, Wheel_R2, translation along the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| Translation (9,1) <br> Translation (9,2) <br> Translation (9,3) | Axle three, Axle3, translation along the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| $\begin{aligned} & \hline \text { Translation }(10,1) \\ & \text { Translation }(10,2) \\ & \text { Translation }(10,3) \end{aligned}$ | Axle three left wheel, Wheel_L3, translation along the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| ```Translation(11,1) Translation(11,2) Translation(11,3)``` | Axle three right wheel, Wheel_R3, translation along the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |

Initial array values to rotate vehicle per part, Rotation - Initial rotation
zeros( 5, 3 ) (default) | zeros( 8, 3 ) | zeros( 11, 3 )
Initial dolly, axle, and wheel rotation about the vehicle Z-down $X$-, $Y$-, and $Z$ - axes, respectively, in m . Array dimensions depend on the Type parameter.

| Type Parameter | Array Dimension |
| :--- | :--- |
| One-axle dolly (default) | 5-by-3 array |
| Two-axle dolly | 8-by-3 array |
| Three-axle dolly | 11-by-3 array |

The parameter contains the initial rotation values according to the dolly, axle, and wheel locations.

| Signal Index | Description |
| :---: | :---: |
| Rotation $(1,1)$ <br> Rotation $(1,2)$ <br> Rotation(1,3) | Dolly rotation, Vehicle, about the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| Rotation $(2,1)$ <br> Rotation $(2,2)$ <br> Rotation $(2,3)$ | Hitch socket, HitchSocket, rotation about the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| Rotation $(3,1)$ <br> Rotation $(3,2)$ <br> Rotation $(3,3)$ | Axle one, Axle1, rotation about the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| Rotation(4,1) <br> Rotation $(4,2)$ <br> Rotation (4,3) | Axle one left wheel, Wheel_L1, rotation about the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| Rotation $(5,1)$ <br> Rotation $(5,2)$ <br> Rotation $(5,3)$ | Axle one right wheel, Wheel_R1, rotation about the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| Rotation $(6,1)$ <br> Rotation $(6,2)$ <br> Rotation $(6,3)$ | Axle two, Axle2, rotation about the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| Rotation $(7,1)$ <br> Rotation $(7,2)$ <br> Rotation(7,3) | Axle two left wheel, Wheel L2, rotation about the vehicle Z-down $X$-, $Y$-, and $\bar{Z}$ - axes |
| Rotation $(8,1)$ <br> Rotation $(8,2)$ <br> Rotation (8,3) | Axle two right wheel, Wheel_R2, rotation about the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| Rotation (9,1) <br> Rotation $(9,2)$ <br> Rotation(9,3) | Axle three, Axle3, rotation about the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |
| Rotation(10,1) <br> Rotation(10,2) <br> Rotation(10,3) | Axle three left wheel, Wheel L3, rotation about the vehicle Z-down $X$-, $Y$-, and $Z$ - axes |


| Signal Index | Description |
| :--- | :--- |
| Rotation $(11,1)$ | Axle three right wheel, Wheel_R3, rotation about the <br> vehicle Z-down $X-, Y$-, and $Z$ - axes |
| Rotation $(11,2)$ |  |
| Rotation $(11,3)$ |  |

## Version History

Introduced in R2021b

## References

[1] Vehicle Dynamics Standards Committee. Vehicle Dynamics Terminology J670. Warrendale, PA: SAE International, 2008.

## See Also

Simulation 3D Scene Configuration

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"
"How 3D Simulation for Vehicle Dynamics Blockset Works"
"Prepare Custom Vehicle Mesh for the Unreal Editor"
"Unreal Engine Simulation Environment Requirements and Limitations"

## Simulation 3D Terrain Sensor

Implement multipoint terrain sensor in 3D environment


## Libraries:

Vehicle Dynamics Blockset / Vehicle Scenarios / Sim3D / Sim3D Vehicle / Components

## Description

The Simulation 3D Terrain Sensor block implements a multipoint terrain sensor in Unreal Engine. Use the block for contact modeling at high vehicle velocities over terrain changes, including speed bumps. The block implements ray tracing to detect the terrain below the tires. Use the block parameters to:

- Sense the terrain under any simulation 3D vehicle actor in the scene, including actors created by the Simulation 3D Vehicle and Simulation 3D Motorcycle blocks.
- Configure the ray origins, directions, and lengths to adjust the terrain sensor pattern for your scene and test scenario.

The block creates a terrain sensor pattern for each of the wheels on the vehicle actor. For specific patterns, this table provides the corresponding parameter settings.

| Pattern | Parameter Settings |
| :---: | :---: |
|  | - Ray origins - zeros $(5,3)$ <br> - Ray directions - [sqrt(3)/2 0-1/2;1/2 <br> $0-$ sqrt(3)/2; $00-1 ;-1 / 20-$ <br> sqrt(3)/2; -sqrt(3)/2 0-1/2] <br> Ray lengths - ones $(5,1) * 6$ <br> Number of wheels on parent vehicle - 4 |
| - Five rays per wheel <br> - Rays originate at point specified by wheel spin axis <br> - Rays extend downward at $15^{\circ}$ intervals <br> - Rays length is 6 m |  |



Tip Verify that the Simulation 3D Scene Configuration block executes before the Simulation 3D Terrain Sensor block. That way, the Unreal Engine 3D visualization environment prepares the data before the Simulation 3D Terrain Sensor block receives it. To check the block execution order, rightclick the blocks and select Properties. On the General tab, confirm these Priority settings:

- Simulation 3D Scene Configuration - 0
- Simulation 3D Terrain Sensor - 1

For more information about execution order, see "Control and Display Execution Order".

## Ports

## Output

Info - Bus signal
bus
Bus signal containing block values. The signals are arrays that depend on the wheel location.

| Signal | Description | Units |
| :--- | :--- | :--- |
| WheelWPosi <br> tions | Wheel $W$ ray hit location relative to ray origin, specified as a real- <br> valued $N$-by-3 array of the form $[X, Y, Z]$ in the 3D visualization <br> engine world coordinate system. $N$ is the number of rays per <br> wheel. | m |
| WheelWStat <br> us | Wheel $W$ ray hit status, specified as a $N$-by-1 array. $N$ is the number <br> of rays per wheel. <br> - Hit an object -1 <br> - Miss an object - 0 | NA |

## Parameters

## Mounting

Sensor identifier, sensorld - Unique sensor identifier
0 (default) | positive integer
Unique sensor identifier, specified as a positive integer. In a multisensor system, the sensor identifier distinguishes between sensors. When you add a new sensor block to your model, the Sensor identifier of that block is $N+1 . N$ is the highest Sensor identifier value among existing sensor blocks in the model.

## Example: 2

Parent name, Vehicleldentifier - Name of parent to which sensor is mounted
SimulinkVehicle1 (default) | vehicle name
Name of the parent to which the sensor is mounted, specified as the name of a vehicle in your model. The vehicle names that you can select correspond to the Name parameters of the simulation 3D vehicle blocks in your model.

## Example: SimulinkVehicle2

## Parameters

## Ray origins, RayOrigins - Ray origin

[0 00 1] (default) | real-valued $N$-by-3 array
Ray origin relative to the wheel spin axis, specified as a real-valued $N$-by- 3 array of the form $[X, Y, Z]$. $N$ is the number of rays. Units are in meters.

If you mount the sensor to a vehicle by setting Parent name to the name of that vehicle, then $X, Y$, and $Z$ are in the 3D visualization engine coordinate system, where:

- The $X$-axis points forward from the vehicle.
- The $Y$-axis points to the right of the vehicle, as viewed when looking in the forward direction of the vehicle.
- The Z-axis points up.

Example: zeros (10, 3)
Ray directions, RayDirections - Normalized ray direction
[0 0 - 1] (default) | real-valued $N$-by-3 array
Normalized ray direction relative to wheel, specified as a real-valued $N$-by-3 array of the form $[X, Y$, $Z] . N$ is the number of rays. Units are in dimensionless.

If you mount the sensor to a vehicle by setting Parent name to the name of that vehicle, then $X, Y$, and $Z$ are in the 3D visualization engine coordinate system, where:

- The $X$-axis points forward from the vehicle.
- The $Y$-axis points to the right of the vehicle, as viewed when looking in the forward direction of the vehicle.
- The Z-axis points up.

Example: ones (10, 3 )
Ray lengths, RayLengths - Length
20 (default) | real-valued $N$-by-1 vector
Ray length, specified as a real-valued $N$-by- 1 vector $N, N$ is the number of rays. Units are in meters.
Example: ones (10, 1) *10
Number of wheels on parent vehicle - Number of wheels
4 (default) | positive integer
Name of wheels the parent to which the sensor is mounted. The vehicle name corresponds to the Name parameters of the simulation 3D vehicle blocks in your model.
Example: 6
Visualize trace line - Visualize ray traces
off (default) | on
Enable trace line visualization.
Sample time - Sample time

- 1 (default) | scalar

Sample time, $T_{s}$. The graphics frame rate is the inverse of the sample time.

## Version History <br> Introduced in R2022a

## See Also

Simulation 3D Scene Configuration | Simulation 3D Vehicle

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"
"Scene Interrogation in 3D Environment"

## External Websites

Unreal Engine

## Simulation 3D Ray Tracer

Implement ray tracing in 3D environment


## Libraries:

Vehicle Dynamics Blockset / Vehicle Scenarios / Sim3D / Sim3D Vehicle / Components

## Description

The Simulation 3D Ray Tracer block implements ray tracing to get the positions, surface normals, surface identifiers, and distances for objects in the scene. You can specify block parameters that configure the ray origins, directions, and lengths to adjust the ray trace sensor pattern for your scene and test scenario.

Tip Verify that the Simulation 3D Scene Configuration block executes before the Simulation 3D Ray Tracer block. That way, the Unreal Engine 3D visualization environment prepares the data before the Simulation 3D Ray Tracer block receives it. To check the block execution order, right-click the blocks and select Properties. On the General tab, confirm these Priority settings:

- Simulation 3D Scene Configuration - 0
- Simulation 3D Terrain Sensor - 1

For more information about execution order, see "Control and Display Execution Order".

## Ports

## Output

HitLocations - Hit locations
real-valued $N(B+1)$-by- 3 array
Hit locations, returned as a real-valued $N(B+1)$-by- 3 array of the form $[X, Y, Z]$, in meters. $N$ is the number of rays and $B$ is the number of bounces per ray.

If you mount the sensor to a vehicle by setting Parent name to the name of that vehicle, then $X, Y$, and $Z$ are in the 3D visualization engine coordinate system, where:

- The $X$-axis points forward from the vehicle
- The $Y$-axis points to the right of the vehicle, as viewed when looking in the forward direction of the vehicle
- The $Z$-axis points up

Data Types: double
HitNormals - Ray normal to hit location
real-valued $N(B+1)$-by- 3 array

Ray normal to the hit location, returned as a real-valued $N(B+1)$-by- 3 array of the form $[X, Y, Z]$, in meters. $N$ is the number of rays and $B$ is the number of bounces per ray.

If you mount the sensor to a vehicle by setting Parent name to the name of that vehicle, then $X, Y$, and $Z$ are in the 3D visualization engine coordinate system, where:

- The $X$-axis points forward from the vehicle
- The $Y$-axis points to the right of the vehicle, as viewed when looking in the forward direction of the vehicle
- The $Z$-axis points up

Data Types: double
HitDistances - Ray distance to hit location
real-valued $N(B+1)$-by- 1 array
Ray distance to hit location, returned as a real-valued $N(B+1)$-by- 1 vector $N$, in meters. $N$ is the number of rays and $B$ is the number of bounces per ray.

Data Types: double
Surfacelds - Object IDs of hit surfaces
integer-valued $N(B+1)$-by- 1 vector | 0
Object identifier of the surfaces hit by the ray, returned as an integer-valued $N(B+1)$-by-1 vector $N . N$ is the number of rays and $B$ is the number of bounces per ray.

The returned surface identifiers are the object values specified when creating custom surfaces in the Unreal Editor. If a surface identifier is unknown, the block assigns it an ID of 0 . For information about adding surfaces, see Add a Surface Type in the Unreal Engine documentation.
Data Types: uint8
IsValidHit - Hit flag
N -by-1 vector
Hit flag, returned as a $N$-by- 1 Boolean vector. $N$ is the number of rays. A value of 1 indicates the ray hit a surface.

Data Types: Boolean

## Parameters

Mounting
Sensor identifier - Unique sensor identifier
1 (default) | positive integer
Specify the unique identifier of the sensor. In a multisensor system, the sensor identifier enables you to distinguish between sensors. When you add a new sensor block to your model, the Sensor identifier of that block is $N+1$, where $N$ is the highest Sensor identifier value among the existing sensor blocks in the model.

Example: 2

Parent name - Name of parent
Scene Origin (default)
Name of parent to which the sensor is mounted, specified as the name of a vehicle in your model, or Scene Origin. The vehicle names that you can select correspond to the Name parameters of the simulation 3D vehicle blocks in your model.

Mounting location - Sensor mounting location
Origin (default)
Sensor mounting location.

- When Parent name is Scene Origin, the block mounts the sensor to the origin of the scene. You can set the Mounting location to Origin only. During simulation, the sensor remains stationary.
- When Parent name is the name of a vehicle, the block mounts the sensor to one of the predefined mounting locations described in the table. During simulation, the sensor travels with the vehicle.

Roll, pitch, and yaw are clockwise-positive when looking in the positive direction of the $X$-axis, $Y$-axis, and $Z$-axis, respectively. When looking at a vehicle from above, the yaw angle (the orientation angle) is counterclockwise-positive because you are looking in the negative direction of the axis.

Specify offset - Specify offset from mounting location
off (default) |on
Select this parameter to specify an offset from the mounting location by using the Relative translation [X, Y, Z] (m) and Relative rotation [Roll, Pitch, Yaw] (deg) parameters.

Relative translation [ $\mathbf{X}, \mathbf{Y}, \mathbf{Z}$ ] ( $\mathbf{m}$ ) - Translation offset relative to mounting location $[0,0,0]$ (default) | real-valued 1-by-3 vector

Translation offset relative to the mounting location of the sensor, specified as a real-valued 1-by-3 vector of the form $[X, Y, Z]$, in meters.

If you mount the sensor to a vehicle by setting Parent name to the name of that vehicle, then $X, Y$, and $Z$ are in the vehicle coordinate system, where:

- The $X$-axis points forward from the vehicle
- The $Y$-axis points to the left of the vehicle, as viewed when looking in the forward direction of the vehicle
- The Z-axis points up

The origin is the mounting location specified in the Mounting location parameter. This origin is different from the vehicle origin, which is the geometric center of the vehicle.

If you mount the sensor to the scene origin by setting Parent name to Scene Origin, then $X, Y$, and $Z$ are in the world coordinates of the scene.

For more details about the vehicle and world coordinate systems, see "Coordinate Systems in Vehicle Dynamics Blockset".
Example: [0,0,0.01]

## Dependencies

To enable this parameter, select Specify offset.
Relative rotation [Roll, Pitch, Yaw] (deg) - Rotational offset relative to mounting location [0, 0, 0] (default) | real-valued 1-by-3 vector

Rotational offset relative to the mounting location of the sensor, specified as a real-valued 1-by-3 vector of the form [Roll, Pitch, Yaw], in degrees. Roll, pitch, and yaw are the angles of rotation about the $X$-, $Y$-, and $Z$-axes, respectively.

If you mount the sensor to a vehicle by setting Parent name to the name of that vehicle, then $X, Y$, and $Z$ are in the vehicle coordinate system, where:

- The $X$-axis points forward from the vehicle.
- The $Y$-axis points to the left of the vehicle, as viewed when looking in the forward direction of the vehicle.
- The $Z$-axis points up.
- Roll, pitch, and yaw are clockwise-positive when looking in the forward direction of the $X$-axis, $Y$ axis, and $Z$-axis, respectively. If you view a scene from a 2 D top-down perspective, then the yaw angle (also called the orientation angle) is counterclockwise-positive because you are viewing the scene in the negative direction of the $Z$-axis.

The origin is the mounting location specified in the Mounting location parameter. This origin is different from the vehicle origin, which is the geometric center of the vehicle.

If you mount the sensor to the scene origin by setting Parent name to Scene Origin, then $X, Y$, and $Z$ are in the world coordinates of the scene.

For more details about the vehicle and world coordinate systems, see "Coordinate Systems in Vehicle Dynamics Blockset".

Example: [0, 0,10]

## Dependencies

To enable this parameter, select Specify offset.

## Parameters

Ray origins, RayOrigins - Ray origin
zeros (10, 3) (default) | real-valued $N$-by-3 array
Ray origin relative to sensor mounting location, specified as a real-valued $N$-by- 3 array of the form $[X$, $Y, Z$ ], in meters. $N$ is the number of rays.

If you mount the sensor to a vehicle by setting Parent name to the name of that vehicle, then $X, Y$, and $Z$ are in the 3D visualization engine coordinate system, where:

- The $X$-axis points forward from the vehicle
- The $Y$-axis points to the right of the vehicle, as viewed when looking in the forward direction of the vehicle
- The $Z$-axis points up

Example: zeros (10, 3)

Ray directions, RayDirections - Normalized ray direction
ones $(10,3)$ (default) | real-valued $N$-by-3 array
Normalized ray direction relative to sensor mounting location, specified as a real-valued $N$-by- 3 array of the form $[X, Y, Z] . N$ is the number of rays. The units are dimensionless.

If you mount the sensor to a vehicle by setting Parent name to the name of that vehicle, then $X, Y$, and $Z$ are in the 3D visualization engine coordinate system, where:

- The $X$-axis points forward from the vehicle
- The $Y$-axis points to the right of the vehicle, as viewed when looking in the forward direction of the vehicle
- The $Z$-axis points up

Example: ones (10,3)
Max ray lengths, RayLengths - Maximum total ray length
ones $(10,1) * 10$ (default) $\mid$ real-valued $N$-by- 1 vector
Maximum total ray length of a multi-bounce trace path, specified as a real-valued $N$-by- 1 vector, in meters. $N$ is the number of rays.
Example: ones $(10,1) * 10$
Number of bounces - Number of bounces per ray
2 (default) | positive integer
Number of bounces that a trace may have before terminating, $B$, specified as an integer.
Example: 0
Visualize trace line - Visualize ray traces
on (default) | off
Whether to enable Unreal Engine trace line visualization for the ray tracer.
Enable optimization - Enable optimization
on (default) | off
Whether to enable optimization of the ray tracer. Enabling this parameter allows the block to perform concurrent traces. Enable this parameter when the number of traces is large and your machine has multiple cores.

## Sample time - Sample time

- 1 (default) | positive scalar

Sample time of the block, in seconds, specified as a positive scalar. The 3D simulation environment frame rate is the inverse of the sample time.

If you set the sample time to -1 , the block inherits its sample time from the Simulation 3D Scene Configuration block.

## Version History

Introduced in R2022b

## See Also

Simulation 3D Camera Get | Simulation 3D Scene Configuration | Simulation 3D Vehicle | Simulation 3D Vehicle with Ground Following

## Topics

"Scene Interrogation in 3D Environment"

## External Websites

Unreal Engine

Scenes

## Straight Road

Straight road 3D environment

## Description

The Straight Road scene is a 3D environment of a straight four-lane divided highway. The scene is rendered using RoadRunner.


## Setup

To simulate a driving maneuver in this scene:
1 Add a Simulation 3D Scene Configuration block to your Simulink model.
2 In this block, set the Scene source parameter to Default Scenes.
3 Set the enabled Scene name parameter to Straight road.

## Layout

The scene uses the world coordinate system to locate objects.
The active area of the scene contains the road.


## Scene Dimensions

This table provides the scene area corner locations in the world coordinate system. Dimensions are in m.

| Locations | $\mathbf{X}$ | $\mathbf{Y}$ | $\mathbf{Z}$ |
| :--- | :--- | :--- | :--- |
|  | $\mathbf{( m )}$ | $(\mathbf{m})$ | $(\mathbf{m})$ |
| Scene - Top left | -1008 | -1008 | 0 |
| Scene - Bottom right | 1008 | 1008 | 0 |
| Active area - Bottom left | -800 | 8.35 | 0 |

## Recommended Starting Location

This table provides the recommended starting location for the vehicle in the world coordinate system. Dimensions are in $m$ and deg.

| Recommended Starting Location |  |  |  |  |  |  | Roll | Pitch |
| :--- | :--- | :--- | :--- | :--- | :--- | :---: | :---: | :---: |
| $\mathbf{X}$ | $\mathbf{Y}$ | $\mathbf{Z}$ | (m) | $(\mathrm{m})$ | $(\mathrm{deg})$ |  |  |  |

## Lane Dimensions

This figure and table provides the lane dimensions, in $m$.


| Variable | Dimension (m) |
| :--- | :--- |
| $l w_{1}$ | 0.625 |
| $l w_{2}$ | 3.85 |
| $l w_{3}$ | 3.85 |
| $l w_{4}$ | 0.34 |
| $l w_{5}$ | 3.85 |
| $l w_{6}$ | 3.85 |
| $l w_{7}$ | 0.625 |
| $m l$ | 1.5 |
| $s$ | 4.5 |


| Variable | Dimension (m) |
| :--- | :--- |
| $m w_{w}$ | 0.125 |
| $m w_{y}$ | 0.125 |
| $W$ | 16.70 |

## World Coordinate System

The 3D visualization environment uses a world coordinate system with axes that are fixed in the inertial reference frame.


| Axis | Description |
| :--- | :--- |
| $X$ | Forward direction of the vehicle <br> Roll $~-~ R i g h t-h a n d e d ~ r o t a t i o n ~ a b o u t ~$ <br> $X$ |
| $Y$ | Extends to the right of the vehicle, parallel to the ground plane <br> Pitch $~-~ R i g h t-h a n d e d ~ r o t a t i o n ~ a b o u t ~$ -axis |, | Extends upwards |
| :--- |
| Yaw - Left-handed rotation about $Z$-axis |

## Tips

- If you have the Vehicle Dynamics Blockset Interface for Unreal Engine 4 Projects support package, then you can modify this scene. In the Unreal Engine project file that comes with the support package, this scene is named HwStrght.

For more details on customizing scenes, see "Customize 3D Scenes for Vehicle Dynamics Simulations".

## Version History <br> Introduced in R2018b

## R2022b: Scene rendered using RoadRunner

Behavior changed in R2022b
Starting from R2022b, the Straight Road scene in the Unreal Engine 3D environment is rendered using RoadRunner. As a result, the locations of scene objects, including cones and parked vehicles, are moved from their pre-R2022b locations.

## See Also

Simulation 3D Scene Configuration | Curved Road | Double Lane Change | Open Surface | Large Parking Lot | Parking Lot | US City Block | US Highway | Virtual Mcity

Topics
"Unreal Engine Simulation Environment Requirements and Limitations"
"How 3D Simulation for Vehicle Dynamics Blockset Works"
"Customize 3D Scenes for Vehicle Dynamics Simulations"

## Curved Road

Curved road 3D environment

## Description

The Curved Road scene is a 3D environment of a curved highway loop. The scene is rendered using RoadRunner.


## Setup

To simulate a driving maneuver in this scene:
1 Add a Simulation 3D Scene Configuration block to your Simulink model.
2 In this block, set the Scene source parameter to Default Scenes.
3 Set the enabled Scene name parameter to Curved road.

## Layout

The scene uses the world coordinate system to locate objects.


## Scene Dimensions

This table provides the scene corner locations in the world coordinate system. Dimensions are in $m$.

| Location | X <br> (m) | Y <br> $(\mathbf{m})$ | Z <br> $(\mathbf{m})$ |
| :--- | :--- | :--- | :--- |
| Scene - Bottom left | -1587.75 | 195.39 | 0 |
| Scene - Top right | 428.26 | -1820.60 | 0 |

## Recommended Starting Location

This table provides the recommended starting location for the vehicle in the world coordinate system. Dimensions are in $m$ and deg.

| Recommended Starting Location |
| :--- | :--- |
| $\mathbf{X}$ |


| $\mathbf{X}$ | $\mathbf{Y}$ | $\mathbf{Z}$ | Roll | Pitch | Yaw |
| :--- | :--- | :--- | :--- | :--- | :--- |
| $(\mathbf{m})$ | $(\mathrm{m})$ | $(\mathrm{m})$ | (deg) | $($ deg $)$ | (deg) |
| 0.2 | -1605.00 | 0 | 0 | 0 | $-156^{\circ}$ |

## Lane Dimensions

This figure and table provides the lane dimensions, in m .


| Variable | Dimension (m) |
| :--- | :--- |
| $l w_{1}$ | 0.625 |
| $l w_{2}$ | 3.85 |
| $l w_{3}$ | 3.85 |
| $l w_{4}$ | 0.34 |
| $l w_{5}$ | 3.85 |
| $l w_{6}$ | 3.85 |
| $l w_{7}$ | 0.625 |
| $m l$ | 1.5 |
| $s$ | 4.5 |
| $m w_{w}$ | 0.125 |
| $m w_{y}$ | 0.125 |


| Variable | Dimension (m) |
| :--- | :--- |
| $W$ | 16.65 |

## World Coordinate System

The 3D visualization environment uses a world coordinate system with axes that are fixed in the inertial reference frame.


| Axis | Description |
| :--- | :--- |
| $X$ | Forward direction of the vehicle <br> Roll $~-~ R i g h t-h a n d e d ~ r o t a t i o n ~ a b o u t ~$ <br> $X$ |
| $Y$ | Extends to the right of the vehicle, parallel to the ground plane <br> Pitch $~-~ R i g h t-h a n d e d ~ r o t a t i o n ~ a b o u t ~$ -axis |$|$| Extends upwards |
| :--- | :--- |
| Yaw $~-~ L e f t-h a n d e d ~ r o t a t i o n ~ a b o u t ~$ |
| $Z$-axis |

## Tips

- If you have the Vehicle Dynamics Blockset Interface for Unreal Engine 4 Projects support package, then you can modify this scene. In the Unreal Engine project file that comes with the support package, this scene is named HwCurve.

For more details on customizing scenes, see "Customize 3D Scenes for Vehicle Dynamics Simulations".

## Version History <br> Introduced in R2018b

R2022b: Scene rendered using RoadRunner
Behavior changed in R2022b

Starting from R2022b, the Curved Road scene in the Unreal Engine 3D environment is rendered using RoadRunner. As a result, the locations of scene objects, including cones and parked vehicles, are moved from their pre-R2022b locations.

## See Also

Simulation 3D Scene Configuration | Double Lane Change | Open Surface | Large Parking Lot | Parking Lot | Straight Road | US City Block | US Highway | Virtual Mcity

## Topics

"Unreal Engine Simulation Environment Requirements and Limitations"
"How 3D Simulation for Vehicle Dynamics Blockset Works"
"Customize 3D Scenes for Vehicle Dynamics Simulations"

## Parking Lot

Parking lot 3D environment

## Description

The Parking Lot scene is a 3D environment of a parking lot. The scene is rendered using RoadRunner.


## Setup

To simulate a driving maneuver in this scene:
1 Add a Simulation 3D Scene Configuration block to your Simulink model.
2 In this block, set the Scene source parameter to Default Scenes.
3 Set the enabled Scene name parameter to Parking lot.

## Layout

The scene uses the world coordinate system to locate objects. The active area of the scene contains the parking lot.


## Scene Dimensions

This table provides the scene and active area corner locations in the world coordinate system. Dimensions are in m.

| Locations | $\mathbf{X}$ | $\mathbf{Y}$ | $\mathbf{Z}$ |
| :--- | :--- | :--- | :--- |
|  | $(\mathbf{m})$ | $(\mathbf{m})$ | $(\mathbf{m})$ |
| Scene - Bottom left | -437.32 | 262.79 | 0 |
| Scene - Top right | 268.28 | -442.81 | 0 |
| Active area - Bottom left | -193.86 | 23.43 | 0 |

## Recommended Starting Location

This table provides the recommended starting location for the vehicle in the world coordinate system. Dimensions are in $m$ and deg.

| Recommended Starting Location |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| (m) | $\begin{aligned} & \mathbf{Y} \\ & (\mathrm{m}) \end{aligned}$ | $\begin{aligned} & \mathrm{Z} \\ & (\mathrm{~m}) \end{aligned}$ | $\begin{aligned} & \text { Roll } \\ & \text { (deg) } \end{aligned}$ | $\begin{aligned} & \text { Pitch } \\ & \text { (deg) } \end{aligned}$ | $\begin{aligned} & \hline \text { Yaw } \\ & \text { (deg) } \end{aligned}$ |
| -104.0 | -9.7 | 0 | 0 | 0 | 0 |

## Parking Space Dimensions

This figure shows the parking space dimensions, in m .


## World Coordinate System

The 3D visualization environment uses a world coordinate system with axes that are fixed in the inertial reference frame.


| Axis | Description |
| :--- | :--- |
| $X$ | Forward direction of the vehicle <br> Roll $~-~ R i g h t-h a n d e d ~ r o t a t i o n ~ a b o u t ~$ <br> $X$ |
| $Y$ | Extends to the right of the vehicle, parallel to the ground plane <br> Pitch $~-~ R i g h t-h a n d e d ~ r o t a t i o n ~ a b o u t ~$ -axis |$|$| Extends upwards |
| :--- | :--- |
| Yaw - Left-handed rotation about Z-axis |

## Tips

- If you have the Vehicle Dynamics Blockset Interface for Unreal Engine 4 Projects support package, then you can modify this scene. In the Unreal Engine project file that comes with the support package, this scene is named SimpleLot.

For more details on customizing scenes, see "Customize 3D Scenes for Vehicle Dynamics Simulations".

## Version History

Introduced in R2018b

## R2022b: Scene rendered using RoadRunner

Behavior changed in R2022b
Starting from R2022b, the Parking Lot scene in the Unreal Engine 3D environment is rendered using RoadRunner. As a result, the locations of scene objects, including cones and parked vehicles, are moved from their pre-R2022b locations.

## See Also

Simulation 3D Scene Configuration | Curved Road | Double Lane Change | Open Surface | Large Parking Lot | Straight Road | US City Block | US Highway | Virtual Mcity

## Topics

"Unreal Engine Simulation Environment Requirements and Limitations"
"How 3D Simulation for Vehicle Dynamics Blockset Works"
"Customize 3D Scenes for Vehicle Dynamics Simulations"

## Large Parking Lot

Large parking lot 3D environment

## Description

The Large Parking Lot scene is a 3D environment of a large parking lot that contains cones, curbs, traffic signs, and parked vehicles. The scene is rendered using RoadRunner.


## Setup

To simulate a driving maneuver in this scene:
1 Add a Simulation 3D Scene Configuration block to your Simulink model.
2 In this block, set the Scene source parameter to Default Scenes.
3 Set the enabled Scene name parameter to Large parking lot.

## Layout

The scene uses the world coordinate system to locate objects.


## Scene Dimensions

This table provides the scene area corner locations in the world coordinate system. Dimensions are in $m$ and deg.

| Locations | X <br> (m) | (m) | Z <br> $(m)$ |
| :--- | :--- | :--- | :--- |
| Scene - Top left | -78.6 | -73.5 | 0 |
| Scene - Bottom right | 72.6 | 77.7 | 0 |

## Recommended Starting Location

This table provides the recommended starting location for the vehicle in the world coordinate system. Dimensions are in m and deg.

| Recommended Starting Location |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & X \\ & (m) \end{aligned}$ | $\begin{aligned} & \mathbf{Y} \\ & (\mathrm{m}) \end{aligned}$ | $\begin{aligned} & \mathrm{Z} \\ & (\mathrm{~m}) \end{aligned}$ | $\begin{aligned} & \text { Roll } \\ & \text { (deg) } \end{aligned}$ | $\begin{aligned} & \text { Pitch } \\ & \text { (deg) } \end{aligned}$ | $\begin{aligned} & \text { Yaw } \\ & \text { (deg) } \end{aligned}$ |
| 45.0 | 54.7 | 0 | 0 | 0 | -90 |

## Parking Space Dimensions

This figure shows the parking space dimensions, in m .


## World Coordinate System

The 3D visualization environment uses a world coordinate system with axes that are fixed in the inertial reference frame.


| Axis | Description |
| :--- | :--- |
| $X$ | Forward direction of the vehicle <br> Roll $~-~ R i g h t-h a n d e d ~ r o t a t i o n ~ a b o u t ~$ |
| $Y$ | Extexis <br> Pitch $~$ Right-handed rotation about $Y$-axis |$|$| Extends upwards |
| :--- |
| Yaw - Left-handed rotation about $Z$-axis |

## Vehicles

## Hatchback, Pickups, and Sedans

This table provides the vehicle tag names and initial locations for other vehicles in the scene, in the world coordinate system. Dimensions are in m and deg.

| Object | Unreal <br> Engine <br> Editor Name | Locations <br> $\mathbf{X}$ <br> $\mathbf{( m )}$ | Y <br> $\mathbf{( m )}$ | Z <br> $\mathbf{( m )}$ | Roll <br> (deg) | Pitch <br> $\mathbf{( d e g )}$ | Yaw <br> $\mathbf{( d e g )}$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Vehicle | CompactCar <br> Node | -21.69 | 38.90 | 0.00 | 0 | 0 | 180 |
| CompactCar <br> Node445 | -16.11 | 4.40 | 0.00 | 0 | 0 | 0 |  |
| CompactCar <br> Node450 | 5.63 | -14.25 | 0.00 | 0 | 0 | 0 |  |
| PickupTruc <br> kNode | 5.61 | -40.40 | 0.00 | 0 | 0 | 180 |  |
| PickupTruc <br> kNode396 | -5.27 | -34.87 | 0.00 | 0 | 0 | 0 |  |


| Object | Unreal <br> Engine Editor Name | Locations |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | (m) | $\begin{aligned} & Y \\ & (\mathrm{~m}) \end{aligned}$ | $\begin{aligned} & \mathrm{Z} \\ & (\mathrm{~m}) \end{aligned}$ | $\begin{aligned} & \text { Roll } \\ & \text { (deg) } \end{aligned}$ | $\begin{aligned} & \text { Pitch } \\ & \text { (deg) } \end{aligned}$ | $\begin{aligned} & \text { Yaw } \\ & \text { (deg) } \end{aligned}$ |
|  | PickupTruc kNode443 | -27.13 | 46.40 | 0.00 | 0 | 0 | 0 |
|  | PickupTruc kNode444 | 11.14 | -0.90 | 0.00 | 0 | 0 | 180 |
|  | SedanNode | -40.71 | 18.40 | 0.00 | 0 | 0 | 180 |
|  | SedanNode4 $46$ | -21.68 | 18.40 | 0.00 | 0 | 0 | 180 |
|  | SedanNode4 $47$ | -27.12 | 18.40 | 0.00 | 0 | 0 | 180 |
|  | SedanNode4 49 | 5.70 | 4.80 | 0.00 | 0 | 0 | 0 |
|  | $\begin{aligned} & \text { SedanNode4 } \\ & 51 \end{aligned}$ | 29.55 | -13.80 | 0.00 | 0 | 0 | 0 |
|  | $\begin{aligned} & \text { SedanNode4 } \\ & 52 \end{aligned}$ | 11.20 | 25.90 | 0.00 | 0 | 0 | 0 |
|  | SuvNode | -24.40 | 18.40 | 0.00 | 0 | 0 | 180 |
|  | SuvNode448 | 11.14 | 4.80 | 0.00 | 0 | 0 | 0 |

## Objects

## Cones



## Locations

This table provides the object names and locations in the world coordinate system. Dimensions are in $m$ and deg.

| Object | Unreal Engine Editor Name | Location |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & X \\ & \hline(\mathrm{~m}) \end{aligned}$ | $\begin{aligned} & \mathbf{Y} \\ & (\mathrm{m}) \end{aligned}$ | $\begin{aligned} & \mathrm{Z} \\ & (\mathrm{~m}) \end{aligned}$ | $\begin{aligned} & \text { Roll } \\ & \text { (deg) } \end{aligned}$ | $\begin{aligned} & \text { Pitch } \\ & \text { (deg) } \end{aligned}$ | $\begin{aligned} & \text { Yaw } \\ & \text { (deg) } \end{aligned}$ |
| Cone | TrafficCo ne01_Prop Node | -21.60 | -23.41 | 0.00 | 0 | 0 | 0 |
|  | TrafficCo ne01_Prop Node453 | -24.41 | 36.19 | 0.00 | 0 | 0 | 0 |
|  | TrafficCo ne01_Prop Node454 | -27.00 | -2.68 | 0.00 | 0 | 0 | 0 |
|  | TrafficCo ne01_Prop Node455 | 13.92 | 28.21 | 0.00 | 0 | 0 | 0 |
|  | TrafficCo ne01_Prop Node475 | -38.02 | 48.02 | 0.00 | 0 | 0 | 0 |

## Traffic Signs



## Locations

This table provides the object names and locations in the world coordinate system. Dimensions are in m and deg.

| Object | Unreal Engine Editor Name | Location |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & X \\ & \hline(m) \end{aligned}$ | $\begin{aligned} & \mathbf{Y} \\ & (\mathrm{m}) \end{aligned}$ | $\begin{aligned} & \mathrm{Z} \\ & (\mathrm{~m}) \end{aligned}$ | $\begin{aligned} & \text { Roll } \\ & \text { (deg) } \end{aligned}$ | Pitch <br> (deg) | $\begin{aligned} & \hline \text { Yaw } \\ & \text { (deg) } \end{aligned}$ |
| Traffic signs | SignPost_10ftNode | 34.78 | 57.38 | 0.00 | 0 | 0 | 90 |
|  | SignPost_10ftNode 456 | 35.30 | 36.38 | 0.00 | 0 | 0 | 90 |
|  | SignPost_10ftNode 457 | 35.28 | 15.95 | 0.00 | 0 | 0 | 90 |
|  | SignPost_10ftNode 458 | 35.35 | -2.92 | 0.00 | 0 | 0 | 90 |
|  | $\begin{aligned} & \text { SignPost_10ftNode } \\ & 459 \end{aligned}$ | 35.69 | -23.64 | 0.00 | 0 | 0 | 90 |
|  | $\begin{aligned} & \text { SignPost_10ftNode } \\ & 460 \end{aligned}$ | 24.01 | 42.80 | 0.00 | 0 | 0 | 0 |
|  | SignPost_10ftNode 461 | 24.29 | -18.12 | 0.00 | 0 | 0 | 0 |
|  | SignPost_10ftNode 462 | 29.56 | -18.12 | 0.00 | 0 | 0 | 0 |
|  | SignPost_10ftNode 463 | 29.27 | 41.80 | 0.00 | 0 | 0 | 180 |
|  | SignPost_10ftNode $464$ | 29.27 | 42.80 | 0.00 | 0 | 0 | 0 |
|  | $\begin{aligned} & \text { SignPost_10ftNode } \\ & 465 \end{aligned}$ | 24.29 | -17.01 | 0.00 | 0 | 0 | 0 |
|  | $\begin{aligned} & \text { SignPost_10ftNode } \\ & 466 \end{aligned}$ | 25.01 | 41.80 | 0.00 | 0 | 0 | 180 |
|  | SignPost_10ftNode 474 | 29.56 | -17.01 | 0.00 | 0 | 0 | 180 |

## Tips

- If you have the Vehicle Dynamics Blockset Interface for Unreal Engine 4 Projects support package, then you can modify this scene. In the Unreal Engine project file that comes with the support package, this scene is named LargeParkingLot.

For more details on customizing scenes, see "Customize 3D Scenes for Vehicle Dynamics Simulations".

## Version History

Introduced in R2018b
R2022a: Scene rendered using RoadRunner
Behavior changed in R2022a

Starting from R2022a, the Large Parking Lot scene in the Unreal Engine 3D environment is rendered using RoadRunner. As a result, the locations of scene objects, including cones and parked vehicles, are moved from their pre-R2022a locations.

## See Also

Simulation 3D Scene Configuration | Curved Road | Double Lane Change | Open Surface | Parking Lot | Straight Road | US City Block | US Highway | Virtual Mcity

## Topics

"Unreal Engine Simulation Environment Requirements and Limitations"
"How 3D Simulation for Vehicle Dynamics Blockset Works"
"Customize 3D Scenes for Vehicle Dynamics Simulations"

## Open Surface

Open surface 3D environment

## Description

The Open Surface scene contains a 3D environment of an open, black road surface. The scene is rendered using RoadRunner.


## Setup

To simulate a driving maneuver in this scene:
1 Add a Simulation 3D Scene Configuration block to your Simulink model.
2 In this block, set the Scene source parameter to Default Scenes.
3 Set the enabled Scene name parameter to Open surface.

## Layout

The scene contains line patterns that you can use for vehicle testing. The scene uses the world coordinate system to locate objects.


## Scene Dimensions

This table provides the scene corner locations in the world coordinate system. Dimensions are in $m$.

| Location | X | Y | Z |
| :--- | :--- | :--- | :--- |
| Scene - Bottom left | -1010.00 | 1010.00 | 0 |
| Scene - Top right | 1010.00 | -1010.00 | 0 |

## Recommended Starting Location

This table provides the recommended starting location for the vehicle in the world coordinate system. Dimensions are in m and deg.

| Recommended Starting Location |  |  |  |  |  |  | Roll | Pitch |
| :--- | :--- | :--- | :--- | :--- | :--- | :---: | :---: | :---: |
| $\mathbf{X}$ | $\mathbf{Y}$ | Z |  |  |  |  |  |  |
| $(\mathrm{m})$ |  |  |  |  |  |  |  |  |

## World Coordinate System

The 3D visualization environment uses a world coordinate system with axes that are fixed in the inertial reference frame.


| Axis | Description |
| :--- | :--- |
| $X$ | Forward direction of the vehicle <br> Roll $~-~ R i g h t-h a n d e d ~ r o t a t i o n ~ a b o u t ~$ <br> $X$ |
| $Y$ | Extends to the right of the vehicle, parallel to the ground plane <br> Pitch $~-~ R i g h t-h a n d e d ~ r o t a t i o n ~ a b o u t ~$ -axis |$|$| Extends upwards |
| :--- | :--- |
| Yaw - Left-handed rotation about Z-axis |

## Tips

- If you have the Vehicle Dynamics Blockset Interface for Unreal Engine 4 Projects support package, then you can modify this scene. In the Unreal Engine project file that comes with the support package, this scene is named BlackLake.

For more details on customizing scenes, see "Customize 3D Scenes for Vehicle Dynamics Simulations".

## Version History

Introduced in R2018b

## R2022b: Scene rendered using RoadRunner

Behavior changed in R2022b
Starting from R2022b, the Open Surface scene in the Unreal Engine 3D environment is rendered using RoadRunner. As a result, the locations of scene objects, including cones and parked vehicles, are moved from their pre-R2022b locations.

## See Also

Simulation 3D Scene Configuration | Curved Road | Double Lane Change | Large Parking Lot | Parking Lot | Straight Road | US City Block | US Highway | Virtual Mcity

## Topics

"Unreal Engine Simulation Environment Requirements and Limitations"
"How 3D Simulation for Vehicle Dynamics Blockset Works"
"Customize 3D Scenes for Vehicle Dynamics Simulations"

## Double Lane Change

Double lane change 3D environment

## Description

The Double Lane Change scene is a 3D environment of a straight road containing cones, traffic signs, and barrels. The cones are set up for a vehicle to perform a double lane change maneuver. The scene is rendered using RoadRunner.


## Setup

To simulate a driving maneuver in this scene:
1 Add a Simulation 3D Scene Configuration block to your Simulink model.
2 In this block, set the Scene source parameter to Default Scenes.
3 Set the enabled Scene name parameter to Double lane change.

## Layout

The scene uses the world coordinate system to locate objects. The active area of the scene contains the road.


## Scene Dimensions

This table provides the scene area corner locations in the world coordinate system. Dimensions are in m.

| Locations | X | Y | Z |
| :--- | :--- | :--- | :--- |
| Scene - Top left | -1008 | -1008 | 0 |
| Scene - Bottom right | 1008 | 1008 | 0 |
| Active area - Bottom left | -800 | 8.35 | 0 |

## Recommended Starting Location

This table provides the recommended starting location for the vehicle in the world coordinate system. Dimensions are in m and deg.

| Recommended Starting Location | Roll | Pitch | Yaw |
| :--- | :--- | :--- | :--- | :--- | :--- |
| $\mathbf{X}$ | $\mathbf{Y}$ | Z |  |
| $(\mathbf{m})$ | (m) |  |  |

## Lane Dimensions

This figure and table provides the lane dimensions, in m.


| Variable | Dimension (m) |
| :--- | :--- |
| $l w_{1}$ | 0.625 |
| $l w_{2}$ | 3.85 |
| $l w_{3}$ | 3.85 |
| $l w_{4}$ | 0.34 |
| $l w_{5}$ | 3.85 |
| $l w_{6}$ | 3.85 |
| $l w_{7}$ | 0.625 |
| $m l$ | 1.5 |
| $s$ | 4.5 |


| Variable | Dimension (m) |
| :--- | :--- |
| $m w_{w}$ | 0.125 |
| $m w_{y}$ | 0.125 |
| $W$ | 16.70 |

## World Coordinate System

The 3D visualization environment uses a world coordinate system with axes that are fixed in the inertial reference frame.


| Axis | Description |
| :--- | :--- |
| $X$ | Forward direction of the vehicle <br> Roll $~-~ R i g h t-h a n d e d ~ r o t a t i o n ~ a b o u t ~$ <br> $X$ |
| $Y$ | Extends to the right of the vehicle, parallel to the ground plane <br> Pitch $~-~ R i g h t-h a n d e d ~ r o t a t i o n ~ a b o u t ~$ -axis |$|$| Extends upwards |
| :--- | :--- |
| Yaw - Left-handed rotation about $Z$-axis |

## Objects

## Traffic Signs



## Locations

This table provides the object names and locations in the world coordinate system. Dimensions are in m.

| Object | Unreal Editor Name | Location |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \mathrm{X} \\ & (\mathrm{~m}) \end{aligned}$ | $\begin{aligned} & \mathbf{Y} \\ & (\mathrm{m}) \end{aligned}$ | $\begin{aligned} & \mathrm{Z} \\ & (\mathrm{~m}) \end{aligned}$ | $\begin{aligned} & \text { Roll } \\ & \text { (deg) } \end{aligned}$ | Pitch <br> (deg) | $\begin{aligned} & \text { Yaw } \\ & \text { (deg) } \end{aligned}$ |
| Traffic sign | $\begin{aligned} & \hline \text { Sign_R1-1_ } \\ & \text { ONode } \end{aligned}$ | 248.80 | -10.00 | 0 | 0 | 0 | 0 |
|  | Sign R1-1 0Node 75 | 248.80 | 10.00 | 0 |  |  |  |

## Traffic Signal Light



In the Unreal Editor, the Double Lane Change scene has a Sim3DGetInteger actor with signal name TrafficLight1. You can use it with the Simulation 3D Message Set block to control the traffic signal light color.

## Locations

This table provides the object names and locations in the world coordinate system. Dimensions are in m.

| Object | Unreal <br> Editor <br> Name | Location <br> (m) | Y <br> (m) | Z <br> (m) | Roll <br> (deg) | Pitch <br> (deg) | Yaw <br> (deg) |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Traffic <br> signal light | SM_Traffic <br> LightsSide <br> Only | 5.43 | 9.00 | 0 | 0 | 0 | $180.00^{\circ}$ |

## Barrels



## Locations

This table provides the object names and locations in the world coordinate system. Dimensions are in m.

| Object | Unreal <br> Editor Name | Location <br> $\mathbf{X}$ <br> $\mathbf{( m )}$ | $\mathbf{Y}$ <br> $(\mathbf{m})$ | $\mathbf{Z}$ <br> $(\mathbf{m})$ | Roll <br> $(\mathbf{d e g})$ | Pitch <br> (deg) | Yaw <br> (deg) |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Barrels | Drum01Node | 252.70 | 7.50 | 0 | 0 | 0 | $180.00^{\circ}$ |
|  | Drum01Node <br> 67 | 252.70 | 5.35 | 0 | 0 | 0 | 0 |
|  | Drum01Node <br> 68 | 252.70 | 3.20 | 0 | 0 | 0 | 0 |
| Drum01Node <br> 69 | 252.70 | -1.05 | 0 | 0 | 0 | 0 |  |
| Drum01Node <br> 70 | 252.70 | -1.1 | 0 | 0 | 0 | 0 |  |
| Drum01Node <br> 71 | 252.70 | -3.25 | 0 | 0 | 0 | 0 |  |
| Drum01Node <br> 72 | 252.70 | -5.40 | 0 | 0 | 0 | 0 |  |
| Drum01Node <br> 73 | 252.70 | -7.55 | 0 | 0 | 0 | 0 |  |

## Tips

- If you have the Vehicle Dynamics Blockset Interface for Unreal Engine 4 Projects support package, then you can modify this scene. In the Unreal Engine project file that comes with the support package, this scene is named DblLnChng.

For more details on customizing scenes, see "Customize 3D Scenes for Vehicle Dynamics Simulations".

## Version History

Introduced in R2018b
R2022b: Scene rendered using RoadRunner
Behavior changed in R2022b
Starting from R2022b, the Double Lane Change scene in the Unreal Engine 3D environment is rendered using RoadRunner. As a result, the locations of scene objects, including cones and parked vehicles, are moved from their pre-R2022b locations.

## See Also

Simulation 3D Scene Configuration | Curved Road | Open Surface | Large Parking Lot | Parking Lot | Straight Road | US City Block | US Highway | Virtual Mcity

## Topics

"Send and Receive Double-Lane Change Scene Data"
"Unreal Engine Simulation Environment Requirements and Limitations"
"How 3D Simulation for Vehicle Dynamics Blockset Works"
"Customize 3D Scenes for Vehicle Dynamics Simulations"

## US City Block

US city block 3D environment

## Description

The US City Block scene is a 3D environment of a US city block that contains 15 intersections and 30 traffic lights. The scene is rendered using RoadRunner.


## Setup

To simulate a driving maneuver in this scene:
1 Add a Simulation 3D Scene Configuration block to your Simulink model.
2 In this block, set the Scene source parameter to Default Scenes.
3 Set the enabled Scene name parameter to US city block.

## Layout

The scene uses the world coordinate system to locate objects.


## Scene Dimensions

This table provides the scene area corner locations in the world coordinate system. Dimensions are in m.

| Locations | X <br> $\mathbf{( m )}$ | Y <br> $(\mathbf{m})$ | Z <br> $(\mathbf{m})$ |
| :--- | :--- | :--- | :--- |
| Scene - Top left | -1020 | -1020 | 0 |
| Scene - Bottom right | 1020 | 1020 | 0 |
| Active area - Bottom left | -240.77 | 151.67 | 0 |

## Recommended Starting Location

This table provides the recommended starting location for the vehicle in the world coordinate system. Dimensions are in m and deg.

| Recommended Starting Location |  |  |  |  |  |  | Roll | Pitch |
| :--- | :--- | :--- | :--- | :--- | :--- | :---: | :---: | :---: |
| $\mathbf{X}$ | $\mathbf{Y}$ | $\mathbf{Z}$ |  |  |  |  |  |  |
| $\mathbf{( m )}$ | 1.65 | (m) <br> (deg) | Yaw <br> (deg) | (deg) |  |  |  |  |
| -125.19 | -0.04 in <br> vehicle Z-down <br> coordinate <br> system | 0 | 0 | 0 |  |  |  |  |

## Intersections

The US city block scene has 15 intersections, as indicated in this diagram.


This table provides the intersection locations in the world coordinate system. Dimensions are in $m$.

| Intersection | Center Location |  |  |
| :---: | :---: | :---: | :---: |
|  | X | Y | Z |
|  | (m) | (m) | (m) |
| 1 | -202.60 | -108 | . 01 |


| Intersection | Center Location |  |  |
| :--- | :--- | :--- | :--- |
|  | $\mathbf{X}$ |  |  |
| (m) |  |  |  |$)$

## Lane Dimensions

The scene contains three types of roads.

## Road Type 1

This figure and table provides the road type 1 lane dimensions, in $m$.


| Variable | Dimension (m) |
| :--- | :--- |
| $l w_{1}$ | 0.65 |
| $l w_{2}$ | 3.85 |
| $l w_{3}$ | 3.85 |
| $l w_{4}$ | 0.65 |
| $m l$ | 1.5 |
| $s$ | 4.5 |
| $m w$ | 0.125 |
| $W$ | 9 |

## Road Type 2

This figure and table provides the road type 2 lane dimensions, in $m$.


| Variable | Dimension (m) |
| :--- | :--- |
| $l w_{1}$ | 0.73 |
| $l w_{2}$ | 3.77 |
| $l w_{3}$ | 3.77 |
| $l w_{4}$ | 4.5 |
| $l w_{5}$ | 0.73 |
| $m l$ | 1.5 |
| $s$ | 4.5 |
| $m w$ | 0.125 |
| $W$ | 13.5 |

## Road Type 3

This figure and table provides the road type 3 lane dimensions, in $m$.


| Variable | Dimension (m) |
| :--- | :--- |
| $l w_{1}$ | 0.65 |
| $l w_{2}$ | 3.85 |
| $l w_{3}$ | 3.85 |
| $l w_{4}$ | 3.15 |
| $m l$ | 1.5 |
| $s$ | 4.5 |
| $m w$ | 0.125 |
| $W$ | 11.5 |

## World Coordinate System

The 3D visualization environment uses a world coordinate system with axes that are fixed in the inertial reference frame.


| Axis | Description |
| :--- | :--- |
| $X$ | Forward direction of the vehicle <br> Roll $~-~ R i g h t-h a n d e d ~ r o t a t i o n ~ a b o u t ~$ <br> $X$ |
| $Y$ | Extends to the right of the vehicle, parallel to the ground plane <br> Pitch $~-~ R i g h t-h a n d e d ~ r o t a t i o n ~ a b o u t ~$ -axis |, | Extends upwards |
| :--- |
| Yaw - Left-handed rotation about Z-axis |

## Objects

## Barrier



## Locations

This table provides the object names and locations in the world coordinate system. Dimensions are in m.

| Unreal Engine Editor Name |  | Location |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | X | Y | Z | Roll | Pitch | Yaw |
|  | PropNode25 52 | 69.71 | 150.15 | 0.09 | 0 | 0 | 0 |
|  | PropNode25 $54$ | 74.43 | 150.15 | 0.01 | 0 | 0 | 0 |
|  | PropNode25 59 | 168.36 | 150.15 | 0.01 | 0 | 0 | 0 |
|  | $\begin{aligned} & \text { PropNode25 } \\ & 94 \end{aligned}$ | -110.71 | -147.37 | 0.01 | 0 | 0 | 0 |
|  | PropNode25 $38$ | -191.29 | 150.15 | 0.08 | 0 | 0 | 0 |
|  | PropNode25 27 | -192.46 | -147.40 | 0.03 | 0 | 0 | 0 |
|  | ```PropNode25 92``` | -102.49 | -147.40 | 0.04 | 0 | 0 | 0 |
|  | PropNode25 68 | 197.05 | 1.98 | 0.01 | 0 | 0 | -90 ${ }^{\circ}$ |
|  | $\begin{aligned} & \hline \text { PropNode25 } \\ & 24 \end{aligned}$ | -204.50 | -147.40 | 0.01 | 0 | 0 | 0 |
|  | PropNode25 $37$ | -240.00 | -120.63 | 0.07 | 0 | 0 | -90 ${ }^{\circ}$ |
|  | PropNode25 $71$ | 197.05 | -101.32 | 0.06 | 0 | 0 | -90 ${ }^{\circ}$ |
|  | PropNode25 86 | -16.60 | -147.40 | 0.01 | 0 | 0 | 0 |
|  | $\begin{aligned} & \text { PropNode25 } \\ & 40 \end{aligned}$ | -182.61 | 150.15 | 0.01 | 0 | 0 | 0 |
|  | PropNode25 $25$ | -200.71 | -147.40 | 0.01 | 0 | 0 | 0 |
|  | $\begin{aligned} & \text { PropNode25 } \\ & 31 \end{aligned}$ | -240.00 | 6.67 | 0.12 | 0 | 0 | -90 ${ }^{\circ}$ |
|  | $\begin{aligned} & \text { PropNode25 } \\ & 30 \end{aligned}$ | -240.00 | 1.93 | 0.01 | 0 | 0 | -90 ${ }^{\circ}$ |
|  | PropNode25 88 | -29.31 | -147.40 | 0.04 | 0 | 0 | 0 |
|  | PropNode25 95 | -114.52 | -147.40 | 0.01 | 0 | 0 | 0 |
|  | PropNode25 84 | -24.42 | -147.40 | 0.01 | 0 | 0 | 0 |
|  | $\begin{aligned} & \hline \text { PropNode25 } \\ & 29 \end{aligned}$ | -240.00 | -1.82 | 0.01 | 0 | 0 | -90 ${ }^{\circ}$ |


| Unreal Engine Editor Name | Location |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | X | Y | Z | Roll | Pitch | Yaw |
| PropNode25 56 | 159.73 | 150.15 | 0.11 | 0 | 0 | 0 |
| $\begin{aligned} & \text { PropNode25 } \\ & 69 \end{aligned}$ | 197.05 | 5.43 | 0.01 | 0 | 0 | -90 ${ }^{\circ}$ |
| PropNode25 <br> 74 | 164.46 | -147.40 | 0.11 | 0 | 0 | $-180^{\circ}$ |
| $\begin{aligned} & \text { PropNode25 } \\ & 26 \end{aligned}$ | -195.90 | -105.25 | 0 | 0 | 0 | 0 |
| $\begin{aligned} & \text { PropNode25 } \\ & 61 \end{aligned}$ | 197.05 | 114.37 | 0.01 | 0 | 0 | -90 ${ }^{\circ}$ |
| $\begin{aligned} & \text { PropNode25 } \\ & 75 \end{aligned}$ | 168.39 | -147.40 | 0.01 | 0 | 0 | 0 |
| PropNode25 $49$ | -16.49 | 150.15 | 0.11 | 0 | 0 | 0 |
| $\begin{array}{\|l} \text { PropNode25 } \\ 81 \end{array}$ | 82.13 | -147.40 | 0.03 | 0 | 0 | 0 |
| $\begin{aligned} & \text { PropNode25 } \\ & 43 \end{aligned}$ | 119.29 | 150.15 | 0.13 | 0 | 0 | 0 |
| ```PropNode25 66``` | 197.05 | 12.11 | 0.05 | 0 | 0 | -90 ${ }^{\circ}$ |
| PropNode25 $93$ | -105.93 | -147.40 | 0.10 | 0 | 0 | 0 |
| $\begin{aligned} & \hline \text { PropNode25 } \\ & 23 \\ & \hline \end{aligned}$ | -208.80 | -147.40 | 0.13 | 0 | 0 | 0 |
| PropNode25 $77$ | 156.30 | -147.40 | 0.03 | 0 | 0 | 0 |
| PropNode25 $90$ | -7.98 | -147.40 | 0.03 | 0 | 0 | 0 |
| PropNode25 $82$ | 65.37 | -147.40 | 0.12 | 0 | 0 | 0 |
| $\begin{aligned} & \text { PropNode25 } \\ & 70 \end{aligned}$ | 197.05 | -114.66 | 0.13 | 0 | 0 | -90 ${ }^{\circ}$ |
| PropNode25 $50$ | -24.53 | 150.15 | 0.01 | 0 | 0 | 0 |
| $\begin{aligned} & \text { PropNode25 } \\ & 48 \end{aligned}$ | -29.31 | 150.15 | 0.06 | 0 | 0 | 0 |
| $\begin{aligned} & \text { PropNode25 } \\ & 67 \end{aligned}$ | 197.05 | -1.90 | 0.01 | 0 | 0 | $-90^{\circ}$ |
| PropNode25 $57$ | 173.10 | 150.15 | 0.12 | 0 | 0 | 0 |


| Unreal Engine Editor Name | Location |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | X | Y | Z | Roll | Pitch | Yaw |
| PropNode25 53 | 83.12 | 150.15 | 0.03 | 0 | 0 | 0 |
| PropNode25 $97$ | -122.75 | -147.37 | 0.04 | 0 | 0 | 0 |
| ```PropNode25 55``` | 78.37 | 150.15 | 0.01 | 0 | 0 | 0 |
| PropNode25 $91$ | -99.03 | -147.40 | 0.04 | 0 | 0 | 0 |
| PropNode25 $60$ | 197.05 | 119.24 | 0.12 | 0 | 0 | -90 ${ }^{\circ}$ |
| PropNode25 $73$ | 197.05 | -106.00 | 0.01 | 0 | 0 | -90 ${ }^{\circ}$ |
| $\begin{aligned} & \text { PropNode25 } \\ & 47 \end{aligned}$ | -110.71 | 150.15 | 0.01 | 0 | 0 |  |
| $\begin{aligned} & \text { PropNode25 } \\ & 33 \end{aligned}$ | -240.00 | 103.96 | 0.04 | 0 | 0 | -90 ${ }^{\circ}$ |
| $\begin{aligned} & \text { PropNode25 } \\ & 34 \end{aligned}$ | -240.00 | 108.62 | 0.01 | 0 | 0 | $-90^{\circ}$ |
| ```PropNode25 79``` | 73.95 | -147.40 | 0.01 | 0 | 0 |  |
| PropNode25 64 | 197.05 | -6.67 | 0.07 | 0 | 0 | -90 ${ }^{\circ}$ |
| PropNode25 $89$ | -32.70 | -147.40 | 0.04 | 0 | 0 |  |
| $\begin{aligned} & \text { PropNode25 } \\ & 20 \end{aligned}$ | -32.70 | -109.92 | 0.01 | 0 | 0 | -90 ${ }^{\circ}$ |
| PropNode25 $62$ | 197.05 | 110.62 | 0.01 | 0 | 0 | -90 ${ }^{\circ}$ |
| $\begin{aligned} & \text { PropNode25 } \\ & 32 \end{aligned}$ | -240.00 | 100.81 | 0.04 | 0 | 0 | -90 ${ }^{\circ}$ |
| PropNode25 $63$ | 197.05 | 105.79 | 0.07 | 0 | 0 | -90 ${ }^{\circ}$ |
| $\begin{aligned} & \text { PropNode25 } \\ & 22 \end{aligned}$ | -240.00 | 101.32 | 0.03 | 0 | 0 | -90 ${ }^{\circ}$ |
| PropNode25 $45$ | -102.57 | 150.15 | 0.03 | 0 | 0 | 0 |
| PropNode25 $41$ | -177.93 | 150.15 | 0.04 | 0 | 0 | 0 |
| PropNode25 $87$ | -11.39 | 147. 40 | 0.12 | 0 | 0 | 0 |


| Unreal Engine Editor Name | Location |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | X | Y | Z | Roll | Pitch | Yaw |
| PropNode25 <br> 58 | 164.52 | 150.15 | 0.12 | 0 | 0 | 0 |
| $\begin{aligned} & \text { PropNode25 } \\ & 46 \end{aligned}$ | -114.50 | 150.15 | 0.01 | 0 | 0 | 0 |
| PropNode25 <br> 65 | -197.05 | 8.89 | 0.11 | 0 | 0 | $-90^{\circ}$ |
| $\begin{aligned} & \text { PropNode25 } \\ & 72 \end{aligned}$ | 197.05 | -109.93 | 0.01 | 0 | 0 | $-90^{\circ}$ |
| $\begin{aligned} & \text { PropNode25 } \\ & 21 \end{aligned}$ | -240.00 | -106.09 | 0.01 | 0 | 0 | $-90^{\circ}$ |
| $\begin{aligned} & \text { PropNode25 } \\ & 36 \end{aligned}$ | -240.00 | 117.19 | 0.13 | 0 | 0 | -90 ${ }^{\circ}$ |
| $\begin{aligned} & \text { PropNode25 } \\ & 28 \end{aligned}$ | -240.00 | -6.67 | 0.07 | 0 | 0 | -90 ${ }^{\circ}$ |
| $\begin{aligned} & \text { PropNode25 } \\ & 83 \end{aligned}$ | 62.05 | -147.40 | 0.04 | 0 | 0 | 0 |
| $\begin{aligned} & \text { PropNode25 } \\ & 44 \end{aligned}$ | -105.91 | 150.15 | 0.10 | 0 | 0 | 0 |
| $\begin{aligned} & \text { PropNode27 } \\ & 94 \end{aligned}$ | 159.70 | -147.40 | 0.11 | 0 | 0 | 0 |
| PropNode25 85 | -20.74 | -147.40 | 0.01 | 0 | 0 | 0 |
| PropNode25 76 | 173.09 | -147.40 | 0.12 | 0 | 0 | 0 |
| PropNode25 $35$ | -240.00 | 112.41 | 0.01 | 0 | 0 | -90 ${ }^{\circ}$ |
| PropNode25 $51$ | -20.68 | 150.15 | 0.01 | 0 | 0 | 0 |
| $\begin{aligned} & \text { PropNode25 } \\ & 78 \end{aligned}$ | 70.13 | -147.40 | 0.01 | 0 | 0 | 0 |
| PropNode25 $96$ | -119.32 | -147.41 | 0.13 | 0 | 0 | 0 |
| PropNode25 $80$ | 78.73 | -147.40 | 0.11 | 0 | 0 | 0 |
| $\begin{aligned} & \text { PropNode25 } \\ & 42 \end{aligned}$ | -174.47 | -150.15 | 0.04 | 0 | 0 | 0 |

## Traffic Lights



The US City Scene contains 30 traffic lights, two at each of the 15 intersections. Each intersection has a traffic light group. If you have the "Customize 3D Scenes for Vehicle Dynamics Simulations" for customizing scenes, you can control the timing of the traffic lights.

## Locations

This table provides the traffic light names and locations in the world coordinate system. Dimensions are in m . Only one of the traffic lights in the group can be green at a time. The traffic lights are green for 10 s and yellow for 3 s . At the start of the simulation, the first traffic lights in the group are green (for example, SM_TrafficLights1_3 and SM_TrafficLights2_3). The second lights in the group are red (for example, SM_TrafficLights1_4 and SM_TrafficLights2_4).

| Intersect ion | Unreal Engine Editor Name |  | Location |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Traffic Light Group | Traffic Light | X | Y | Z | Roll | Pitch | Yaw |
| 1 | TrafficLig htGroup | $\begin{aligned} & \text { SM_Tr } \\ & \text { affic } \\ & \text { Light } \\ & \text { s1_3 } \end{aligned}$ | -196.55 | -100.65 | 0 | 0 | 0 | $90^{\circ}$ |
|  |  | $\begin{aligned} & \text { SM_Tr } \\ & \text { affic } \\ & \text { Light } \\ & \text { s1_4 } \end{aligned}$ | -210.20 | -113.40 | 0 | 0 | 0 | 0 |
| 2 | TrafficLig htGroup2 | $\begin{aligned} & \text { SM_Tr } \\ & \text { affic } \\ & \text { Light } \\ & \text { s2_3 } \end{aligned}$ | -106.35 | 98.35 | 0 | 0 | 0 | -90 ${ }^{\circ}$ |
|  |  | $\begin{aligned} & \text { SM_Tr } \\ & \text { affic } \\ & \text { Light } \\ & \text { s2_4 } \end{aligned}$ | -120.40 | -113.50 | 0 | 0 | 0 | 0 |
| 3 | TrafficLig htGroup3 | $\begin{aligned} & \text { SM_Tr } \\ & \text { affic } \\ & \text { Light } \\ & \text { s3_1 } \end{aligned}$ | -13.10 | -116.20 | 0.2 | 0 | 0 | $90^{\circ}$ |


| Intersect ion | Unreal Engine Editor Name |  | Location |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Traffic Light Group | Traffic Light | X | Y | Z | Roll | Pitch | Yaw |
|  |  | $\begin{aligned} & \text { SM_Tr } \\ & \text { affic } \\ & \text { Light } \\ & \text { s3_4 } \end{aligned}$ | -30.60 | -113.80 | 0 | 0 | 0 | 0 |
| 4 | $\begin{aligned} & \text { TrafficLig } \\ & \text { htGroup4 } \end{aligned}$ | $\begin{aligned} & \text { SM_Tr } \\ & \text { affic } \\ & \text { Light } \\ & \text { s4_3 } \end{aligned}$ | 71.40 | -100.30 | 0 | 0 | 0 | $-100^{\circ}$ |
|  |  | $\begin{aligned} & \text { SM_Tr } \\ & \text { affic } \\ & \text { Light } \\ & \text { s4_4 } \end{aligned}$ | 64.80 | -113.0 | 0 | 0 | 0 | 0 |
| 5 | TrafficLig htGroup5 | $\begin{aligned} & \text { SM_Tr } \\ & \text { affic } \\ & \text { Light } \\ & \text { s5_1 } \end{aligned}$ | 171.50 | -115.70 | 0 | 0 | 0 | $90^{\circ}$ |
|  |  | $\begin{aligned} & \text { SM_Tr } \\ & \text { affic } \\ & \text { Light } \\ & \text { s5_4 } \end{aligned}$ | 157.40 | -113.50 | 0 | 0 | 0 | 0 |
| 6 | TrafficLig htGroup6 | $\begin{aligned} & \text { SM_Tr } \\ & \text { affic } \\ & \text { Light } \\ & \text { s6_2 } \end{aligned}$ | -177.30 | 5.70 | 0 | 0 | 0 | $180^{\circ}$ |
|  |  | $\begin{aligned} & \text { SM_Tr } \\ & \text { affic } \\ & \text { Light } \\ & \text { s6_3 } \end{aligned}$ | -189.60 | 7.40 | 0 | 0 | 0 | -90 ${ }^{\circ}$ |
| 7 | TrafficLig htGroup7 | $\begin{aligned} & \text { SM_Tr } \\ & \text { affic } \\ & \text { Light } \\ & \text { s7_2 } \end{aligned}$ | -105.20 | 5.50 | 0 | 0 | 0 | $180^{\circ}$ |
|  |  | SM Tr affic <br> Light <br> s7_3 | -117.80 | 7.70 | 0.2 | 0 | 0 | -90 ${ }^{\circ}$ |
| 8 | TrafficLig htGroup8 | $\begin{aligned} & \text { SM_Tr } \\ & \text { affic } \\ & \text { Light } \\ & \text { s8_1 } \end{aligned}$ | -13.10 | -7.60 | 0.1 | 0 | 0 | $90^{\circ}$ |


| Intersect ion | Unreal Engine Editor Name |  | Location |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Traffic Light Group | Traffic Light | X | Y | Z | Roll | Pitch | Yaw |
|  |  | $\begin{aligned} & \text { SM_Tr } \\ & \text { affic } \\ & \text { Light } \\ & \text { s8_2 } \end{aligned}$ | -10.90 | 5.60 | 0 | 0 | 0 | $180^{\circ}$ |
| 9 | TrafficLig htGroup9 | $\begin{aligned} & \text { SM_Tr } \\ & \text { affic } \\ & \text { Light } \\ & \text { s9_2 } \end{aligned}$ | 85.90 | 7.60 | 0.2 | 0 | 0 | $180^{\circ}$ |
|  |  | $\begin{aligned} & \text { SM_Tr } \\ & \text { affic } \\ & \text { Light } \\ & \text { s9_3 } \end{aligned}$ | 70.90 | 9.20 | 0 | 0 | 0 | $-90^{\circ}$ |
| 10 | TrafficLig htGroup10 | $\begin{aligned} & \text { SM_Tr } \\ & \text { affic } \\ & \text { Light } \\ & \text { s10_1 } \end{aligned}$ | 172.10 | -7.70 | 0 | 0 | 0 | $90^{\circ}$ |
|  |  | $\begin{aligned} & \text { SM_Tr } \\ & \text { affic } \\ & \text { Light } \\ & \text { s10_2 } \end{aligned}$ | 173.70 | 7.50 | 0 | 0 | 0 | $180^{\circ}$ |
| 11 | TrafficLig htGroupl1 | $\begin{aligned} & \text { SM_Tr } \\ & \text { affic } \\ & \text { Light } \\ & \text { s11_3 } \end{aligned}$ | -189.80 | 118.45 | 0 | 0 | 0 | $-90^{\circ}$ |
|  |  | $\begin{aligned} & \text { SM_Tr } \\ & \text { affic } \\ & \text { Light } \\ & \text { s11_4 } \end{aligned}$ | -191.05 | 104.55 | 0 | 0 | 0 | 0 |
| 12 | TrafficLig htGroup12 | $\begin{aligned} & \text { SM_Tr } \\ & \text { affic } \\ & \text { Light } \\ & \text { s12_3 } \end{aligned}$ | -117.60 | 117.60 | 0 | 0 | 0 | $-90^{\circ}$ |
|  |  | $\begin{aligned} & \hline \text { SM_Tr } \\ & \text { affic } \\ & \text { Light } \\ & \text { s12_4 } \end{aligned}$ | -120.50 | 105.40 | 0 | 0 | 0 | 0 |
| 13 | TrafficLig htGroup13 | $\begin{aligned} & \text { SM_Tr } \\ & \text { affic } \\ & \text { Light } \\ & \text { s13_1 } \\ & \hline \end{aligned}$ | -12.80 | 102.50 | 0 | 0 | 0 | $90^{\circ}$ |


| Intersect ion | Unreal Engine Editor Name |  | Location |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Traffic Light Group | Traffic Light | X | Y | Z | Roll | Pitch | Yaw |
|  |  | $\begin{aligned} & \text { SM_Tr } \\ & \text { affic } \\ & \text { Light } \\ & \text { s13_4 } \end{aligned}$ | -30.50 | 105.30 | 0 | 0 | 0 | 0 |
| 14 | TrafficLig htGroup14 | $\begin{aligned} & \text { SM_Tr } \\ & \text { affic } \\ & \text { Light } \\ & \text { s14_3 } \end{aligned}$ | 70.90 | 118.70 | 0 | 0 | 0 | -90 ${ }^{\circ}$ |
|  |  | $\begin{aligned} & \text { SM_Tr } \\ & \text { affic } \\ & \text { Light } \\ & \text { s14_4 } \end{aligned}$ | 69.30 | 105.30 | 0 | 0 | 0 | 0 |
| 15 | TrafficLig htGroup15 | $\begin{aligned} & \text { SM_Tr } \\ & \text { affic } \\ & \text { Light } \\ & \text { s15_1 } \end{aligned}$ | 171.40 | 105.20 | 0 | 0 | 0 | $90^{\circ}$ |
|  |  | $\begin{aligned} & \text { SM_Tr } \\ & \text { affic } \\ & \text { Light } \\ & \text { s15_4 } \end{aligned}$ | 158.40 | 107.20 | 0 | 0 | 0 | 0 |

## Tips

- If you have the Vehicle Dynamics Blockset Interface for Unreal Engine 4 Projects support package, then you can modify this scene. In the Unreal Engine project file that comes with the support package, this scene is named USCityBlock.

For more details on customizing scenes, see "Customize 3D Scenes for Vehicle Dynamics Simulations".

## Version History

Introduced in R2018b

## R2022b: Scene rendered using RoadRunner

Behavior changed in R2022b
Starting from R2022b, the US City Block scene in the Unreal Engine 3D environment is rendered using RoadRunner. As a result, the locations of scene objects, including cones and parked vehicles, are moved from their pre-R2022b locations.

## See Also

Simulation 3D Scene Configuration | Curved Road | Double Lane Change | Open Surface | Large Parking Lot | Parking Lot | Straight Road | Virtual Mcity | US Highway

## Topics

"Unreal Engine Simulation Environment Requirements and Limitations"
"How 3D Simulation for Vehicle Dynamics Blockset Works"
"Customize 3D Scenes for Vehicle Dynamics Simulations"

## US Highway

US highway 3D environment

## Description

The US Highway scene is a 3D environment of a US highway that contains barriers, cones, and traffic signs. The scene is rendered using RoadRunner.


## Setup

To simulate a driving maneuver in this scene:
1 Add a Simulation 3D Scene Configuration block to your Simulink model.
2 In this block, set the Scene source parameter to Default Scenes.
3 Set the enabled Scene name parameter to US highway.

## Layout

The scene uses the world coordinate system to locate objects. The active area of the scene contains the road.


## Scene Dimensions

This table provides the scene area corner locations in the world coordinate system. Dimensions are in m.

| Locations | $\mathbf{X}$ | $\mathbf{Y}$ | $\mathbf{Z}$ |
| :--- | :--- | :--- | :--- |
|  | $(\mathbf{m})$ | $(\mathbf{m})$ | $(\mathbf{m})$ |
| Scene - Top left | -5080 | -5080 | 1 |
| Scene - Bottom right | 5080 | 5080 | 1 |
| Active area - Bottom left | 2867.41 | 3169.93 | 1 |

## Recommended Starting Location

This table provides the recommended starting location for the vehicle in the world coordinate system. Dimensions are in m and deg.

| Recommended Starting Location |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :---: |
| $\mathbf{X}$ | $\mathbf{Y}$ | $\mathbf{Z}$ | Roll |  |  |  |
| (m) | 2617.00 | (deg) | Pitch <br> (deg) | (deg) |  |  |
| 3592.00 | (d.00 <br> -1.00 in <br> vehicle Z-down <br> coordinate <br> system | 0 | 0 | 0 |  |  |

## Lane Dimensions

This figure and table provides the lane dimensions, in m .


| Variable | Dimension (m) |
| :--- | :--- |
| $l w_{1}$ | 0.625 |
| $l w_{2}$ | 3.85 |
| $l w_{3}$ | 3.85 |
| $l w_{4}$ | 0.625 |
| $m l$ | 1.5 |
| $s$ | 4.5 |
| $m w$ | 0.125 |
| $W$ | 8.95 |

## World Coordinate System

The 3D visualization environment uses a world coordinate system with axes that are fixed in the inertial reference frame.


| Axis | Description |
| :--- | :--- |
| $X$ | Forward direction of the vehicle |
| Roll - Right-handed rotation about $X$-axis |  |\(\left|\begin{array}{ll|}\hline Extends to the right of the vehicle, parallel to the ground plane <br>


Pitch - Right-handed rotation about Y -axis\end{array}\right|\)| Extends upwards |  |
| :--- | :--- |
| $Z$ | $Y a w ~-~ L e f t-h a n d e d ~ r o t a t i o n ~ a b o u t ~ Z-a x i s ~$ |,

## Objects

## Barrier



## Locations

This table provides the object names and locations in the world coordinate system. Dimensions are in m.

| Unreal Engine Editor Name |  | Location |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | X | Y | Z | Roll | Pitch | Yaw |
|  |  | (m) | (m) | (m) | (deg) | (deg) | (deg) |
| f_shaped barrier_m esh_ | PropNode | 2866.45 | 2609.80 | 1.01 | 0 | 0 | -90 ${ }^{\circ}$ |
|  | PropNode99 <br> 14 | 2866.45 | 2593.70 | 1.01 |  |  |  |
|  | PropNode99 $12$ | 2866.45 | 2606.03 | 1.01 |  |  |  |
|  | PropNode99 $13$ | 2866.45 | 2597.61 | 1.01 |  |  |  |

## Cones



## Locations

This table provides the cone tag names and locations in the world coordinate system. Dimensions are in $m$.

| Unreal Engine Editor Name |  | Location |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | X | Y | Z | Roll | Pitch | Yaw |
|  |  | (m) | (m) | (m) | (deg) | (deg) | (deg) |
| $\begin{aligned} & \text { TrafficCo } \\ & \text { ne01_ } \end{aligned}$ | $\begin{aligned} & \text { PropNode49 } \\ & 70 \end{aligned}$ | 3022.85 | 2599.90 | 1 | 0 | 0 | 0 |
|  | PropNode49 $69$ | 3022.85 | 2599.10 | 1 |  |  |  |
|  | PropNode49 $68$ | 3022.85 | 2598.25 | 1 |  |  |  |
|  | PropNode49 $67$ | 3022.85 | 2597.30 | 1 |  |  |  |
|  | PropNode49 66 | 3022.85 | 2596.50 | 1 |  |  |  |
|  | PropNode49 65 | 3022.85 | 2595.65 | 1 |  |  |  |
|  | PropNode49 <br> 64 | 3022.85 | 2594.70 | 1 |  |  |  |
|  | PropNode49 $63$ | 3022.85 | 2593.90 | 1 |  |  |  |
|  | PropNode49 $62$ | 3022.85 | 2593.05 | 1 |  |  |  |
|  | $\begin{aligned} & \text { PropNode49 } \\ & 61 \end{aligned}$ | 3022.85 | 2592.20 | 1 |  |  |  |
|  | PropNode | 3022.85 | 2591.40 | 1 |  |  |  |

## Traffic Signs



## Locations

This table provides the traffic sign tag names and locations in the world coordinate system. Dimensions are in m.

| Unreal Engine Editor <br> Name | Location <br> X <br> (m) |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |

## Tips

- If you have the Vehicle Dynamics Blockset Interface for Unreal Engine 4 Projects support package, then you can modify this scene. In the Unreal Engine project file that comes with the support package, this scene is named USHighway.

For more details on customizing scenes, see "Customize 3D Scenes for Vehicle Dynamics Simulations".

## Version History

Introduced in R2018b

## R2022b: Scene rendered using RoadRunner

Behavior changed in R2022b
Starting from R2022b, the US Highway scene in the Unreal Engine 3D environment is rendered using RoadRunner. As a result, the locations of scene objects, including cones and parked vehicles, are moved from their pre-R2022b locations.

## See Also

Simulation 3D Scene Configuration | Curved Road | Double Lane Change | Open Surface | Large Parking Lot | Parking Lot | Straight Road | US City Block | Virtual Mcity

Topics
"Unreal Engine Simulation Environment Requirements and Limitations"
"How 3D Simulation for Vehicle Dynamics Blockset Works"
"Customize 3D Scenes for Vehicle Dynamics Simulations"

## Virtual Mcity

Virtual Mcity 3D environment

## Description

The Virtual Mcity scene is a 3D environment containing a virtual representation of Mcity ${ }^{\circledR}$, which is a testing ground belonging to the University of Michigan. For more details, see Mcity Test Facility.

The scene is rendered using the Unreal Engine from Epic Games.


## Setup

To simulate a driving maneuver in this scene:
1 Add a Simulation 3D Scene Configuration block to your Simulink model.
2 In this block, set the Scene source parameter to Default Scenes.
3 Set the enabled Scene name parameter to Virtual Mcity.

## Layout

The scene uses the world coordinate system to locate objects. The active area of the scene contains the road.


## Scene Dimensions

This table provides the scene area corner locations in the world coordinate system. Dimensions are in m.
$\left.\begin{array}{|l|l|l|l|}\hline \text { Locations } & \mathbf{X} & \mathbf{Y} \\ \mathbf{( m )}\end{array}\right)$

## Recommended Starting Location

This table provides the recommended starting location for the vehicle in the world coordinate system. Dimensions are in m and deg.

| Recommended Starting Location |
| :--- | :--- |
| $\mathbf{X}$ |


| $\mathbf{X}$ | Y | Z | Roll | Pitch | Yaw |
| :--- | :--- | :--- | :--- | :--- | :--- |
| $(\mathbf{m})$ | $(\mathrm{m})$ | (m) | (deg) | $($ deg $)$ | $($ deg $)$ |
| -26.00 | 76.0 | 0 | 0 | 0 | -40 |

## World Coordinate System

The 3D visualization environment uses a world coordinate system with axes that are fixed in the inertial reference frame.


| Axis | Description |
| :--- | :--- |
| $X$ | Forward direction of the vehicle <br> Roll $~-~ R i g h t-h a n d e d ~ r o t a t i o n ~ a b o u t ~$ <br> $X$ |
| $Y$ | -axis |
| $Z$ | Extends to the right of the vehicle, parallel to the ground plane <br> Yaw <br> Yaw $~-~ L e f t-h a n d e d ~ r o t a t i o n ~ a b o u t ~$ -axis |$|$

## Vehicles

## Trucks, Bicycles, and Sedans

This table provides the vehicle tag names and initial locations for other vehicles in the scene, in the world coordinate system. Dimensions are in m and deg.

| Object | Unreal <br> Engine <br> Editor <br> Name | Locations <br> (m) | Y <br> (m) | (m) <br> (m) | Roll <br> (deg) | Pitch <br> (deg) | Yaw <br> (deg) |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Vehicle | SK_BoxTr <br> uck | 20.96 | -136.90 | 0 | 0 | 0 | -90 |
|  | SM_Motor <br> cycle | 42.50 | -157.60 | 0 | 0 | 0 | -20 |
|  | SK_Sedan <br> Car | 5.83 | -117.91 | 0 | 0 | 0 | 0 |
|  | SM_Bicyc <br> le- | 10.88 | -84.42 | 0 | 0 | 0 | 90 |

## Objects

## Cones



## Locations

This table provides the object names and locations in the world coordinate system. Dimensions are in m and deg.

| Object | Unreal <br> Engine <br> Editor <br> Name | Location <br> $\mathbf{( m )}$ | Y <br> $\mathbf{( m )}$ | $\mathbf{Z}$ <br> $(\mathbf{m})$ | Roll <br> (deg) | Pitch <br> (deg) | Yaw <br> (deg) |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Cone | SM_Cone | 22.33 | -131.51 | 0 | 0 | 0 | 0 |
|  | SM_Cone2 | 21.23 | -131.51 | 0 | 0 | 0 | 0 |
|  | SM_Cone3 | 20.03 | -131.51 | 0 | 0 | 0 | 0 |
|  | SM_Cone4 | 18.93 | -131.51 | 0 | 0 | 0 | 0 |

## Barrier



## Locations

This table provides the object names and locations in the world coordinate system. Dimensions are in $m$ and deg.

| Object | Unreal Engine Editor Name | Location |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & X \\ & \hline(m) \end{aligned}$ | $\begin{aligned} & \mathbf{Y} \\ & (\mathrm{m}) \end{aligned}$ | $\begin{aligned} & \mathrm{Z} \\ & (\mathrm{~m}) \end{aligned}$ | $\begin{array}{\|l\|} \hline \text { Roll } \\ \text { (deg) } \end{array}$ | Pitch (deg) | $\begin{aligned} & \text { Yaw } \\ & \text { (deg) } \end{aligned}$ |
| Barrier | $\begin{aligned} & \text { SM Barrie } \\ & \text { r1 } \overline{3} \end{aligned}$ | 79.65 | -173.39 | 0 | 0 | 0 | -35 |
|  | $\begin{aligned} & \text { SM_Barrie } \\ & \text { r1 } \end{aligned}$ | 77.31 | -175.94 | 0 | 0 | 0 | -55 |
|  | $\begin{aligned} & \text { SM Barrie } \\ & \text { r15 } \end{aligned}$ | 74.42 | -177.49 | 0 | 0 | 0 | -80 |
|  | $\begin{aligned} & \text { SM Barrie } \\ & \text { r1 } \end{aligned}$ | 71.18 | -177.64 | 0 | 0 | 0 | -95 |

## Animals



## Locations

This table provides the object names and locations in the world coordinate system. Dimensions are in $m$ and deg.
$\left.\begin{array}{|l|l|l|l|l|l|l|l|}\hline \text { Object } & \begin{array}{l}\text { Unreal } \\ \text { Engine } \\ \text { Editor } \\ \text { Name }\end{array} & \text { Location } & \text { X } & \text { (m) } & \text { Y } & \text { Z } & \text { Roll } \\ \text { (m) }\end{array}\right)$

## Traffic Signs

## STOP

## Locations

This table provides the object names and locations in the world coordinate system. Dimensions are in m and deg.

| Object | Unreal <br> Engine <br> Editor <br> Name | Location |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Object | Unreal Engine Editor Name | Location |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & X \\ & (m) \end{aligned}$ | $\begin{aligned} & \mathbf{Y} \\ & (\mathrm{m}) \end{aligned}$ | $\begin{aligned} & \mathrm{Z} \\ & (\mathrm{~m}) \end{aligned}$ | $\begin{aligned} & \text { Roll } \\ & \text { (deg) } \end{aligned}$ | $\begin{aligned} & \text { Pitch } \\ & \text { (deg) } \end{aligned}$ | $\begin{aligned} & \text { Yaw } \\ & \text { (deg) } \end{aligned}$ |
|  | LargeDoub leArrowSi gn3 | 47.54 | -218.00 | 0 | 0 | 0 | -15 |
|  | SM_StopSi $\mathrm{gn} \overline{9}$ | 70.32 | -195.66 | 0 | 0 | 0 | 0 |
|  | SM Yellow RoadSign3 | 82.66 | -285.75 | -. 02 | 0 | 0 | 15 |
|  | SM_SpeedL imitSign2 | 80.89 | -226.85 | -. 06 | 0 | 0 | 0 |
|  | LargeDoub leArrowSi gn5 | 104.10 | -212.80 | 0 | 0 | 0 | 80 |
|  | ChevronAl ignmentSi gn | 98.45 | -191.22 | 0 | 0 | 0 | 101 |
|  | ChevronAl ignmentSi gn2 | 102.05 | -197.62 | 0 | 0 | 0 | 76.5 |
|  | ChevronAl ignmentSi gn3 | 103.98 | -206.06 | 0 | 0 | 0 | 85 |
|  | SM_Large Exit_Sign | 122.45 | -212.50 | 0 | 0 | 0 | 0 |
|  | SM_Large Exit_Sign 2 | 101.79 | -151.66 | 0 | 0 | 0 | 180 |
|  | SM_StopSi $\mathrm{gn} \overline{3}$ | 32.01 | -163.68 | 0 | 0 | 0 | 160 |
|  | SM_StopSi $\mathrm{gn} \overline{2}$ | 54.98 | -177.12 | 0 | 0 | 0 | 90 |
|  | $\begin{aligned} & \text { SM_StopSi } \\ & \mathrm{gn} \overline{5} \end{aligned}$ | 126.63 | -58.50 | 0 | 0 | 0 | 155 |
|  | SM_StopSi gn6 | 125.28 | -130.73 | 0 | 0 | 0 | -180 |
|  | $\begin{aligned} & \text { SM_StopSi } \\ & \mathrm{gn} \overline{8} \end{aligned}$ | 82.01 | -192.74 | 0 | 0 | 0 | -180 |
|  | $\begin{aligned} & \text { SM_StopSi } \\ & \text { gn4 } \end{aligned}$ | 59.90 | -161.03 | 0 | 0 | 0 | -25 |
|  | LargeSing leArrowSi gn | 121.01 | -148.56 | 0 | 0 | 0 | 0 |


| Object | Unreal Engine Editor Name | Location |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & X \\ & (m) \end{aligned}$ | $\begin{aligned} & \mathbf{Y} \\ & (\mathrm{m}) \end{aligned}$ | $\begin{aligned} & \mathrm{Z} \\ & (\mathrm{~m}) \end{aligned}$ | $\begin{aligned} & \text { Roll } \\ & \text { (deg) } \end{aligned}$ | Pitch <br> (deg) | $\begin{aligned} & \hline \text { Yaw } \\ & \text { (deg) } \end{aligned}$ |
|  | SM YieldS ign2 | 162.22 | -109.64 | 0 | 0 | 0 | 25 |
|  | SM Windin gRoadSign | 127.11 | -50.21 | . 01 | 0 | 0 | 50 |
|  | SchoolBus OnlySign | 44.03 | -51.11 | 0 | 0 | 0 | 90 |
|  | SM Yellow RoadSign5 | 68.05 | -47.03 | . 01 | 0 | 0 | -175 |
|  | SM_CrossS ignal8 | 74.37 | -14.11 | 0 | 0 | 0 | -165 |
|  | SM_CrossS ignal7 | 64.69 | -22.69 | 0 | 0 | 0 | -150 |
|  | SM_CrossS ignal6 | 62.51 | -20.34 | 0 | 0 | 0 | 40 |
|  | SM CrossS igñal5 | 72.42 | -12.06 | 0 | 0 | 0 | 40 |
|  | SM Yellow RoadSign2 | 60.01 | -2.69 | -. 01 | 0 | 0 | 50 |
|  | SM_CrossS ignal2 | 28.53 | -20.58 | 0 | 0 | 0 | -20 |
|  | SM_CrossS ignal | 21.19 | -17.95 | 0 | 0 | 0 | -20 |
|  | SM_CrossS ignal3 | 17.55 | -21.53 | 0 | 0 | 0 | -170 |
|  | SM_CrossS ignal4 | 6.59 | -27.66 | 0 | 0 | 0 | -145 |
|  | SM_YieldS ign4 | 4.89 | -23.42 | 0 | 0 | 0 | -140 |
|  | SM Yellow RoadSign4 | 9.23 | -45.63 | 0 | 0 | 0 | -175 |
|  | SM BikeLa neSign | 24.13 | -92.03 | . 15 | 0 | 0 | 0 |

## Traffic Lights



## Locations

This table provides the object names and locations in the world coordinate system. Dimensions are in $m$ and deg.

| Object | Unreal Engine Editor Name | Location |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \mathrm{X} \\ & (\mathrm{~m}) \end{aligned}$ | $\begin{aligned} & \mathbf{Y} \\ & (\mathrm{m}) \end{aligned}$ | $\begin{aligned} & \mathrm{Z} \\ & (\mathrm{~m}) \end{aligned}$ | $\begin{aligned} & \hline \text { Roll } \\ & \text { (deg) } \end{aligned}$ | Pitch <br> (deg) | Yaw <br> (deg) |
| Traffic lights | SM Traffi cLights | 27.40 | -138.55 | . 16 | 0 | 0 | 90 |
|  | SM_Traffi cLights2 | 9.38 | -106.90 | . 16 | 0 | 0 | -90 |
|  | SM Traffi cLightsSi deOnly3 | 8.44 | -47.95 | -. 03 | 0 | 0 | -92.2 |
|  | SM Traffi cLīghtsSi deOnly4 | 1.64 | -55.10 | . 16 | 0 | 0 | -5 |
|  | SM Traffi cLīghtsSi deOnly5 | 9.24 | -67.70 | . 16 | 0 | 0 | 85 |
|  | SM Traffi cLightsSi deOnly6 | 24.50 | -67.82 | . 16 | 0 | 0 | 85 |
|  | SM Traffi cLights3 | 27.89 | -109.86 | . 16 | 0 | 0 | 180 |
|  | SM_Hangin gTrafficL ightSingl e | 74.43 | -69.25 | 7.37 | 0 | 0 | 0 |


| Object | Unreal Engine Editor Name | Location |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \mathrm{X} \\ & (\mathrm{~m}) \end{aligned}$ | $\begin{aligned} & \mathbf{Y} \\ & (\mathrm{m}) \end{aligned}$ | $\begin{aligned} & \mathrm{Z} \\ & (\mathrm{~m}) \end{aligned}$ | $\begin{aligned} & \text { Roll } \\ & \text { (deg) } \end{aligned}$ | Pitch <br> (deg) | $\begin{aligned} & \hline \text { Yaw } \\ & \text { (deg) } \end{aligned}$ |
|  | SM_Hangin gTrafficL ightSingl e2 | 76.13 | -69.10 | 7.34 | 0 | 0 | 0 |
|  | SM_Hangin gTrafficL ightSingl e3 | 82.58 | -60.10 | 7.57 | 0 | 0 | -90 |
|  | SM_Hangin gTrafficL ightSingl e4 | 82.65 | -61.48 | 7.54 | 0 | 0 | -90 |
|  | SM_Hangin gTrafficL ightSingl e6 | 73.67 | -51.25 | 7.97 | 0 | 0 | -180 |
|  | SM_Hangin gTrafficL ightSingl e7 | 75.07 | -51.25 | 7.95 | 0 | 0 | -180 |
|  | SM_Hangin gTrafficL ight | -24.78 | -61.49 | 6.71 | 0 | 0 | 100 |
|  | SM Railro adत̄rossin g4 | -18.21 | -86.63 | . 01 | 0 | 0 | 8 |
|  | SM Railro adC̄rossin g5 | -26.73 | -90.78 | . 01 | 0 | 0 | -172 |

## Limitations

- In the Vehicle Dynamics Blockset Interface for Unreal Engine 4 Projects support package, this scene is not available for customization.

For details on which scenes you can customize, see "Customize 3D Scenes for Vehicle Dynamics Simulations".

## Version History

Introduced in R2018b

## See Also

Simulation 3D Scene Configuration | Curved Road | Double Lane Change | Open Surface | Large
Parking Lot | Parking Lot | Straight Road | US City Block | US Highway
Topics
"Unreal Engine Simulation Environment Requirements and Limitations"
"How 3D Simulation for Vehicle Dynamics Blockset Works"
"Customize 3D Scenes for Vehicle Dynamics Simulations"
External Websites
Mcity Test Facility

## Vehicle Dimensions

## Hatchback

Hatchback vehicle dimensions

## Description

Hatchback is one of the vehicles that you can use within the 3D simulation environment. This environment is rendered using the Unreal Engine from Epic Games. The diagram provides the dimensions of this vehicle. The height dimensions are with respect to the vertical ground plane. The length and width dimensions are with respect to the origin of the vehicle in the vehicle coordinate system. The origin is on the ground, at the geometric center of the vehicle. For more detailed views of these diagrams, see the Dimensions section.


To add this type of vehicle to the 3D simulation environment:
1 Add a Simulation 3D Vehicle or Simulation 3D Vehicle with Ground Following block to your Simulink model.
2 In the block, set the Type parameter to Hatchback.

## Dimensions

Top-down view - Vehicle width dimensions
diagram


Side view - Vehicle length, front overhang, and rear overhang dimensions diagram


Front view - Tire width and front axle dimensions
diagram


Rear view - Vehicle height and rear axle dimensions
diagram


## Sensor Mounting Locations

In the 3D simulation sensor blocks, use the Mounting location parameter to mount sensors at predefined locations on the vehicle. The table shows the $X, Y$, and $Z$ positions of the mounting locations relative to the vehicle origin. These locations are in the vehicle coordinate system, where:

- The $X$-axis points forward from the vehicle.
- The $Y$-axis points to the left of the vehicle, as viewed when facing forward.
- The $Z$-axis points up from the ground.

Hatchback - Sensor Locations Relative to Vehicle Origin

| Mounting Location | $\mathbf{X ( m )}$ | $\mathbf{Y}(\mathbf{m})$ | $\mathbf{Z}(\mathbf{m})$ |
| :--- | :--- | :--- | :--- |
| Front bumper | 1.93 | 0 | 0.51 |
| Rear bumper | -1.93 | 0 | 0.51 |
| Right mirror | 0.43 | -0.84 | 1.01 |
| Left mirror | 0.43 | 0.84 | 1.01 |
| Rearview mirror | 0.32 | 0 | 1.27 |
| Hood center | 1.44 | 0 | 1.01 |
| Roof center | 0 | 0 | 1.57 |

## See Also

Simulation 3D Scene Configuration | Simulation 3D Vehicle | Simulation 3D Vehicle with Ground Following

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"
"How 3D Simulation for Vehicle Dynamics Blockset Works"

## Muscle Car

Muscle car vehicle dimensions

## Description

Muscle Car is one of the vehicles that you can use within the 3D simulation environment. This environment is rendered using the Unreal Engine from Epic Games. The following diagram provides the dimensions of this vehicle. The height dimensions are with respect to the vertical ground plane. The length and width dimensions are with respect to the origin of the vehicle in the vehicle coordinate system. The origin is on the ground, at the geometric center of the vehicle. For more detailed views of these diagrams, see the Dimensions section.


To add this type of vehicle to the 3D simulation environment:
1 Add a Simulation 3D Vehicle or Simulation 3D Vehicle with Ground Following block to your Simulink model.
2 In the block, set the Type parameter to Muscle car.
Dimensions
Top-down view - Vehicle width dimensions
diagram


Side view - Vehicle length, front overhang, and rear overhang dimensions
diagram


Front view - Tire width and front axle dimensions
diagram


Rear view - Vehicle height and rear axle dimensions
diagram


## Sensor Mounting Locations

In the 3D simulation sensor blocks, use the Mounting location parameter to mount sensors at predefined locations on the vehicle. The table shows the $X, Y$, and $Z$ positions of the mounting locations relative to the vehicle origin. These locations are in the vehicle coordinate system, where:

- The $X$-axis points forward from the vehicle.
- The $Y$-axis points to the left of the vehicle, as viewed when facing forward.
- The $Z$-axis points up from the ground.

Muscle Car - Sensor Locations Relative to Vehicle Origin

| Mounting Location | $\mathbf{X}(\mathbf{m})$ | $\mathbf{Y}(\mathbf{m})$ | $\mathbf{Z}(\mathbf{m})$ |
| :--- | :--- | :--- | :--- |
| Front bumper | 2.47 | 0 | 0.45 |
| Rear bumper | -2.47 | 0 | 0.45 |
| Right mirror | 0.43 | -1.08 | 1.01 |
| Left mirror | 0.43 | 1.08 | 1.01 |
| Rearview mirror | 0.32 | 0 | 1.20 |
| Hood center | 1.28 | 0 | 1.14 |
| Roof center | -0.25 | 0 | 1.58 |

## See Also

Simulation 3D Scene Configuration | Simulation 3D Vehicle | Simulation 3D Vehicle with Ground Following

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"
"How 3D Simulation for Vehicle Dynamics Blockset Works"

## Sedan

Sedan vehicle dimensions

## Description

Sedan is one of the vehicles that you can use within the 3D simulation environment. This environment is rendered using the Unreal Engine from Epic Games. The diagram provides the dimensions of this vehicle. The height dimensions are with respect to the vertical ground plane. The length and width dimensions are with respect to the origin of the vehicle in the vehicle coordinate system. The origin is on the ground, at the geometric center of the vehicle. For more detailed views of these diagrams, see the Dimensions section.


To add this type of vehicle to the 3D simulation environment:
1 Add a Simulation 3D Vehicle or Simulation 3D Vehicle with Ground Following block to your Simulink model.
2 In the block, set the Type parameter to Sedan.

## Dimensions

Top-down view - Vehicle width dimensions
diagram


Side view - Vehicle length, front overhang, and rear overhang dimensions
diagram


Front view - Tire width and front axle dimensions
diagram


Rear view - Vehicle height and rear axle dimensions
diagram


## Sensor Mounting Locations

In the 3D simulation sensor blocks, use the Mounting location parameter to mount sensors at predefined locations on the vehicle. The table shows the $X, Y$, and $Z$ positions of the mounting locations relative to the vehicle origin. These locations are in the vehicle coordinate system, where:

- The $X$-axis points forward from the vehicle.
- The $Y$-axis points to the left of the vehicle, as viewed when facing forward.
- The $Z$-axis points up from the ground.


## Sedan - Sensor Locations Relative to Vehicle Origin

| Mounting Location | $\mathbf{X}(\mathbf{m})$ | $\mathbf{Y}(\mathbf{m})$ | $\mathbf{Z}(\mathbf{m})$ |
| :--- | :--- | :--- | :--- |
| Front bumper | 2.42 | 0 | 0.51 |
| Rear bumper | -2.42 | 0 | 0.51 |
| Right mirror | 0.59 | -0.94 | 1.09 |
| Left mirror | 0.59 | 0.94 | 1.09 |
| Rearview mirror | 0.43 | 0 | 1.31 |
| Hood center | 1.46 | 0 | 1.11 |
| Roof center | -0.45 | 0 | 1.69 |

## See Also

Simulation 3D Scene Configuration | Simulation 3D Vehicle | Simulation 3D Vehicle with Ground Following

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"
"How 3D Simulation for Vehicle Dynamics Blockset Works"

## Sport Utility Vehicle

Sport utility vehicle dimensions

## Description

Sport Utility Vehicle is one of the vehicles that you can use within the 3D simulation environment. This environment is rendered using the Unreal Engine from Epic Games. The following diagram provides the dimensions of this vehicle. The height dimensions are with respect to the vertical ground plane. The length and width dimensions are with respect to the origin of the vehicle in the vehicle coordinate system. The origin is on the ground, at the geometric center of the vehicle. For more detailed views of these diagrams, see the Dimensions section.


To add this type of vehicle to the 3D simulation environment:
1 Add a Simulation 3D Vehicle or Simulation 3D Vehicle with Ground Following block to your Simulink model.
2 In the block, set the Type parameter to Sport utility vehicle.

## Dimensions

Top-down view - Vehicle width dimensions
diagram


Side view - Vehicle length, front overhang, and rear overhang dimensions
diagram


Front view - Tire width and front axle dimensions
diagram


Rear view - Vehicle height and rear axle dimensions
diagram


## Sensor Mounting Locations

In the 3D simulation sensor blocks, use the Mounting location parameter to mount sensors at predefined locations on the vehicle. The table shows the $X, Y$, and $Z$ positions of the mounting locations relative to the vehicle origin. These locations are in the vehicle coordinate system, where:

- The $X$-axis points forward from the vehicle.
- The $Y$-axis points to the left of the vehicle, as viewed when facing forward.
- The $Z$-axis points up from the ground.

Sport Utility Vehicle - Sensor Locations Relative to Vehicle Origin

| Mounting Location | $\mathbf{X}(\mathbf{m})$ | $\mathbf{Y}(\mathbf{m})$ | $\mathbf{Z}(\mathbf{m})$ |
| :--- | :--- | :--- | :--- |
| Front bumper | 2.42 | 0 | 0.51 |
| Rear bumper | -2.42 | 0 | 0.51 |
| Right mirror | 0.60 | -1 | 1.35 |
| Left mirror | 0.60 | 1 | 1.35 |
| Rearview mirror | 0.39 | 0 | 1.55 |
| Hood center | 1.58 | 0 | 1.39 |
| Roof center | -0.56 | 0 | 2 |

## See Also

Simulation 3D Scene Configuration | Simulation 3D Vehicle | Simulation 3D Vehicle with Ground Following

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"
"How 3D Simulation for Vehicle Dynamics Blockset Works"

## Small Pickup Truck

Small pickup truck vehicle dimensions

## Description

Small Pickup Truck is one of the vehicles that you can use within the 3D simulation environment. This environment is rendered using the Unreal Engine from Epic Games. The following diagram provides the dimensions of this vehicle. The height dimensions are with respect to the vertical ground plane. The length and width dimensions are with respect to the origin of the vehicle in the vehicle coordinate system. The origin is on the ground, at the geometric center of the vehicle. For more detailed views of these diagrams, see the Dimensions section.


To add this type of vehicle to the 3D simulation environment:
1 Add a Simulation 3D Vehicle or Simulation 3D Vehicle with Ground Following block to your Simulink model.
2 In the block, set the Type parameter to Small pickup truck.

## Dimensions

Top-down view - Vehicle width dimensions
diagram


Side view - Vehicle length, front overhang, and rear overhang dimensions diagram


Front view - Tire width and front axle dimensions
diagram


Rear view - Vehicle height and rear axle dimensions
diagram


## Sensor Mounting Locations

In the 3D simulation sensor blocks, use the Mounting location parameter to mount sensors at predefined locations on the vehicle. The table shows the $X, Y$, and $Z$ positions of the mounting locations relative to the vehicle origin. These locations are in the vehicle coordinate system, where:

- The $X$-axis points forward from the vehicle.
- The $Y$-axis points to the left of the vehicle, as viewed when facing forward.
- The $Z$-axis points up from the ground.

Small Pickup Truck - Sensor Locations Relative to Vehicle Origin

| Mounting Location | $\mathbf{X ( m )}$ | $\mathbf{Y}(\mathbf{m})$ | $\mathbf{Z}(\mathbf{m})$ |
| :--- | :--- | :--- | :--- |
| Front bumper | 3.07 | 0 | 0.51 |
| Rear bumper | -3.07 | 0 | 0.51 |
| Right mirror | 1.10 | -1.13 | 1.52 |
| Left mirror | 1.10 | 1.13 | 1.52 |
| Rearview mirror | 0.85 | 0 | 1.77 |
| Hood center | 2.22 | 0 | 1.59 |
| Roof center | 0 | 0 | 2.27 |

## See Also

Simulation 3D Scene Configuration | Simulation 3D Vehicle | Simulation 3D Vehicle with Ground Following

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"
"How 3D Simulation for Vehicle Dynamics Blockset Works"

## Box Truck

Box truck vehicle dimensions

## Description

Box truck is one of the vehicles that you can use within the 3D simulation environment. This environment is rendered using the Unreal Engine from Epic Games. The following diagram provides the dimensions of this vehicle. The height dimensions are with respect to the vertical ground plane. The length and width dimensions are with respect to the origin of the vehicle in the vehicle coordinate system. The origin is on the ground, at the geometric center of the vehicle. For more detailed views of these diagrams, see the Dimensions section.

To add this type of vehicle to the 3D simulation environment:
1 Add a Simulation 3D Vehicle or Simulation 3D Vehicle with Ground Following block to your Simulink model.
2 In the block, set the Type parameter to Box truck.

## Dimensions

Top-down view - Vehicle width dimensions
diagram


Side view - Vehicle length, front overhang, and rear overhang dimensions
diagram


Front view - Tire width and front axle dimensions
diagram


Rear view - Vehicle height and rear axle dimensions
diagram


## Sensor Mounting Locations

In the 3D simulation sensor blocks, use the Mounting location parameter to mount sensors at predefined locations on the vehicle. The table shows the $X, Y$, and $Z$ positions of the mounting locations relative to the vehicle origin. These locations are in the vehicle coordinate system, where:

- The $X$-axis points forward from the vehicle.
- The $Y$-axis points to the left of the vehicle, as viewed when facing forward.
- The $Z$-axis points up from the ground.


## Box Truck - Sensor Locations Relative to Vehicle Origin

| Mounting Location | $\mathbf{X ( m )}$ | $\mathbf{Y}(\mathbf{m})$ | $\mathbf{Z}(\mathbf{m})$ |
| :--- | :--- | :--- | :--- |
| Front bumper | 5.10 | 0 | 0.60 |
| Rear bumper | -5 | 0 | 0.60 |
| Right mirror | 2.90 | 1.60 | 2.10 |
| Left mirror | 2.90 | -1.60 | 2.10 |
| Rearview mirror | 2.60 | 0.20 | 2.60 |
| Hood center | 3.80 | 0 | 2.10 |
| Roof center | 1.30 | 0 | 4.20 |

## See Also

Simulation 3D Scene Configuration | Simulation 3D Vehicle | Simulation 3D Vehicle with Ground Following

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"
"How 3D Simulation for Vehicle Dynamics Blockset Works"

## Formula Student Vehicle

Formula student vehicle dimensions

## Description

Formula Student Vehicle is one of the vehicles that you can use within the 3D simulation environment. This environment is rendered using the Unreal Engine from Epic Games. The Dimensions section provides the dimensions of this vehicle. The height dimensions are with respect to the vertical ground plane. The length and width dimensions are with respect to the origin of the vehicle in the vehicle coordinate system. The origin is on the ground, at the geometric center of the vehicle.

To add this type of vehicle to the 3D simulation environment:
1 Add a Simulation 3D Vehicle or Simulation 3D Vehicle with Ground Following block to your Simulink model.
2 In the block, set the Type parameter to Formula student vehicle.

## Dimensions

Top-down view - Top-down view of vehicle diagram


Side view - Vehicle length, front overhang, and rear overhang dimensions diagram


Front view - Tire width and front axle dimensions
diagram


Rear view - Vehicle height and rear axle dimensions diagram


## Sensor Mounting Locations

Formula Student Vehicle - Sensor Locations Relative to Vehicle Origin

| Mounting <br> Location | $\mathbf{X ( m )}$ | $\mathbf{Y ( m )}$ | $\mathbf{Z}(\mathbf{m})$ | Roll <br> (radian) | Pitch <br> (radian) | Yaw <br> (radian) |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Front <br> bumper | 1.3 | 0 | 0.3 | 0 | 0 | 0 |
| Rear <br> bumper | -1.4 | 0 | 0.3 | 0 | 0 | pi |
| Roll bar <br> center | -0.6 | 0 | 1.05 | 0 | 0 | 0 |

## See Also

Simulation 3D Scene Configuration | Simulation 3D Vehicle | Simulation 3D Vehicle with Ground Following

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"
"How 3D Simulation for Vehicle Dynamics Blockset Works"

## Cab-Over Tractor

Cab-over tractor dimensions

## Description

Cab-Over Tractor is one of the tractors that you can use in the 3D simulation environment. The environment is rendered using the Unreal Engine from Epic Games. The Dimensions section provides the dimensions of this tractor. The height dimensions are with respect to the vertical ground plane. The length and width dimensions are with respect to the origin of the tractor in the vehicle coordinate system. The origin is on the ground plane, at the normal projection of the mid-point of the rear axles along the vehicle centerline.

To add this type of tractor to the 3D simulation environment:
1 Add a Simulation 3D Tractor block to your Simulink model.
2 In the block, set the Type parameter to Cab-over tractor.

## Dimensions

Top-down view - Tractor width dimensions
diagram


Side view - Tractor length, front overhang, and rear overhang dimensions
diagram


Front view - Tire width and front axle dimensions
diagram


## See Also

Simulation 3D Tractor | Simulation 3D Scene Configuration

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"
"How 3D Simulation for Vehicle Dynamics Blockset Works"

## Conventional Tractor

Conventional tractor dimensions

## Description

Conventional Tractor is one of the tractors that you can use in the 3D simulation environment. The environment is rendered using the Unreal Engine from Epic Games. The Dimensions section provides the dimensions of this tractor. The height dimensions are with respect to the vertical ground plane. The length and width dimensions are with respect to the origin of the tractor in the vehicle coordinate system. The origin is on the ground plane, at the normal projection of the mid-point of the rear axles along the vehicle centerline.

To add this type of tractor to the 3D simulation environment:
1 Add a Simulation 3D Tractor block to your Simulink model.
2 In the block, set the Type parameter to Conventional tractor.
Dimensions
Top-down view - Tractor width dimensions
diagram


Side view - Tractor length, front overhang, and rear overhang dimensions diagram


Front view - Tire width and front axle dimensions
diagram


## See Also

Simulation 3D Tractor | Simulation 3D Scene Configuration

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"
"How 3D Simulation for Vehicle Dynamics Blockset Works"

## One-Axle Trailer

One-axle trailer dimensions

## Description

One-Axle Trailer is one of the trailers that you can use in the 3D simulation environment. The environment is rendered using the Unreal Engine from Epic Games. The Dimensions section provides the dimensions of this trailer. The height dimensions are with respect to the vertical ground plane. The length and width dimensions are with respect to the origin of the trailer in the vehicle coordinate system. The origin is on the ground plane, at the normal projection of the hitch.

To add this type of trailer to the 3D simulation environment:
1 Add a Simulation 3D Trailer block to your Simulink model.
2 In the block, set the Type parameter to One-axle trailer.

## Dimensions

Top-down view - Top-down view of trailer
diagram


Side view - Trailer length, front overhang, and rear overhang dimensions
diagram


Front view - Tire width and front axle dimensions
diagram


Back view - Rear axle dimensions
diagram


## See Also

Simulation 3D Trailer | Simulation 3D Scene Configuration

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"
"How 3D Simulation for Vehicle Dynamics Blockset Works"

## Two-Axle Trailer

Two-axle trailer dimensions

## Description

Two-Axle Trailer is one of the trailers that you can use in the 3D simulation environment. The environment is rendered using the Unreal Engine from Epic Games. The Dimensions section provides the dimensions of this trailer. The height dimensions are with respect to the vertical ground plane. The length and width dimensions are with respect to the origin of the trailer in the vehicle coordinate system. The origin is on the ground plane, at the normal projection of the hitch.

To add this type of trailer to the 3D simulation environment:
1 Add a Simulation 3D Trailer block to your Simulink model.
2 In the block, set the Type parameter to Two-axle trailer.

## Dimensions

Top-down view - Trailer width dimensions
diagram

Side view - Trailer length, front overhang, and rear overhang dimensions diagram


Back view - Tire width and front axle dimensions
diagram


## See Also

Simulation 3D Trailer | Simulation 3D Scene Configuration

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"
"How 3D Simulation for Vehicle Dynamics Blockset Works"

## Three-Axle Trailer

Three-axle trailer dimensions

## Description

Three-Axle Trailer is one of the trailers that you can use in the 3D simulation environment. The environment is rendered using the Unreal Engine from Epic Games. The Dimensions section provides the dimensions of this trailer. The height dimensions are with respect to the vertical ground plane. The length and width dimensions are with respect to the origin of the trailer in the vehicle coordinate system. The origin is on the ground plane, at the normal projection of the hitch.

To add this type of trailer to the 3D simulation environment:
1 Add a Simulation 3D Trailer block to your Simulink model.
2 In the block, set the Type parameter to Three-axle trailer.

## Dimensions

Top-down view - Trailer width dimensions
diagram


Side view - Trailer length, front overhang, and rear overhang dimensions diagram


Front view - Tire width and front axle dimensions
diagram


## See Also

Simulation 3D Trailer | Simulation 3D Scene Configuration

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"
"How 3D Simulation for Vehicle Dynamics Blockset Works"

## One-Axle Dolly

One-axle dolly dimensions

## Description

The One-Axle Dolly is one of the dollies that you can use in the 3D simulation environment. The environment is rendered using the Unreal Engine from Epic Games. The Dimensions section provides the dimensions of this dolly. The height dimensions are with respect to the vertical ground plane. The length and width dimensions are with respect to the origin of the dolly in the vehicle coordinate system. The origin is on the ground plane, at the projection of the hitch socket.

To add this type of dolly to the 3D simulation environment:
1 Add a Simulation 3D Dolly block to your Simulink model.
2 In the block, set the Type parameter to One-axle dolly.

## Dimensions

Top-down view - Dolly width
diagram


Side view - Dolly length and height
diagram


Front view - Dolly width
diagram


## See Also

Simulation 3D Trailer | Simulation 3D Scene Configuration

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"
"How 3D Simulation for Vehicle Dynamics Blockset Works"

## Two-Axle Dolly

Two-axle dolly dimensions

## Description

The Two-Axle Dolly is one of the dollies that you can use in the 3D simulation environment. The environment is rendered using the Unreal Engine from Epic Games. The Dimensions section provides the dimensions of this dolly. The height dimensions are with respect to the vertical ground plane. The length and width dimensions are with respect to the origin of the dolly in the vehicle coordinate system. The origin is on the ground plane, at the projection of the hitch socket.

To add this type of dolly to the 3D simulation environment:
1 Add a Simulation 3D Dolly block to your Simulink model.
2 In the block, set the Type parameter to Two-axle dolly.

## Dimensions

Top-down view - Dolly and tire width diagram


Side view - Dolly length and height
diagram


Front view - Dolly width
diagram


## See Also

Simulation 3D Trailer | Simulation 3D Scene Configuration

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"
"How 3D Simulation for Vehicle Dynamics Blockset Works"

## Three-Axle Dolly

Three-axle dolly dimensions

## Description

The Three-Axle Dolly is one of the dollies that you can use in the 3D simulation environment. The environment is rendered using the Unreal Engine from Epic Games. The Dimensions section provides the dimensions of this dolly. The height dimensions are with respect to the vertical ground plane. The length and width dimensions are with respect to the origin of the dolly in the vehicle coordinate system. The origin is on the ground plane, at the projection of the hitch socket.

To add this type of dolly to the 3D simulation environment:
1 Add a Simulation 3D Dolly block to your Simulink model.
2 In the block, set the Type parameter to Three-axle dolly.

## Dimensions

Top-down view - Dolly and tire width
diagram


Side view - Dolly length and height
diagram


Front view - Dolly width
diagram


## See Also

Simulation 3D Trailer | Simulation 3D Scene Configuration

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"
"How 3D Simulation for Vehicle Dynamics Blockset Works"

## Scooter

Scooter dimensions

## Description

The Scooter is one of the motorcycles that you can use in the 3D simulation environment. The environment is rendered using the Unreal Engine from Epic Games. The Dimensions section provides the dimensions of this scooter. The height dimensions are with respect to the vertical ground plane. The length and width dimensions are with respect to the origin of the scooter in the vehicle coordinate system. The origin is on the ground plane, at the projection of the hitch socket.

To add this type of scooter to the 3D simulation environment:
1 Add a Simulation 3D Motorcycle block to your Simulink model.
2 In the block, set the Type parameter to Scooter.

## Dimensions

Side view - Scooter length and detailed dimensions diagram


Front view - Scooter width and height
diagram


## See Also

Simulation 3D Motorcycle | Simulation 3D Scene Configuration

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"
"How 3D Simulation for Vehicle Dynamics Blockset Works"

## Motor Bike

Motor bike dimensions

## Description

The Motor bike is one of the motorcycles that you can use in the 3D simulation environment. The environment is rendered using the Unreal Engine from Epic Games. The Dimensions section provides the dimensions of this dolly. The height dimensions are with respect to the vertical ground plane. The length and width dimensions are with respect to the origin of the dolly in the vehicle coordinate system. The origin is on the ground plane, at the projection of the hitch socket.

To add this type of dolly to the 3D simulation environment:
1 Add a Simulation 3D Motorcycle block to your Simulink model.
2 In the block, set the Type parameter to Motor bike.

## Dimensions

Side view - Motor bike length and detailed dimensions
diagram


Front view - Motor bike width and height
diagram


## See Also

Simulation 3D Motorcycle | Simulation 3D Scene Configuration

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"
"How 3D Simulation for Vehicle Dynamics Blockset Works"

## Sports Bike

Sports bike dimensions

## Description

The Sports bike is one of the motorcycles that you can use in the 3D simulation environment. The environment is rendered using the Unreal Engine from Epic Games. The Dimensions section provides the dimensions of this dolly. The height dimensions are with respect to the vertical ground plane. The length and width dimensions are with respect to the origin of the dolly in the vehicle coordinate system. The origin is on the ground plane, at the projection of the hitch socket.

To add this type of dolly to the 3D simulation environment:
1 Add a Simulation 3D Motorcycle block to your Simulink model.
2 In the block, set the Type parameter to Sports bike.

## Dimensions

Side view - Sports bike length and detailed dimensions
diagram


Front view - Sports bike width and height
diagram


## See Also

Simulation 3D Motorcycle | Simulation 3D Scene Configuration

## Topics

"Coordinate Systems in Vehicle Dynamics Blockset"
"How 3D Simulation for Vehicle Dynamics Blockset Works"

## Blocks in Reference Applications

## 3D Engine

Configure scenes in reference applications

## Description

The 3D Engine block implements the 3D simulation environment. Vehicle Dynamics Blockset integrates the 3D simulation environment with Simulink so that you can query the world around the vehicle for virtually testing perception, control, and planning algorithms.

To position the vehicle in the scene:
1 Select the position initialization method:

- Recommended for scene - Set the initial vehicle position to values recommended for the scene
- User-specified - Set your own initial vehicle position

2 Click Update the model workspaces with the initial values to overwrite the initial vehicle position in the model workspaces with the applied values.

## Ports

Input
VehFdbk - Vehicle feedback
Bus
Bus containing vehicle feedback signals, including velocity, acceleration, and steering wheel torque.

## Parameters

## 3D Engine

3D Engine - Enable 3D visualization
off (default) | on
Enable 3D visualization.

## Scene - 3D scene

Straight road|Curved road|Parking lot|Double lane change|Open surface|US city block|US highway|Virtual Mcity|Large parking lot

Specify the name of the 3D scene.

## Engine frame rate, dt3D - Graphics

. 03 (default)
Graphics frame rate, in s. The graphics frame rate is the inverse of the sample time.
Recommended for scene - Initial vehicle position
on (default) | off

Use vehicle positions that are recommended for the scene.
User-specified - Initial vehicle position
off (default) | on
Specify to set your own initial vehicle position values.
Initial longitudinal position, X_o - Initial longitudinal position
off (default) | on
Initial vehicle CG position along the earth-fixed $X$-axis, in m.
Initial lateral position, Y_o - Initial lateral position
off (default) | on
Initial vehicle CG position along the earth-fixed $Y$-axis, in $m$.
Initial vertical position, Z_o - Initial vertical position
off (default) | on
Initial vehicle CG position along the earth-fixed $Z$-axis, in m.
Initial roll angle, phi_o - Roll
off (default) | on
Rotation of the vehicle-fixed frame about the earth-fixed $X$-axis (roll), in rad.
Initial pitch angle, theta_o - Pitch
off (default) | on
Rotation of the vehicle-fixed frame about the earth-fixed $Y$-axis (pitch), in rad.
Initial yaw angle, psi_o - Yaw
off (default) | on
Rotation of the vehicle-fixed frame about the earth-fixed $Z$-axis (yaw), in rad.

## Version History

Introduced in R2019a

See Also<br>Curved Road | Double Lane Change | Open Surface | Large Parking Lot | Parking Lot | Straight Road | US City Block | US Highway | Virtual Mcity<br>Topics<br>"Double-Lane Change Maneuver"<br>"Slowly Increasing Steering Maneuver"<br>"Swept-Sine Steering Maneuver"<br>"How 3D Simulation for Vehicle Dynamics Blockset Works"<br>"Unreal Engine Simulation Environment Requirements and Limitations"

## External Websites

Unreal Engine

## Bicycle Model

Implement a single track 3DOF rigid vehicle body to calculate longitudinal, lateral, and yaw motion

## Description

The Bicycle Model block implements a rigid two-axle single track vehicle body model to calculate longitudinal, lateral, and yaw motion. The block accounts for body mass, aerodynamic drag, and weight distribution between the axles due to acceleration and steering. There are two types of Bicycle Model blocks.


To calculate the normal forces on the front and rear axles, the block uses rigid-body vehicle motion, suspension system forces, and wind and drag forces. The block resolves the force and moment components on the rigid vehicle body frame.

## Ports

Input
WhIAngF - Wheel angle
scalar
Front wheel angle, in rad.
FxF - Force Input: Total longitudinal force on the front axle scalar

Longitudinal force on the front axle, $F x_{F}$, along vehicle-fixed $x$-axis, in N .

Bicycle Model - Force Input block input port.
FxR - Force Input: Total longitudinal force on the rear axle
scalar
Longitudinal force on the rear axle, $F x_{R}$, along vehicle-fixed $x$-axis, in N .
Bicycle Model - Force Input block input port.
xdotin - Velocity Input: Longitudinal velocity
scalar
Vehicle CG velocity along vehicle-fixed $x$-axis, in $m / s$.
Bicycle Model - Velocity Input block input port.

## Output

Info - Bus signal
bus
Bus signal containing these block values.

| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| InertFrm | Cg | Disp | X | Vehicle CG displacement along the earth-fixed $X$ axis | Computed | m |
|  |  |  | Y | Vehicle CG displacement along the earth-fixed $Y$ axis | Computed | m |
|  |  |  | Z | Vehicle CG displacement along the earth-fixed $Z$ axis | 0 | m |
|  |  | Vel | Xdot | Vehicle CG velocity along the earth-fixed $X$-axis | Computed | m/s |
|  |  |  | Ydot | Vehicle CG velocity along the earth-fixed $Y$-axis | Computed | m/s |
|  |  |  | Zdot | Vehicle CG velocity along the earth-fixed $Z$-axis | 0 | m/s |
|  |  | Ang | phi | Rotation of the vehiclefixed frame about the earth-fixed $X$-axis (roll) | 0 | rad |
|  |  |  | theta | Rotation of the vehiclefixed frame about the earth-fixed $Y$-axis (pitch) | 0 | rad |
|  |  |  | psi | Rotation of the vehiclefixed frame about the earth-fixed $Z$-axis (yaw) | Computed | rad |


| Signal |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: |
| FrntAxl | Disp | X | Front wheel displacement along the earth-fixed $X$ axis | Computed | m |
|  |  | Y | Front wheel displacement along the earth-fixed $Y$ axis | Computed | m |
|  |  | Z | Front wheel displacement along the earth-fixed Zaxis | 0 | m |
|  | Vel | Xdot | Front wheel velocity along the earth-fixed $X$-axis | Computed | $\mathrm{m} / \mathrm{s}$ |
|  |  | Ydot | Front wheel velocity along the earth-fixed $Y$-axis | Computed | m/s |
|  |  | Zdot | Front wheel velocity along the earth-fixed $Z$-axis | 0 | m/s |
| RearAxl | Disp | X | Rear wheel displacement along the earth-fixed $X$ axis | Computed | m |
|  |  | Y | Rear wheel displacement along the earth-fixed $Y$ axis | Computed | m |
|  |  | Z | Rear wheel displacement along the earth-fixed Zaxis | 0 | m |
|  | Vel | Xdot | Rear wheel velocity along the earth-fixed $X$-axis | Computed | m/s |
|  |  | Ydot | Rear wheel velocity along the earth-fixed $Y$-axis | Computed | m/s |
|  |  | Zdot | Rear wheel velocity along the earth-fixed $Z$-axis | 0 | m/s |
| Hitch | Disp | X | Hitch offset from axle plane along the earthfixed $X$-axis | Computed | m |
|  |  | Y | Hitch offset from center plane along the earthfixed $Y$-axis | Computed | m |
|  |  | Z | Hitch offset from axle plane along the earthfixed $Z$-axis | Computed | m |
|  | Vel | Xdot | Hitch offset velocity from axle plane along the earth-fixed $X$-axis | Computed | m |


| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Ydot | Hitch offset velocity from center plane along the earth-fixed $Y$-axis | Computed | m |
|  |  |  | Zdot | Hitch offset velocity from axle plane along the earth-fixed Z-axis | Computed | m |
|  | Geom | Disp | X | Vehicle chassis offset from axle plane along the earth-fixed $X$-axis | Computed | m |
|  |  |  | Y | Vehicle chassis offset from center plane along the earth-fixed $Y$-axis | Computed | m |
|  |  |  | Z | Vehicle chassis offset from axle plane along the earth-fixed $Z$-axis | Computed | m |
|  |  | Vel | Xdot | Vehicle chassis offset velocity along the earthfixed $X$-axis | Computed | m/s |
|  |  |  | Ydot | Vehicle chassis offset velocity along the earthfixed $Y$-axis | Computed | m/s |
|  |  |  | Zdot | Vehicle chassis offset velocity along the earthfixed Z-axis | Computed | $\mathrm{m} / \mathrm{s}$ |
| BdyFrm | Cg | Vel | xdot | Vehicle CG velocity along the vehicle-fixed $x$-axis | Computed | m/s |
|  |  |  | ydot | Vehicle CG velocity along the vehicle-fixed $y$-axis | Computed | m/s |
|  |  |  | zdot | Vehicle CG velocity along the vehicle-fixed $z$-axis | 0 | m/s |
|  |  | Ang | Beta | Body slip angle, $\beta$ $\beta=\frac{V_{y}}{V_{x}}$ | Computed | rad |
|  |  | AngVel | p | Vehicle angular velocity about the vehicle-fixed $x$ axis (roll rate) | 0 | $\mathrm{rad} / \mathrm{s}$ |
|  |  |  | q | Vehicle angular velocity about the vehicle-fixed $y$ axis (pitch rate) | 0 | rad/s |
|  |  |  | r | Vehicle angular velocity about the vehicle-fixed $z$ axis (yaw rate) | Computed | rad/s |



| Signal |  |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | External force on vehicle CG along the vehicle-fixed $z$-axis | 0 | N |
|  | Hitch | Fx |  | Hitch force applied to body at the hitch location along the vehicle-fixed $x$ axis | Input | N |
|  |  | Fy |  | Hitch force applied to body at the hitch location along the vehicle-fixed $y$ axis | Input | N |
|  |  | Fz |  | Hitch force applied to body at the hitch location along the vehicle-fixed $z$ axis | Input | N |
|  | FrntAxl | Fx |  | Longitudinal force on front wheel, along the vehicle-fixed $x$-axis | Computed | N |
|  |  | Fy |  | Lateral force on front wheel along the vehiclefixed $y$-axis | Computed | N |
|  |  | Fz |  | Normal force on front wheel, along the vehiclefixed $z$-axis | Computed | N |
|  | RearAxl | Fx |  | Longitudinal force on rear wheel, along the vehiclefixed $x$-axis | Computed | N |
|  |  | Fy |  | Lateral force on rear wheel along the vehiclefixed $y$-axis | Computed | N |
|  |  | Fz |  | Normal force on rear wheel, along the vehiclefixed $z$-axis | Computed | N |
|  | Tires | FrntTire | Fx | Front tire force, along the vehicle-fixed $x$-axis | Computed | N |
|  |  |  | Fy | Front tire force, along the vehicle-fixed $y$-axis | Computed | N |
|  |  |  | Fz | Front tire force, along the vehicle-fixed $z$-axis | Computed | N |
|  |  | $\begin{aligned} & \text { RearTir } \\ & \mathrm{e} \end{aligned}$ | $\begin{aligned} & \text { FxF } \\ & \mathrm{x} \end{aligned}$ | Rear tire force, along the vehicle-fixed $x$-axis | Computed | N |
|  |  |  | Fy | Rear tire force, along the vehicle-fixed $y$-axis | Computed | N |


| Signal |  |  |  | Description | Value | Units |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  |  |  |  |  | Rear tire force, along the <br> vehicle-fixed $z$-axis | Computed |


| Signal |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Mz | External moment on vehicle CG about the vehicle-fixed $z$-axis | 0 | $\mathrm{N} \cdot \mathrm{m}$ |
|  | Hitch | Mx | Hitch moment at the hitch location about vehiclefixed $x$-axis | 0 | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | My | Hitch moment at the hitch location about vehiclefixed $y$-axis | Computed | $\mathrm{N} \cdot \mathrm{m}$ |
|  |  | Mz | Hitch moment at the hitch location about vehiclefixed $z$-axis | 0 | $\mathrm{N} \cdot \mathrm{m}$ |
| FrntAxl | Disp | x | Front wheel displacement along the vehicle-fixed $x$ axis | Computed | m |
|  |  | y | Front wheel displacement along the vehicle-fixed $y$ axis | Computed | m |
|  |  | z | Front wheel displacement along the vehicle-fixed $z$ axis | Computed | m |
|  | Vel | xdot | Front wheel velocity along the vehicle-fixed $x$-axis | Computed | m/s |
|  |  | ydot | Front wheel velocity along the vehicle-fixed $y$-axis | Computed | m/s |
|  |  | zdot | Front wheel velocity along the vehicle-fixed $z$-axis | 0 | m/s |
|  | Steer | WhlangFL | Front left wheel steering angle | Computed | rad |
|  |  | WhlangFR | Front right wheel steering angle | Computed | rad |
| RearAxl | Disp | x | Rear wheel displacement along the vehicle-fixed $x$ axis | Computed | m |
|  |  | y | Rear wheel displacement along the vehicle-fixed $y$ axis | Computed | m |
|  |  | z | Rear wheel displacement along the vehicle-fixed $z$ axis | Computed | m |
|  | Vel | xdot | Rear wheel velocity along the vehicle-fixed $x$-axis | Computed | m/s |
|  |  | ydot | Rear wheel velocity along the vehicle-fixed $y$-axis | Computed | m/s |



| Signal | Ang | Bet <br> a | Body slip angle, $\beta$ <br> $\beta=\frac{V_{y}}{V_{x}}$ | Value | Units |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  |  |  | Computed | rad |  |


| Signal |  |  | Description | Value | Units |
| :---: | :---: | :---: | :---: | :---: | :---: |
| PwrInfo | PwrTrnsfrd | PwrFxExt | Externally applied longitudinal force power | Comp uted | W |
|  |  | PwrFyExt | Externally applied lateral force power | Comp uted | W |
|  |  | PwrMzExt | Externally applied roll moment power | Comp uted | W |
|  |  | PwrFwFx | Longitudinal force applied at the front axle power | Comp uted | W |
|  |  | PwrFwFy | Lateral force applied at the front axle power | Comp uted | W |
|  |  | PwrFwRx | Longitudinal force applied at the rear axle power | Comp uted | W |
|  |  | PwrFwRy | Lateral force applied at the rear axle power | Comp uted | W |
|  | PwrNotTrnsfr d | PwrFxDrag | Longitudinal drag force power | Comp uted | W |
|  |  | PwrFyDrag | Lateral drag force power | Comp uted | W |
|  |  | PwrMzDrag | Drag pitch moment power | Comp uted | W |
|  | PwrStored | PwrStoredGrvty | Rate change in gravitational potential energy | Comp uted | W |
|  |  | PwrStoredxdot | Rate of change of longitudinal kinetic energy | Comp uted | W |
|  |  | PwrStoredydot | Rate of change of lateral kinetic energy | Comp uted | W |
|  |  | PwrStoredr | Rate of change of rotational yaw kinetic energy | Comp uted | W |

xdot - Vehicle body longitudinal velocity

## scalar

Vehicle CG velocity along vehicle-fixed x -axis, in $\mathrm{m} / \mathrm{s}$.
ydot - Vehicle body lateral velocity
scalar
Vehicle CG velocity along vehicle-fixed y -axis, in $\mathrm{m} / \mathrm{s}$.
psi - Yaw
scalar
Rotation of the vehicle-fixed frame about earth-fixed Z-axis (yaw), in rad..
$\mathbf{r}$ - Yaw rate
scalar
Vehicle angular velocity, $r$, about the vehicle-fixed $z$-axis (yaw rate), in rad/s.

## Parameters

## Longitudinal

Number of wheels on front axle, NF - Front wheel count
2 (default) | scalar
Number of wheels on front axle, $N_{F}$. The value is dimensionless.
Number of wheels on rear axle, NR - Rear wheel count
2 (default) | scalar
Number of wheels on rear axle, $N_{R}$. The value is dimensionless.
Vehicle mass, m - Vehicle mass
2000 (default) | scalar
Vehicle mass, $m$, in kg .
Longitudinal distance from center of mass to front axle, a-Front axle distance
1.4 (default) | scalar

Horizontal distance $a$ from the vehicle CG to the front wheel axle, in $m$.
Longitudinal distance from center of mass to rear $\mathbf{a x l e}, \mathbf{b}$ - Rear axle distance
1.6 (default) | scalar

Horizontal distance $b$ from the vehicle CG to the rear wheel axle, in $m$.
Vertical distance from center of mass to axle plane, $\mathbf{h}$ - Height
0.35 (default) | scalar

Height of vehicle CG above the axles, $h$, in $m$.
Longitudinal distance from center of mass to hitch, dh - Distance from CM to hitch 1 (default) | scalar

Longitudinal distance from center of mass to hitch, $d h$, in $m$.

## Dependencies

To enable this parameter, on the Input signals pane, select Hitch forces or Hitch moments.
Vertical distance from hitch to axle plane, $\mathbf{h h}$ - Distance from hitch to axle plane 0.2 (default) | scalar

Vertical distance from hitch to axle plane, $h h$, in $m$.

## Dependencies

To enable this parameter, on the Input signals pane, select Hitch forces or Hitch moments.
Initial inertial frame longitudinal position, X_o - Position
0 (default) | scalar
Initial vehicle CG displacement along earth-fixed $X$-axis, in $m$.
Initial longitudinal velocity, xdot_o - Velocity
0 (default) | scalar
Initial vehicle CG velocity along vehicle-fixed $x$-axis, in $m / s$.

## Dependencies

For the Vehicle Body 3DOF Single Track or Vehicle Body 3DOF Dual Track blocks, to enable this parameter, set Axle forces to one of these options:

- External longitudinal forces
- External forces


## Lateral

Front tire corner stiffness, Cy_f - Stiffness
12e3 (default) | scalar
Front tire corner stiffness, $C y_{f}$, in $\mathrm{N} / \mathrm{rad}$.

## Dependencies

For the Vehicle Body 3DOF Single Track or Vehicle Body 3DOF Dual Track blocks, to enable this parameter:

1 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces


## 2 Clear Mapped corner stiffness.

## Rear tire corner stiffness, Cy_r - Stiffness

11e3 (default) | scalar
Rear tire corner stiffness, $C y_{r}$, in N/rad.

## Dependencies

For the Vehicle Body 3DOF Single Track or Vehicle Body 3DOF Dual Track blocks, to enable this parameter:

1 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces


## 2 Clear Mapped corner stiffness.

Initial inertial frame lateral displacement, Y_o - Position
0 (default) | scalar
Initial vehicle CG displacement along earth-fixed $Y$-axis, in $m$.
Initial lateral velocity, ydot_o - Velocity
0 (default) | scalar
Initial vehicle CG velocity along vehicle-fixed $y$-axis, in $\mathrm{m} / \mathrm{s}$.

## Yaw

Yaw polar inertia, Izz - Inertia
4000 (default) | scalar
Yaw polar inertia, in $\mathrm{kg}^{*} \mathrm{~m}^{\wedge} 2$.
Initial yaw angle, psi_o - Psi rotation
0 (default) | scalar
Rotation of the vehicle-fixed frame about earth-fixed Z-axis (yaw), in rad.
Initial yaw rate, r_o - Yaw rate
0 (default) | scalar
Vehicle angular velocity about the vehicle-fixed $z$-axis (yaw rate), in rad/s.

## Aerodynamic

Longitudinal drag area, Af - Effective vehicle cross-sectional area
2 (default) | scalar
Effective vehicle cross-sectional area, $A_{f}$, to calculate the aerodynamic drag force on the vehicle, in $\mathrm{m}^{2}$.

Longitudinal drag coefficient, Cd - Air drag coefficient
. 3 (default) | scalar
Air drag coefficient, $C_{d}$. The value is dimensionless.
Longitudinal lift coefficient, CI - Air lift coefficient
. 1 (default) | scalar
Air lift coefficient, $C_{l}$. The value is dimensionless.
Longitudinal drag pitch moment, Cpm - Pitch drag
. 1 (default) | scalar
Longitudinal drag pitch moment coefficient, $C_{p m}$. The value is dimensionless.
Relative wind angle vector, beta_w - Wind angle
[0:0.01:0.3] (default) | vector
Relative wind angle vector, $\beta_{w}$, in rad.

Side force coefficient vector, Cs - Side force coefficient
[0:0.03:0.9] (default)| vector
Side force coefficient vector coefficient, $C_{s}$. The value is dimensionless.
Yaw moment coefficient vector, Cym - Yaw moment drag
[0:0.01:0.3] (default) | vector
Yaw moment coefficient vector coefficient, $C_{y m}$. The value is dimensionless.

## Environment

Absolute air pressure, Pabs - Pressure
101325 (default) | scalar | scalar
Environmental absolute pressure, $P_{a b s}$, in Pa.
Air temperature, Tair - Temperature
273 (default) | scalar
Environmental absolute temperature, $T$, in K .

## Dependencies

To enable this parameter, clear Air temperature.
Gravitational acceleration, g-Gravity
9.81 (default) | scalar

Gravitational acceleration, $g$, in $\mathrm{m} / \mathrm{s}^{\wedge} 2$.
Nominal friction scaling factor, $\mathbf{m u}$ - Friction scale factor
1 (default) | scalar
Nominal friction scale factor, $\mu$. The value is dimensionless.

## Dependencies

For the Vehicle Body 3DOF Single Track or Vehicle Body 3DOF Dual Track blocks, to enable this parameter:

1 Set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces


## 2 Clear External Friction.

Simulation
Longitudinal velocity tolerance, xdot_tol - Tolerance
. 01 (default) | scalar
Longitudinal velocity tolerance, in $\mathrm{m} / \mathrm{s}$.
Nominal normal force, Fznom - Normal force
5000 (default) | scalar

Nominal normal force, in N .

## Dependencies

For the Vehicle Body 3DOF Single Track or Vehicle Body 3DOF Dual Track blocks, to enable this parameter, set Axle forces to one of these options:

- External longitudinal velocity
- External longitudinal forces

Geometric longitudinal offset from axle plane, longOff - Longitudinal offset 0 (default) | scalar

Vehicle chassis offset from axle plane along body-fixed $x$-axis, in $m$. When you use the 3D visualization engine, consider using the offset to locate the chassis independent of the vehicle CG.

Geometric lateral offset from center plane, latOff - Lateral offset
0 (default) | scalar
Vehicle chassis offset from center plane along body-fixed $y$-axis, in $m$. When you use the 3D visualization engine, consider using the offset to locate the chassis independent of the vehicle CG.

Geometric vertical offset from axle plane, vertOff - Vertical offset
0 (default) | scalar
Vehicle chassis offset from axle plane along body-fixed $z$-axis, in $m$. When you use the 3D visualization engine, consider using the offset to locate the chassis independent of the vehicle CG.

Wrap Euler angles, wrapAng - Selection
off (default) | on
Wrap the Euler angles to the interval [-pi, pi]. For vehicle maneuvers that might undergo vehicle yaw rotations that are outside of the interval, consider deselecting the parameter if you want to:

- Track the total vehicle yaw rotation.
- Avoid discontinuities in the vehicle state estimators.


## Version History

## Introduced in R2018a

## References

[1] Gillespie, Thomas. Fundamentals of Vehicle Dynamics. Warrendale, PA: Society of Automotive Engineers (SAE), 1992.

## Driver Commands

Configure driver

## Description

The Driver Commands block implements the driver model that the reference application uses to generate acceleration, braking, gear, and steering commands. By default, if you select the Reference Generator block parameter Use maneuver-specific driver, initial position, and scene, the reference application selects the driver for the maneuver that you specified.

| Vehicle Command <br> Mode Setting | Implementation |
| :--- | :--- |
| Longitudinal Driver | Longitudinal Driver block - Longitudinal speed-tracking controller. Based <br> on reference and feedback velocities, the block generates normalized <br> acceleration and braking commands that can vary from 0 through 1. Use <br> the block to model the dynamic response of a driver or to generate the <br> commands necessary to track a longitudinal drive cycle. |
| Predictive Driver <br> (default) | Predictive Driver block - Controller that generates normalized steering, <br> acceleration, and braking commands to track longitudinal velocity and a <br> lateral reference displacement. The normalized commands can vary <br> between -1 to 1. The controller uses a single-track (bicycle) model for <br> optimal single-point preview control. |
| Open Loop | Implements an open-loop system so that you can configure the reference <br> application for constant or signal-based steering, acceleration, braking, <br> and gear command input. |

## Ports

## Input

VehRef - Vehicle reference signals
Bus
Bus containing the vehicle reference signals, including longitudinal and lateral displacement, and steering.

VehFdbk - Vehicle feedback signals
Bus
Bus containing vehicle displacement feedback signals.

## Output

Driver - Command signals
Bus
Bus containing the commands, including steering, acceleration, braking, and gear commands.

## Parameters

Vehicle command mode - Enable 3D visualization
Predictive Driver (default)|Longitudinal Driver|Open Loop
Specify driver model.

## Version History

Introduced in R2019a

## See Also

Longitudinal Driver | Predictive Driver

## Reference Generator

Generate maneuver reference signals

## Description

The Reference Generator block sets the parameters that configure the maneuver and 3D simulation environment. By default, the block is set for the constant radius maneuver with the 3D simulation engine environment disabled.

## Model

Use the Maneuver parameter to specify the type of maneuver. After you select the maneuver, use the parameters to specify the maneuver settings. By default:

- Use maneuver-specific driver, initial position, and scene - Set to on
- Maneuver start time - Set to 3s
- Longitudinal velocity reference - Set to 30 s
- Longitudinal entrance velocity setpoint units - Set to mph

| Maneuver Setting | Implementation |
| :--- | :--- |
| Double Lane Change | "Double-Lane Change Maneuver" <br> - Vehicle width - Lane signals for the Visualization subsystem; used <br> for the left and right lane boundaries |
| - Lateral reference data - Lateral reference trajectory as a function |  |
| of the longitudinal distance |  |
| - Distance after target speed to begin reference - Start the |  |
| maneuver at specified distance after the vehicle reaches the target |  |
| speed |  |$|$| "Slowly Increasing Steering Maneuver" |
| :--- |
| - Handwheel rate - Linear rate to increase steering wheel angle |
| - Maximum handwheel angle - Maximum steering wheel angle |


| Maneuver Setting | Implementation |
| :---: | :---: |
| Sine with Dwell | In the test, the vehicle: <br> - Accelerates until it hits a target velocity. <br> - Maintains the target velocity. <br> - Responds to a sinusoidal with dwell steering command. <br> - Steer frequency - Sinusoidal wave frequency <br> - Steer amplitude - Sinusoidal wave amplitude <br> - Dwell time - Dwell time |
| Constant Radius | "Constant Radius Maneuver" <br> - Radius value - Turn radius |
| Fishhook | In the test, the vehicle: <br> - Accelerates until it hits a target velocity. <br> - Maintains the target velocity. <br> - Responds to initial rapid steering input. <br> - Responds to steering overcorrection. <br> - Steer and countersteer speed - Steering rate <br> - Initial dwell time - Initial steer time <br> - Countersteer dwell time - Countersteer time |

## 3D Engine

The 3D engine implements the 3D simulation environment. Vehicle Dynamics Blockset integrates the 3D simulation environment with Simulink so that you can query the world around the vehicle for virtually testing perception, control, and planning algorithms. For 3D engine requirements, see "Unreal Engine Simulation Environment Requirements and Limitations". To enable the 3D engine, on the 3D Engine tab, select Enabled.

To position the vehicle in the scene:
1 Select the position initialization method:

- Recommended for scene - Set the initial vehicle position to values recommended for the scene
- User-specified - Set your own initial vehicle position

2 Click Update the model workspaces with the initial values to overwrite the initial vehicle position in the model workspaces with the applied values.

## Ports

Input
VehFdbk - Vehicle feedback
Bus

Bus containing vehicle feedback signals, including velocity, acceleration, and steering wheel torque.

## Output

Vis - Visualization reference signals
Bus
Bus containing the visualization reference signals, including longitudinal and lateral displacement, and steering.

Ref - Vehicle reference signals
Bus
Bus containing the vehicle reference signals, including longitudinal and lateral displacement, and steering.

Fdbk - Vehicle location feedback signals
Bus
Bus containing vehicle location feedback signals, including position.

## Parameters

Configuration
Maneuver - Select maneuver
Constant Radius (default)|Double Lane Change|Increasing Steer|Swept Sine|Sine with Dwell

Specify the scene type.
Maneuver start time - Start time
scalar
Maneuver start time, in s.
Longitudinal velocity reference - Target velocity
scalar
Target velocity.
Longitudinal entrance velocity setpoint units - Units
mph (default)
Units for target velocity.
Simulation time - Simulation time
scalar
Time, in s.

## Constant Radius

Radius value - Radius
scalar

Radius value, in m.
Turn direction - Turn direction
Right (default)| Left
Turn direction.
Lateral acceleration threshold - Lateral acceleration
scalar
Lateral acceleration threshold, in g.
Stop simulation at lateral acceleration threshold - Selection
off (default) | on
Stop simulation if vehicle exceeds lateral acceleration threshold.

```
Double Lane Change
Inertial longitudinal position of gate entrance - Position
scalar
```

Inertial longitudinal position of gate entrance, in m.
Distance after target speed to begin reference - Start distance scalar

Distance after target speed to begin reference, in $m$.
Vehicle width - Vehicle width
scalar
Vehicle width, in m.
The left and right lane boundaries are a function of the Vehicle width parameter.
Lateral offset - Lateral offset
scalar
Lateral offset, in m.
Lateral reference position breakpoints - Breakpoints
scalar
Lateral reference position breakpoints, in m.
Use the Lateral reference position breakpoints and Lateral reference data parameters to specify the lateral reference trajectory as a function of the longitudinal distance.

Lateral reference data - Lateral data
scalar
Use the Lateral reference position breakpoints and Lateral reference data parameters to specify the lateral reference trajectory as a function of the longitudinal distance.

Increasing Steer
Handwheel rate - Handwheel rate
scalar
Handwheel rate, in deg/s.
Maximum handwheel angle - Maximum handwheel
scalar
Maximum handwheel angle, in deg.
Steering hold time after max angle reached - Steering hold scalar

Steering hold, in s.
Lateral acceleration threshold - Lateral acceleration
scalar
Lateral acceleration threshold, in g.
Stop simulation at lateral acceleration threshold - Selection
off (default) | on
Stop simulation if vehicle exceeds lateral acceleration threshold.

## Swept Sign

Swept time - Sweep time scalar

Sweep time, in s.
Steering amplitude - Steering amplitude scalar

Sinusoidal steering amplitude, in deg.
Final frequency - Final frequency
scalar
Cut off frequency to stop the maneuver, in Hz .
Fishhook
Steer and countersteer speed, steerRate - Steer and countersteer speed scalar

Steer and countersteer speed, in deg/s.
Steer amplitude, steerAFH - Steer amplitude scalar

Steer amplitude, in deg.

Initial dwell time, tDwell1 - Initial dwell time scalar

Initial dwell time, in s.
Countersteer dwell time, tDwell2 - Countersteer dwell time scalar

Countersteer dwell time, in s.
Return to center time, tSteer3 - Return to center time scalar

Return to center time, in s.
Roll rate countersteer initiation zero crossing threshold, pZero - Crossing threshold scalar

Roll rate countersteer initiation zero crossing threshold, in deg.

## 3D Engine

3D Engine - Enable 3D visualization
off (default) | on
Enable 3D visualization.

## Scene - 3D scene

Straight road|Curved road|Parking lot|Double lane change|Open surface|US city block|US highway|Virtual Mcity|Large parking lot

Specify the name of the 3D scene.
Engine frame rate, dt3D - Graphics
. 03 (default)
Graphics frame rate, in s . The graphics frame rate is the inverse of the sample time.
Recommended for scene - Initial vehicle position
on (default) | off
Use vehicle positions that are recommended for the scene.
User-specified - Initial vehicle position
off (default) | on
Specify to set your own initial vehicle position values.
Initial longitudinal position, X_o - Initial longitudinal position
off (default) | on
Initial vehicle CG position along the earth-fixed $X$-axis, in $m$.
Initial lateral position, Y_o - Initial lateral position off (default) | on

Initial vehicle CG position along the earth-fixed $Y$-axis, in $m$.
Initial vertical position, Z_o - Initial vertical position
off (default) | on
Initial vehicle CG position along the earth-fixed $Z$-axis, in m.
Initial roll angle, phi_o - Roll
off (default) | on
Rotation of the vehicle-fixed frame about the earth-fixed $X$-axis (roll), in rad.
Initial pitch angle, theta_o - Pitch
off (default) | on
Rotation of the vehicle-fixed frame about the earth-fixed $Y$-axis (pitch), in rad.
Initial yaw angle, psi_o - Yaw
off (default) | on
Rotation of the vehicle-fixed frame about the earth-fixed $Z$-axis (yaw), in rad.

## Version History

## Introduced in R2019a

## See Also

3D Engine | Driver Commands

## Topics

"Braking Test"
"Constant Radius Maneuver"
"Double-Lane Change Maneuver"
"Slowly Increasing Steering Maneuver"
"Swept-Sine Steering Maneuver"
"How 3D Simulation for Vehicle Dynamics Blockset Works"
"Unreal Engine Simulation Environment Requirements and Limitations"
External Websites
Unreal Engine

## Straight Maneuver Reference Generator

Generate straight maneuver reference signals

## Description

The Straight Maneuver Reference Generator block generates accelerator and brake commands to conduct a straight line maneuver for the "Braking Test". The acceleration begins at the specified rate until the vehicle achieves the longitudinal velocity setpoint. The vehicle controller maintains the longitudinal velocity setpoint for the specified time or distance. The controller then decelerates the vehicle.

Use the Maneuver Parameters to specify the maneuver start time, velocity setpoint, acceleration, and deceleration.

Optionally, on the Tracking Parameters tab, select Enable fault tracking before braking. Use the parameters to specify fault conditions before braking during a split-mu test. If the vehicle speed, steering angle, or yaw rate is not within the allowable range before braking, the block sets a fault condition. The default values represent compliance with ISO $14512^{1}$.

## Ports

Input
VehFdbk - Vehicle feedback
Bus
Bus containing vehicle feedback signals, including velocity, acceleration, and steering wheel torque.

## Output

Ref - Vehicle reference signals
Bus
Bus containing the vehicle reference signals, including longitudinal and lateral displacement, and steering.

## Parameters

## Maneuver Parameters

Maneuver start time, t_start - Start time
2 (default) | scalar
Maneuver start time, in s.

## Longitudinal acceleration at t_start, ax - Longitudinal acceleration

0.5 (default) | scalar

Longitudinal acceleration at maneuver start, in g.

Longitudinal velocity reference, $\mathbf{x d o t} \mathbf{r}$ - Longitudinal velocity reference, $x$ dot_r 20 (default) | scalar

Longitudinal velocity reference, xdot_r, in units specified by Units of velocity, xdotUnit.
Units of velocity, xdotUnit - Units
m/s (default) | km/h | char
Units of velocity.
Brake pedal actuation - Deceleration trigger
Longitudinal displacement (default) | Time
Method to start deceleration.
Select Longitudinal displacement to specify a displacement to start decelerating the vehicle.
Select Time to specify a time to start decelerating the vehicle.
Longitudinal displacement of vehicle CG, x_brake - Displacement
200 (default) | scalar
Longitudinal displacement of vehicle CG to start deceleration, in m.
Dependency
To enable this parameter, set Brake pedal actuation to Longitudinal displacement.
Brake actuation time, t_brake - Time
15 (default) | scalar
Time to start deceleration, in s.

## Dependency

To enable this parameter, set Brake pedal actuation to Time.
Longitudinal deceleration at t_brake, ax_dec - Deceleration
1 (default) | scalar
Longitudinal deceleration at braking time, in g.
Transport delay buffer size, BufferSize - Buffer
4096 (default) | scalar
Transport delay buffer size.
Select handwheel angle to $\mathbf{0}$ deg after braking - Selection
on (default) | off
Set the handwheel angle to 0 after braking.
Tracking Parameters
Enable fault tracking before braking - Enable fault tracking on (default) | off

Select this parameter to enable fault tracking before braking. Use the parameters to specify fault conditions before braking during a split-mu test. If the vehicle speed, steering angle, or yaw rate is not within the allowable range before braking, the block sets a fault condition. The default values represent compliance with ISO $14512^{1}$.

Longitudinal velocity and mean longitudinal velocity, xdot_rmax - Maximum velocity tolerance 1 (default) | scalar

The longitudinal velocity and mean longitudinal velocity tolerance. If the longitudinal velocity or mean longitudinal velocity exceeds the allowable range, the block sets a fault condition.

## Dependencies

To enable this parameter, on the Tracking Parameters tab, select Enable fault tracking before braking.

Mean longitudinal velocity and longitudinal velocity reference, xdot_rmean - Mean velocity tolerance
2 (default) | scalar
The mean longitudinal velocity and longitudinal velocity reference tolerance. If the mean longitudinal velocity or longitudinal velocity exceeds the allowable range, the block sets a fault condition.

## Dependencies

To enable this parameter, on the Tracking Parameters tab, select Enable fault tracking before braking.

Yaw velocity and mean yaw velocity, r_max - Yaw velocity tolerance
1 (default) | scalar
The yaw velocity and mean yaw velocity tolerance, in deg/s. If the yaw velocity or mean yaw velocity exceeds the allowable range, the block sets a fault condition.

## Dependencies

To enable this parameter, on the Tracking Parameters tab, select Enable fault tracking before braking.

Handwheel angle and mean handwheel angle, hw_max - Handwheel angle tolerance 3 (default) | scalar

Handwheel angle and mean handwheel angle, in deg. If the handwheel angle or mean handwheel angle exceeds the allowable range, the block sets a fault condition.

## Dependencies

To enable this parameter, on the Tracking Parameters tab, select Enable fault tracking before braking.

Stop simulation when fault occurs - Select to stop simulation
off (default) | on
Select this parameter to stop the simulation if a fault occurs.

## Dependencies

To enable this parameter, on the Tracking Parameters tab, select Enable fault tracking before braking.

## Version History

Introduced in R2021a

## See Also

Road Track Friction

## Topics

"Braking Test"

## Road Track Friction

Configure road for braking test

## Description

The Road Track Friction block implements the road, including friction, for the "Braking Test". Use the Type of surface parameter to specify the friction coefficient scaling factor:

- Constant friction coefficient scaling factor - Constant surface friction during the maneuver
- Split friction coefficient scaling factor - Two friction coefficients

Select this option to specify the friction scaling coefficients for a split-mu braking test. Use the enabled parameters to set the ground friction and rectangular surface friction coefficient scaling factors.

## Ports

## Input

XWhI - Wheel displacement along X-axis
4-by-1 array
Wheel displacement along the earth-fixed X -axis, specified as a 4-by-1 array.
YWhI - Wheel displacement along Y -axis
4-by-1 array
Wheel displacement along the earth-fixed Y -axis, specified as a 4-by-1 array.
$\mathbf{C g}$ - Vehicle CG
3-by-1 array
Vehicle cg, along earth-fixed axis, specified as a 3-by-1 array.

## Output

FricCoeffLambda - Friction coefficient applied to wheels
4-by-1 array
Wheel friction coefficient, specified as a 4-by-1 array.

## Parameters

Type of surface - Friction
Split friction coefficient scaling factor (default)|Constant friction coefficient scaling factor

- Constant friction coefficient scaling factor - Constant surface friction during the maneuver
- Split friction coefficient scaling factor - Two friction coefficients Select this option to specify the friction scaling coefficients for a split-mu braking test. Use the enabled parameters to set the ground friction and rectangular surface friction coefficient scaling factors.

Scaling factor for the friction coefficient of ground, lambda_g - Scaling factor
. 6 (default) | scalar
Scaling factor for the ground friction coefficient.
Scaling factor for the friction coefficient of rectangular surface, lambda_r - Scaling factor . 8 (default) | scalar

Scaling factor for the friction coefficient of the rectangular surface.

## Dependencies

To enable this parameter, set Type of surface/track to Split friction coefficient scaling factor.
$X$ coordinate of lower left corner of rectangular surface, $\mathbf{r}_{-} \times 0-X$ coordinate
175 (default) | scalar
X coordinate of lower left corner of rectangular surface, in earth-fixed coordinate system, in m .

## Dependencies

To enable this parameter, set Type of surface/track to Split friction coefficient scaling factor.
$\mathbf{Y}$ coordinate of lower left corner of rectangular surface, $\mathbf{r}_{\mathbf{\prime}} \mathbf{y 0} \mathbf{- X}$ coordinate

- 100 (default) | scalar

Y coordinate of lower left corner of rectangular surface, in earth-fixed coordinate system.

## Dependencies

To enable this parameter, set Type of surface/track to Split friction coefficient scaling factor.

Rectangular surface width in X direction, $\mathbf{r}_{\mathbf{-}} \mathbf{x w}$ - Rectangular surface
1000 (default) | scalar
Rectangular surface width in X direction, in m .

## Dependencies

To enable this parameter, set Type of surface/track to Split friction coefficient scaling factor.

Rectangular surface width in Y direction, r_yw - Rectangular surface 500 (default) | scalar

Rectangular surface width in $Y$ direction, in $m$.

## Dependencies

To enable this parameter, set Type of surface/track to Split friction coefficient scaling factor.

## Version History

Introduced in R2021a

## See Also

Straight Maneuver Reference Generator

## Topics

"Braking Test"

## Lane Change Reference Generator

Generate double-lane change maneuver reference signals

## Description

The Lane Change Reference Generator block sets the parameters that configure the double-lane change maneuver.

After the vehicle reaches the reference velocity, the block commands a zero acceleration signal and generates a lateral reference trajectory as a function of the longitudinal displacement. The block also generates signals indicating the left and right lane boundaries as a function of the axle width.

Use the Steady-state initial conditions parameter to specify the initial conditions for the maneuver. By default, the parameter is set to Initialize from model, and the simulation starts with the vehicle at rest at the specified initial position. If you want to start the simulation at the non-zero steady-state velocity:

1 Set Steady-state initial conditions to Solve using block parameters.
2 On the Steady-State Solver tab, specify the initial conditions, workspace variable, and solver settings. Click Generate steady state solution.
3 After the simulation completes, set Steady-state initial conditions to Resume from a workspace variable.
4 Set Steady-state solution to start from, ssVar to the workspace variable you specified in step 2.

5 Run the simulation.
For an example, see "Start Double-Lane Change Maneuver at Target Velocity".

## Ports

Input
VehFdbk - Vehicle feedback
Bus
Bus containing vehicle feedback signals, including velocity, acceleration, and steering wheel torque.

## Output

Lane - Lane boundaries
Bus
Bus containing left, right, and lateral reference lane boundaries.
Ref - Vehicle reference signals
Bus
Bus containing the vehicle reference signals, including longitudinal and lateral displacement, and steering.

## Parameters

Maneuver

Steady-state initial conditions - Start maneuver from steady-state
Initialize from model (default)|Solve using block parameters|Resume from a workspace variable

Use the Steady-state initial conditions parameter to specify the steady-state initial conditions for the maneuver. By default, the simulation will not find or start the simulation at the steady-state operating points.

| Setting | Description |
| :--- | :--- |
| Initialize from model | Simulation starts maneuver at the simulation start time <br> specified by Maneuver start time, t_start at <br> longitudinal velocity of 0. |
| Solve using block parameters | Simulation finds the steady-state operating points using <br> the parameters on the Steady-State Solver tab. |
| Resume from a workspace variable | Simulation starts at the steady-state operating points <br> workspace variable specified by Steady-state solution <br> to start from, ssVar. |

Steady-state solution to start from, ssVar - Workspace variable with steady-state operating points
char
Workspace variable containing the steady-state operating points.

## Dependencies

To enable this parameter, set Steady-state initial conditions to Resume from a workspace variable.

Maneuver start time, t_start - Start time
scalar
Maneuver start time, in s.

## Dependencies

To enable this parameter, set Steady-state initial conditions to Initialize from model.
Inertial longitudinal position of gate entrance, XGate - Position
175 (default) | scalar
Inertial longitudinal position of gate entrance, in m .
Longitudinal entrance velocity setpoint, xdot_r - Target velocity
35 (default) | scalar
Target velocity.

## Dependencies

To enable this parameter, set Steady-state initial conditions to Initialize from model or Solve using block parameters.

Longitudinal entrance velocity setpoint units, xdotUnit - Units
mph (default)
Units for target velocity.
Dependencies
To enable this parameter, set Steady-state initial conditions to Initialize from model or Solve using block parameters.

Vehicle width, vehW - Vehicle width
2 (default) | scalar
Vehicle width, in m.
The left and right lane boundaries are a function of the Vehicle width parameter.
Lateral offset, latoff - Lateral offset
scalar
Lateral offset, in m.
Lateral reference position breakpoints, latRefbp - Breakpoints
scalar
Lateral reference position breakpoints, in $m$.
Use the Lateral reference position breakpoints and Lateral reference data parameters to specify the lateral reference trajectory as a function of the longitudinal distance.

Lateral reference data, latRef - Lateral data
scalar
Use the Lateral reference position breakpoints and Lateral reference data parameters to specify the lateral reference trajectory as a function of the longitudinal distance.

## Dependencies

To enable this parameter, set Steady-state initial conditions to Initialize from model or Solve using block parameters.

## Steady-State Solver

Initial longitudinal position, X_o - Initial longitudinal position
175 (default) | scalar
Initial vehicle CG position along the earth-fixed $X$-axis, in $m$.

## Dependencies

To enable this parameter, set Steady-state initial conditions to Solve using block parameters.

Initial lateral position, Y_o - Initial lateral position scalar

Initial vehicle CG position along the earth-fixed $Y$-axis, in $m$.

## Dependencies

To enable this parameter, set Steady-state initial conditions to Solve using block parameters.

Initial heading (yaw) angle, psi_o - Initial yaw angle
scalar
Initial vehicle yaw angle about the earth-fixed $Z$-axis, in rad.

## Dependencies

To enable this parameter, set Steady-state initial conditions to Solve using block parameters.

Steady-state solver tolerance, ssTol - Solver velocity tolerance
scalar
Steady-state solver velocity tolerance.

## Dependencies

To enable this parameter, set Steady-state initial conditions to Solve using block parameters.

Maximum simulated time to reach steady-state, ssMaxTime - Max time scalar

Maximum simulated time to reach steady-state, in s.

## Dependencies

To enable this parameter, set Steady-state initial conditions to Solve using block parameters.

Workspace variable name to generate, ssWSName - Steady-state operating points scalar

Name of workspace variable containing steady-state operating points.

## Dependencies

To enable this parameter, set Steady-state initial conditions to Solve using block parameters.

## Version History

Introduced in R2019a

## See Also

Driver Commands

## Topics

"Double-Lane Change Maneuver"
"Start Double-Lane Change Maneuver at Target Velocity"

## Slowly Increasing Steer Reference Generator

Generate slowly increasing steer maneuver reference signals

## Description

The Slowly Increasing Steer Reference Generator block sets the parameters that configure the slowly increasing steer maneuver.

The block generates steering, accelerator, and brake commands to conduct a linearly increasing steering maneuver. The steering command begins at the specified rate once the vehicle reaches the longitudinal velocity setpoint. After the vehicle achieves the maximum steering angle, the vehicle maintains the steering angle for a desired duration. The block then reduces the steering angle to zero at the same rate. A longitudinal controller regulates the vehicle at the prescribed speed throughout the maneuver.

Use the Steady-state solver mode parameter to specify the initial conditions for the maneuver. By default, the parameter is set to Initialize from model, and the simulation starts with the vehicle at rest at the specified initial position. If you want to start the simulation at the non-zero steady-state velocity:

1 Set Steady-state solver mode to Solve using block parameters.
2 On the Steady-State Solver tab, specify the initial conditions, workspace variable, and solver settings. Click Generate steady state solution.
3 After the simulation completes, set Steady-state solver mode to Resume from a workspace variable.

4 Set Steady-state solution to start from, ssVar to the workspace variable you specified in step 2.

5 Run the simulation.

## Ports

Input
VehFdbk - Vehicle feedback
Bus
Bus containing vehicle feedback signals, including velocity, acceleration, and steering wheel torque.

## Output

Ref - Vehicle reference signals
Bus
Bus containing the vehicle reference signals, including longitudinal and lateral displacement, and steering.

## Parameters

Maneuver
Steady-state solver mode - Start maneuver from steady-state
Initialize from model (default)|Solve using block parameters|Resume from a workspace variable

Use the Steady-state solver mode parameter to specify the steady-state initial conditions for the maneuver. By default, the simulation will not find or start the simulation at the steady-state operating points.

| Setting | Description |
| :--- | :--- |
| Initialize from model | Simulation starts maneuver at the simulation start time <br> specified by Maneuver start time, t_start at <br> longitudinal velocity of 0. |
| Solve using block parameters | Simulation finds the steady-state operating points using <br> the parameters on the Steady-State Solver tab. |
| Resume from a workspace variable | Simulation starts at the steady-state operating points <br> workspace variable specified by Steady-state solution <br> to start from, ssVar. |

Steady-state solution to start from, ssVar - Workspace variable with steady-state operating points
char
Workspace variable containing the steady-state operating points.

## Dependencies

To enable this parameter, set Steady-state initial conditions to Resume from a workspace variable.

Maneuver start time, t_start - Start time
scalar
Maneuver start time, in s.

## Dependencies

To enable this parameter, set Steady-state initial conditions to Initialize from model.
Longitudinal speed setpoint, xdot_r - Target velocity
50 (default) | scalar
Target velocity.
Longitudinal speed setpoint units, xdotUnit - Units
mph (default)
Units for target velocity.
Handwheel rate, omega_hw - Handwheel rate scalar

Handwheel rate, in deg/s.
Maximum absolute handwheel angle, theta_max - Maximum handwheel scalar

Maximum handwheel angle, in deg.
Steering hold time after max angle reached, t_stop - Steering hold scalar

Steering hold, in s.
Lateral acceleration absolute threshold, ay_max - Lateral acceleration scalar

Lateral acceleration threshold, in g.
Steady-State Solver
Initial longitudinal position, X_o - Initial longitudinal position
175 (default) | scalar
Initial vehicle CG position along the earth-fixed $X$-axis, in m.

## Dependencies

To enable this parameter, set Steady-state initial conditions to Solve using block parameters.

Initial lateral position, Y_o - Initial lateral position
scalar
Initial vehicle CG position along the earth-fixed $Y$-axis, in $m$.

## Dependencies

To enable this parameter, set Steady-state initial conditions to Solve using block parameters.

Initial heading (yaw) angle, psi_o - Initial yaw angle scalar

Initial vehicle yaw angle about the earth-fixed $Z$-axis, in rad.

## Dependencies

To enable this parameter, set Steady-state initial conditions to Solve using block parameters.

Steady-state solver tolerance, ssTol - Solver velocity tolerance scalar

Steady-state solver velocity tolerance.

## Dependencies

To enable this parameter, set Steady-state initial conditions to Solve using block parameters.

Maximum simulated time to reach steady-state, ssMaxTime - Max time scalar

Maximum simulated time to reach steady-state, in s.

## Dependencies

To enable this parameter, set Steady-state initial conditions to Solve using block parameters.

Workspace variable name to generate, ssWSName - Steady-state operating points scalar

Name of workspace variable containing steady-state operating points.

## Dependencies

To enable this parameter, set Steady-state initial conditions to Solve using block parameters.

# Version History <br> Introduced in R2019a 

## See Also

Driver Commands

## Topics

"Slowly Increasing Steering Maneuver"

## Swept Sine Reference Generator

Generate swept-sine maneuver reference signals

## Description

The Swept Sine Reference Generator block sets the parameters that configure the swept-sine maneuver. Once the vehicle reaches the target longitudinal velocity, the block generates a sinusoidal steering command with linearly increasing frequency, up to the maximum specified in the allotted time.

Use the Steady-state solver mode parameter to specify the initial conditions for the maneuver. By default, the parameter is set to Initialize from model, and the simulation starts with the vehicle at rest at the specified initial position. If you want to start the simulation at the non-zero steady-state velocity:

1 Set Steady-state solver mode to Solve using block parameters.
2 On the Steady-State Solver tab, specify the initial conditions, workspace variable, and solver settings. Click Generate steady state solution.
3 After the simulation completes, set Steady-state solver mode to Resume from a workspace variable.
4 Set Steady-state solution to start from, ssVar to the workspace variable you specified in step 2.

5 Run the simulation.

## Ports

Input
VehFdbk - Vehicle feedback
Bus
Bus containing vehicle feedback signals, including velocity, acceleration, and steering wheel torque.

## Output

Ref - Vehicle reference signals
Bus
Bus containing the vehicle reference signals, including longitudinal and lateral displacement, and steering.

## Parameters

## Maneuver

Steady-state solver mode - Start maneuver from steady-state
Initialize from model (default)|Solve using block parameters|Resume from a workspace variable

Use the Steady-state solver mode parameter to specify the steady-state initial conditions for the maneuver. By default, the simulation will not find or start the simulation at the steady-state operating points.

| Setting | Description |
| :--- | :--- |
| Initialize from model | Simulation starts maneuver at the simulation start time <br> specified by Maneuver start time, t_start at <br> longitudinal velocity of 0. |
| Solve using block parameters | Simulation finds the steady-state operating points using <br> the parameters on the Steady-State Solver tab. |
| Resume from a workspace variable | Simulation starts at the steady-state operating points <br> workspace variable specified by Steady-state solution <br> to start from, ssVar. |

## Steady-state solution to start from, ssVar - Workspace variable with steady-state operating points <br> char

Workspace variable containing the steady-state operating points.

## Dependencies

To enable this parameter, set Steady-state initial conditions to Resume from a workspace variable.

Maneuver start time, t_start - Start time
scalar
Maneuver start time, in s.

## Dependencies

To enable this parameter, set Steady-state initial conditions to Initialize from model.

## Longitudinal velocity setpoint, xdot_ref - Target velocity

## 50 (default) | scalar

Target velocity.

## Longitudinal speed setpoint units, xdotUnit - Units

mph (default)
Units for target velocity.

## Steering amplitude, theta_hw - Steering amplitude

 scalarSinusoidal steering amplitude, in deg.
Final frequency, theta_hw_final - Final frequency scalar

Cut off frequency to stop the maneuver, in Hz .

## Swept time, t_sweep - Sweep time

## scalar

Sweep time, in s.
Steady-State Solver
Initial longitudinal position, X_o - Initial longitudinal position
175 (default) | scalar
Initial vehicle CG position along the earth-fixed $X$-axis, in m.
Dependencies
To enable this parameter, set Steady-state initial conditions to Solve using block parameters.

Initial lateral position, Y_o - Initial lateral position
scalar
Initial vehicle CG position along the earth-fixed $Y$-axis, in $m$.

## Dependencies

To enable this parameter, set Steady-state initial conditions to Solve using block parameters.

Initial heading (yaw) angle, psi_o - Initial yaw angle
scalar

Initial vehicle yaw angle about the earth-fixed $Z$-axis, in rad.

## Dependencies

To enable this parameter, set Steady-state initial conditions to Solve using block parameters.

Steady-state solver tolerance, ssTol - Solver velocity tolerance
scalar
Steady-state solver velocity tolerance.

## Dependencies

To enable this parameter, set Steady-state initial conditions to Solve using block parameters.

Maximum simulated time to reach steady-state, ssMaxTime - Max time scalar

Maximum simulated time to reach steady-state, in s.

## Dependencies

To enable this parameter, set Steady-state initial conditions to Solve using block parameters.

Workspace variable name to generate, ssWSName - Steady-state operating points scalar

Name of workspace variable containing steady-state operating points.
Dependencies
To enable this parameter, set Steady-state initial conditions to Solve using block parameters.

# Version History <br> Introduced in R2019a 

## See Also

Driver Commands

## Topics

"Swept-Sine Steering Maneuver"

11

Classes

## sim3d.Editor

Interface to the Unreal Engine project

## Description

Use the sim3d.Editor class to interface with the Unreal Editor.
To develop scenes with the Unreal Editor and co-simulate with Simulink, you need the Vehicle Dynamics Blockset Interface for Unreal Engine 4 Projects support package. The support package contains an Unreal Engine project that allows you to customize the Vehicle Dynamics Blockset scenes. For information about the support package, see "Customize 3D Scenes for Vehicle Dynamics Simulations".

## Creation

## Syntax

sim3d.Editor(project)

## Description

MATLAB creates an sim3d.Editor object for the Unreal Editor project specified in sim3d.Editor( project).

Input Arguments
project - Project path and name
string array
Project path and name.
Example: "C:\Local\AutoVrtlEnv\AutoVrtlEnv.uproject"
Data Types: string

## Properties

## Uproject - Project path and name <br> string array

This property is read-only.
Project path and name with Unreal Engine project file extension.
Example: "C:\Local\AutoVrtlEnv\AutoVrtlEnv.uproject"
Data Types: string

## Object Functions

open Open the Unreal Editor

## Examples

## Open Project in Unreal Editor

Open an Unreal Engine project in the Unreal Editor.
Create an instance of the sim3d.Editor class for the Unreal Engine project located in C: \Local \AutoVrtlEnv\AutoVrtlEnv.uproject.
editor = sim3d.Editor(fullfile("C:\Local\AutoVrtlEnv\AutoVrtlEnv.uproject"))
Open the project in the Unreal Editor.
editor.open();

## Version History

Introduced in R2019b

## See Also

## Topics

"Customize 3D Scenes for Vehicle Dynamics Simulations"
"How 3D Simulation for Vehicle Dynamics Blockset Works"
"Unreal Engine Simulation Environment Requirements and Limitations"

## open

Open the Unreal Editor

## Syntax

[status,result] = open(sim3dEditor0bj)

## Description

[status, result] = open(sim3dEditorObj) opens the Unreal Engine project in the Unreal Editor.

To develop scenes with the Unreal Editor and co-simulate with Simulink, you need the Vehicle Dynamics Blockset Interface for Unreal Engine 4 Projects support package. The support package contains an Unreal Engine project that allows you to customize the Vehicle Dynamics Blockset scenes. For information about the support package, see "Customize 3D Scenes for Vehicle Dynamics Simulations".

## Input Arguments

sim3dEditorObj - sim3d.Editor object
sim3d.Editor object
sim3d.Editor object for the Unreal Engine project.

## Output Arguments

## status - Command exit status

0 | nonzero integer
Command exit status, returned as either 0 or a nonzero integer. When the command is successful, status is 0 . Otherwise, status is a nonzero integer.

- If command includes the ampersand character ( $\delta$ ), then status is the exit status when command starts
- If command does not include the ampersand character ( $\&$ ), then status is the exit status upon command completion.
result - Output of operating system command
character vector
Output of the operating system command, returned as a character vector. The system shell might not properly represent non-Unicode ${ }^{\circledR}$ characters.


## Version History

Introduced in R2019b

## See Also

sim3d.Editor

## Topics

"Customize 3D Scenes for Vehicle Dynamics Simulations"
"How 3D Simulation for Vehicle Dynamics Blockset Works"
"Unreal Engine Simulation Environment Requirements and Limitations"

## ASim3dActor

Abstract class to use as a base class for user-defined Unreal Engine C++ or blueprint actors

## Description

ASim3dActor is an abstract class that you can use as a base class for user-defined Unreal Engine C+ + or blueprint actors.

The base classes are inherently synchronized during co-simulation with a Simulink model.
Additionally, the Simulation 3D Actor Transform Set block can control the base class. To extend behavior of ASim3dActor, you can use the message interface functions to override the class methods so they send and receive messages to and from a model.

ASim3dActor is included in the Vehicle Dynamics Blockset Interface for Unreal Engine 4 Projects. For information about the support package, see "Customize 3D Scenes for Vehicle Dynamics Simulations".

## Properties

## Translation - Actor translation

1-by-3 (default) | number of parts per actor-by-3
This property is protected. It is used in the derived C++ class. Value is set by the Simulation 3D Actor Transform Set block.

Actor translation along world $X$-, $Y$, and $Z$ - axes, respectively, in m. Array dimensions are number of parts per actor-by-3.
Data Types: float

## Rotation - Actor rotation

1-by-3 (default) | number of parts per actor-by-3
This property is protected. It is used in the derived C++ class. Value is set by the Simulation 3D Actor Transform Set block.

Actor rotation across a $[-\mathrm{pi} / 2, \mathrm{pi} / 2]$ range about world $X$-, $Y$, and $Z$ - axes, respectively, in rad. Array dimensions are number of parts per actor-by-3.

## Data Types: float

## Scale - Actor scale

1-by-3 (default) | number of parts per actor-by-3
This property is protected. It is used in the derived C++ class. Value is set by the Simulation 3D Actor Transform Set block.

Actor scale. Array dimensions are number of parts per actor-by-3.
Data Types: float

## Object Functions

Sim3dSetup C++ method that sets up actor in Unreal Engine 3D simulation
Sim3dStep C++ method that steps actor in Unreal Engine 3D simulation
Sim3dRelease C++ method that releases actor in Unreal Engine 3D simulation

## Version History

Introduced in R2020b

See Also<br>StartSimulation3DMessageReader | ReadSimulation3DMessage |<br>StopSimulation3DMessageReader|StartSimulation3DMessageWriter|<br>WriteSimulation3DMessage|StopSimulation3DMessageWriter

External Websites
Unreal Engine 4 Documentation

## Sim3dSetup

C++ method that sets up actor in Unreal Engine 3D simulation

## Syntax

void ASetGetActorLocation::Sim3dSetup()

## Description

The C++ method void ASetGetActorLocation::Sim3dSetup() sets up an actor in the Unreal Engine 3D simulation environment. The Unreal Engine AActor: : BeginPlay class calls the Sim3dSetup method every frame.

## Examples

## Set Up Actor

void ASetGetActorLocation: :Sim3dSetup()
\{
Super::Sim3dSetup();
if (Tags.Num() != 0) \{
FString tagName = Tags. Top().ToString();
FString MessageReaderTag = tagName;
MessageReaderTag.Append(TEXT("SimulinkMessage_OUT")); // a message from Simulink model
MessageReader = StartSimulation3DMessageReader (TCHAR_TO_ANSI (*MessageReaderTag), MAX_MESSAGE_SIZE);
FString MessageWriterTag = tagName;
MessageWriterTag.Append(TEXT("SimulinkMessage_IN")); // a message to Simulink model
MessageWriter = StartSimulation3DMessageWriter (TCHAR_TO_ANSI (*MessageWriterTag) ), MAX_MESSAGE_SIZE);
\}
\}

## Version History

Introduced in R2020b

## See Also

ASim3dActor

## Topics

"Customize 3D Scenes for Vehicle Dynamics Simulations"

## External Websites

Unreal Engine 4 Documentation

## Sim3dStep

C++ method that steps actor in Unreal Engine 3D simulation

## Syntax

void ASetGetActorLocation::Sim3dStep(float DeltaSeconds)

## Description

The C++ method void ASetGetActorLocation::Sim3dStep(float DeltaSeconds) steps an actor in the Unreal Engine 3D simulation environment. The Unreal Engine AActor: :Tick class calls the Sim3dStep method.

## Examples

## Step Actor

```
void ASetGetActorLocation::Sim3dStep(float DeltaSeconds)
```

\{
Super::Sim3dStep(DeltaSeconds);
uint32 messageSize = MAX_MESSAGE_SIZE;
int statusR = ReadSimulātion3DMessage (MessageReader, \&messageSize, message);
int statusW = WriteSimulation3DMessage (MessageWriter, messageSize, message);
\}

## Input Arguments

DeltaSeconds - Elapsed time
. 01
Time elapsed since Unreal Engine modified the frame.
Data Types: float

## Version History <br> Introduced in R2020b

## See Also

ASim3dActor

## Topics

"Customize 3D Scenes for Vehicle Dynamics Simulations"

## External Websites

Unreal Engine 4 Documentation

## Sim3dRelease

C++ method that releases actor in Unreal Engine 3D simulation

## Syntax

void ASetGetActorLocation::Sim3dRelease()

## Description

The C++ method void ASetGetActorLocation::Sim3dRelease() releases an actor in the Unreal Engine 3D simulation environment. The Unreal Engine AActor: : EndPlay class calls the Sim3dRelease method when the 3D simulation ends.

## Examples

```
Release Actor
void ASetGetActorLocation::Sim3dRelease()
{
    Super::Sim3dRelease();
    if (MessageReader) {
            StopSimulation3DMessageReader (SignalReader);
    }
    MessageReader = nullptr;
    if (MessageWriter) {
            StopSimulation3DMessageWriter (SignalWriter);
    }
    MessageWriter = nullptr;
}
```


## Version History

Introduced in R2020b

## See Also

ASim3dActor

## Topics

"Customize 3D Scenes for Vehicle Dynamics Simulations"

## External Websites

Unreal Engine 4 Documentation

## StartSimulation3DMessageReader

Constructs a message reader object in the Unreal Editor

## Syntax

MessageReader = StartSimulation3DMessageReader(topicName, maxDataSize)

## Description

MessageReader = StartSimulation3DMessageReader(topicName, maxDataSize) constructs a message reader object in the Unreal Editor.

The C++ syntax is
void *StartSimulation3DMessageReader(const char* topicName,uint32 maxDataSize);

## Input Arguments

topicName - Simulink signal topic name
mySignal
Name of the Simulink signal with the message topic.
Data Types: char *
maxDataSize - Maximum size of data
number of bytes|scalar
Maximum size of the data, in bytes.
Data Types: uint32

## Output Arguments

MessageReader - Pointer to message reader object
object pointer
Pointer to message reader object, ReadSimulation3DMessage.
Data Types: void *

## Version History

Introduced in R2020b

## See Also

ASim3dActor

## Topics

"Customize 3D Scenes for Vehicle Dynamics Simulations"

## External Websites

Unreal Engine 4 Documentation

## ReadSimulation3DMessage

Receives message from Simulink model using a message reader object

## Syntax

status=ReadSimulation3DMessage(MessageReader, dataSize, data)

## Description

status=ReadSimulation3DMessage(MessageReader, dataSize, data) receives a message from a Simulink model using a message reader object.

The C++ syntax is
int ReadSimulation3DMessage(void *MessageReader, uint32 dataSize, void *data);

## Input Arguments

## MessageReader - Pointer to message reader object

object pointer
Pointer to message reader object, ReadSimulation3DMessage.
Data Types: void *
dataSize - Size of data
number of bytes|scalar
Size of data, that is, data (sizeof(datatype) *num of elements). For example, if you want to read a vector of 3 floats, the data size is sizeof (float) $\bar{*} * 3$.

Data Types: uint32
data - Pointer to data object
object pointer
Pointer to data object.
Data Types: void *

## Output Arguments

## status - Operation exit status

0 | nonzero integer
Status, returned as either 0 or a nonzero integer. When the operation is successful, status is 0 . Otherwise, status is a nonzero integer.

## Version History

Introduced in R2020b

## See Also

ASim3dActor

## Topics

"Customize 3D Scenes for Vehicle Dynamics Simulations"

## External Websites

Unreal Engine 4 Documentation

## StopSimulation3DMessageReader

Deletes message reader object in the Unreal Editor

## Syntax

status=StopSimulation3DMessageReader(MessageReader)

## Description

status=StopSimulation3DMessageReader(MessageReader) deletes the Unreal Editor 3D message reader object.

The C++ syntax is
int StopSimulation3DMessageReader(void * MessageReader);

## Input Arguments

MessageReader - Pointer to message reader object
object pointer
Pointer to message reader object, ReadSimulation3DMessage.
Data Types: void *

## Output Arguments

## status - Operation exit status

0 | nonzero integer
Status, returned as either 0 or a nonzero integer. When the operation is successful, status is 0 . Otherwise, status is a nonzero integer.

## Version History

Introduced in R2020b

## See Also

ASim3dActor

## Topics

"Customize 3D Scenes for Vehicle Dynamics Simulations"
External Websites
Unreal Engine 4 Documentation

## StartSimulation3DMessageWriter

Constructs a message writer object in the Unreal Editor

## Syntax

MessageWriter $=$ StartSimulation3DMessageWriter(topicName, maxDataSize)

## Description

MessageWriter = StartSimulation3DMessageWriter(topicName, maxDataSize) constructs a message writer object in the Unreal Editor.

The C++ syntax is
void *StartSimulation3DMessageWriter(const char* topicName, uint32 maxDataSize);

## Input Arguments

topicName - Simulink signal topic name
mySignal
Name of the Simulink signal with the message topic.
Data Types: char *
maxDataSize - Maximum size of data
number of bytes|scalar
Maximum size of the data, in bytes.
Data Types: uint32

## Output Arguments

MessageWriter - Pointer to message writer object
object pointer
Pointer to message writer object, WriteSimulation3DMessage.
Data Types: void *

## Version History

Introduced in R2020b

## See Also

ASim3dActor

## Topics

"Customize 3D Scenes for Vehicle Dynamics Simulations"

## External Websites

Unreal Engine 4 Documentation

## WriteSimulation3DMessage

Sends message to Simulink model using a message writer object

## Syntax

status=WriteSimulation3DMessage(MessageWriter, dataSize, data)

## Description

status=WriteSimulation3DMessage(MessageWriter, dataSize, data) sends a message to a Simulink model using a message writer object.

The C++ syntax is
int WriteSimulation3DMessage(void * MessageWriter, uint32 dataSize, void *data);

## Input Arguments

## MessageWriter - Pointer to message writer object

object pointer
Pointer to message writer object, WriteSimulation3DMessage.
Data Types: void *
dataSize - Size of data
number of bytes|scalar
Size of data, that is, data (sizeof(datatype) *num_of_elements). For example, if you want to read a vector of 3 floats, the data size is sizeof (float) $\bar{*} * 3$.

Data Types: uint32
data - Pointer to data object
object pointer
Pointer to data object.
Data Types: void *

## Output Arguments

## status - Operation exit status

0 | nonzero integer
Status, returned as either 0 or a nonzero integer. When the operation is successful, status is 0 . Otherwise, status is a nonzero integer.

## Version History

Introduced in R2020b

## See Also

ASim3dActor

## Topics

"Customize 3D Scenes for Vehicle Dynamics Simulations"

## External Websites

Unreal Engine 4 Documentation

## StopSimulation3DMessageWriter

Deletes message writer object in the Unreal Editor

## Syntax

status=StopSimulation3DMessageWriter(MessageWriter)

## Description

status=StopSimulation3DMessageWriter(MessageWriter) deletes the Unreal Editor 3D message writer object.

The C++ syntax is
int StopSimulation3DMessageWriter(void *MessageWriter);

## Input Arguments

MessageWriter - Pointer to message writer object
object pointer
Pointer to message writer object, WriteSimulation3DMessage.
Data Types: void *

## Output Arguments

status - Operation exit status
0 | nonzero integer
Status, returned as either 0 or a nonzero integer. When the operation is successful, status is 0 . Otherwise, status is a nonzero integer.

## Version History

Introduced in R2020b

## See Also

ASim3dActor

## Topics

"Customize 3D Scenes for Vehicle Dynamics Simulations"
External Websites
Unreal Engine 4 Documentation

## copyExampleSim3dProject

Copy support package files and plugins to specified folders

## Syntax

sim3d.utils.copyExampleSim3dProject(DestFldr)
sim3d.utils.copyExampleSim3dProject(DestFldr, Name=Value)

## Description

sim3d.utils.copyExampleSim3dProject(DestFldr) copies the Vehicle Dynamics Blockset Interface for Unreal Engine 4 Projects support package project files to the destination folder, DestFldr. By default, copyExampleSim3dProject copies the plugins to your Epic Games installation folder.
sim3d.utils.copyExampleSim3dProject(DestFldr, Name=Value) copies support package files to the destination with additional options specified by name-value arguments.

Running the sim3d.utils.copyExampleSim3dProject function configures your environment so that you can customize scenes. The support package contains these Vehicle Dynamics Blockset Interface for Unreal Engine 4 Projects.

- An Unreal project, defined in AutoVrtlEnv. uproject, and its associated files. The project includes editable versions of the prebuilt 3D scenes that you can select from the Scene name parameter of the Simulation 3D Scene Configuration block.
- Three plugins, MathWorkSimulation: RoadRunnerMaterials, and MathWorksAutomotiveContent. These plugins establish the connection between MATLAB and the Unreal Editor and are required for co-simulation.


## Input Arguments

## DestFldr - Destination folder for Unreal project files

character vector
Destination folder name, specified as a character vector.
Running copyExampleSim3dProject copies the Unreal project, defined in AutoVrtlEnv.uproject, and its associated files to the destination folder.

Note You must have write permission for the destination folder.

Example: C:\project
Data Types: char|string

## Name-Value Pair Arguments

Specify optional pairs of arguments as Name1=Value1, . . . NameN=ValueN, where Name is the argument name and Value is the corresponding value. Name-value arguments must appear after other arguments, but the order of the pairs does not matter.

## Source - Support package source folder

character vector
Support package source folder, specified as a character vector. The folder contains the downloaded support packages files.

By default, if you do not specify the source folder, copyExampleSim3dProject copies the file from the support package installation folder, matlabshared.supportpkg.getSupportPackageRoot().
Example: Source="shared\sim3dprojects\spkg\"
Data Types: char \| string

## PluginDestination - Option to change the plugin destination folder

character vector
Option to change the plugin destination folder, specified as a character vector.
By default, if you do not change the plugin installation folder location, copyExampleSim3dProject tries to copy the plugins to C:\Program Files $\backslash$ Epic Games\UE_4.27\Engine\Plugins \MathWorks.
Example: PluginDestination="C:\Program Files\Epic Games\UE_4.27\Engine\Plugins \MathWorks"
Data Types: char | string

## VerboseOutput - Option to enable verbose logging

0 or false (default) | 1 or true
Option to enable verbose logging, specified as a logical 0 (false) or 1 (true). Verbose logging displays intermediate iteration information on the MATLAB command line.

## Example: VerboseOutput=true

Data Types: logical

## Examples

## Copy Support Package Files to Destination Folder

Copy the support package files to $C: \backslash p r o j e c t$.

```
sim3d.utils.copyExampleSim3dProject("C:\project");
```

Copy the support package files to C:\project with VerboseOutput set to true.

```
sim3d.utils.copyExampleSim3dProject("C:\project", VerboseOutput=true)
Copying ...\spkg\project\AutoVrtlEnv to C:\project\AutoVrtlEnv
Creating C:\project\AutoVrtlEnv\Plugins
```

Copying ...\spkg\plugins\mw_aerospace\MathWorksAerospace to C:\project\AutoVrtlEnv\Plugins\MathW Copying ...\spkg\plugins\mw_automotive\MathWorksAutomotiveContent to C:\project\AutoVrtlEnv\Plug Copying ... \spkg\plugins\mw simulation\MathWorksSimulation to C:\project\AutoVrtlEnv\Plugins\Mat Copying ...\spkg\plugins\mw_uav\MathWorksUAVContent to C:\project\AutoVrtlEnv\Plugins\MathWorksU Copying ...\spkg\plugins\rr_materials \RoadRunnerMaterials to C:\project\AutoVrtlEnv\Plugins\Road
Ensuring C:\project\AutoVrtlEnv\AutoVrtlEnv.uproject is writable
Enabling plugin MathWorksSimulation in C:\project $\backslash$ AutoVrtlEnv\AutoVrtlEnv.uproject
Enabling plugin MathWorksUAVContent in C:\project\AutoVrtlEnv\AutoVrtlEnv.uproject
Enabling plugin MathWorksAutomotiveContent in C:\project\AutoVrtlEnv\AutoVrtlEnv.uproject
Enabling plugin RoadRunnerMaterials in C:\project\AutoVrtlEnv\AutoVrtlEnv.uproject

## Version History

Introduced in R2022b

## See Also

## Topics

"Install Support Package and Configure Environment"
"How 3D Simulation for Vehicle Dynamics Blockset Works"
"Unreal Engine Simulation Environment Requirements and Limitations"

## External Websites

Unreal Engine
Using Unreal Engine with Simulink

## sim3d.maps

Access additional scenes from the server

## Description

Use the sim3d.maps to download and access additional scenes from the server so that they can be automatically available in the Simulation 3D Scene Configuration block.

Object Functions<br>sim3d.maps.Map.download Download maps from the server<br>sim3d.maps.Map.server List of maps available for download from the server<br>sim3d.maps.Map.delete Delete local maps downloaded from the server<br>sim3d.maps.Map.local List of locally available maps

## Troubleshooting

- If you cannot reach the server, the download will fail due to a timeout.
- If the download fails while updating an existing map, the existing outdated file will remain functional.
- If you delete the CSV file, you will lose automatic tracking of updates for the existing maps.


## Version History

Introduced in R2022b

## See Also

Simulation 3D Scene Configuration

## sim3d.maps.Map.download

Download maps from the server

## Syntax

sim3d.maps.Map.download(Scene)

## Description

sim3d.maps.Map.download(Scene) downloads the map Scene from the server.

## Examples

## Download Suburban Scene Map

This example shows how to download and access the Suburban scene map from the Simulation 3D Scene Configuration block.

To begin, check the maps available in the server.

```
sim3d.maps.Map.server
```

MapName
"Suburban scene"

Description
"a suburban area beyond the city's border"

Version
"1"

MinimumRelease
"R2022b"

Download the Suburban scene from the server.
sim3d.maps.Map.download('Suburban scene')
Map is susccesfully downloaded and is up-to-date
Check if the downloaded maps are available in your local machine.
sim3d.maps.Map.local

MapName
"Suburban scene"

Description
"a suburban area beyond the city's border"

Version
"1"

MinimumRelease
"R2022b"
Add the Simulation 3D Scene Configuration block to your model.


Open the block mask and select the suburban scene from Scene name.


Run the model.


## Input Arguments

## Scene - Name of scene

string | character array
Name of the map being downloaded from the server, specified as a string or character array. Maps are downloaded in the default folder that is added to MATLAB search path at startup.

Maps are stored by user profile. For multiuser setup with a single MATLAB installation, the maps will be downloaded multiple times.

If a new version of the map is available on the server, you will see a warning message asking you to download the map again to get the recent version.

## Version History

Introduced in R2022b

## See Also

sim3d.maps|sim3d.maps.Map.server|sim3d.maps.Map.delete|sim3d.maps.Map.local

## sim3d.maps.Map.server

List of maps available for download from the server

## Syntax

sim3d.maps.Map.server

## Description

sim3d.maps.Map.server lists the available maps in the server.

## Examples

## Download Suburban Scene Map

This example shows how to download and access the Suburban scene map from the Simulation 3D Scene Configuration block.

To begin, check the maps available in the server.
sim3d.maps.Map.server

MapName
"Suburban scene"

Description
"a suburban area beyond the city's border"

Version
"1"

MinimumRelease
"R2022b"

Download the Suburban scene from the server.
sim3d.maps.Map.download('Suburban scene')
Map is susccesfully downloaded and is up-to-date
Check if the downloaded maps are available in your local machine.
sim3d.maps.Map.local

MapName
"Suburban scene"

Description
"a suburban area beyond the city's border"

Version
"1"

Add the Simulation 3D Scene Configuration block to your model.


Open the block mask and select the suburban scene from Scene name.


Run the model.


## Version History

Introduced in R2022b

## See Also

sim3d.maps | sim3d.maps.Map.download|sim3d.maps.Map.delete| sim3d.maps.Map.local

## sim3d.maps.Map.delete

Delete local maps downloaded from the server

## Syntax

sim3d.maps.Map.delete(Scene)

## Description

sim3d.maps.Map.delete(Scene) deletes the map Scene from your local system.

## Examples

## Download Suburban Scene Map

This example shows how to download and access the Suburban scene map from the Simulation 3D Scene Configuration block.

To begin, check the maps available in the server.
Add the Simulation 3D Scene Configuration block to your model.


Open the block mask and select the suburban scene from Scene name.


Run the model.


Delete the model and check if the map is till available locally.

```
sim3d.maps.Map.delete('Suburban scene')
Suburban scene was successfully deleted
```


## Input Arguments

## Scene - Name of scene

string | character array
Name of the map being deleted, specified as a string or character array. Once the map is deleted, it automatically disappears from the Simulation 3D Scene Configuration block mask menu.

## Version History

Introduced in R2022b

```
See Also
sim3d.maps|sim3d.maps.Map.download| sim3d.maps.Map.server |
sim3d.maps.Map.local
```


## sim3d.maps.Map.local

List of locally available maps

## Syntax

sim3d.maps.Map.local

## Description

sim3d.maps.Map. local lists the locally available maps.

## Examples

## Download Suburban Scene Map

This example shows how to download and access the Suburban scene map from the Simulation 3D Scene Configuration block.

To begin, check the maps available in the server.

```
sim3d.maps.Map.server
```

MapName
"Suburban scene"

Description
"a suburban area beyond the city's border"

Version
"1"

MinimumRelease "R2022b"

Download the Suburban scene from the server.
sim3d.maps.Map.download('Suburban scene')
Map is susccesfully downloaded and is up-to-date
Check if the downloaded maps are available in your local machine.
sim3d.maps.Map.local

MapName
"Suburban scene"

Description
"a suburban area beyond the city's border"

Version
"1"

Add the Simulation 3D Scene Configuration block to your model.


Open the block mask and select the suburban scene from Scene name.


Run the model.


## Version History

Introduced in R2022b

## See Also

sim3d.maps | sim3d.maps.Map.download|sim3d.maps.Map.server| sim3d.maps.Map.delete

Apps

## Virtual Vehicle Composer

Configure, build, and analyze a virtual automotive vehicle

## Description

The Virtual Vehicle Composer app enables you to quickly configure and build a virtual vehicle that you can use for system-level performance testing and analysis, including component sizing, fuel economy, drive cycle tracking, vehicle handling maneuvers, software integration testing, and hardware-in-the-loop (HIL) testing. Use the app to enter your vehicle parameter data, build a virtual vehicle model, run test scenarios, and analyze the results.

The virtual vehicle model utilizes sets of blocks and reference application subsystems available with Powertrain Blockset ${ }^{\mathrm{TM}}$, Vehicle Dynamics Blockset, and Simscape ${ }^{\mathrm{TM}}$ add-ons. Virtual Vehicle Composer simplifies the task of configuring the architecture and entering parameter data.

If you have Powertrain Blockset, use the app to:

- Configure conventional vehicle, electric vehicle (EV), and hybrid-electric vehicle (HEV) architectures.
- Operate the vehicle in test conditions such as FTP cycles.
- Analyze design tradeoffs and size components.

If you have Vehicle Dynamics Blockset, use the app to:

- Configure passenger cars and analyze their ride-and-handling characteristics by running standard test maneuvers.
- Configure and test a motorcycle. Requires a Simscape license.
- Visualize your virtual vehicle in the Unreal Engine simulation environment.

If you have Simscape and these Simscape add-ons, you can use the app to configure vehicles with Simscape subsystems:

- Simscape Driveline ${ }^{\mathrm{TM}}$
- Simscape Electrical ${ }^{\mathrm{TM}}$
- Simscape Fluids ${ }^{\text {TM }}$
- Simscape Multibody ${ }^{\mathrm{TM}}$ - Required for motorcycles

To build, operate, and analyze your virtual vehicle, use the Composer tab. The options and settings depend on the available products.

| Step | Section | Button |  | Description |
| :--- | :--- | :--- | :--- | :--- |
| 1 | Configure |  |  | Setup <br> - |

## Required Products

The Virtual Vehicle Composer requires either of these products:

- "Powertrain Blockset"
- "Vehicle Dynamics Blockset"

With "Vehicle Dynamics Blockset" you can run your virtual vehicle in the Unreal Engine 3D simulation environment. See the requirements in "Unreal Engine Simulation Environment Requirements and Limitations".

If you have Simscape and these Simscape add-ons, you can use the app to configure vehicles with Simscape subsystems.

- "Simscape Driveline"
- "Simscape Electrical"
- "Simscape Fluids"
- "Simscape Multibody" - Required for motorcycles



## Open the Virtual Vehicle Composer App

- MATLAB Toolstrip: On the Apps tab, under Automotive, click the Virtual Vehicle Composer icon.
- MATLAB Command Window: Enter virtualVehicleComposer.


## Examples

- "Get Started with the Virtual Vehicle Composer"


## Parameters

## Setup

Start here to quickly enter your virtual vehicle class, powertrain architecture, model template, and vehicle dynamics.

Project path - Project location
C: \Users\username\MATLAB\Projects\examples (default)
Project location, specified as a character vector.

Note The combined Project path and Configuration name must be less than 80 characters.

## Data Types: char

Configuration name - Name of vehicle and test configuration
ConfiguredVirtualVehicle (default)
Name of the vehicle and test configuration.

Note The combined Project path and Configuration name must be less than 80 characters.

## Data Types: char

Vehicle class - Type of vehicle
Passenger car (default) | Motorcycle
Use this parameter to specify the vehicle type.
The parameter options depend on the available products. This table summarizes the options available with Powertrain Blockset and Vehicle Dynamics Blockset.

| Setting | Powertrain <br> Blockset | Vehicle <br> Dynamics <br> Blockset | Description |
| :--- | :---: | :---: | :--- |
| Passenger |  | $\checkmark$ | Four-wheeled passenger car. |
| car |  |  |  |


| Setting | Powertrain <br> Blockset | Vehicle <br> Dynamics <br> Blockset | Description |
| :--- | :--- | :--- | :--- |
|  |  | $\boldsymbol{V}$ | Two-wheeled motorcycle. |
| Motorcycle |  |  |  |

## Dependencies

If you set Vehicle class to Motorcycle, the app sets the parameter Model template to Simscape.
If you have Simscape and these Simscape add-ons, you can use the app to configure vehicles with Simscape subsystems:

- Simscape Driveline
- Simscape Electrical
- Simscape Fluids
- Simscape Multibody - Required for motorcycles

Powertrain architecture - Conventional, electric (EV), or hybrid electric (HEV) passenger vehicle. Conventional or electric motorcycle Conventional Vehicle|Electric Vehicle 1EM|Electric Vehicle 2EM|Electric Vehicle 3EM Dual Front|Electric Vehicle 3EM Dual Rear|Electric Vehicle 4EM| Hybrid Electric P0|Hybrid Electric P1|Hybrid Electric P2|Hybrid Electric P3| Hybrid Electric P4|Hybrid Electric MM|Hybrid Electric IPS|Conventional Motorcycle with Chain Drive|Electric Motorcycle with Chain Drive

The parameter options depend on the available products. This table summarizes the options available with Powertrain Blockset and Vehicle Dynamics Blockset.

Note To refer back to your Powertrain architecture diagram, click the Setup tab. You will see the configuration of the system, including motor placement.

| Setting | Powertrain <br> Blockset | Vehicle <br> Dynamics <br> Blockset | Description |
| :--- | :---: | :---: | :--- |
| Conventional <br> Vehicle | $\boldsymbol{\checkmark}$ | $\boldsymbol{\checkmark}$ | Vehicle with an SI or CI internal combustion <br> engine, transmission, and corresponding <br> control units. May be FWD, RWD, or AWD. |
| Electric Vehicle <br> 1EM | $\checkmark$ | $\boldsymbol{\checkmark}$ | Vehicle with one electric motor, and battery, <br> driveline, and corresponding control units. <br> May be FWD, RWD, or AWD. |
| Electric Vehicle <br> 2EM | $\boldsymbol{\checkmark}$ |  | Vehicle with one motor driving the front axle <br> and one motor driving the rear axle; battery, <br> driveline, and corresponding control units. |


| Setting | Powertrain Blockset | Vehicle Dynamics Blockset | Description |
| :---: | :---: | :---: | :---: |
| Electric Vehicle 3EM Dual Front | $\checkmark$ |  | Vehicle with two independent motors driving the front axle and one motor driving the rear axle; battery, driveline, and corresponding control units. |
| Electric Vehicle 3EM Dual Rear | $\checkmark$ |  | Vehicle with one motor driving the front axle and two independent motors driving the rear axle; battery, driveline, and corresponding control units. |
| ```Electric Vehicle 4EM``` | $\checkmark$ |  | Vehicle with one independent motor driving each wheel; battery, and corresponding control units. |
| Hybrid Electric P0 | $\checkmark$ |  | Vehicle with P0 hybrid-electric propulsion, including an SI engine, transmission, motor, battery, and corresponding control units. |
| Hybrid Electric P1 | $\checkmark$ |  | Vehicle with P1 hybrid-electric propulsion, including an SI engine, transmission, motor, battery, and corresponding control units. |
| Hybrid Electric P2 | $\checkmark$ |  | Vehicle with P2 hybrid-electric propulsion, including an SI engine, transmission, motor, battery, and corresponding control units. |
| Hybrid Electric P3 | $\checkmark$ |  | Vehicle with P3 hybrid-electric propulsion, including an SI engine, transmission, motor, battery, and corresponding control units. |
| Hybrid Electric P4 | $\checkmark$ |  | Vehicle with P4 hybrid-electric propulsion, including an SI engine, transmission, motor, battery, and corresponding control units. |
| Hybrid Electric MM | $\checkmark$ |  | Vehicle with multi-mode hybrid-electric propulsion, including an SI engine, transmission, motor, generator, battery, and corresponding control units. |
| Hybrid Electric IPS | $\checkmark$ |  | Vehicle with input power split hybridelectric propulsion, including an SI engine, transmission, motor, generator, battery, and corresponding control units. |
| Conventional Motorcycle with Chain Drive |  | $\checkmark$ | Motorcycle with an SI engine, transmission and chain reduction, and corresponding control units. <br> Requires Simscape. |
| Electric Motorcycle with Chain Drive |  | $\checkmark$ | Motorcycle with an electric motor, gear and chain reductions, battery, and corresponding control units. <br> Requires Simscape. |

If you have Simscape and Simscape add-ons, you can use the app to configure vehicles that incorporate Simscape subsystems, including motorcycles.

Model template - Vehicle plant model and powertrain architecture template Simulink (default) | Simscape

Use this parameter to specify a Simulink or Simscape vehicle plant model and powertrain architecture. By default, the virtual vehicle uses a Simulink model template.

If you have Simscape and these Simscape add-ons, you can use the app to configure vehicles with Simscape subsystems:

- Simscape Driveline
- Simscape Electrical
- Simscape Fluids
- Simscape Multibody - Required for motorcycles


## Dependencies

If you set Vehicle class to Motorcycle, the app sets Model template to Simscape. You cannot configure a motorcycle and select Simulink as model template.

Vehicle dynamics - Virtual vehicle longitudinal (3 DOF) or combined (6 DOF) dynamics Longitudinal vehicle dynamics (default)|Combined longitudinal and lateral vehicle dynamics

| Vehicle Class Setting | Vehicle Dynamics Setting | Goal |
| :---: | :---: | :---: |
| Passenger car | Longitudinal vehicle dynamics | Fuel economy and energy management analysis. |
|  | Combined longitudinal and lateral vehicle dynamics | Vehicle handling, stability, and ride comfort analysis. |
| Motorcycle | In-plane motorcycle | Fuel economy and energy management analysis. |


| Vehicle Class Setting | Vehicle Dynamics Setting | Goal |
| :--- | :--- | :--- |
|  | motorcycleout-of-plane <br> dynamics | Motorcycle handling, stability, <br> and ride comfort analysis. |
|  | ars |  |

The virtual vehicle uses the Z-up coordinate system as defined in SAE J670 and ISO 8855. For more information, see "Coordinate Systems in Vehicle Dynamics Blockset".

The parameter options depend on the available products. This table summarizes the options available with Powertrain Blockset and Vehicle Dynamics Blockset.

| Setting | Powertrain Blockset | Vehicle Dynamics Blockset | Description |
| :---: | :---: | :---: | :---: |
| Longitudinal vehicle dynamics | $\checkmark$ | $\checkmark$ | Three degree-of-freedom (DOF) conventional vehicle model suitable for fuel economy and energy management analysis. |
| Combined longitudinal and lateral vehicle dynamics |  | $\checkmark$ | Six DOF conventional vehicle suitable for vehicle handling, stability, and ride comfort analysis. <br> Not available with Passenger car when Model template is set to Simscape. |
| In-plane motorcycle dynamics |  | $\checkmark$ | Three DOF motorcycle model suitable for fuel economy and energy management analysis. <br> The model implements a longitudinal inplane motorcycle body model to calculate longitudinal, vertical, and pitch motion. <br> Available if you have Simscape and Simscape add-ons. |
| Out-of-plane motorcycle dynamics |  | $\checkmark$ | Six DOF motorcycle suitable for vehicle handling, stability, and ride comfort analysis. <br> Available if you have Simscape and Simscape add-ons. |

## Dependencies

If you set Vehicle class to Passenger car and then set Model template to Simscape, the app sets Vehicle dynamics to Combined longitudinal and lateral vehicle dynamics.

## Data and Calibration

Use the app to quickly set your virtual vehicle parameters, such as chassis and suspension, tires, powertrain, and driver. Select one of the options for each parameter. The available options depend on your Setup selections.

| Parameter | Description |
| :--- | :--- |
| Chassis | Select the chassis type. <br> The available options depend on the Vehicle class and Vehicle dynamics <br> settings. |
| Tire | Select the tire model and tire data. <br> The available options depend on the Vehicle class and Vehicle dynamics <br> settings. |
| Brake Type | Select the brake type. Use the Brake Control Unit parameter to specify the <br> brake control. |
| Powertrain | Select the engine, electric motors, transmission, drivetrain, differential system, <br> and electrical system parameters. <br> The available options depend on the Powertrain architecture selected. |
| Driver/Rider | If you set Vehicle class to Passenger car, select the Driver. The parameter <br> setting Longitudinal Driver implements a longitudinal speed-tracking <br> controller. If you have Vehicle Dynamics Blockset, you can set Driver to <br> Predictive Driver or Predictive Stanley Driver to track longitudinal <br> velocity and a lateral displacement relative to a reference pose. <br> If you set Vehicle class to Motorcycle, select the Rider. You can set Rider to <br> Rigid or to 6DOF and External Forces and Moments. |
| Environment | Use the parameter setting Standard Ambient to specify the ambient <br> environment. |
| Steering <br> System | If you set Vehicle class to Passenger car, and you have Vehicle Dynamics <br> Blockset and set Vehicle dynamics to Combined longitudinal and lateral <br> vehicle dynamics, you can specify the steering system. <br> If you set Vehicle class to Motorcycle and set Vehicle dynamics to Out - of - <br> plane motorcycle dynamics, you can specify the steering system. |
| Suspension | If you set Vehicle class to Passenger car, and you have Vehicle Dynamics <br> Blockset and set Vehicle dynamics to Combined longitudinal and lateral <br> vehicle dynamics, you can specify the suspension. <br> If you set Vehicle class to Motorcycle and set Vehicle dynamics to Out - of - <br> plane motorcycle dynamics, you can specify the suspension. |

## Passenger Car Chassis

Chassis - Chassis type
Vehicle Body 1DOF Longitudinal|Vehicle Body 3DOF Longitudinal|Vehicle Body 6DOF Longitudinal and Lateral

The parameter options depend on the available products. This table summarizes the options available with Powertrain Blockset and Vehicle Dynamics Blockset.

| Setting | Powertrain <br> Blockset | Vehicle <br> Dynamics <br> Blockset | Description |
| :--- | :---: | :---: | :--- |
| Vehicle Body 1DOF <br> Longitudinal | $\checkmark$ | $\checkmark$ | Chassis model for 1DOF longitudinal vehicle <br> dynamics. Available when you set Vehicle <br> dynamics to Longitudinal vehicle <br> dynamics. |
| Vehicle Body 3DOF <br> Longitudinal | $\boldsymbol{\checkmark}$ | $\boldsymbol{\checkmark}$ | Chassis model for 3DOF longitudinal vehicle <br> dynamics. Available when you set Vehicle <br> dynamics to Longitudinal vehicle <br> dynamics. |
| Vehicle Body 6DOF <br> Longitudinal and <br> Lateral |  | $\checkmark$ | Chassis model for 6DOF longitudinal and <br> lateral vehicle dynamics. Available when you <br> set Vehicle dynamics to Combined <br> longitudinal and lateral vehicle <br> dynamics. |

## Dependencies

To enable this parameter, on the Setup pane, set Vehicle class to Passenger car.

## Passenger Car Tire

Tire - Model and specifications of tires
MF Tires Longitudinal|Fiala Tires Longitudinal and Lateral |MF Tires Longitudinal and Lateral|Longitudinal Combined Slip Tire

The parameter options depend on the available products. This table summarizes the options available with Powertrain Blockset and Vehicle Dynamics Blockset.
\(\left.$$
\begin{array}{|l|c|c|l|}\hline \text { Setting } & \begin{array}{l}\text { Powertrain } \\
\text { Blockset }\end{array} & \begin{array}{l}\text { Vehicle } \\
\text { Dynamics } \\
\text { Blockset }\end{array} & \text { Description } \\
\hline \begin{array}{l}\text { MF Tires } \\
\text { Longitudinal }\end{array} & \checkmark & \boldsymbol{\checkmark} & \begin{array}{l}\text { Tire model suitable for longitudinal vehicle } \\
\text { dynamics studies, including fuel economy } \\
\text { and energy management analysis. }\end{array} \\
\hline \begin{array}{l}\text { Fiala Tires } \\
\text { Longitudinal and } \\
\text { Lateral }\end{array} & & \boldsymbol{\checkmark} & \begin{array}{l}\text { Tire model suitable for lateral vehicle } \\
\text { dynamics studies, including vehicle } \\
\text { handling, stability, and ride comfort analysis. }\end{array} \\
\begin{array}{l}\text { Implements a simplified tire with lateral and }\end{array}
$$ <br>
longitudinal slip capability. Uses a <br>
translational friction model to calculate the <br>
forces and moments during combined <br>

longitudinal and lateral slip.\end{array}\right\}\)| Consider this setting if you do not have the |
| :--- |
| tire coefficients needed by the Magic |
| Formula and are conducting studies that do |
| not involve extensive nonlinear combined |
| lateral slip or lateral dynamics. |$|$


| Setting | Powertrain Blockset | Vehicle Dynamics Blockset | Description |
| :---: | :---: | :---: | :---: |
| MF Tires <br> Longitudinal and Lateral |  | $\checkmark$ | Tire models suitable for lateral vehicle dynamics studies, including vehicle handling, stability, and ride comfort analysis. |
| Combined Slip <br> Tires Longitudinal |  | $\checkmark$ | Tire model implements the longitudinal and lateral behavior of a wheel characterized by the Magic Formula. You can use Tire Data parameter to specify fitted tire data sets provided by the Global Center for Automotive Performance Simulation (GCAPS) for tires, including: <br> - Light passenger car 205/60R15 <br> - Mid-size passenger car 235/45R18 <br> - Performance car 225/40R19 <br> - SUV 265/50R20 <br> - Light truck 275/65R18 <br> - Commercial truck 295/75R22.5 |

## Dependencies

To enable this parameter, on the Setup pane, set Vehicle class to Passenger car.

## Passenger Car Brake Type

Brake Type - Virtual vehicle brakes
Disc | Drum | Mapped
The parameter options depend on the available products. This table summarizes the options available with Powertrain Blockset and Vehicle Dynamics Blockset.

| Setting | Powertrain <br> Blockset | Vehicle <br> Dynamics <br> Blockset | Description |
| :--- | :---: | :---: | :--- |
| Disc | $\boldsymbol{\checkmark}$ | $\boldsymbol{\checkmark}$ | Brake model converts the brake fluid <br> pressure into a braking torque. |
| Drum | $\boldsymbol{\checkmark}$ | $\boldsymbol{\checkmark}$ | Brake model converts the brake fluid <br> pressure and brake geometry into a braking <br> torque. |
| Mapped | $\boldsymbol{\checkmark}$ | $\boldsymbol{\checkmark}$ | Brake torque is a mapped function of the <br> wheel speed and the brake fluid pressure. |

## Dependencies

To enable this parameter, on the Setup pane, set Vehicle class to Passenger car.

Brake Control Unit - Brake control
Open Loop (default)|Bang Bang ABS|Five-State ABS and TCS
The parameter options depend on the available products. This table summarizes the options available with Powertrain Blockset and Vehicle Dynamics Blockset.

| Setting | Powertrain <br> Blockset | Vehicle <br> Dynamics <br> Blockset | Description |
| :--- | :---: | :---: | :--- |
| Open Loop | $\boldsymbol{\nu}$ | $\boldsymbol{\checkmark}$ | Open loop brake control. The controller <br> commands brake pressure as a sole function <br> of the brake command. |
| Bang Bang ABS | $\checkmark$ | $\checkmark$ | Anti-lock braking system (ABS) feedback <br> controller that switches between two states <br> to regulate wheel slip, to minimize the error <br> between the actual slip and the desired slip. <br> Here, the desired slip is the value where the <br> friction coefficient of the tires reaches its <br> maximum. |
| Five-State ABS and <br> TCS | $\checkmark$ | $\checkmark$ | Five-state ABS and traction control system <br> (TCS) that uses logic-switching based on <br> wheel deceleration and vehicle acceleration <br> to control the braking pressure at each <br> wheel. |
| Consider using five-state ABS and TCS |  |  |  |
| control to prevent wheel lock-up, decrease |  |  |  |
| braking distance, or maintain yaw stability |  |  |  |
| during maneuvers. The default ABS |  |  |  |
| parameters are set to work on roads that |  |  |  |
| have a constant friction coefficient scaling |  |  |  |
| factor of 0.6. |  |  |  |$|$

## Dependencies

To enable this parameter, on the Setup pane, set Vehicle class to Passenger car.

## Passenger Car Powertrain

Engine - Internal combustion engine
Simple Engine (SI) (default)|Simple Engine (CI)|CI Engine|CI Mapped Engine|SI Engine|SI Mapped Engine|SI Deep Learning Engine|FMU Engine

The parameter options depend on the available products. This table summarizes the options available with Powertrain Blockset and Vehicle Dynamics Blockset.

| Setting | Powertrain <br> Blockset | Vehicle <br> Dynamics <br> Blockset | Description |
| :--- | :---: | :---: | :--- |
| Simple Engine (SI) | $\boldsymbol{\checkmark}$ | $\boldsymbol{\checkmark}$ | Simplified SI engine model using a <br> maximum torque versus engine speed table, <br> two scalar fuel mass properties, and one <br> scalar engine efficiency parameter to <br> estimate engine torque and fuel flow. |
| Simple Engine (CI) | $\boldsymbol{\checkmark}$ | $\boldsymbol{\checkmark}$ | Selecting Simple Engine SI sets the <br> Engine Control Unit parameter to Simple <br> ECU. |
| CI Engine |  | Simplified CI engine model using a <br> maximum torque versus engine speed table, <br> two scalar fuel mass properties, and one <br> scalar engine efficiency parameter to <br> estimate engine torque and fuel flow. <br> Selecting Simple Engine CI sets the |  |
| Engine Control Unit parameter to Simple |  |  |  |
| ECU. |  |  |  |$|$| Compression-ignition (CI) engine modeled |
| :--- |
| from intake to the exhaust port. |
| Selecting CI Engine sets the Engine |
| Control Unit parameter to CI Engine |
| Controller. |


| Setting | Powertrain Blockset | Vehicle Dynamics Blockset | Description |
| :---: | :---: | :---: | :---: |
| SI Mapped Engine | $\checkmark$ | $\checkmark$ | Mapped SI engine model using power, air mass flow, fuel flow, exhaust temperature, efficiency, and emission performance lookup tables. <br> Selecting SI Mapped Engine sets the Engine Control Unit parameter to SI Engine Controller. <br> If you have the Model-Based Calibration Toolbox, you can generate a static calibration. Select from options on Calibrate from Data. For more information, see "Calibrate Mapped SI Engine Using Data" (Powertrain Blockset). |
| SI Deep Learning Engine | $\checkmark$ |  | Deep learning SI engine. <br> Available if you have the Deep Learning Toolbox ${ }^{\mathrm{TM}}$ and Statistics and Machine Learning Toolbox ${ }^{\mathrm{TM}}$ licenses. Use this setting to generate a dynamic deep learning SI engine model to use for powertrain control, diagnostic, and estimator algorithm design. <br> Selecting SI Deep Learning Engine sets the Engine Control Unit parameter to SI Engine Controller. |


| Setting | Powertrain Blockset | Vehicle Dynamics Blockset | Description |  |
| :---: | :---: | :---: | :---: | :---: |
| FMU Engine | $\checkmark$ | $\checkmark$ | The functional mockup unit (FMU) engine implements an FMU block with these engine inputs and outputs. |  |
|  |  |  | Inputs | Outputs |
|  |  |  | Torque command <br> Engine RPM | Brake torque <br> Fuel flow <br> Air flow <br> Exhaust gas temperature <br> Exhaust gas temperature <br> Air fuel ratio <br> Brake-specific fuel consumption (BSFC) <br> Crank angle |
|  |  |  | To implement <br> 1 Set Engin <br> 2 Use Brow <br> 3 Select Re and outputs <br> - If veri FMU i signal subsys <br> - If verif FMU match subsys import connec <br> 4 Select Im the virtua subsystem | e FMU engine model: <br> to FMU Engine. <br> to select the FMU file. to verify the FMU inputs <br> ation passes, the number of uts and outputs matches the in the FMU Import <br> m. <br> ation warns, the number of uts and outputs does not e signals in the FMU Import <br> m. However, you can still <br> he FMU file and manually the signals. <br> ort to integrate the FMU in ehicle FMU Import |

## Dependencies

To enable this parameter, on the Setup pane, set Vehicle class to Passenger car.

Transmission - Virtual vehicle transmission
Ideal Fixed Gear Transmission|Automatic Transmission with Torque Converter| Automated Manual Transmission

The parameter options depend on the available products. This table summarizes the options available with Powertrain Blockset and Vehicle Dynamics Blockset.

| Setting | Powertrain <br> Blockset | Vehicle <br> Dynamics <br> Blockset | Description |
| :--- | :---: | :---: | :--- |
| Ideal Fixed Gear <br> Transmission | $\boldsymbol{\checkmark}$ | $\boldsymbol{\checkmark}$ | Idealized fixed-gear transmission without a <br> clutch or synchronization. Use this setting to <br> model the gear ratios and power loss when <br> you do not need a detailed transmission <br> model. |
| Automatic <br> Transmission with <br> Torque Converter |  |  |  |
| Automated Manual <br> Transmission | $\boldsymbol{\checkmark}$ | Automatic transmission with planetary gears <br> and a torque converter. |  |

## Dependencies

To enable this parameter, on the Setup pane:

- Set Vehicle class to Passenger car.
- Set Powertrain architecture to any of these options:
- Conventional Vehicle
- Hybrid Electric Vehicle P0
- Hybrid Electric Vehicle P1
- Hybrid Electric Vehicle P2
- Hybrid Electric Vehicle P3
- Hybrid Electric Vehicle P4

Transmission Control Unit - Virtual vehicle transmission control
PRNDL Controller
The parameter options depend on the available products. This table summarizes the options available with Powertrain Blockset and Vehicle Dynamics Blockset.

| Setting | Powertrain <br> Blockset | Vehicle <br> Dynamics <br> Blockset | Description |
| :--- | :---: | :---: | :--- |
| PRNDL Controller | $\boldsymbol{\checkmark}$ | $\boldsymbol{V}$ | Controller that executes forward, reverse, <br> neutral, park, and N-speed gear shifts <br> according to the selected shift schedule. You <br> can supply multiple schedules and select <br> them using a block input. |

## Dependencies

To enable this parameter, on the Setup pane:

- Set Vehicle class to Passenger car.
- Set Powertrain architecture to any of these options:
- Conventional Vehicle
- Hybrid Electric Vehicle P0
- Hybrid Electric Vehicle P1
- Hybrid Electric Vehicle P2
- Hybrid Electric Vehicle P3
- Hybrid Electric Vehicle P4


## Drivetrain - Virtual vehicle drivetrain

Front Wheel Drive (default)|Rear Wheel Drive|All Wheel Drive
The parameter options depend on the available products. This table summarizes the options available with Powertrain Blockset and Vehicle Dynamics Blockset.

| Setting | Powertrain <br> Blockset | Vehicle <br> Dynamics <br> Blockset | Description |
| :--- | :--- | :---: | :--- |
| Front Wheel Drive | $\boldsymbol{\checkmark}$ | $\boldsymbol{\checkmark}$ | Drives both wheels on the front axle. |
| Rear Wheel Drive | $\boldsymbol{\checkmark}$ | $\boldsymbol{\checkmark}$ | Drives both wheels on the rear axle. |
| All Wheel Drive | $\boldsymbol{\checkmark}$ | $\boldsymbol{\checkmark}$ | Drives all four wheels. |

## Dependencies

To enable this parameter, on the Setup pane, set Vehicle class to Passenger car.
Front Differential System - Final drive ratio and differential action Open Differential (default)|Active Differential|Limited Slip Differential

The parameter options depend on the available products. This table summarizes the options available with Powertrain Blockset and Vehicle Dynamics Blockset.

| Setting | Powertrain <br> Blockset | Vehicle <br> Dynamics <br> Blockset | Description |
| :--- | :---: | :---: | :--- |
| Open Differential | $\boldsymbol{\checkmark}$ | $\boldsymbol{\checkmark}$ | Implements differential action with equal <br> torque to both wheels. |
| Active <br> Differential | $\boldsymbol{\checkmark}$ | $\boldsymbol{\checkmark}$ | Couples active elements to an open <br> differential to achieve the desired axle <br> torque bias. <br> Not available if you set Model template to <br> Simscape. |
| Limited Slip <br> Differential | $\boldsymbol{\checkmark}$ | $\boldsymbol{\checkmark}$ | Couples passive friction elements to an open <br> differential to achieve the desired axle <br> torque bias. |

## Dependencies

To enable this parameter, set Vehicle class to Passenger car and Drivetrain to Front Wheel Drive or All Wheel Drive.

Rear Differential System - Final drive ratio and differential action Open Differential (default)|Active Differential|Limited Slip Differential

The parameter options depend on the available products. This table summarizes the options available with Powertrain Blockset and Vehicle Dynamics Blockset.

| Setting | Powertrain <br> Blockset | Vehicle <br> Dynamics <br> Blockset | Description |
| :--- | :---: | :---: | :--- |
| Open Differential | $\boldsymbol{\checkmark}$ | $\boldsymbol{\checkmark}$ | Implements differential action with equal <br> torque to both wheels. |
| Active <br> Differential | $\boldsymbol{\checkmark}$ | $\boldsymbol{\checkmark}$ | Couples active elements to an open <br> differential to achieve the desired axle <br> torque bias. |
| Not available if you set Model template to <br> Simscape. |  |  |  |
| Limited Slip <br> Differential | $\boldsymbol{\checkmark}$ | $\boldsymbol{\checkmark}$ | Couples passive friction elements to an open <br> differential to achieve the desired axle <br> torque bias. |

## Dependencies

To enable this parameter, set Vehicle class to Passenger car and Drivetrain to Rear Wheel Drive or All Wheel Drive.

Axle Interconnect - Coupling between front and rear axles
Transfer Case (default)
Coupling between front and rear axles, specified as a transfer case.

## Dependencies

To enable this parameter, set Vehicle class to Passenger car and Drivetrain to All Wheel Drive.

DC-DC Converter - Power electronics device to change voltage of supplied current DC-DC Converter (default) | No DC-DC Converter

DC-to-DC converter that supports bidirectional boost and buck (lower) operations.

## Dependencies

To enable this parameter, set Vehicle class to Passenger car and Powertrain architecture to one of these options:

- Electric Vehicle $x E M$, where $x$ is 1,2 , or 4
- Electric Vehicle 3EM Dual Front
- Electric Vehicle 3EM Dual Rear
- Hybrid Electric Vehicle Px, where $x$ is $0,1,2,3$ or 4
- Hybrid Electric Vehicle MM
- Hybrid Electric Vehicle IPS

Electric Machine $\boldsymbol{x}$-Virtual vehicle electric motor
Electric Vehicle 1EM|Electric Vehicle 2EM|Electric Vehicle 3EM Dual Front| Electric Vehicle 3EM Dual Rear|Electric Vehicle 4EM|Hybrid Electric Vehicle P0|Hybrid Electric Vehicle P1|Hybrid Electric Vehicle P2|Hybrid Electric Vehicle P3|Hybrid Electric Vehicle P4|Hybrid Electric Vehicle MM|Hybrid Electric Vehicle IPS

Virtual vehicle electric machine settings for motor in location $x$ as seen on the Powertrain architecture diagram on the Setup pane.

## Dependencies

To enable this parameter, set Vehicle class to Passenger car and Powertrain architecture to one of these options:

- Electric Vehicle $x$ EM, where $x$ is 1,2 , or 4
- Electric Vehicle 3EM Dual Front
- Electric Vehicle 3EM Dual Rear
- Hybrid Electric Vehicle Px, where $x$ is $0,1,2,3$ or 4
- Hybrid Electric Vehicle MM
- Hybrid Electric Vehicle IPS

Energy Storage - Virtual vehicle energy storage type
Mapped Battery|Ideal Voltage Source
The parameter options depend on the available products. This table summarizes the options available with Powertrain Blockset and Vehicle Dynamics Blockset.

| Setting | Powertrain <br> Blockset | Vehicle <br> Dynamics <br> Blockset | Description |
| :--- | :--- | :--- | :--- |
| Mapped Battery | $\boldsymbol{\checkmark}$ | $\boldsymbol{\checkmark}$ | Open-circuit voltage and internal resistance <br> are mapped functions of the state-of charge <br> (SOC) and battery temperature |
| Ideal Voltage <br> Source | $\boldsymbol{\checkmark}$ | $\boldsymbol{\checkmark}$ | Constant-voltage source with infinite <br> storage capacity |

## Dependencies

To enable this parameter, set Vehicle class to Passenger car and Powertrain architecture to one of these options:

- Electric Vehicle $x E M$, where $x$ is 1,2 , or 4
- Electric Vehicle 3EM Dual Front
- Electric Vehicle 3EM Dual Rear
- Hybrid Electric Vehicle Px, where $x$ is $0,1,2,3$ or 4
- Hybrid Electric Vehicle MM
- Hybrid Electric Vehicle IPS

Vehicle Control Unit - Vehicle system to direct the energy flows in electric and hybrid-electric vehicles
EV 1EM with BMS|EV 2EM|EV 3EM Dual Front|EV 3EM Dual Rear|EV 4EM|HEVP0 Optimal|HEVP1 Optimal|HEVP2 Optimal|HEVP3 Optimal|HEVP4 Optimal|HEVMM RuleBased|HEVIPS RuleBased

The parameter options depend on the available products. This table summarizes the options available with Powertrain Blockset and Vehicle Dynamics Blockset.

| Setting | Powertrain <br> Blockset | Vehicle <br> Dynamics <br> Blockset | Powertrain <br> Architectu <br> re | Description |
| :--- | :---: | :---: | :--- | :--- |
| EV 1EM with BMS | $\boldsymbol{\nu}$ | $\boldsymbol{\nu}$ | Electric <br> Vehicle <br> 1EM | Controls the motor with torque <br> arbitration and power management. <br> Implements regenerative braking. |
| EV 2EM | $\boldsymbol{\nu}$ |  | Electric <br> Vehicle <br> 2EM |  |
| EV 3EM Dual <br> Front | $\boldsymbol{\checkmark}$ |  | Electric <br> Vehicle <br> 3EM Dual <br> Front |  |
| EV 3EM Dual Rear | $\boldsymbol{\checkmark}$ |  | Electric <br> Vehicle <br> 3EM Dual <br> Rear |  |


| Setting | Powertrain Blockset | Vehicle Dynamics Blockset | Powertrain Architectu re | Description |
| :---: | :---: | :---: | :---: | :---: |
| EV 4EM | $\checkmark$ |  | Electric Vehicle 4EM |  |
| HEVP0 Optimal | $\checkmark$ |  | Hybrid Electric Vehicle P0 | Implements an equivalent consumption minimization strategy (ECMS) to control the energy management of hybrid electric vehicles (HEVs). The strategy optimizes the torque split between the engine and motor to minimize energy consumption while maintaining the battery state of charge (SOC). Implements regenerative braking. |
| HEVP1 Optimal | $\checkmark$ |  | Hybrid Electric Vehicle P1 |  |
| HEVP2 Optimal | $\checkmark$ |  | Hybrid Electric Vehicle P2 |  |
| HEVP3 Optimal | $\checkmark$ |  | Hybrid Electric Vehicle P3 |  |
| HEVP4 Optimal | $\checkmark$ |  | Hybrid Electric Vehicle P4 |  |
| HEVMM RuleBased | $\checkmark$ |  | Hybrid <br> Electric <br> Vehicle <br> MM | Controls the motor, generator, and engine through a set of rules and decision logic implemented in Stateflow. Implements regenerative braking. |
| HEVIPS RuleBased | $\checkmark$ |  | Hybrid Electric Vehicle IPS |  |

## Dependencies

To enable this parameter, on the Setup pane, set Vehicle class to Passenger car.

## Passenger Car Driver

Driver - Virtual vehicle driver

## Longitudinal Driver|Predictive Driver|Predictive Stanley Driver

The parameter options depend on the available products. This table summarizes the options available with Powertrain Blockset and Vehicle Dynamics Blockset.

| Setting | Powertrain <br> Blockset | Vehicle <br> Dynamics <br> Blockset | Description |
| :--- | :--- | :---: | :--- |
| Longitudinal <br> Driver | $\boldsymbol{\checkmark}$ | $\boldsymbol{\checkmark}$ | Implements a longitudinal speed-tracking <br> controller. |
| Predictive Driver |  | $\boldsymbol{\checkmark}$ | Tracks longitudinal velocity and a lateral <br> displacement relative to a reference pose. <br> Available when you set Vehicle dynamics <br> to Combined longitudinal and <br> lateral vehicle dynamics. |
| Predictive Stanley <br> Driver |  | $\boldsymbol{\checkmark}$ | Adjusts the steering angle command to <br> match the current pose of a vehicle to a <br> reference pose, given the vehicle's current <br> velocity and direction. |
| Available when you set Vehicle dynamics <br> to Combined longitudinal and <br> lateral vehicle dynamics. |  |  |  |

## Dependencies

To enable this parameter, on the Setup pane, set Vehicle class to Passenger car.

## Passenger Car Steering System

Steering System - Virtual vehicle steering
Kinematic Steering|Mapped Steering|Dynamic Steering|Steering System|No Steering

The parameter options depend on the available products. This table summarizes the options available with Powertrain Blockset and Vehicle Dynamics Blockset.

| Setting | Powertrain <br> Blockset | Vehicle <br> Dynamics <br> Blockset | Description |
| :--- | :--- | :---: | :--- |
| Kinematic Steering |  | $\boldsymbol{\checkmark}$ | Kinematic model for ideal rack-and-pinion <br> steering. Gears convert the steering wheel <br> rotation into linear rack motion. |
| Mapped Steering |  | $\boldsymbol{\checkmark}$ | Mapped rack-and-pinion steering model. |
| Dynamic Steering |  | $\boldsymbol{\checkmark}$ | Dynamic model for ideal rack-and-pinion <br> steering. Gears convert the steering wheel <br> rotation into linear rack motion. |
| Steering System |  | $\boldsymbol{\checkmark}$ | Steering system for Ackerman and rack-and- <br> pinion steering mechanisms. |
| No Steering |  | $\boldsymbol{\checkmark}$ | No steering. |

## Dependencies

To enable this parameter, on the Setup pane:

- Set Vehicle class to Passenger car.
- Set Vehicle dynamics to Combined longitudinal and lateral vehicle dynamics.


## Passenger Car Suspension

Suspension - Virtual vehicle suspension system
Kinematics and Compliance Independent Suspension|MacPherson Front Suspension Solid Axle Rear Suspension|Kinematics and Compliance Twist Beam Suspension| No Suspension

The parameter options depend on the available products. This table summarizes the options available with Powertrain Blockset and Vehicle Dynamics Blockset.

| Setting | Powertrain <br> Blockset | Vehicle <br> Dynamics <br> Blockset | Description |
| :--- | :--- | :---: | :--- |
| Kinematics and <br> Compliance <br> Independent <br> Suspension |  | $\boldsymbol{V}$ | Kinematics and compliance (K \& C) test <br> suspension characteristics measured from <br> simulated or actual laboratory suspension <br> tests. |
| MacPherson Front <br> Suspension Solid <br> Axle Rear <br> Suspension |  | $\boldsymbol{V}$ | Independent MacPherson front suspension <br> and solid rear axle. |
| Kinematics and <br> Compliance Twist <br> Beam Suspension |  | $\boldsymbol{v}$ | Kinematics and compliance characteristics <br> of: <br> - Independent suspension on front axle. |
| No Suspension |  |  |  |

## Dependencies

To enable this parameter, on the Setup pane:

- Set Vehicle class to Passenger car.
- Set Vehicle dynamics to Combined longitudinal and lateral vehicle dynamics.


## Motorcycle Chassis

## Front Tire - Linear front tire

## Linear Front SSC Tire (default)

The parameter options depend on the available products. This table summarizes the options available with Powertrain Blockset and Vehicle Dynamics Blockset.

| Setting | Powertrain <br> Blockset | Vehicle <br> Dynamics <br> Blockset | Description |
| :--- | :--- | :--- | :--- |
| Linear Front SSC <br> Tire |  | $\boldsymbol{\vee}$ | Tire with linear force and moment model, <br> using Simscape modeling. |


| Setting | Powertrain <br> Blockset | Vehicle <br> Dynamics <br> Blockset | Description |
| :--- | :--- | :--- | :--- |
| *Motorcycle configuration options require Simscape and Simscape add-ons. |  |  |  |

## Dependencies

To enable this parameter, on the Setup pane, set Vehicle class to Motorcycle.

## Rear Tire - Linear rear tire

Linear Rear SSC Tire (default)
The parameter options depend on the available products. This table summarizes the options available with Powertrain Blockset and Vehicle Dynamics Blockset.

| Setting | Powertrain <br> Blockset | Vehicle <br> Dynamics <br> Blockset | Description |
| :--- | :--- | :--- | :--- |
| Linear Rear SSC <br> Tire |  | $\boldsymbol{\checkmark}$ | Tire with linear force and moment model, <br> using Simscape modeling. |
| Motorcycle configuration options require Simscape and Simscape add-ons. |  |  |  |

## Dependencies

To enable this parameter, on the Setup pane, set Vehicle class to Motorcycle.
Front Brake Type - Brake type
Disc (default) | Drum | Mapped
The parameter options depend on the available products. This table summarizes the options available with Powertrain Blockset and Vehicle Dynamics Blockset.

| Setting | Powertrain <br> Blockset | Vehicle <br> Dynamics <br> Blockset | Description |  |
| :--- | :--- | :--- | :--- | :---: |
| Disc |  | $\checkmark$ | Brake model converts the brake fluid <br> pressure into a braking torque. |  |
| Drum | $\boldsymbol{\nu}$ | Brake model converts the brake fluid <br> pressure and brake geometry into a braking <br> torque. |  |  |
| Mapped | Brake torque is a mapped function of the <br> wheel speed and the brake fluid pressure. |  |  |  |
| Motorcycle configuration options require Simscape and Simscape add-ons. |  |  |  |  |

## Dependencies

To enable this parameter, on the Setup pane, set Vehicle class to Motorcycle.
Rear Brake Type - Brake type
Disc (default) | Drum | Mapped

The parameter options depend on the available products. This table summarizes the options available with Powertrain Blockset and Vehicle Dynamics Blockset.

| Setting | Powertrain <br> Blockset | Vehicle <br> Dynamics <br> Blockset | Description |
| :--- | :--- | :--- | :--- |
| Disc |  | $\checkmark$ | Brake model converts the brake fluid <br> pressure into a braking torque. |
| Drum | $\boldsymbol{\checkmark}$ | Brake model converts the brake fluid <br> pressure and brake geometry into a braking <br> torque. |  |
| Mapped |  | $\checkmark$ | Brake torque is a mapped function of the <br> wheel speed and the brake fluid pressure. |
| *Motorcycle configuration options require Simscape and Simscape add-ons. |  |  |  |

## Dependencies

To enable this parameter, on the Setup pane, set Vehicle class to Motorcycle.

## Brake Control Unit - Brake control

Open Loop (default)|Bang Bang ABS|Five-State ABS and TCS
The parameter options depend on the available products. This table summarizes the options available with Powertrain Blockset and Vehicle Dynamics Blockset.

| Setting | Powertrain <br> Blockset | Vehicle <br> Dynamics <br> Blockset | Description |
| :--- | :--- | :--- | :--- |
| Open Loop | $\boldsymbol{V}$ | Open loop brake control. The controller <br> commands brake pressure as a sole function <br> of the brake command. |  |
| Bang Bang ABS |  | $\boldsymbol{V}$ | Anti-lock braking system (ABS) feedback <br> controller that switches between two states <br> to regulate wheel slip, with the aim of <br> minimizing the error between the actual slip <br> and the desired slip. Here, the desired slip is <br> the value where the tires' friction coefficient <br> reaches its maximum. |


| Setting | Powertrain <br> Blockset | Vehicle <br> Dynamics <br> Blockset | Description |  |  |
| :--- | :--- | :--- | :--- | :---: | :---: |
| Five-State ABS and <br> TCS |  | Five-state ABS and traction control system <br> (TCS) that uses logic-switching based on <br> wheel deceleration and vehicle acceleration <br> to control the braking pressure at each <br> wheel. |  |  |  |

## Dependencies

To enable this parameter, on the Setup pane, set Vehicle class to Motorcycle.

## Steering System - Steering <br> Steering (default)|No Steering

The parameter options depend on the available products. This table summarizes the options available with Powertrain Blockset and Vehicle Dynamics Blockset.

| Setting | Powertrain <br> Blockset | Vehicle <br> Dynamics <br> Blockset | Description |
| :--- | :--- | :--- | :--- |
| Steering |  | $\boldsymbol{\checkmark}$ | Handlebar-steered front fork on a frame- <br> mounted revolute joint. |
| No Steering |  | $\boldsymbol{\checkmark}$ | Steering angle fixed at zero. |
| *Motorcycle configuration options require Simscape and Simscape add-ons. |  |  |  |

## Dependencies

To enable this parameter, on the Setup pane:

- Set Vehicle class to Motorcycle.
- Set Vehicle dynamics to Out-of-plane motorcycle dynamics.


## Steering Damper - Damper

Simple Damper (default) | No Damper
The parameter options depend on the available products. This table summarizes the options available with Powertrain Blockset and Vehicle Dynamics Blockset.

| Setting | Powertrain <br> Blockset | Vehicle <br> Dynamics <br> Blockset | Description |
| :--- | :--- | :--- | :--- |
| No Damper |  | $\boldsymbol{\checkmark}$ | No damping. |
| Simple Damper |  | $\boldsymbol{\nu}$ | Torsional damper about steering axis, with <br> linear viscous damping. |
| *Motorcycle configuration options require Simscape and Simscape add-ons. |  |  |  |

## Dependencies

To enable this parameter, on the Setup pane:

- Set Vehicle class to Motorcycle.
- Set Vehicle dynamics to Out-of-plane motorcycle dynamics.

Front Suspension - Motorcycle suspension
Simple Spring and Damper Suspension (default)
The parameter options depend on the available products. This table summarizes the options available with Powertrain Blockset and Vehicle Dynamics Blockset.

| Setting | Powertrain <br> Blockset | Vehicle <br> Dynamics <br> Blockset | Description |
| :--- | :--- | :--- | :--- |
| Simple Spring and <br> Damper Suspension |  | $\boldsymbol{V}$ | Telescoping fork with linear spring and <br> damper. |
| *Motorcycle configuration options require Simscape and Simscape add-ons. |  |  |  |

## Dependencies

To enable this parameter, on the Setup pane:

- Set Vehicle class to Motorcycle.
- Set Vehicle dynamics to Out-of-plane motorcycle dynamics.

Rear Suspension - Motorcycle suspension
Simple Spring and Damper Suspension (default)
The parameter options depend on the available products. This table summarizes the options available with Powertrain Blockset and Vehicle Dynamics Blockset.

| Setting | Powertrain <br> Blockset | Vehicle <br> Dynamics <br> Blockset | Description |
| :--- | :--- | :--- | :--- |
| Simple Spring and <br> Damper Suspension |  | $\boldsymbol{\nu}$ | Swing arm with linear spring and damper. |
| *Motorcycle configuration options require Simscape and Simscape add-ons. |  |  |  |

## Dependencies

To enable this parameter, on the Setup pane:

- Set Vehicle class to Motorcycle.
- Set Vehicle dynamics to Out-of-plane motorcycle dynamics.


## Motorcycle Powertrain

## Propulsion System - Motorcycle propulsion system

Simple Engine|Mapped Engine |Moto Electrical System
The parameter options depend on the available products. This table summarizes the options available with Powertrain Blockset and Vehicle Dynamics Blockset.

| Setting | Powertrain Blockset | Vehicle Dynamics Blockset | Description |
| :---: | :---: | :---: | :---: |
| Simple Engine |  | $\checkmark$ | Simplified SI engine model using a maximum torque versus engine speed table, two scalar fuel mass properties, and one scalar engine efficiency parameter to estimate engine torque and fuel flow. <br> Available when you set Powertrain architecture to Conventional Motorcycle with Chain Drive. |
| SI Mapped Engine |  | $\checkmark$ | Mapped SI engine model using power, air mass flow, fuel flow, exhaust temperature, efficiency, and emission performance lookup tables. <br> Available when you set Powertrain architecture to Conventional Motorcycle with Chain Drive. |
| Moto Electrical System |  | $\checkmark$ | Electric propulsion system. <br> Available when you set Powertrain architecture to Electric Motorcycle with Chain Drive. |
| *Motorcycle configuration options require Simscape and Simscape add-ons. |  |  |  |

## Dependencies

To enable this parameter, on the Setup pane, set Vehicle class to Motorcycle.

## Chain - Motorcycle chain and sprocket drive system

Chain Drive (default)
The parameter options depend on the available products. This table summarizes the options available with Powertrain Blockset and Vehicle Dynamics Blockset.

| Setting | Powertrain <br> Blockset | Vehicle <br> Dynamics <br> Blockset | Description |
| :--- | :--- | :--- | :--- |
| Chain Drive |  | Inextensible chain which meshes with front <br> and rear sprockets. Rear sprocket is mounted <br> to wheel with a torsional damper. |  |
| *Motorcycle configuration options require Simscape and Simscape add-ons. |  |  |  |

## Dependencies

To enable this parameter, on the Setup pane, set Vehicle class to Motorcycle.

## Motorcycle Rider

## Rider - Rider type

Rigid (default)|6DOF and External Forces and Moments
The parameter options depend on the available products. This table summarizes the options available with Powertrain Blockset and Vehicle Dynamics Blockset.

| Setting | Powertrain <br> Blockset | Vehicle <br> Dynamics <br> Blockset | Description |
| :--- | :--- | :--- | :--- |
| Rigid |  | $\checkmark$ | Rider implemented as a rigid body so that <br> their relative motion to the motorcycle frame <br> is zero. No crouching, and their lean angle is <br> the same as the motorcycle frame. |
| 6 DOF and External <br> Forces and Moments |  | $\checkmark$ | Rider body implemented with six degrees-of- <br> freedom (DOF) relative to the motorcycle <br> frame. Able to lean and crouch independently <br> of frame. |
| *Motorcycle configuration options require Simscape and Simscape add-ons. |  |  |  |

## Dependencies

To enable this parameter, on the Setup pane, set Vehicle class to Motorcycle.
Rider Control - Motorcycle control type
Open Loop (default)
The parameter options depend on the available products. This table summarizes the options available with Powertrain Blockset and Vehicle Dynamics Blockset.

| Setting | Powertrain <br> Blockset | Vehicle <br> Dynamics <br> Blockset | Description |
| :--- | :--- | :--- | :--- |
| Open Loop |  | Steering of front fork as prescribed by test <br> scenario. |  |
|  |  |  |  |

## Dependencies

To enable this parameter, on the Setup pane, set Vehicle class to Motorcycle.
Environment
Environment - Virtual vehicle environment
Standard Ambient
The parameter setting Standard Ambient implements an ambient environment model.

## Scenario and Test

Assemble a test plan for your virtual vehicle.
If you set Scenario to Drive Cycle, you can use:

- Drive cycles from predefined sources. By default, the block includes the FTP-75 drive cycle. To install additional drive cycles from the support package, see "Support Package for Maneuver and Drive Cycle Data". The support package has drive cycles that include the gear shift schedules, for example, JC08 and CUEDC.
- Workspace variables that define your own drive cycles.
- .mat, .xls, .xlsx, or .txt files.
- Wide open throttle (WOT) parameters, including initial and nominal reference speeds, deceleration start time, and final reference speed.

For a Passenger car, if you have Vehicle Dynamics Blockset and set Vehicle dynamics to Combined longitudinal and lateral vehicle dynamics, you can select maneuvers for vehicle handling, stability, and ride analysis. Maneuvers include:

- Increasing Steer
- Swept Sine
- Sine with Dwell
- Fishhook

For a Motorcycle, if you set Vehicle dynamics to Out-of-plane motorcycle dynamics, you can select maneuvers for vehicle handling, stability, and ride analysis. Maneuvers include:

- Steady Turning
- Handle Hit

If you want to run your virtual vehicle in the Unreal Engine 3D simulation environment, set 3D Scene Selection to 3D Scene. For hardware requirements, see "Unreal Engine Simulation Environment Requirements and Limitations".

## Logging

On the Logging tab, select the signals to log. The app has a default set of signals in the Selected Signals list. The default list depends on the vehicle configuration. You can add or remove signals. Options include energy-related quantities, and vehicle position, velocity, and acceleration.

## Build

Click Virtual Vehicle to build your vehicle. When you build, the Virtual Vehicle Composer app creates a Simulink model that incorporates the vehicle architecture and parameters that you have specified and associates it with the test plan you configured.

The build takes time to complete. View progress in the MATLAB Command Window.

## Operate

To operate the model, on the Composer tab in the Operate section, click Run Test Plan


The simulations take time to complete. View progress in the MATLAB Command Window.

## Analyze

Click Simulation Data Inspector to view and analyze simulation signals you chose to log during operation.

If your test plan includes more than one test scenario, the Simulation Data Inspector displays the results from the last scenario. To see results from earlier scenarios, load the archived results.

## Programmatic Use

Entering the command virtualVehicleComposer opens a new session of the app, enabling you to configure, build, and analyze your virtual vehicle.

## Version History

## Introduced in R2022a

## R2023a: Configure motorcycles with Simscape subsystems

If you have Simscape and these Simscape add-ons, you can use the app to configure vehicles with Simscape subsystems:

- Simscape Driveline
- Simscape Electrical
- Simscape Fluids
- Simscape Multibody - Required for motorcycles

When you build your virtual vehicle, on the Setup tab, set Model template to Simscape.
The app provides the Simscape subsystem templates for longitudinal vehicle analysis.

## R2022b: Configure vehicles with Simscape subsystems

If you have these Simscape products, you can use the Virtual Vehicle Composer app to configure the vehicle plant model with Simscape subsystems.

- Simscape Driveline
- Simscape Electrical

When you build your virtual vehicle, on the Setup tab, set Model template to Simscape.
The app provides the Simscape subsystem templates for longitudinal vehicle analysis.

## See Also

## Topics

"Get Started with the Virtual Vehicle Composer"
"Simulation Data Inspector"
"How 3D Simulation for Vehicle Dynamics Blockset Works"


[^0]:    $T_{R} \quad$ Input torque

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[^4]:    Programmatic Use
    Block Parameter: g_bias
    Type: character vector

